

SUSTAINABLE DRAINAGE ASSESSMENT AND OPERATION AND MAINTENANCE PLAN

Thomas Telford UTC Morgan Sindall Construction February 2021

CWA-20-196-SUDS-001 UC0030-CWA-XX-XX-RP-C-0001

A Hardy	Prepared by:
S Wedge	Authorised by:
	Signed:
15.02.21	Dated:



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1.00 INTRODUCTION

- 1.01 CWA was commissioned by Morgan Sindall Construction to prepare a Sustainable Drainage Assessment and Operation and Maintenance Plan for the planning application for a new development on the site at the West Midlands Construction (WMC) University Technical College (UTC) on Cambridge Street in Wolverhampton.
- 1.02 The Sustainable Drainage Assessment and Operation and Maintenance Plan will be part of a planning application to be made to Wolverhampton City Council.
- 1.03 The proposed development is for a planning application comprising an expansion teaching building for the existing facilities, a sports hall, mixed use sports pitch and parking and infrastructure.
- 1.04 The development lies entirely within Flood Zone 1 where there is a low probability of fluvial flooding occurring.
- 1.05 This Sustainable Drainage Assessment and Operation and Maintenance Plan follows government and local guidance on development and is undertaken in consultation with the relevant bodies.



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2.00 SITE LOCATION AND DESCRIPTION

- 2.01 The development site is 1.1ha in size of which 0.8ha is being redeveloped. It is located at Cambridge Street in Wolverhampton WV10 0JR. The Ordnance Survey National Grid reference to the centre of the site is E391880, N299461.
- 2.02 A site location Plan and aerial view can be found in **Appendix 1.**
- 2.03 The site comprises existing West Midlands Construction University Technical College and derelict land, on the former site of the M&B Springfield Brewery. The existing frontage remains as a listed building.
- 2.04 Parts of the existing UTC car parking area and sports pitch will be replaced by the new development, with the access bring retained.
- 2.05 The neighbouring land use is as follows:
 - North Cannock Road and Sports fields.
 - East Cambridge Street and residential.
 - South Industrial units.
 - West Rail line, canal, and industrial units
- 2.06 The site slopes from west at 137.00m AOD to east at 133.50mAOD with a noticeable embankment step midway across the site.
- 2.07 An existing access road has been installed around the north and west of the development plot.
- 2.08 A Topographical Survey can be found in **Appendix 2**.



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3.00 DEVELOPMENT PROPOSALS

- 3.01 The development is subject to a planning application. Reference should be made to the Design and Access Statement¹ for further detail on the planning application.
- 3.02 The development will consist of a new teaching complex adjoining the existing facilities, which will be retained.
- 3.03 A new standalone sports facility building will be provided with an adjoined outdoor multi use sports pitch.
- 3.04 Parking will be revised to provide 43 parking spaces accessed via the existing junction to the north.
- 3.05 The listed brewery wall fronting Cambridge Street is to be retained.
- 3.06 A copy of the Illustrative Masterplan Option can be found in **Appendix 3**.

¹ Associated Architects, 2021, Thomas Telford UTC Design and Access Statement.



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4.00 EXISTING GROUND CONDITIONS

- 4.01 Site Geology and Hydrology
 - 4.01.1 Applied Geology have undertaken a ground investigation survey² on the site in February 2020.
- 4.02 Ground Conditions
 - 4.02.1 Ground Geology
 - Hardstanding or made ground to 0.3m
 - Made ground to 0.3 to 3.4m
 - Glacial Till to 2.1 to 9.0m
 - Clent and Enville Sandstone and Mudstone formation from 8.43m
 - 4.02.2 Hydrogeology (subsurface water features)

Groundwater was found to be between 1.23 and 1.72m below ground.

4.02.3 Soakaway Design

The deep made ground and high water table would preclude the practical use of soakaways on this site.

4.02.4 Hydrology (surface water features)

The canal is located within 10m of the west of the site, but separated from it by the rail line. The River Stour is approximately 2.5km to the west.

² Applied Geology, February 2020, Report on Ground Investigation at Thomas Telford UTC, Wolverhampton, AG3187-20-AL75



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5.00 CONSULTATION AND POLICY

5.01 Drainage Authority

- 5.01.1 Severn Trent Water (STW) has been contacted for information regarding existing public storm and foul water sewers in the vicinity of the site.
- 5.01.2 A copy of the response from STW and the sewer records can be found in **Appendix 4.**
- 5.01.3 The sewer records provided by STW identify the following public sewers in the vicinity of the site:
 - A 300mm diameter foul sewer in Cambridge Street suitable for direct or indirect sewer connection
 - An unrecorded size storm sewer in Cambridge Street

5.01.4 Additional note:

Since 1st October 2011 many private sewers have been transferred into the ownership of the water authority as public sewers, where two or more properties in separate ownership are served by those sewers. Most of these former private sewers will not be shown on the public sewer records, therefore a full site survey should be carried out prior to any layout design or construction works to identify where these sewers may be and to avoid later delays and possible added costs.

5.02 Private Drainage

- 5.02.1 Two detailed CCTV surveys³ of the drainage on the site have been undertaken. This combined with historical design drawings for the existing UTC development, highlight a number of private sewers. This survey can be found in **Appendix 5**.
- 5.02.2 The existing site discharges storm water to the north into sewers in the road. This includes a flow control designed at 30 l/s restriction and an existing attenuation culvert sized at approximately 120m³.
- 5.02.3 The existing site discharges foul sewerage to the south into the public sewer.

³ Malcolm Hughes Chartered Land Surveyors, October 2020, Springfield Brewery Site Underground Survey 56212/UG

⁴ Sewer Surveys UK, September 2020, Thomas Telford UTC, CCTV Drainage Survey 20/338.



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- 5.03 Lead Local Flood Authority
 - 5.03.1 The Lead Local Flood Authority (LLFA) Wolverhampton City Council (WCC).
 - 5.03.2 The LLFA Local Policy is detailed in the Black Country Core Strategy⁵ Policy ENV5 Flood Risk, Sustainable Drainage Systems and Urban Heat Islands. Key criteria in this policy are:
 - Incorporate sustainable drainage Systems unless impact would be impractical, so as to improve water quality and reduce surface water runoff.
 - Open up culverted watercourses.
 - Reduces surface water flows back to equivalent greenfield rates.
 - Create new green spaces, increase tree cover and or provide green roofs.
 - 5.03.3 The LLFA also publish the Local Strategy for Flood Risk Management⁶. This reiterates the content of ENV5 and lists 6 key objectives for developments.
 - Understand and communicate flood risks
 - Manage the likelihood and impacts of flooding.
 - Help citizens to manage their own risk.
 - Ensure appropriate development.
 - Improve flood prediction, warning and recovery.
 - Work in partnership with others
 - 5.03.4 WCC may use Staffordshire County Council (SCC) as their LLFA consultant. SCC were contacted for preapplication advice, but advised that they were unable to offer this at the time of request. See correspondence in **Appendix 6**.
 - 5.03.5 SCC publish a SuDS Handbook⁷ which has been considered in the design of this development. This includes a SuDS proforma, a copy of which is included in Appendix 6.
- 5.04 Environment Agency
 - 5.04.1 The Environment Agency (EA) regulate main rivers and critical drainage areas and will be consulted as part of the planning application process. There are no key receptors in the vicinity of this development.

⁵ Black Country Core Strategy, February 2011

⁶ WSP, February 2016, Local Strategy for Flood Risk Management – The Black Country

⁷ Staffordshire County Council, February 2017, Sustainable Drainage Systems (SuDS) Handbook



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5.05 Applicable Policy and Guidance

5.05.1 National Planning Policy Framework

- 5.05.1.1 Planning Practice Guidance to the National Planning Policy Framework (NPPF) was introduced in March 2014 and was most recently updated in June 2019; it deals specifically with development planning zones. The NPPF requires that major developments should incorporate sustainable drainage systems unless there is clear evidence that this would be inappropriate. The systems used should:
 - Take account of advice from the lead local flood authority.
 - Have appropriate proposed minimum operational standards.
 - Have maintenance arrangements in place to ensure an acceptable standard of operation for the lifetime of the development.
 - Where possible, provide multifunctional benefits.

5.06 CIRIA C753 SuDS Manual

5.06.01 The SuDS Manual includes guidance for the planning, design, construction and maintenance of various types of sustainable drainage systems. Contained within the SuDS manual are various design checklists for the design of SuDS features, that seek to ensure correct design and efficient use of SuDS features proposed for a site.



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6.00 FLOOD RISK

- 6.01 The site is located in Flood Zone 1, the lowest risk of flooding with a probability of less than 0.1% in any one year.
- 6.02 A detailed Flood Risk Assessment for the wider UTC site was undertaken by Hydrock in 2015⁸. The findings of this assessment have been considered in this design.
- 6.03 As the area to be developed falls below 1ha in size, a specific Flood Risk Assessment has not been considered necessary. In the event one was required, the site would **pass the Sequential Test** as it is located in Flood Zone 1, and the Exception Test would not be required.

Table 1 - Flood Risk Assessment Summary

Aspects of Flood Risk	Assessment/Comment
Area liable to flooding	The development site lies entirely within FZ1 of the Environment Agency Flood Zone Map.
Probability of flooding occurring	Flooding from surface water at the site will be considered during the level and drainage design.
Standard of existing flood defences and their effectiveness	N/A
Likely depth of flooding	N/A
Rates of flow likely to be involved	N/A
Likelihood of impacts to other areas, properties and habitats	Any increase in the surface area, SUDS will be used for surface water management.
Effects of climate	The effects of climate change on flooding at the site are likely to be limited, due to the use of SuDS techniques and the system will be designed for 1 in 100 year storm event plus 40% climate change.

⁸ Hydrock, January 2015, Proposed University Technology College, Springfield Brewery, Wolverhampton, Flood Risk Assessment R/C14962/001.02



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7.00 SUSTAINABLE DRAINAGE PROPOSALS

- 7.01 Storm Water Management and SuDS
 - 7.01.1 Sustainable Drainage Systems (SuDS) involve the management of storm water from developments effectively in order to reduce the impact of run-off both to the site in question and properties downstream, and not to exacerbate existing problems. This is achieved by not increasing peak flows that will otherwise result from the development. The philosophy of SuDS is to mimic as closely as possible, the natural drainage from a site before development, and to ensure that storm water runoff is treated so there is no detriment to water quality of the receiving watercourse.

Using SuDS may provide water quantity and quality control, as well as increased amenity value. Appropriately designed and maintained schemes may improve the sustainable water management on site by:

- Reducing peak flows to watercourses or sewers and potentially reducing the risk of flooding downstream.
- Reducing the volume, rate of discharge, and the frequency of water flowing directly to watercourses or sewers from the developed sites.
- Improving water quality compared with conventional surface water sewers by removing pollutants.
- 7.01.2 The following section represents the considered views on suitable SuDS options appropriate to this site both as part of the detailed infrastructure scheme and outline illustrative masterplan. CIRIA C753° The SuDS Manual was consulted to examine the use of SuDS on this site. Conclusions are based on the assessment of the site and the evaluation of the relevant design requirements and regulatory consultation.
- 7.02 Potential SuDS Techniques Considered for this Site
 - 7.02.1 Green Roofs

Green roofs comprise a multi-layered system that covers the roof of a building or podium structure with vegetation cover, over a drainage layer. They are designed to intercept and retain precipitation, reducing the volume of run-off and attenuating peak flows.

Cost to the structure can be considerable and poor maintenance will leave it looking unsightly.

Not recommended for the site.

⁹ CIRIA, 2016. The SuDS Manual C753



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7.02.2 Soakaways

Soakaways are square or circular excavations either filled with rubble or lined with brickwork, precast concrete or polyethylene rings/perforated storage structures surrounded by granular backfill. They can be grouped and linked together to drain large areas including highways. The supporting structure and backfill can be substituted by modular geocellular units. Soakaways provide storm water attenuation, storm water treatment and groundwater recharge.

Ground Investigation data has shown a depth of made ground and high water table across the site. The use of infiltration will not therefore be viable.

Not viable for the site.

7.02.3 Swales

Swales are linear vegetated drainage features in which surface water can be stored or conveyed. They can be designed to allow infiltration, where appropriate. They should promote low flow velocities to allow much of the suspended particulate load in the storm water runoff to settle out, thus providing effective pollutant removal. Roadside swales can replace conventional gullies and drainage pipes.

Open water is not recommended for educational establishments due to safety concerns.

Not recommended for the site.

7.02.4 Pervious Pavements

Pervious pavements provide a pavement suitable for pedestrian and/or vehicular traffic, while allowing rainwater to infiltrate through the surface and into the underlying layers. The water is temporarily stored between infiltration to the ground, reuse or discharge to a watercourse or other drainage system. Pavements with aggregate sub-bases can provide good water quality treatment.

Due to the restricted site access, the use of permeable paving is not advisable due likely damage and loss of satisfactory function both during construction stage and in operation.

Not recommended for the site.



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7.02.5 Permeable Pitches

Pervious pitches such as MUGAs provide a pavement suitable for the undertaking of sports, while allowing rainwater to infiltrate through the surface and into the underlying layers. The water is temporarily stored between infiltration to the ground, reuse or discharge to a watercourse or other drainage system. Pavements with aggregate sub-bases can provide good water quality treatment.

The large mixed use games pitch is ideally suited to being a permeable surface with an open graded subbase for water attenuation and quality enhancement.

Recommended and proposed for the site.

7.02.6 Geo-cellular/Modular Systems

Modular plastic geo-cellular systems with a high void ratio that can be used to create a below ground storage structure.

Modular tanks can be used for runoff attenuation but requires silt trap protection and a suitable means of access for cleaning and inspection.

Recommended and proposed for the site.

7.02.7 Ponds/Infiltration Basin

Ponds can provide both storm water attenuation and treatment. They are designed to support emergent and submerged aquatic vegetation along their shoreline. Run off from each rain event is detained and treated in the pool. The retention time promotes removal through sedimentation and the opportunity for biological uptake mechanisms to reduce nutrient concentrations.

Open water is not recommended for educational establishments due to safety concerns and there is insufficient space on site for a viable size feature.

Not recommended for the site.



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8.00 SUSTAINABLE DRAINAGE MAINTENANCE

- 8.01 The various SuDS features will remain privately owned and be maintained by the Development's Maintenance team. The exact details of this arrangement will be defined with the future development.
- 8.02 The SuDS operation and maintenance strategy will be in accordance with CIRIA C753 best practice, as tabled below:

Table 2 – SuDS Operation and Maintenance Requirements

Type of maintenance	Details	Frequency	Duration	Large plant required	Cost
Routine maintenance	Inspect flow control chamber for evidence of poor operation.	Monthly for 3 months then annually.	1 hr	X	Low
	Remove debris from catchment surface and sports pitch.	Monthly	0.5 day	X	Low
	Remove sediment from catch-pits, flow control sumps.	Annually, or as required by inspection	0.5 day	√	medium
Remedial actions	Replace malfunctioning flow control parts.	As required	1 day	√	medium
Monitoring	Inspect all inlets, outlets, vents and overflows to ensure that they are in good condition and operating as designed.	Annually	1 hr	Х	Low
	Survey inside of attenuation tanks for sediment build up and remove if necessary.	Every 5 years or as required by inspection.	1 day	V	medium



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9.00 DRAINAGE STRATEGY

9.01 Drainage Strategy

- 9.01.1 The drainage strategy at the site must include consideration of the existing drainage infrastructure present.
- 9.01.2 It is intended that the existing UTC building drainage be retained with a separate outfall to that of the new development, thus retaining the historically agreed discharge rates of 30 l/s for that part of the site. Some localised diversion of drainage is required within the site to facilitate this including relocation of the existing attenuation provision.
- 9.01.3 In accordance with LLFA guidance, surface water discharge should be via natural means before consideration of discharge to a sewer network. As there are no watercourses accessible from the site and infiltration is not viable, discharge to the public sewer via the existing connection to Cambridge Street is proposed.

9.02 Proposed Surface Water Runoff Rate

- 9.02.1 The site consists of a total area of 1.09ha of which approximately 0.8ha is to be developed.
- 9.02.2 Based on the Modified Rational Method the existing site area brownfield run-off rate is estimated to be 151 l/s in the 50mm/hour intensity storm.
- 9.02.3 The design life for the development will be more than 40 years. Based on the Environment Agency Guidance for climate change published in February 2016¹⁰, a climate change allowance of 40% should be considered.
- 9.02.4 Using IH124 methodology the following greenfield runoff rates are anticipated for the new development:

Event	1 in 1 yr	1 in 30 yr	1 in 100 yr	Q _{bar}
Rate I/s	4.37	10.52	13.52	5.26

- 9.02.5 It is therefore proposed to restrict the new development area to a total discharge rate equivalent to Q_{bar} at **5.3 l/s**
- 9.02.6 This discharge restriction is over 95% betterment on theoretical brownfield runoff rate.

¹⁰ Gov.uk, 19 February 2016, Guidance Flood Risk Assessments: Climate Change Allowances



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9.03 Attenuation Volume

- 9.03.1 Using hydraulic modelling software, the total required attenuation for the total development is **380m**³ in a 100 year + 40% storm event.
- 9.03.2 This attenuation is provided via two below ground attention tanks at a total of 300m³, and open graded granular storage below the sports pitch at a total of 80m³.
- 9.03.3 The use of a petrol interceptor has not been deemed necessary as the parking area consists of less than 50 spaces and does not discharge to a sensitive receptor.

9.04 Exceedance Flows

9.04.1 The system is designed to contain the drainage in up to the design storm event. Should this be exceeded, overland flow will be directed away from the building to low points within the external parking and paved areas, from where it can be safely drained as the storm wanes.

9.05 Foul Drainage

9.05.01 The foul drainage for the new development will discharge via gravity at a new connection to the existing foul sewer to the north of the site. It is not feasible to direct flow to the existing site connection to the south, due to the constraints of the existing retained building.

9.06 Design and Calculations

- 9.06.1 CWA have prepared a drainage strategy drawing see **Appendix 7**.
- 9.06.2 Detailed hydraulic calculations for a range of intensity and duration storms have been undertaken using Causeway FLOW software. These can be found in **Appendix 8.**
- 9.06.3 A S106 indirect connection approval will be required from STW for the storm and foul connections.



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10.00 CONCLUSIONS

- 10.01 CWA was commissioned by Morgan Sindall Construction to prepare a Sustainable Drainage Assessment and Operation and Maintenance Plan for the planning application for a new development on the site at the West Midlands Construction University Technical College on Cambridge Street in Wolverhampton.
- 10.02 The proposed development is for a planning application comprising an expansion teaching building for the existing facilities, a sports hall, mixed use sports pitch and parking and infrastructure.
- 10.03 The existing UTC building drainage and outfall is to remain independent at the historically agreed 30 l/s restricted rate. Some on site drain division is however required.
- 10.04 Surface water for the new development will be designed to cater for storm events up to 1 in 100 plus 40% climate change. The new development areas will drain at a restricted rate of 5.3 l/s via vortex flow controls into the public sewer via existing site connections.
- 10.05 Approximately 380m³ of attenuation is required on site, split between underground tanks and open graded stone below a permeable sports pitch.
- 10.06 The site does not pose any increased flood risk to the site itself or adjacent developments and is not susceptible to flooding by other techniques.
- 10.07 The use of SuDS has been considered and can be incorporated within the design. The following SuDS techniques are proposed for the site:
 - Pervious sports pitches
 - Attenuation storage tank
- 10.08 Soakaways and infiltration techniques are not suitable for the site due to depths of made ground and high water table.
- 10.09 This report has been prepared to meet the requirements of the National Planning Policy Framework (NPPF) and in accordance with CIRIA C753 the SuDS Manual.



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APPENDICES

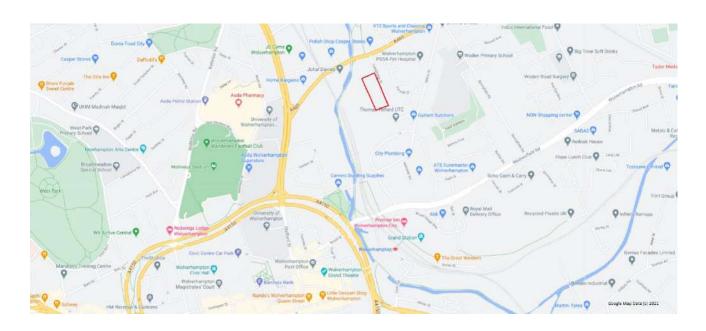


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Appendix 1 – Location Plan and Aerial View



CWA-20-196 TT UTC LOCATION PLAN







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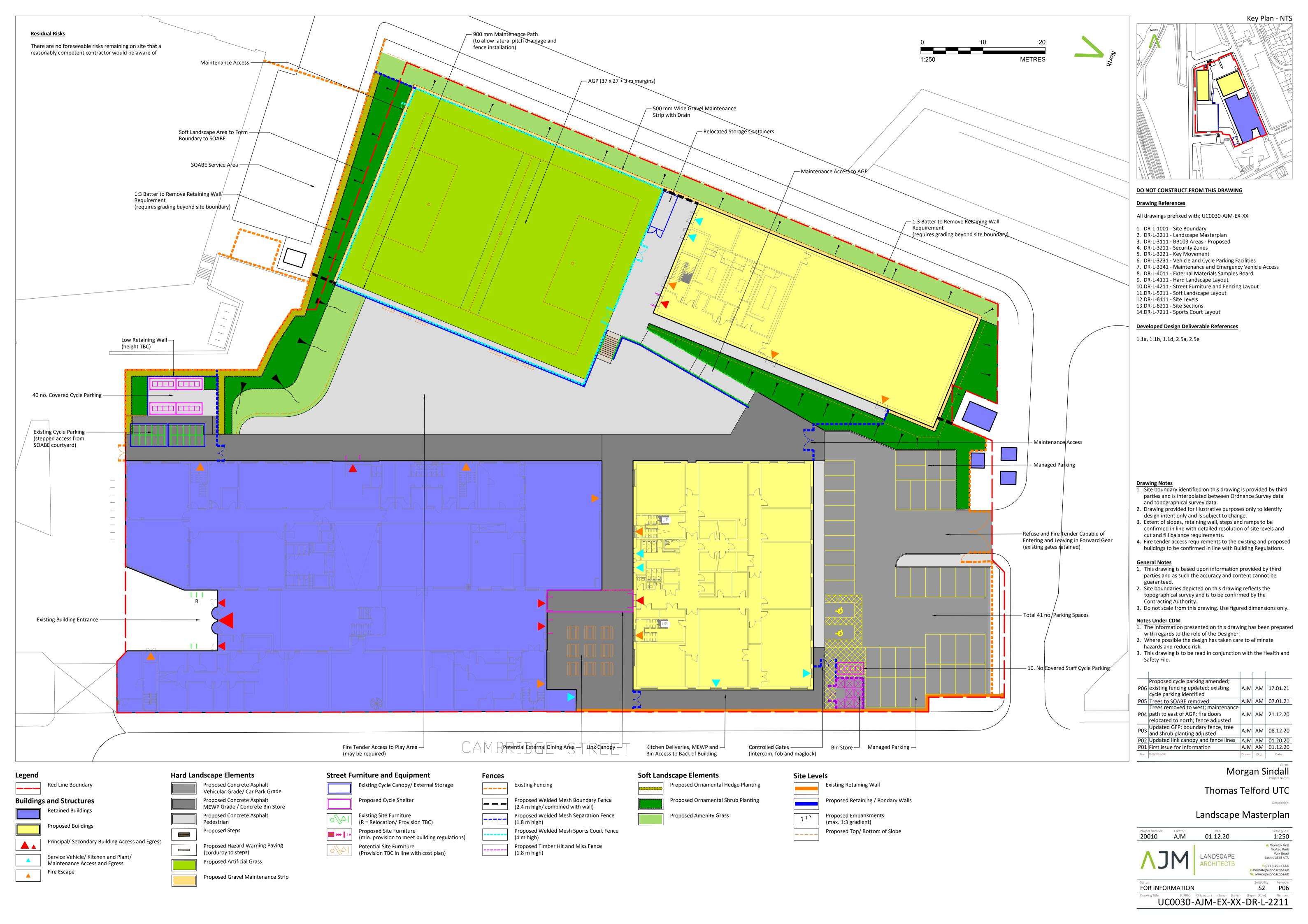
Appendix 2 - Topographical Survey





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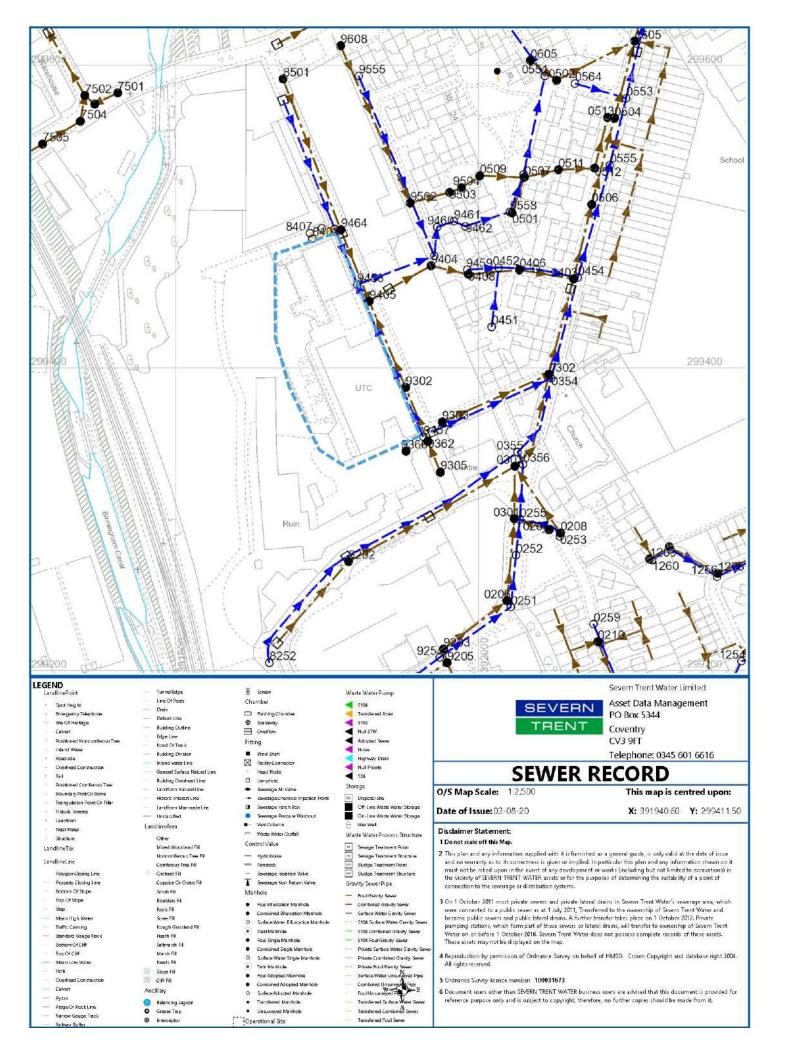
Appendix 3 – Masterplan





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Appendix 4 – Sewer Records



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SO92991014 136.02 134.91	SO91999453	133.235	131.385	130.08	s	VC	С	300	<unk></unk>	41.54	
SOS2990301 134.69 131.97 131.45 F VC C 225 LUNK> 66.73 311/21899 0000000 000000000 000000000000	SO92990501	130.9499	128.93	128.32	F	VC	С	150	<unk></unk>	40.85	
SO92991201 131.5399 129.15 127.97 F VC C 225 <unks 00.00.00="" 1889="" 2="" 31="" 99.17="" td="" ="" <=""><td>SO92990104</td><td>136.02</td><td>134.91</td><td><unk></unk></td><td>F</td><td>VC</td><td>С</td><td>225</td><td><unk></unk></td><td>0</td><td></td></unks>	SO92990104	136.02	134.91	<unk></unk>	F	VC	С	225	<unk></unk>	0	
SO92991207 133.3 131.48 130.96 F VC C 225 LUNKS 69.88 311/21/899 00:00:00 C 225 LUNKS 20:00:00 C 225 LUNKS 20:00:00:00 C 225 LUNKS 20:00:00:00:00:00:00:00:00:00:00:00:00:0	SO92990301	134.69	131.97	131.45	F	VC	С	225	<unk></unk>	66.73	31/12/1899 00:00:00
SO92991601 125.7799 123.88 121.48 F	SO92991201	131.5399	129.15	127.97	F	VC	С	225	<unk></unk>	99.17	
SO92991756 124.6399 122.8 122.31 S VC C 225 <unks 0="" 00.00.00="" 117.69="" 12="" 127.27="" 128.22="" 128.37="" 128.96="" 129.37="" 129.41="" 129.94="" 130.53="" 130.6399="" 130.9299="" 131.1849="" 131.19="" 131.24="" 131.32="" 131.47="" 131.68="" 132.41="" 132.52="" 132.7="" 132.95="" 132.975="" 133.16="" 133.4799="" 133.6="" 133.6999="" 133.8="" 134.02="" 134.06="" 134.86="" 134.87="" 134.94="" 134.95="" 134.96="" 135.63="" 135.7299="" 135.82="" 135.96="" 189.91="" 1899="" 208.56="" 225="" 300="" 31="" 375="" 46.13="" 50.62="" 53.42="" 600="" 64.54="" 774="" 88.5="" <unks="" c="" co="" f="" s="" so91999462="" so92990059="" so92990060="" so92990150="" so92990151="" so92990152="" so92990152<="" so92990155="" so92990303="" so92990403="" so92990560="" so92991011="" so9299103="" so92991112="" so92991260="" so931="" td="" vc="" =""><td>SO92991207</td><td>133.3</td><td>131.48</td><td>130.96</td><td>F</td><td>VC</td><td>С</td><td>225</td><td><unk></unk></td><td>69.88</td><td>31/12/1899 00:00:00</td></unks>	SO92991207	133.3	131.48	130.96	F	VC	С	225	<unk></unk>	69.88	31/12/1899 00:00:00
SO91999462 131.1849 129.41 129.37 S VC C 300 <unk> 774 311/271899 00:00:00 C C C C C C C C C </unk>	SO92991601	125.7799	123.88	121.48	F	VC	С	<unk></unk>	<unk></unk>	31.13	
SO92990155 135.96 134.96 134.87 S VC C 225 <unk> 208.56 31/12/1899 00.00.00 SO92990303 134.02 131.19 129.94 F VC C 300 <unk> 53.42 31/12/1899 00.00.00 SO92990403 135.63 134.06 133.8 S VC C 225 <unk> 88.5 31/12/1899 00.00.00 SO92990403 130.9299 128.37 127.27 F VC C 275 <unk> 46.13 31/12/1899 00.00.00 SO92991112 133.6999 132.52 132.41 F VC C 225 <unk> 189.91 31/12/1899 00.00.00 SO92991260 133.4799 131.32 131.24 S VC C 225 <unk> 173.63 31/12/1899 00.00.00 SO92991011 133.6 131.68 <unk> F VC C 225 <unk> 0 31/12/1899 00.00.00 SO92991011 133.6 131.68 <unk> F VC C 225 <unk> 0 31/12/1899 00.00.00 SO92990103 135.82 134.95 134.94 F VC C 225 <unk> 1276 31/12/1899 00.00.00 SO92990260 135.7299 132.89 132.02 F VC C 225 <unk> 50.62 31/12/1899 00.00.00 SO92990560 130.6399 128.96 128.22 S VC C 225 <unk> 50.62 31/12/1899 00.00.00 SO92990560 130.6399 128.96 128.22 S VC C 375 <unk> 58.5 31/12/1899 00.00.00 SO92990152 134.86 132.7 131.47 S CO C 600 <unk> 58.9 31/12/1899 00.00.00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO02990152 134.86 31/12/1899 SO02990152 134.86 133.16</unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk>	SO92991756	124.6399	122.8	122.31	S	VC	С	225	<unk></unk>	117.69	
SO92990303 134.02 131.19 129.94 F VC C 300 <unk> 53.42 31/12/1899 00:00:00</unk>	SO91999462	131.1849	129.41	129.37	S	VC	С	300	<unk></unk>	774	
SO92990059 135.63 134.06 133.8 S VC C 225 <unk> 88.5 31/12/1899 00:00:00 SO92990403 130.9299 128.37 127.27 F VC C 375 <unk> 46.13 31/12/1899 00:00:00 SO92991112 133.6999 132.52 132.41 F VC C 225 <unk> 189.91 31/12/1899 00:00:00 SO92991260 133.4799 131.32 131.24 S VC C 225 <unk> 173.63 31/12/1899 00:00:00 SO92991011 133.6 131.68 <unk> F VC C 225 <unk> 0 31/12/1899 00:00:00 SO92991011 133.849 129.555 129.54 S VC C 300 <unk> 585 31/12/1899 00:00:00 SO92990103 135.82 134.94 F VC C 225 <unk> 1276 31/12/1899 00:00:00 SO92990206 135.7299 132.89 132.02 F VC C 225 <unk> 62.55 31/12/1899 SO92990451 131.9799 130.53 129.75 S VC C 225 <unk> 50.62 31/12/1899 SO92990560 130.6399 128.96 128.22 S VC C 375 <unk> 89.85 31/12/1899 SO92990152 134.86 132.7 131.47 S CO C 600 <unk> 35.89 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 33.16 33.16 33.16 33.16 33.17 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 34.86 33.16 33.16 33.16 33.16 33.17 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 34.86 33.16 33.16 33.16 33.16 33.16 33.16 33.16 33.16 33.1</unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk>	SO92990155	135.96	134.96	134.87	S	VC	С	225	<unk></unk>	208.56	
SO92990403 130.9299 128.37 127.27 F VC C 375 <unk> 46.13 31/12/1899 00:00:00 00:00:0</unk>	SO92990303	134.02	131.19	129.94	F	VC	С	300	<unk></unk>	53.42	
SO92991112 133.6999 132.52 132.41 F	SO92990059	135.63	134.06	133.8	S	VC	С	225	<unk></unk>	88.5	
SO92991260 133.4799 131.32 131.24 S VC C 225 <unk> 173.63 31/12/1899 0:00:00:00 SO92991011 133.6 131.68 <unk> F VC C 225 <unk> 0 31/12/1899 0:00:00:00 SO91999460 131.3849 129.555 129.54 S VC C 300 <unk> 585 31/12/1899 0:00:00:00 SO92990103 135.82 134.95 134.94 F VC C 225 <unk> 1276 31/12/1899 0:00:00:00 SO92990206 135.7299 132.89 132.02 F VC C 225 <unk> 62.55 31/12/1899 0:00:00:00 SO92990451 131.9799 130.53 129.75 S VC C 225 <unk> 50.62 31/12/1899 0:00:00:00 SO92990560 130.6399 128.96 128.22 S VC C 375 <unk> 89.85 31/12/1899 0:00:00:00 SO92990152 134.86 132.7 S VC C 375 <unk> 64.54 31/12/1899 0:00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 0:00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 0:00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 0:00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 0:00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 0:00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 0:00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 0:00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 0:00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 0:00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 0:00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 S S S S S S S S S </unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk>	SO92990403	130.9299	128.37	127.27	F	VC	С	375	<unk></unk>	46.13	
SO92991011 133.6 131.68 CUNK> F VC C 225 CUNK> 0 31/12/1899 00:00:00	SO92991112	133.6999	132.52	132.41	F	VC	С	225	<unk></unk>	189.91	
SO91999460 131.3849 129.555 129.54 S VC C 300 <unk> 585 31/12/1899 00:00:00 SO92990103 135.82 134.95 134.94 F VC C 225 <unk> 1276 31/12/1899 00:00:00 SO92990206 135.7299 132.89 132.02 F VC C 225 <unk> 62.55 31/12/1899 00:00:00 SO92990451 131.9799 130.53 129.75 S VC C 225 <unk> 50.62 31/12/1899 00:00:00 SO92990560 130.6399 128.96 128.22 S VC C 375 <unk> 89.85 31/12/1899 00:00:00 SO92990151 134.86 132.7 131.47 S CO C 600 <unk> 35.89 31/12/1899 00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 00:00:00 SO92990152 34.86 33.1</unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk>	SO92991260	133.4799	131.32	131.24	S	VC	С	225	<unk></unk>	173.63	
SO92990103 135.82 134.95 134.94 F VC C 225 <unk> 1276 31/12/1899 00:00:00 SO92990206 135.7299 132.89 132.02 F VC C 225 <unk> 62.55 31/12/1899 00:00:00 SO92990451 131.9799 130.53 129.75 S VC C 225 <unk> 50.62 31/12/1899 00:00:00 SO92990560 130.6399 128.96 128.22 S VC C 375 <unk> 89.85 31/12/1899 00:00:00 SO92990151 134.86 132.7 131.47 S CO C 600 <unk> 35.89 31/12/1899 00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 34.86 33.16 33.16 33.75 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 34.86 33.16 33.16 33.75 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 34.86 33.16 33.16 33.75 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 34.86 34.72 34.86 34.72 34.86 34.72 34.86 34.72 34.86 34.72 34.86 34.72 34.86 34.72 34.86 34.72 34.86 34.72 34.86 34.72 34.86 34.72 34.86 34.72 34.86 34.86 34.72 34.86 34</unk></unk></unk></unk></unk></unk></unk></unk></unk></unk></unk>	SO92991011	133.6	131.68	<unk></unk>	F	VC	С	225	<unk></unk>	0	
SO92990206 135.7299 132.89 132.02 F VC C 225 <unk> 62.55 31/12/1899 00:00:00 SO92990451 131.9799 130.53 129.75 S VC C 225 <unk> 50.62 31/12/1899 00:00:00 SO92990560 130.6399 128.96 128.22 S VC C 375 <unk> 89.85 31/12/1899 00:00:00 SO92990151 134.86 132.7 131.47 S CO C 600 <unk> 35.89 31/12/1899 00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899</unk></unk></unk></unk></unk>	SO91999460	131.3849	129.555	129.54	S	VC	С	300	<unk></unk>	585	
SO92990451 131.9799 130.53 129.75 S VC C 225 <unk> 50.62 31/12/1899 00:00:00 </unk>	SO92990103	135.82	134.95	134.94	F	VC	С	225	<unk></unk>	1276	
SO92990560 130.6399 128.96 128.22 S VC C 375 <unk> 89.85 31/12/1899 00:00:00 SO92990151 134.86 132.7 131.47 S CO C 600 <unk> 35.89 31/12/1899 00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899 SO92990152 SO92990</unk></unk></unk></unk>	SO92990206	135.7299	132.89	132.02	F	VC	С	225	<unk></unk>	62.55	
SO92990151 134.86 132.7 131.47 S CO C 600 <unk> 35.89 31/12/1899 00:00:00 SO92990152 134.86 133.16 132.7 S VC C 375 <unk> 64.54 31/12/1899</unk></unk>	SO92990451	131.9799	130.53	129.75	S	VC	С	225	<unk></unk>	50.62	
Note	SO92990560	130.6399	128.96	128.22	S	VC	С	375	<unk></unk>	89.85	
	SO92990151	134.86	132.7	131.47	S	СО	С	600	<unk></unk>	35.89	
	SO92990152	134.86	133.16	132.7	S	VC	С	375	<unk></unk>	64.54	

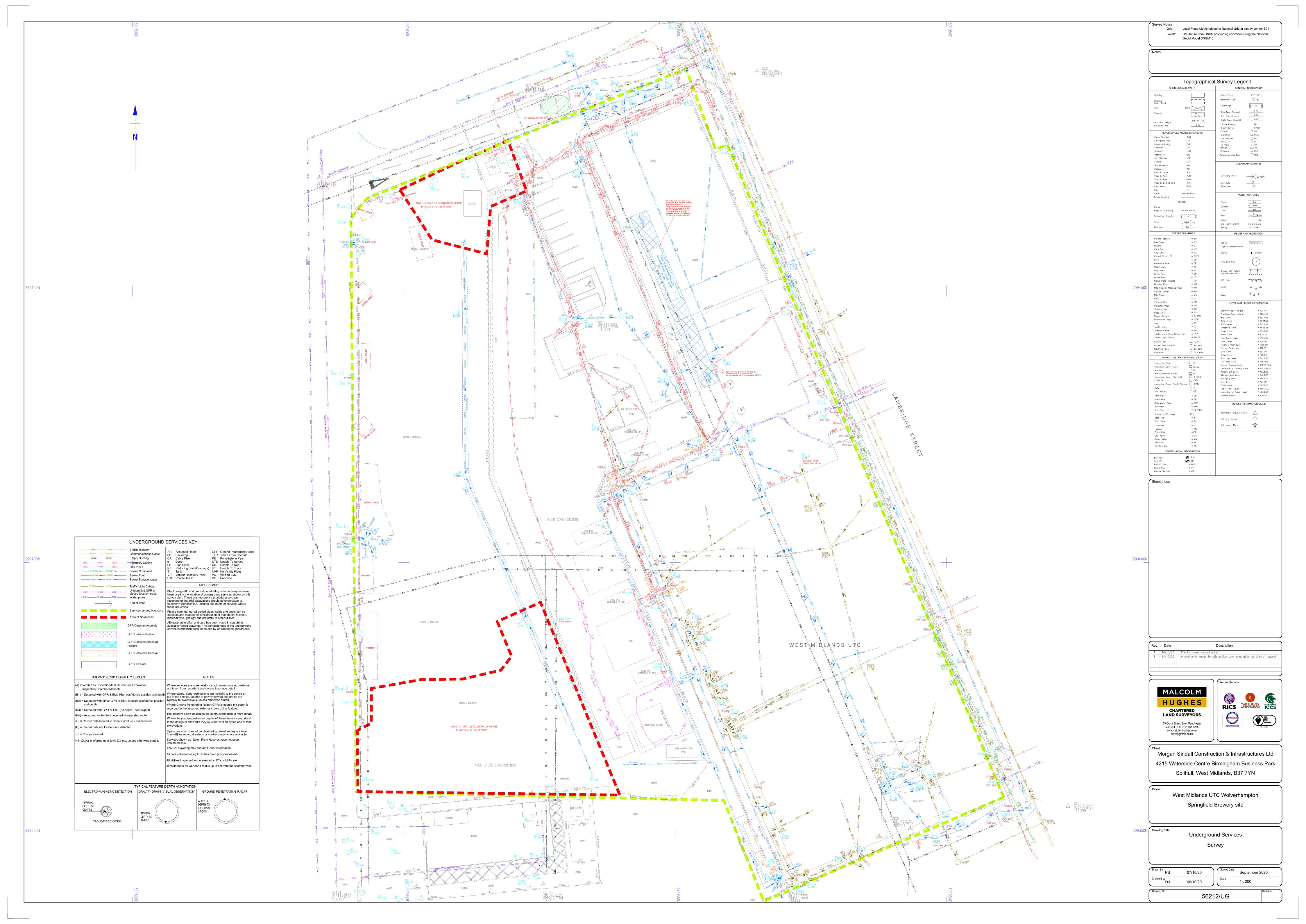
			.с. т.рс							
Reference	Cover Level	Invert Level Upstream	Invert Level Downstream	Purpose	Material	Pipe Shape	Max Size	Min Size	Gradient	Year Laid
SO92990152	134.86	133.16	132.7	S	VC	С	375	<unk></unk>	64.59	31/12/1899 00:00:00
SO92990354	132.6499	131.19	129.28	S	VC	С	300	<unk></unk>	36.05	31/12/1899 00:00:00
SO92990512	129.36	127.79	127.06	F	VC	С	150	<unk></unk>	47.34	31/12/1899 00:00:00
SO92990555	129.0099	127.34	126.17	S	VC	С	225	<unk></unk>	38.97	31/12/1899 00:00:00
SO92991059	133.8	132.1	132.02	S	VC	С	225	<unk></unk>	226.13	31/12/1899 00:00:00
SO92991109	133.72	132.02	131.71	F	VC	С	225	<unk></unk>	143.87	31/12/1899 00:00:00
SO92991156	133.6799	131.93	131.79	S	СО	С	400	<unk></unk>	166.5	31/12/1899 00:00:00
SO92991161	133.55	132.14	132.04	S	VC	С	225	<unk></unk>	152.1	31/12/1899 00:00:00
SO92991652	125.773	124.28	123.7	S	VC	С	225	<unk></unk>	71.52	31/12/1899 00:00:00
SO91999303	133.8849	130.76	129.99	F	VC	С	225	<unk></unk>	100.29	31/12/1899 00:00:00
SO92990654	129.8	127.67	<unk></unk>	S	VC	С	375	<unk></unk>	0	31/12/1899 00:00:00
SO92990253	134.58	133.19	132.98	S	VC	С	225	<unk></unk>	144.1	31/12/1899 00:00:00
SO92990502	129.16	125.77	124.71	F	VC	С	300	<unk></unk>	54.59	31/12/1899 00:00:00
SO91999404	131.4499	128.78	129.3	F	VC	С	300	<unk></unk>	<unk></unk>	31/12/1899 00:00:00
SO92990251	135.6999	133.95	133.47	S	VC	С	300	<unk></unk>	71.63	31/12/1899 00:00:00
SO92990355	133.9199	132.26	131.2	S	VC	С	300	<unk></unk>	52.44	31/12/1899 00:00:00
SO92990452	131.1499	129.69	129.41	S	VC	С	225	<unk></unk>	87.93	31/12/1899 00:00:00
SO92990455	130.9499	129.41	129.26	S	VC	С	225	<unk></unk>	187.73	31/12/1899 00:00:00
SO92990507	130.4799	128.3	127.97	F	VC	С	150	<unk></unk>	70.21	31/12/1899 00:00:00
SO92990509	131.41	128.79	128.3	F	VC	С	150	<unk></unk>	60.04	31/12/1899 00:00:00
SO92990210	134.3399	133.12	132.55	F	VC	С	225	<unk></unk>	130.16	31/12/1899 00:00:00
SO92990302	132.58	129.94	128.58	F	VC	С	375	<unk></unk>	42.89	31/12/1899 00:00:00
SO92990506	129.66	127.25	125.87	F	VC	С	375	<unk></unk>	42.71	31/12/1899 00:00:00
SO92990553	127.8199	126.15	124.55	S	VC	С	225	<unk></unk>	19.71	31/12/1899 00:00:00
SO92990564	128.69	127.44	126.24	S	VC	С	225	<unk></unk>	29.3	31/12/1899 00:00:00
SO92991753	125.83	122.45	121.99	S	VC	С	450	<unk></unk>	110.26	31/12/1899 00:00:00
SO92991163	133.71	132.02	131.85	S	vc	С	225	<unk></unk>	143.94	31/12/1899 00:00:00
SO92991151	133.4799	131.19	130.17	S	СО	С	750	<unk></unk>	38.15	31/12/1899 00:00:00
SO92991158	133.74	132.01	131.96	S	VC	С	300	<unk></unk>	521.8	31/12/1899 00:00:00
SO92991256	132.44	130.9	129.81	S	VC	С	225	<unk></unk>	31.16	31/12/1899 00:00:00
SO92991258	133.25	131.15	130.92	S	VC	С	225	<unk></unk>	155.87	31/12/1899 00:00:00
SO91999461	131.285	129.505	129.41	S	VC	С	300	<unk></unk>	82.5	31/12/1899 00:00:00
SO92990757	129.27	126.97	125.34	S	vc	С	225	<unk></unk>	35.13	31/12/1899 00:00:00
SO92990205	134.66	132.15	132.04	F	vc	С	225	<unk></unk>	220	31/12/1899 00:00:00
SO92990454	130.94	129.25	127.35	S	VC	С	225	<unk></unk>	40.67	31/12/1899 00:00:00
SO92990513	128.6199	127.06	126.09	F	VC	С	150	<unk></unk>	4.67	31/12/1899 00:00:00
SO92991154	133.91	131.78	131.73	s	со	С	400	<unk></unk>	366.4	31/12/1899 00:00:00
SO92991205	132.41	130.92	129.21	F	VC	С	225	<unk></unk>	19.82	31/12/1899 00:00:00
SO91997101	145.6979	141.18	144.11	F	BR	С	450	<unk></unk>	<unk></unk>	31/12/1899 00:00:00
SO92990156	136.02	134.87	134.1	S	VC	С	225	<unk></unk>	59.47	31/12/1899 00:00:00
SO92990705	128.75	126	125.4	F	VC	С	225	<unk></unk>	43.28	31/12/1899 00:00:00
SO92990208	134.63	131.82	131.47	F	VC	С	300	<unk></unk>	152.54	31/12/1899 00:00:00

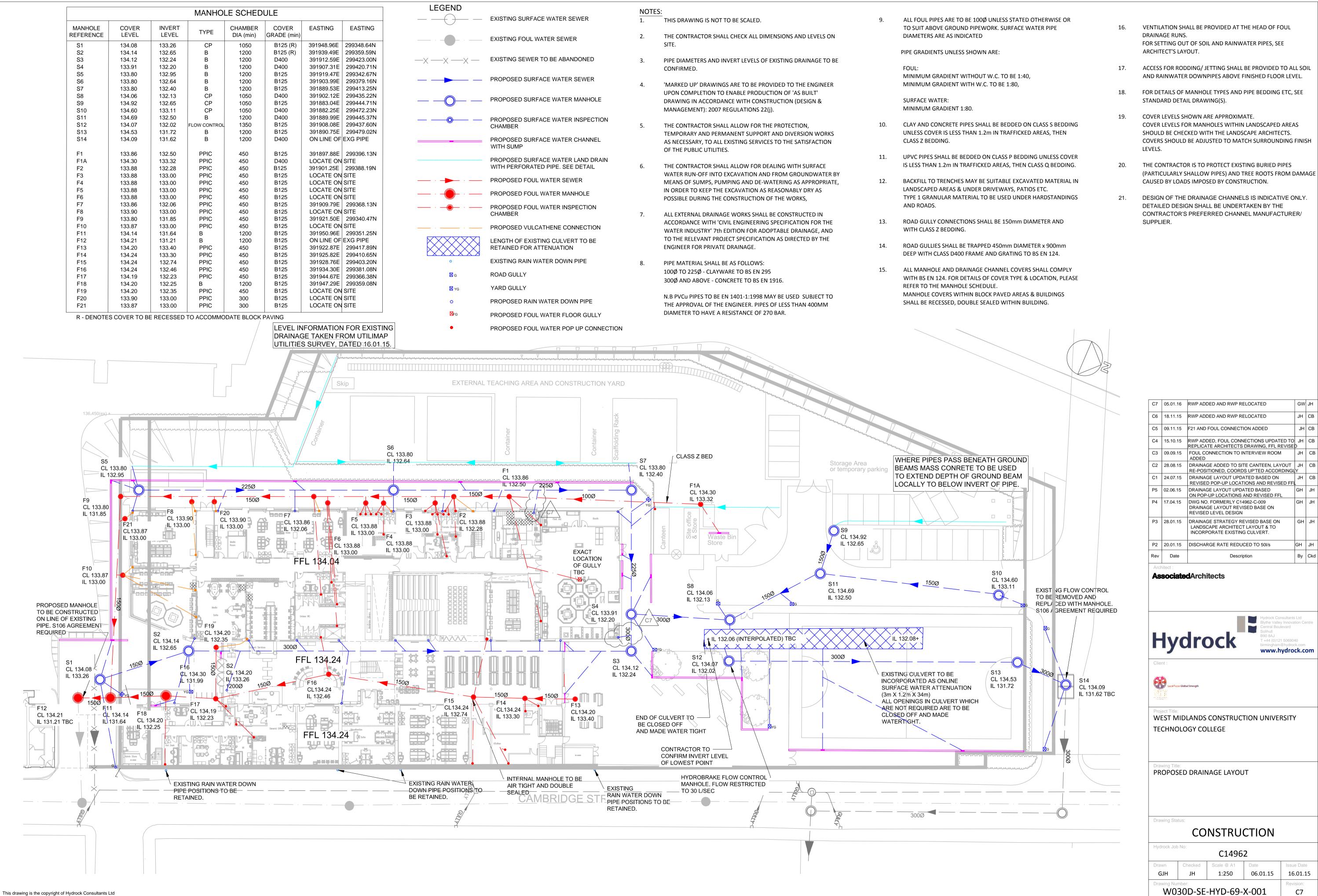
Reference	Cover Level	Invert Level Upstream	Invert Level Downstream	Purpose	Material	Pipe Shape	Max Size	Min Size	Gradient	Year Laid
SO92990511	129.9799	127.97	127.81	F	VC	С	150	<unk></unk>	150.13	31/12/1899 00:00:00
SO92991010	133.8399	132.74	132.55	F	VC	С	225	<unk></unk>	145.58	31/12/1899 00:00:00
SO92991105	133.94	132.41	132.25	F	VC	С	225	<unk></unk>	144	31/12/1899 00:00:00
SO92991202	132.38	129.71	128.9	F	VC	С	225	<unk></unk>	99.4	31/12/1899 00:00:00
SO92991253	131.8399	129.73	128.18	S	VC	С	225	<unk></unk>	77.23	31/12/1899 00:00:00
SO92991254	132.55	130.13	129.21	s	СО	С	750	<unk></unk>	93.62	31/12/1899 00:00:00
SO92990252	135.13	133.4	132.94	s	VC	С	300	<unk></unk>	51.8	31/12/1899 00:00:00
SO92990255	134.6199	132.92	132.67	S	VC	С	300	<unk></unk>	146.28	31/12/1899 00:00:00
SO92990356	134.08	132.63	132.28	S	VC	С	300	<unk></unk>	25.06	31/12/1899 00:00:00
SO92990406	131.1	128.95	128.53	F	VC	С	300	<unk></unk>	86.48	31/12/1899 00:00:00
SO92990558	130.94	129.26	128.96	S	VC	С	375	<unk></unk>	88.57	31/12/1899 00:00:00
SO92990605	129.5399	126.74	126.01	F	VC	С	225	<unk></unk>	29.62	31/12/1899 00:00:00
SO92990259	134.24	132.16	131.83	S	со	С	300	<unk></unk>	264.61	31/12/1899 00:00:00
SO92990504	128.2799	125.87	124.59	F	VC	С	375	<unk></unk>	41.27	31/12/1899 00:00:00
SO92991103	133.9799	132.53	132.41	F	VC	С	225	<unk></unk>	186.25	31/12/1899 00:00:00
SO92991152	134.0299	131.47	131.19	S	со	С	600	<unk></unk>	186.43	31/12/1899 00:00:00
SO92991209	133.46	131.58	131.54	F	VC	С	225	<unk></unk>	386	31/12/1899 00:00:00
SO92991605	126.97	124.51	123.97	F	VC	С	375	<unk></unk>	123.8	31/12/1899 00:00:00
SO92991107	133.66	132.21	132.03	F	VC	С	225	<unk></unk>	136.83	31/12/1899 00:00:00
SO92991604	125.0299	121.91	121.59	F	VC	С	300	<unk></unk>	173.72	31/12/1899 00:00:00
SO92991100	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	U	100	<unk></unk>	<unk></unk>	31/12/1899 00:00:00
<unk></unk>	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	<unk></unk>	<unk></unk>	<unk></unk>	<unk></unk>	31/12/1899 00:00:00
<unk></unk>	<unk></unk>	<unk></unk>	<unk></unk>	S	VC	<unk></unk>	<unk></unk>	<unk></unk>	<unk></unk>	31/12/1899 00:00:00



February 2021 Page 23 Thomas Telford UTC SuDS Assessment and Operation and Maintenance Plan

Appendix 5 – CCTV Drainage Surveys





- FOR SETTING OUT OF SOIL AND RAINWATER PIPES, SEE
- FOR DETAILS OF MANHOLE TYPES AND PIPE BEDDING ETC, SEE
- COVER LEVELS FOR MANHOLES WITHIN LANDSCAPED AREAS SHOULD BE CHECKED WITH THE LANDSCAPE ARCHITECTS. COVERS SHOULD BE ADJUSTED TO MATCH SURROUNDING FINISH
- THE CONTRACTOR IS TO PROTECT EXISTING BURIED PIPES (PARTICULARLY SHALLOW PIPES) AND TREE ROOTS FROM DAMAGE
- DESIGN OF THE DRAINAGE CHANNELS IS INDICATIVE ONLY. DETAILED DESIGN SHALL BE UNDERTAKEN BY THE CONTRACTOR'S PREFERRED CHANNEL MANUFACTURER/

JH CB

By Ckd

www.hydrock.com

16.01.15

C7



February 2021 Page 24 Thomas Telford UTC SuDS Assessment and Operation and Maintenance Plan

Appendix 6 – LLFA Correspondence

Andrew Hardy

From: Flood Risk Management Team <flood.team@staffordshire.gov.uk>

Sent: 01 December 2020 11:39

To: Andrew Hardy

Subject: RE: Request for Pre-application advice - Thomas Telford UTC, Wolverhampton

Good morning Andrew,

Thank you for your enquiry. We are unable to offer a pre-application advice service direct to applicants for development sites outside of Staffordshire. Our agreement with City of Wolverhampton Council relates to Statutory consultations only, but they can request pre-application advice from us for a fee when we have the capacity to deliver this.

Unfortunately, due to current workload, we are not able to offer the pre-application service at this time.

We apologise for the inconvenience.



County Council

Kind regards

Flood Risk Management Team, Staffordshire County Council
Office Location: Lichfield Highways, Trent Valley Road, Lichfield, WS13 6EU
Postal Address: 2 Staffordshire Place, Tipping Street, Stafford, ST16 2DH

: www.staffordshire.gov.uk

Providing a Flood Risk Management service for Staffordshire County, Sandwell, Walsall and Wolverhampton Councils.

From: Andrew Hardy <ahardy@cwa-eng.com>

Sent: 01 December 2020 08:58

To: Flood Risk Management Team <flood.team@staffordshire.gov.uk>

Subject: Request for Pre-application advice - Thomas Telford UTC, Wolverhampton

Dear Flood Team

We are developing a new build extension block and associated external sports facilities for the existing Thomas Telford UTC education building at Cambridge Street in Wolverhampton. We understand that Staffordshire County Council act as LLFA for the City of Wolverhampton.

We would like to seek pre-application advice with regard to this development prior to the issue of a formal planning submission in the coming months. We are aware of your SuDS Handbook and the best practice advice given within it, and would look to observe this with the new development. Our main requirement for pre-application advice, would be to understand and seek agreement for the integration of this new build element with the existing drainage systems, without impeding the established development.

We note that a review of the draft strategy has a charge of £360+vat.

Please can you confirm that that SCC are the correct authority acting as LLFA for this area, and that the Developer Online Advice/Data Request Form is the most appropriate means of requesting this advice.

Andrew Hardy Associate Director	
M: 07736 164 776 T: 0121 270 6962 ahardy@cwa-eng.com www.cwa-eng.com	Lancaster House 67 Newhall Street Birmingham B3 1NQ
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Registered Office: Spring Lodge, 172 Chester Road, Helsby, Cheshire, England, WA6 0AR. Registered Company Number: 07709882. VAT Number: GB 125 2007 63

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Thank you for your assistance.

Regards

Andrew

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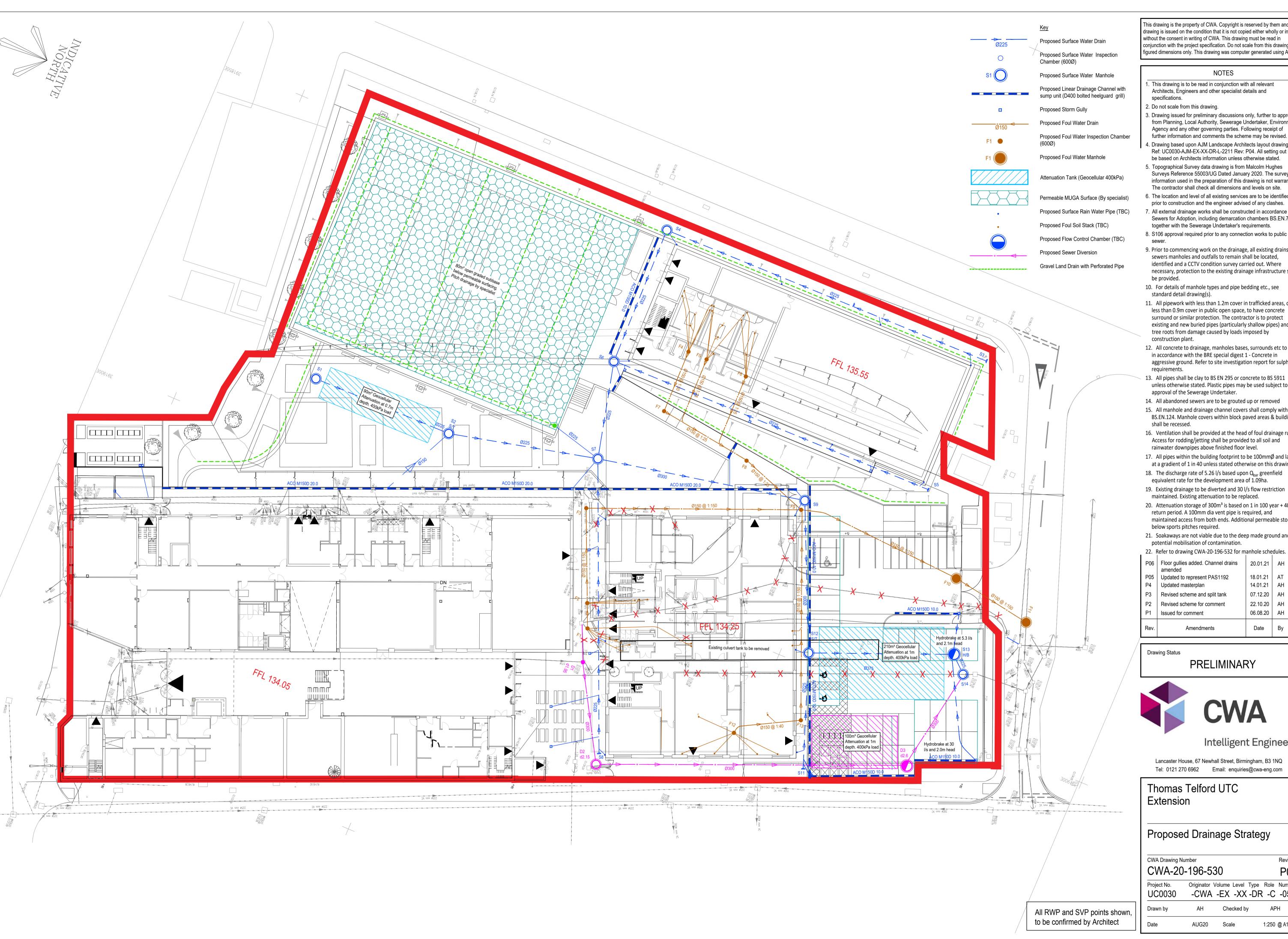
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Appendix 7 – Drainage Strategy Drawing



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- This drawing is to be read in conjunction with all relevant Architects, Engineers and other specialist details and
- 2. Do not scale from this drawing.
- 3. Drawing issued for preliminary discussions only, further to approval from Planning, Local Authority, Sewerage Undertaker, Environment
- 4. Drawing based upon AJM Landscape Architects layout drawing: Ref: UC0030-AJM-EX-XX-DR-L-2211 Rev: P04. All setting out is to
- be based on Architects information unless otherwise stated. 5. Topographical Survey data drawing is from Malcolm Hughes Surveys Reference 55003/UG Dated January 2020. The survey
- information used in the preparation of this drawing is not warranted. The contractor shall check all dimensions and levels on site. 6. The location and level of all existing services are to be identified
- prior to construction and the engineer advised of any clashes. 7. All external drainage works shall be constructed in accordance with
- Sewers for Adoption, including demarcation chambers BS.EN.752 together with the Sewerage Undertaker's requirements.
- 8. S106 approval required prior to any connection works to public
- 9. Prior to commencing work on the drainage, all existing drains, sewers manholes and outfalls to remain shall be located, identified and a CCTV condition survey carried out. Where necessary, protection to the existing drainage infrastructure shall be provided.
- 10. For details of manhole types and pipe bedding etc., see standard detail drawing(s).
- 11. All pipework with less than 1.2m cover in trafficked areas, or less than 0.9m cover in public open space, to have concrete surround or similar protection. The contractor is to protect existing and new buried pipes (particularly shallow pipes) and tree roots from damage caused by loads imposed by construction plant.
- 12. All concrete to drainage, manholes bases, surrounds etc to be in accordance with the BRE special digest 1 - Concrete in aggressive ground. Refer to site investigation report for sulphate
- 13. All pipes shall be clay to BS EN 295 or concrete to BS 5911 unless otherwise stated. Plastic pipes may be used subject to the approval of the Sewerage Undertaker.
- 14. All abandoned sewers are to be grouted up or removed 15. All manhole and drainage channel covers shall comply with
- BS.EN.124. Manhole covers within block paved areas & buildings
- 16. Ventilation shall be provided at the head of foul drainage runs. Access for rodding/jetting shall be provided to all soil and rainwater downpipes above finished floor level.
- 17. All pipes within the building footprint to be 100mmØ and laid at a gradient of 1 in 40 unless stated otherwise on this drawing.
- 18. The discharge rate of 5.26 l/s based upon Q_{bar} greenfield equivalent rate for the development area of 1.09ha.
- 19. Existing drainage to be diverted and 30 l/s flow restriction maintained. Existing attenuation to be replaced.
- 20. Attenuation storage of 300m³ is based on 1 in 100 year + 40% return period. A 100mm dia vent pipe is required, and maintained access from both ends. Additional permeable storage below sports pitches required.
- 21. Soakaways are not viable due to the deep made ground and potential mobilisation of contamination.
- 22. Refer to drawing CWA-20-196-532 for manhole schedules.

P06	Floor gullies added. Channel drains amended	20.01.21	АН	ME
P05	Updated to represent PAS1192	18.01.21	ΑT	ME
P4	Updated masterplan	14.01.21	AH	ME
P3	Revised scheme and split tank	07.12.20	AH	ME
P2	Revised scheme for comment	22.10.20	AH	ME
P1	Issued for comment	06.08.20	AH	ME
Rev.	Amendments	Date	Ву	Chkd.

Drawing Status

PRELIMINARY



Lancaster House, 67 Newhall Street, Birmingham, B3 1NQ Tel: 0121 270 6962 Email: enquiries@cwa-eng.com

Intelligent Engineering

Thomas Telford UTC

Proposed Drainage Strategy

CWA-20-196-530 Originator Volume Level Type Role Number -CWA -EX -XX -DR -C -0530 AUG20 1:250 @ A1

Node Name	Easting (m)	Northing (m)	CL (m)	Depth (m)	MH Dia (mm)	Cover Type	MH Type	IL (m)	Dia (mm)
S1	391888.829	299368.734	134.250	1.150	1200	675x676 D400	Type 2 Silt Trap		
								133.100	150
\$2	391888.631	299390.593	134.120	1.670	1200	675x676	Type 2	132.450	150
						D400	Silt Trap	132.732	150
	004040	202121 215	105 500	4.400				132.450	150
S3	391846.300	299461.615	135.500	1.400			Rodding Eye		
								134.100	150
S4	391847.184	299409.107	135.500	2.333	1200	675x676 D400	Туре 2	133.217	150
								133.167	150
S5	391867.741	299461.186	135.400	1.300			Rodding Eye		
								134.100	150
S6	391868.725	299409.475	135.500	2.547	1200	675x676	Type 2	133.231	150
						D400		132.953	150
								132.953	150
S7	391883.303	299413.004	134.000	1.955	1500	675x676	Type 2	132.045	225
						D400		132.804	150
								132.145	225
								132.220	150
S8	391924.732	299430.400	134.288	1.488			Rodding Eye	132.070	300
								132.800	225
S9	391877.020	299444.131	134.340	2.400	1500	675x676 D400	Type 2	131.940	300
								131.940	300
S11	391912.735	299459.073	134.340	1.940			Rodding Eye		
								132.400	225
S1 2	391899.914	299453.763	134.340	2.510	1500	675x676	Type 2	132.166	225
						D400	Silt Trap	131.830	300
								131.830	375
S13	391891.560	299474.130	134.600	2.843	1500	1200x1200 D400	Hydrobrake 5.3 l/s	131.757	375
						5-00	at 2.1m head		
_								131.757	375
S14	391891.866	299476.981	134.550	2.802	1500	675x676 D400	Type 2	131.748	375
								131.748	375
Existing	391891.008	299478.990	134.500	2.760	1200	675x676 D400	Existing	131.740	375
								131.740	375
								701.740	- 0,0

F1	391907.709				(mm)	Туре		(m)	(mm)
F2		299421.623	134.100	0.500	600	430x430 C250	Туре 3		
F2								133.600	150
	391904.096	299420.216	134.100	0.526	600	430x430 C250	Type 3	133.574	150
								133.574	150
F3	391889.956	299414.308	134.100	0.628	600	430x430 C250	Type 3	133.472	150
								133.472	150
F4	391862.791	299419.292	135.550	0.750	750x675	430x430 C250 Double Sealed	Type 4		
								134.800	150
F5	391862.787	299422.389	135.550	0.750	750x675	430x430 C250 Double Sealed	Type 4		
								134.800	150
F6	391862.997	299428.859	135.550	0.750	750x675	430x430 C250 Double Sealed	Type 4		
								134.800	150
F7	391872.558	299419.460	135.200	0.847	600	430x430	Type 3	134.353	150 150
						C250		134.436 134.409	150 150
								134.353	150
F8	391874.908	299433.956	134.500	0.734	600	430x430 C250	Type 3	133.766	150
								133.766	150
F9	391878.553	299444.511	134.100	0.843	600	430x430	Туре 3	133.330	150
						D400		133.394	150
								133.257 133.257	150 150
F10	391878.831	299470.339	134.700	1.615	1200	675x675 D400	Type 4	133.085	150
								133.085	150
F12	391913.502	299448.338	134.250	0.450	750x675	430x430 C250 Double Sealed	Type 2		
								133.800	150
F13	391907.782	299456.915	134.100	0.558	1200	430x430 D400	Type 3	133.542	150
								133.542	150
F11	391874.398	299480.684	134.500	1.490	1200	675x675 D400	Type 2	133.010	150
Node Name	Easting (m)	Northing (m)	CL (m)	Depth (m)	MH Dia (mm)	Cover Type	Manhole Type	IL (m)	Pipe Dia
D1	391911.684	299424.240	135.000	2.700	1500	675x675 D400	Type 2		
								400.000	20-
D2	391922.151	299428.590	134.500	2.420	1500	675x675 D400	Type 2	132.300	225 225
								120 000	97 5
	201900 414	299482.076	134.400	2.550	1500	675x675	Type 2	132.080 131.850	375 375
D3	391899.414	200-02.010							

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NOTES

1. Refer to drawing CWA-20-196-530 for drainage layout.

P04	Cover levels updated. S10 deleted	20.01.21	АН	ME
P03	Updated to represent PAS1192 numbering system	18.01.21	AT	ME
P2	Updated masterplan to suit P04	14.01.21	АН	ME
P1	Issued for comment	06.08.20	АН	ME
Rev.	Amendments	Date	Ву	Chkd.

Drawing Status

PRELIMINARY



Lancaster House, 67 Newhall Street, Birmingham, B3 1NQ
Tel: 0121 270 6962 Email: enquiries@cwa-eng.com

Thomas Telford UTC Extension

131.850

375

Proposed Drainage Schedules

CWA Drawing Number
CWA-20-196-532

Project No.

UC0030

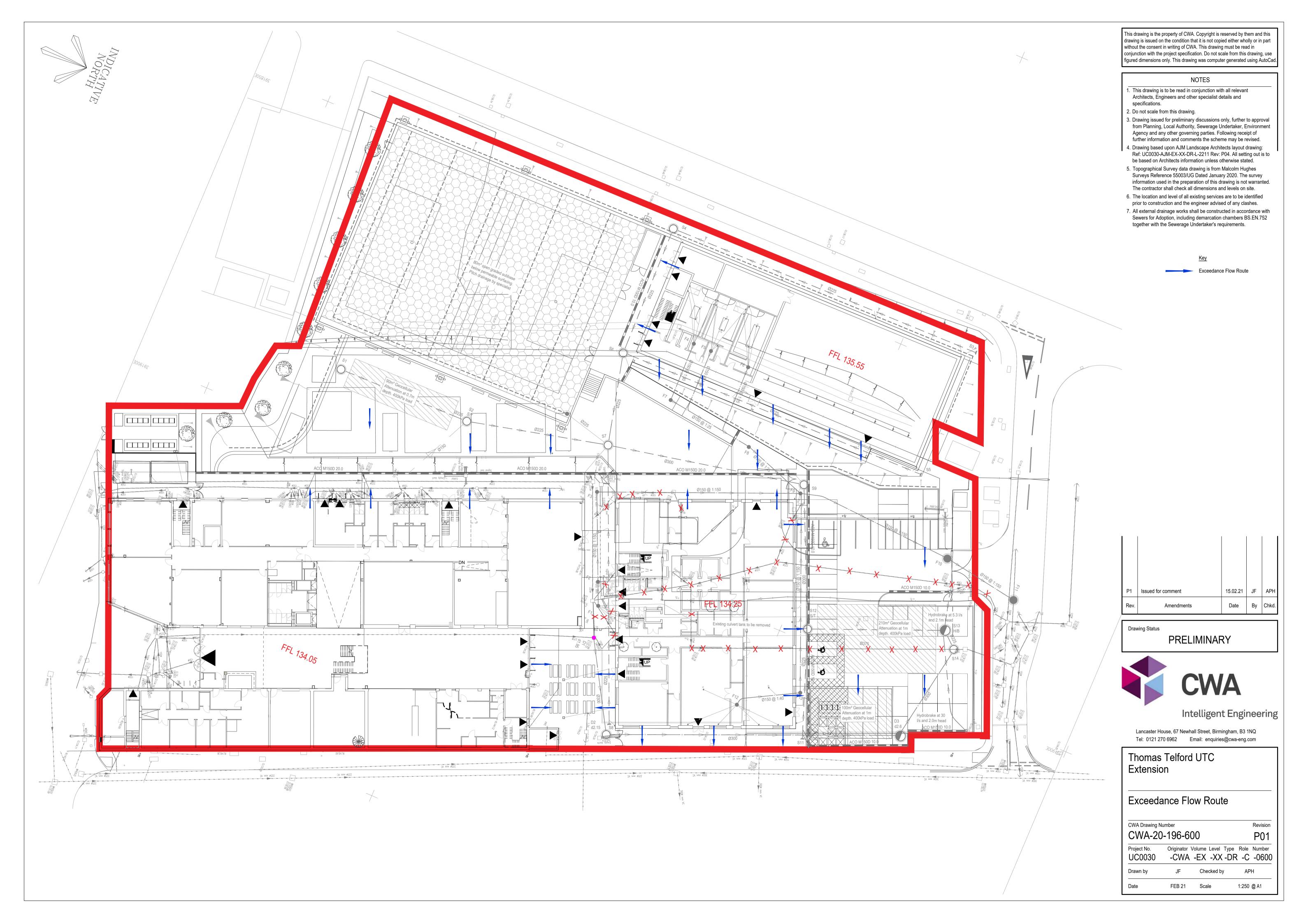
Originator Volume Level Type Role Number

-CWA -EX -XX -DR -C -0532

Drawn by

AH Checked by ME

AUG20 Scale NTS @ A1





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Appendix 8 – Drainage Calculations



Drainage Design Report

Flow

v8.1

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Network Storm Network

Filename C:\Users\ahardy\OneDrive - CWA\Andy Desktop\CWA-20-196-SWS FINAL SCHEME 2.pfd

Username Andrew Hardy (ahardy@cwa-eng.com)

Last analysed 20/01/2021 10:30:11 **Report produced on** 20/01/2021 10:31:39

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Rainfall Methodology	FSR
Return Period (years)	100
Additional Flow (%)	0
FSR Region	England and Wales
M5-60 (mm)	20.000
Ratio-R	0.400
cv	0.750
Time of Entry (mins)	5.00
Maximum Time of Concentration (mins)	30.00
Maximum Rainfali (mm/hr)	50.0
Minimum Velocity (m/s)	1.00
Connection Type	Level Soffits
Minimum Backdrop Height (m)	0.200
Preferred Cover Depth (m)	1.200
Include Intermediate Ground	
Enforce best practice design rules	



Link Name	Length (m)	Slope (1:X)	Dia (mm)	Link Type	US CL (m)	US IL (m)	US Depth (m)	DS CL (m)	DS IL (m)	DS Depth (m)	US Node Name	Dia (mm)	Width (mm)	Node Type	МН Туре	DS Node Name	Dia (mm)	Width (mm)	Node Type	MH Type
.000	10.929	59.4	150	Circular	134.250	133.100	1.000	134.250	132.916	1.184	31	1200		Manhole	Adoptable	Tank1	1200		Manhole	Adoptable
.001	10.930	59.4	150	Circular	134.250	132.916	1.184	134.120	132.732	1.238	Γank1	1200		Manhole	Adoptable	S2	1200		Manhole	Adoptable
2.000	12.155	81.0	150	Circular	133.940	132.600	1.190	134.120	132.450	1.520	G1	1200		Manhole	Adoptable	S2	1200		Manhole	Adoptable
.002	23.036	100.2	150	Circular	134.120	132.450	1.520	134.000	132.220	1.630	52	1200		Manhole	Adoptable	S7	1500		Manhole	Adoptable
3.000	24.816	168.8	225	5 Circular	135.678	134.275	1.178	135.419	134.128	1.066	Pitch	1200		Manhole	Adoptable	Outlet	1200		Manhole	Adoptable
3.001	8.527	4.3	225	5 Circular	135.419	134.128	1.066	134.000	132.145	1.630	Outlet	1200		Manhole	Adoptable	S7	1500		Manhole	Adoptable
1.000	52.515	59.5	150	Circular	135.500	134.100	1.250	135.500	133.217	2.133	53	1200		Manhole	Adoptable	S4	1200		Manhole	Adoptable
1.001	21.544	100.7	150	Circular	135.500	133.167	2.183	135.500	132.953	2.397	64	1200		Manhole	Adoptable	S6	1200		Manhole	Adoptable
5.000	51.720	59.5	150	OCircular	135.400	134.100	1.150	135.500	133.231	2.119	35	1200		Manhole	Adoptable	S6	1200		Manhole	Adoptable
1.002	14.999	100.7	150	Circular	135.500	132.953	2.397	134.000	132.804	1.046	36	1200		Manhole	Adoptable	S7	1500		Manhole	Adoptable
6.000	44.933	59.5	225	5 Circular	134.288	132.800	1.263	134.000	132.045	1.730	S8	1200		Manhole	Adoptable	S7	1500		Manhole	Adoptable
.003	31.755	244.3	300	Circular	134.000	132.070	1.630	134.340	131.940	2.100	S7	1500		Manhole	Adoptable	S9	1500		Manhole	Adoptable
.004	24.838	225.8	300	Circular	134.340	131.940	2.100	134.340	131.830	2.210	39	1500		Manhole	Adoptable	S12	1500		Manhole	Adoptable
3.000	13.877	59.3	225	5 Circular	134.340	132.400	1.715	134.340	132.166	1.949	511	1200		Manhole	Adoptable	S12	1500		Manhole	Adoptable
.005	11.419	285.5	375	Circular	134.340	131.830	2.135	134.530	131.790	2.365	312	1500		Manhole	Adoptable	Tank2	1500		Manhole	Adoptable
.006	10.595	321.0	375	Circular	134.530	131.790	2.365	134.600	131.757	2.468	Γank2	1500		Manhole	Adoptable	S13	1500		Manhole	Adoptable
.007	2.867	318.6	375	Circular	134.600	131.757	2.468	134.550	131.748	2.427	513	1500		Manhole	Adoptable	S14	1500		Manhole	Adoptable
.008	2.185	273.1	375	Circular	134.550	131.748	2.427	134.500	131.740	2.385	514	1500		Manhole	Adoptable	Existing	1200		Manhole	Adoptable
.009	7.883	56.3	375	Circular	134.500	131.740	2.385	134.250	131.600	2.275	Existing	1200		Manhole	Adoptable	Street	1200		Manhole	Adoptable



Node Name	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Width (mm)	Node Type	MH Type		Link ID	IL (m)	Dia (mm)	Link Type
1	391888.829	299368.734	134.250	1.150	1200		Manhole	Adoptable					
									+				
									0	1.000	133.100	150	Circular
ank1	391888.730	299379.663	134.250	1.334	1200		Manhole	Adoptable	1	1.000	132.916	150	Circular
											400.044		
2	391888.631	299390.593	134.120	1.670	1200		Manhole	Adoptable	0	1.001 2.000	132.916 132.450		Circular Circular
	391000.031	299390.593	134.120	1.070	1200		Marmole	Adoptable	2	1.001	132.732		Circular
									-	1.001	102.702	100	Oirodiai
									0	1.002	132.450	150	Circular
31	391899.677	299385.521	133.940	1.340	1200		Manhole	Adoptable					
									-				
									0	2.000	132.600	150	Circular
Pitch	391865.815	299385.290	135.678	1.403	1200		Manhole	Adoptable		2.000	102.000	100	Oliodidi
									0	3.000	134.275		Circular
Outlet	391881.240	299404.730	135.419	1.291	1200		Manhole	Adoptable	1	3.000	134.128	225	Circular
									0	3.001	134.128	225	Circular
33	391846.300	299461.615	135.500	1.400	1200		Manhole	Adoptable					
									0	4.000	134.100	150	Circular
64	391847.184	299409.107	135.500	2.333	1200		Manhole	Adoptable	1	4.000	133.217		Circular
	00.10.11.10.1	200100.101	100.000	2.000	.200		- Indiniolo	, taopitable	+		100.211		Oli Gallai
									0	4.001	133.167	150	Circular
5	391867.741	299461.186	135.400	1.300	1200		Manhole	Adoptable					
									0	5.000	134.100	150	Circular
66	391868.725	299409.475	135.500	2.547	1200		Manhole	Adoptable	1	5.000	133.231		Circular



								2	4.001	132.953	150 Circular
								-		102.000	
								0	4.002	132.953	150 Circular
7	391883.303	299413.004	134.000	1.955	1500	Manhole	Adoptable	1	6.000	132.045	225 Circular
								2	4.002	132.804	150 Circular
								3	3.001	132.145	225 Circular
								4	1.002	132.220	150 Circular
								0	1.003	132.070	300 Circular
88	391924.732	299430.400	134.288	1.488	1200	Manhole	Adoptable				
								0	6.000	132.800	225 Circular
S9	391877.020	299444.131	134.340	2.400	1500	Manhole	Adoptable	1	1.003	131.940	300 Circular
								0	1.004	131.940	300 Circular
S11	391912.735	299459.073	134.340	1.940	1200	Manhole	Adoptable				
								0	8.000	132.400	225 Circular
S12	391899.914	299453.763	134.340	2.510	1500	Manhole	Adoptable	1	8.000	132.166	225 Circular
								2	1.004	131.830	300 Circular
								0	1.005	131.830	375 Circular
Tank2	391895.583	299464.329	134.530	2.740	1500	Manhole	Adoptable	1	1.005	131.790	375 Circular
								0	1.006	131.790	375 Circular
S13	391891.560	299474.130	134.600	2.843	1500	Manhole	Adoptable	1	1.006	131.757	375 Circular
								0	1.007	131.757	375 Circular
S14	391891.866	299476.981	134.550	2.802	1500	Manhole	Adoptable	1	1.007	131.748	375 Circular
								0	1.008	131.748	375 Circular
Existing	391891.008	299478.990	134.500	2.760	1200	Manhole	Adoptable	1	1.008	131.740	375 Circular
								0	1.009	131.740	375 Circular



Street	391890.781	299486.870	134.250	2.650	1200		Manhole	Adoptable	1	1.009	131.600	375	Circular	
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Rainfall Methodology	FSR	Return Period (years)	Climate Change (%)
FSR Region	England and Wales	30	(
M5-60 (mm)	20.000	100	C
Ratio-R	0.400	100	40
Summer CV	0.750		
Winter CV	0.840		
Analysis Speed	Normal		
Skip Steady State	х		
Drain Down Time (mins)	240		
Additional Storage (m³/ha)	20.0		
Storm Durations (mins)	15		
	30		
	60		
	120		
	180		
	240		
	360		
	480		
	600		
	720		
	960		
	1440		
Check Discharge Rate(s)	х		
1 year (l/s)			
30 year (I/s)			
100 year (l/s)			
Check Discharge Volume	х		
100 year 360 minute (m³)			



Hydro-Brake®												
Node	Flap Valve	Online / Offline	Replaces Downstream Link	Loop to Node	invert Level (m)	Design Depth (m)	Design Flow (l/s)	Objective	Sump Available	Product Number	Min Outlet Diameter (m)	Min Node Diameter (mm)
S13	x	Online			131.757	2.100	5.3	(HE) Minimise upstream storage		CTL-SHE-0093-5300-2100-5300	0.150	1200



Depth/Area/Inf Area									
Node	Base Inf Coefficient (m/hr)	Side inf Coefficient (m/hr)	Safety Factor	Porosity	Invert Level (m)	Time to half empty (mins)	Depth (m)	Area (m²)	Inf. Area (m²)
Tank1	0.00000	0.00000	2.0	0.95	132.916	208	0.000	90.0	0.0
							1.000	90.0	0.0
							1.001	0.0	0.0
Tank2	0.00000	0.00000	2.0	0.95	131.790		0.000	210.0	0.0
							1.000	210.0	0.0
							1.001	0.0	0.0
Pitch	0.00000	0.00000	2.0	0.30	134.275	0	0.000	1400.0	0.0
							0.250	1400.0	0.0
							0.251	0.0	0.0



Event	Peak Intensity (mm/hr)	Average Intensity (mm/hr)
30 year 15 minute summer	268.706	76.035
30 year 15 minute winter	188.566	76.035
30 year 30 minute summer	174.929	49.499
30 year 30 minute winter	122.757	49.499
30 year 60 minute summer	116.589	30.811
30 year 60 minute winter	77.459	30.811
30 year 120 minute summer	70.438	18.615
30 year 120 minute winter	46.797	18.615
30 year 180 minute summer	53.298	13.715
30 year 180 minute winter	34.645	13.715
30 year 240 minute summer	41.604	10.995
30 year 240 minute winter	27.641	10.995
30 year 360 minute summer	31.221	8.034
30 year 360 minute winter	20.295	8.034
30 year 480 minute summer	24.324	6.428
30 year 480 minute winter	16.160	6.428
30 year 600 minute summer	19.756	5.404
30 year 600 minute winter	13.498	5.404
30 year 720 minute summer	17.490	4.687
30 year 720 minute winter	11.754	4.687
30 year 960 minute summer	14.215	3.743
30 year 960 minute winter	9.416	3.743
30 year 1440 minute summer	10.161	2.723
30 year 1440 minute winter	6.829	2.723
100 year 15 minute summer	348.738	98.681
100 year 15 minute winter	244.728	98.681
100 year 30 minute summer	228.965	64.789
100 year 30 minute winter	160.677	64.789
100 year 60 minute summer	153.288	40.510
100 year 60 minute winter	101.841	40.510
100 year 120 minute summer	92.562	24.461
100 year 120 minute winter	61.496	24.461
100 year 180 minute summer	69.806	17.964
100 year 180 minute winter	45.376	17.964
100 year 240 minute summer	54.269	14.342
100 year 240 minute winter	36.055	14.342
100 year 360 minute summer	40.484	10.418



100 year 360 minute winter	26.315	10.418
100 year 480 minute summer	31.414	8.302
100 year 480 minute winter	20.871	8.302
100 year 600 minute summer	25.431	6.956
100 year 600 minute winter	17.376	6.956
100 year 720 minute summer	22.452	6.017
100 year 720 minute winter	15.089	6.017
100 year 960 minute summer	18.166	4.784
100 year 960 minute winter	12.033	4.784
100 year 1440 minute summer	12.896	3.456
100 year 1440 minute winter	8.667	3.456
100 year +40% 15 minute summer	488.233	138.153
100 year +40% 15 minute winter	342.620	138.153
100 year +40% 30 minute summer	320.551	90.705
100 year +40% 30 minute winter	224.948	90.705
100 year +40% 60 minute summer	214.603	56.713
100 year +40% 60 minute winter	142.577	56.713
100 year +40% 120 minute summer	129.587	34.246
100 year +40% 120 minute winter	86.094	34.246
100 year +40% 180 minute summer	97.729	25.149
100 year +40% 180 minute winter	63.526	25.149
100 year +40% 240 minute summer	75.977	20.078
100 year +40% 240 minute winter	50.477	20.078
100 year +40% 360 minute summer	56.677	14.585
100 year +40% 360 minute winter	36.841	14.585
100 year +40% 480 minute summer	43.979	11.622
100 year +40% 480 minute winter	29.219	11.622
100 year +40% 600 minute summer	35.604	9.738
100 year +40% 600 minute winter	24.327	9.738
100 year +40% 720 minute summer	31.433	8.424
100 year +40% 720 minute winter	21.125	8.424
100 year +40% 960 minute summer	25.432	6.697
100 year +40% 960 minute winter	16.847	6.697
100 year +40% 1440 minute summer	18.055	4.839
100 year +40% 1440 minute winter	12.134	4.839



Results for 30 year (US Node ID	ation. Lowest r	nass balance:	99.34%			Flood (m³)	Status	Link ID		Outflow (Vs)	Velocity (m/s)		Link Vol (m³)	Discharge Vol (m³)
Event		Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m²)				DS Node ID			Flow/Cap		
15 minute summer	S1	9	133.207	0.107	13.8	0.1988	0.000	ООК	1.000	Tank1	13.9	1.835	0.603	0.0848	
30 minute winter	Tank1	23	132.971	0.055	11.3	4.7764	0.000	ООК	1.001	S2	6.1	1.073	0.264	0.0621	
15 minute winter	S2	11	132.547	0.097	13.2	0.1451	0.000	OOK	1.002	S7	13.3	1.008	0.747	0.3319	
15 minute summer	G1	1	132.600	0.000	0.0	0.0000	0.000	ООК	2.000	S2	0.0	0.000	0.000	0.0705	
120 minute winter	Pitch	86	134.342	0.067	15.4	28.5162	0.000	ООК	3.000	Outlet	6.3	1.093	0.159	0.1526	
120 minute winter	Outlet	86	134.153	0.025	6.3	0.0277	0.000	ООК	3.001	S7	6.3	1.039	0.025	0.1778	
15 minute winter	S3	10	134.163	0.063	8.6	0.0931	0.000	ООК	4.000	S4	8.4	1.027	0.364	0.6449	
15 minute winter	S4	12	133.706	0.539	20.5	0.7719	0.000	SURCHARGED	4.001	S6	15.6	0.889	0.884	0.3793	
15 minute winter	S5	10	134.163	0.063	8.6	0.0949	0.000	ООК	5.000	S6	8.4	1.116	0.364	0.6324	
15 minute winter	S6	12	133.512	0.559	34.1	0.7865	0.000	SURCHARGED	4.002	S7	31.5	1.790	1.781	0.2614	
360 minute winter	S7	352	132.469	0.424	16.8	0.9869	0.000	SURCHARGED	1.003	S9	16.7	0.765	0.237	2.2362	
15 minute winter	S8	10	132.859	0.059	10.4	0.0904	0.000	OOK	6.000	S7	10.2	0.354	0.151	1.0791	
360 minute winter	S9	352	132.468	0.528	18.1	1.0655	0.000	SURCHARGED	1.004	S12	17.3	0.600	0.235	1.7491	
15 minute winter	S11	10	132.472	0.072	13.8	0.1114	0.000	OOK	8.000	S12	13.6	1.293	0.202	0.1464	
360 minute winter	S12	352	132.468	0.638	20.5	1.2798	0.000	SURCHARGED	1.005	Tank2	20.1	0.787	0.170	1.2595	
360 minute winter	Tank2	352	132.468	0.678	20.1	136.4503	0.000	SURCHARGED	1.006	S13	4.3	0.087	0.038	1.1686	
360 minute winter	S13	352	132.468	0.711	4.5	1.5313	0.000	SURCHARGED	Hydro-Brake®	S14	4.3				
60 minute summer	S14	114	131.795	0.047	4.3	0.0830	0.000	OOK	1.008	Existing	4.3	0.674	0.036	0.0141	
60 minute summer	Existing	114	131.774	0.034	4.3	0.0389	0.000	ООК	1.009	Street	4.3	0.889	0.016	0.0383	71.
60 minute summer	Street	114	131.633	0.033	4.3	0.0000	0.000	ООК							



Results for 100 year	US Node Pe	ration. Lowest	mass balance	: 99.34%			Flood (m³)	Status	Link ID					Link Vol (m³)	Discharge Voi (m³)
Event		Peak (mins)	Level (m)	Depth (m)	inflow (I/s)	Node Vol (m²)				DS Node ID	Outflow (l/s)	Velocity (m/s)	Flow/Cap		
15 minute winter	S1	10	133.227	0.127	18.9	0.2372	0.000	ООК	1.000	Tank1	18.9	1.858	0.818	0.1105	
30 minute winter	Tank1	22	132.983	0.067	14.7	5.8398	0.000	ООК	1.001	S2	8.6	1.171	0.374	0.0806	
15 minute winter	S2	13	132.787	0.337	18.0	0.5027	0.000	SURCHARGED	1.002	S7	16.5	1.024	0.932	0.4055	
15 minute winter	G1	13	132.787	0.187	4.3	0.2115	0.000	SURCHARGED	2.000	S2	-4.3	-0.289	-0.217	0.2140	
120 minute winter	Pitch	84	134.358	0.083	20.2	35.0479	0.000	ООК	3.000	Outlet	9.5	1.228	0.238	0.2025	
120 minute winter	Outlet	84	134.158	0.030	9.5	0.0335	0.000	ООК	3.001	S7	9.5	1.082	0.038	0.1827	
15 minute winter	S3	12	134.179	0.079	11.2	0.1173	0.000	ООК	4.000	S4	11.0	1.032	0.476	0.7086	
15 minute winter	S4	12	134.080	0.913	26.7	1.3068	0.000	SURCHARGED	4.001	S6	19.3	1.095	1.090	0.3793	
15 minute winter	S5	10	134.173	0.073	11.2	0.1104	0.000	ООК	5.000	S6	11.0	1.123	0.476	0.6746	
15 minute winter	S6	12	133.804	0.851	42.8	1.1964	0.000	SURCHARGED	4.002	S7	38.8	2.203	2.192	0.2614	
360 minute winter	S7	360	132.786	0.741	22.3	1.7268	0.000	SURCHARGED	1.003	S9	21.2	0.778	0.299	2.2362	
15 minute winter	S8	10	132.867	0.067	13.5	0.1033	0.000	ООК	6.000	S7	13.3	0.447	0.197	1.1174	
360 minute winter	S9	360	132.786	0.846	22.9	1.7061	0.000	SURCHARGED	1.004	S12	22.6	0.596	0.307	1.7491	
360 minute winter	S11	360	132.786	0.386	2.5	0.5951	0.000	SURCHARGED	8.000	S12	2.5	0.796	0.037	0.5519	
360 minute winter	S12	360	132.786	0.956	26.6	1.9171	0.000	SURCHARGED	1.005	Tank2	26.2	0.844	0.222	1.2595	
360 minute winter	Tank2	360	132.786	0.996	26.2	200.3919	0.000	SURCHARGED	1.006	S13	3.7	0.083	0.034	1.1686	
360 minute winter	S13	360	132.786	1.029	4.6	2.2156	0.000	SURCHARGED	Hydro-Brake®	S14	4.3				
30 minute winter	S14	222	131.795	0.047	4.3	0.0830	0.000	OOK	1.008	Existing	4.3	0.674	0.036	0.0141	
30 minute summer	Existing	145	131.774	0.034	4.3	0.0389	0.000	OOK	1.009	Street	4.3	0.889	0.016	0.0383	66.
30 minute summer	Street	145	131.633	0.033	4.3	0.0000	0.000	ООК							



Event	r +40% Critical St	orm Duration. I	Lowest mass b	alance: 99.34%	6		Flood (m³)	Status	Link ID	DS Node ID	Outflow (I/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
	US Node ID	Peak (mins)	Level (m)	Depth (m)	inflow (l/s)	Node Vol (m²)									
480 minute winter	S1	464	133.844	0.743	2.9	1.3836	0.0000	SURCHARGED	1.000	Tank1	2.9	0.876	0.126	0.1924	
480 minute winter	Tank1	464	133.843	0.927	17.6	80.3457	0.0000	SURCHARGED	1.001	S2	-15.8	-0.898	-0.684	0.1924	
480 minute winter	S2	464	133.843	1.393	16.3	2.0761	0.0000	FLOOD RISK	1.002	S7	-15.0	-0.852	-0.845	0.4055	
480 minute winter	G1	464	133.843	1.243	0.3	1.4062	0.0000	FLOOD RISK	2.000	S2	-0.3	-0.024	-0.015	0.2140	
60 minute winter	Pitch	45	134.384	0.109	46.1	46.1824	0.0000	ОК	3.000	Outlet	16.0	1.416	0.400	0.2916	
60 minute winter	Outlet	45	134.166	0.038	16.0	0.0430	0.0000	ОК	3.001	S7	16.0	0.599	0.063	0.1884	
15 minute winter	S3	13	134.977	0.877	15.7	1.3046	0.0000	SURCHARGED	4.000	S4	12.4	1.017	0.538	0.9245	
15 minute winter	S4	13	134.790	1.622	33.1	2.3218	0.0000	SURCHARGED	4.001	S6	24.1	1.369	1.362	0.3793	
15 minute winter	S5	13	134.525	0.425	15.7	0.6443	0.0000	SURCHARGED	5.000	S6	14.0	1.120	0.608	0.9105	
15 minute winter	S6	12	134.324	1.371	53.9	1.9276	0.0000	SURCHARGED	4.002	S7	49.1	2.792	2.778	0.2614	
480 minute winter	S7	464	133.843	1.798	25.8	4.1895	0.0000	FLOOD RISK	1.003	S9	25.0	0.742	0.354	2.2362	
480 minute winter	S8	464	133.843	1.043	2.0	1.6000	0.0000	SURCHARGED	6.000	S7	2.0	0.137	0.030	1.7870	
480 minute winter	S9	464	133.843	1.903	27.0	3.8374	0.0000	SURCHARGED	1.004	S12	26.7	0.538	0.363	1.7491	
480 minute winter	S11	464	133.842	1.442	2.7	2.2252	0.0000	SURCHARGED	8.000	S12	2.7	0.776	0.040	0.5519	
480 minute winter	S12	464	133.842	2.012	31.1	4.0367	0.0000	SURCHARGED	1.005	Tank2	30.7	0.846	0.261	1.2595	
480 minute winter	Tank2	464	133.841	2.051	30.7	203.2242	0.0000	SURCHARGED	1.006	S13	4.9	0.084	0.044	1.1686	
480 minute winter	S13	464	133.842	2.085	6.6	4.4908	0.0000	SURCHARGED	Hydro-Brake®	S14	5.2				
480 minute winter	S14	464	131.800	0.051	5.2	0.0910	0.0000	OK	1.008	Existing	5.2	0.711	0.043	0.0162	
480 minute winter	Existing	464	131.778	0.038	5.2	0.0428	0.0000	ОК	1.009	Street	5.2	0.938	0.020	0.0440	177.9
480 minute winter	Street	464	131.636	0.036	5.2	0.0000	0.0000	OK							