



**STRUCTURAL  
SOILS LTD**

**MR JONATHAN UNGAR**

**INTERPRATIVE REPORT**  
**on**  
**GROUND INVESTIGATION**  
**at**  
**84 ST. ALDATE'S**  
**OXFORD**

**JUNE 2014**

**REPORT NO: 729180**

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**DOCUMENT ISSUE RECORD**

**STRUCTURAL  
SOILS LTD**

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Contract No: 729180

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Client: Mr Jonathan Ungar

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Contract: 84 St. Aldate's, Oxford

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Document: Interpretive Report on Ground Investigation

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Approved by:

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Date:

9 June 2014

**REVISION RECORD**

Revision	Date	Description	Prepared by

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## 1 INTRODUCTION

This investigation was carried out on the instructions of Mann Williams on behalf of Mr Jonathan Ungar. It is proposed that a former timber framed building is reinstated on the site and that a new 4 storey residential block is built adjoining the timber framed building.

The purpose of the work was to investigate ground conditions and provide information for foundation design and to provide information for preliminary contamination assessment purposes. The work included an intrusive investigation, laboratory testing and the preparation of this report, which contains a description of the site and the works carried out, the exploratory hole logs, in-situ and laboratory testing results.

The report gives recommendations relating to geotechnical aspects such as foundation design. It presents an appraisal of geoenvironmental aspects such as soil contamination and gives recommendations on risk reduction. It should not be assumed that these would meet the requirements of the local authority, whose advice should be sought regarding planning permission.

The ground investigation has been carried out using intrusive ground investigation techniques in general accordance with the recommendations of BS5930: 1999 *Code of Practice for Site Investigations* (including Amendment A2, 2010). Whilst every attempt is made to record full details of the strata encountered in the exploratory holes, techniques of hole formation and sampling will inevitably lead to disturbance, mixing or loss of material in some soils and rocks.

All information, comments and opinions given in this report are based on the ground conditions encountered during the site work, and on the results of laboratory and field tests performed during the investigation. However, there may be conditions at the site that have not been taken into account, such as unpredictable soil strata, contaminant concentrations and water conditions between or below exploratory holes. It should be noted that groundwater levels, gas concentrations and gas flows usually vary due to seasonal, atmospheric and/or other effects and may at times differ to those measured during the investigation.

This report was prepared by Structural Soils Limited for the sole and exclusive use of Mr Jonathan Ungar in response to particular instructions. Any other parties using the information contained in this report do so at their own risk and any duty of care to those parties is excluded. No liability will be accepted after a period of 6 years from the date of the report.



## **2 SITE DESCRIPTION**

### **2.1 Location and Topography**

The site is located at the rear of 84 St. Aldate's, Oxford (see Site Location Map in Appendix A). The British National Grid Reference of the site is SP 513 058.

The site is approximately 5m by 20m in size (see Exploratory Hole Location Plan in Appendix A). The site comprises of three distinct different areas. Firstly, an existing building, which lies at the eastern end of the site, which is currently used for commercial and residential purposes. Secondly, the central area which has the same base level as the existing building, but which was previously a timber framed building, where only the exterior walls now remain. This section of the site is predominantly concrete slab with overlying tiles and lino flooring, running along the southern side of this is a brick paved area, where the Victorian-era drain runs. Thirdly, the western end of the site is a concrete slab, which lies around 0.60m above the base level of the rest of the site and which sits around 0.15m above the street level to the west of the site.

The site is bound by a property to the south, which shares a wall with the existing building on the site, there is also the original historic wall which supported the timber framed building running the length of the southern boundary of the site. The north of the site is bound by a cobbled access road which is 3m wide and runs the full length of the site. The west of the site is bound by a paved footpath which links the access road to the courtyard of Oxfordshire County Councils buildings and Magistrates Courts. The east of the site is bound by St. Aldate's (A420).

### **2.2 Geology**

Information on the geology of the site was obtained from the following sources published by the the British Geological Survey (BGS):

- BGS survey map (sheet 236 Witney, scale 1:50,000 published 1982).
- The BGS digital geology map, which utilises the most up to date names for geological units ([www.bgs.ac.uk/data](http://www.bgs.ac.uk/data)).
- The BGS Lexicon of Named Rock Units, which provides typical descriptions for most geological units ([www.bgs.ac.uk/lexicon](http://www.bgs.ac.uk/lexicon)).



The site is shown to be underlain by the following descending sequence of strata:

<b>TABLE 1: SUMMARY OF SITE GEOLOGY</b>	
<b>Geological Unit Name</b>	<b>Description</b>
Alluvium	Sands and gravels
River Terrace Deposits	Clay, Silt, Sand and Gravel
Oxford Clay Formation and West Walton Formation (undifferentiated)	Claystone grading to Mudstone

Note: Information obtained from BGS digital records © NERC.

The BGS National Geoscience Data Centre collection of onshore scanned boreholes, shafts and well records was consulted. These showed that there was up to 2.75m of Made Ground, overlying up to 2.00m of Alluvium which was overlying up to 2.00m of River Terrace Deposits. The boreholes showed that the Oxford Clay Formation was encountered at roughly 5.50m depth in all the surrounding boreholes.



### 3 FIELDWORK

#### 3.1 Scope of Works

The following works were completed on 22 April 2014 at locations shown on the Exploratory Hole Location Plan in Appendix A:

TABLE 2: SCOPE OF INTRUSIVE WORKS AND IN-SITU TESTING		
Number	Exploratory Hole or In-Situ Test Type	Hole Numbers
2	Window Sample Holes.	WS1 & WS2
6	Hand Dug Trial Pits	TP1 – TP6

The scope of investigation and choice of investigation equipment was decided by Mann Williams. The positions were selected by Mann Williams and set out by Structural Soils LTD and adjusted where necessary to take account of buried or overhead services, or other restrictions.

The exploratory holes were logged by an engineer in accordance with the recommendations of BS5930: 1999 (Amendment A2, 2010, which incorporates the requirements of BS EN ISO 14688-1, 14688-2 and 14689-1). Detailed descriptions, together with relevant comments, are given in the logs included in Appendix B.

Prior to the commencement of the trail pits and window sample holes, a scan was carried out using a cable avoidance tool (CAT) and signal generator ('genny'). Inspection pits were hand dug at the window sample locations.

#### 3.2 Window Sampling

The window sample exploratory holes were drilled using a tracked rig with chain driven drop weight to 4.50 m & 6.00m. Steel sample tubes containing a plastic sample liner were used. The holes reduce in diameter with depth, as reported on the logs. Small and bulk disturbed soil samples were subsampled at regular intervals. Hand vane or hand penetrometer tests were carried out on intact cohesive soils, the results of which are included on the logs contained in Appendix B.

Standard Penetration Tests (SPT) were carried out at 1.00m intervals in the window sample holes using the rig's integral drop weight/hammer (see In-Situ Testing, below).





### **3.3 In-Situ Testing**

Standard Penetration Tests (SPT) were carried out in the exploratory holes, where noted in the preceding sections, in accordance with BS EN ISO 22476-3 using a hammer which had been calibrated for efficiency. The calibration certificate is included in Appendix C. Seating drives have been recorded in increments of 75mm in accordance with recommended UK practice.

The SPT N-values are reported on the exploratory hole logs, on which the serial number of the hammer used is recorded. The full results are presented in tabular format on the Summary of Standard Penetration Tests in Appendix C, on which the normalised  $N_{60}$  values are also reported, which are the equivalent N-value for a hammer delivering 60% of the theoretical drop energy. Plots showing both N and  $N_{60}$  values versus depth are also included.

### **3.4 Trial Pits**

The hand dug trial pits were approximately 0.30m x 0.30m in plan and ranged from 0.70m to 1.25m deep. The purpose of the pits was to expose the foundations to existing walls. The foundation details exposed are shown on the trial pit logs. Small and bulk disturbed soil samples were taken from the trial pits at regular intervals.

### **3.5 Chemical Contamination Sampling**

Samples for contamination testing were taken from the exploratory holes where indicated on the exploratory hole logs, recorded as ES.

All samples were placed in appropriate contamination sample containers that were supplied by the laboratory. Containers for volatiles testing of soil samples were filled to capacity. All samples were then kept in cool boxes with ice packs and were transported to the laboratories under Chain of Custody documentation, as promptly as possible to maintain sample integrity.

### **3.6 Backfill**

On completion all exploratory holes were backfilled with arisings. The trial pits were backfilled with arisings and compacted.



## 4 LABORATORY TESTING

Samples for potential geotechnical testing were returned to one of the Company's UKAS accredited laboratories, and those for potential contamination testing were sent to a sister company Envirolab Limited, a MCERTS and UKAS accredited chemical testing laboratory. Laboratory tests were scheduled by Structural Soils Limited in consultation with Mann Williams.

### 4.1 Geotechnical Laboratory Testing

Geotechnical laboratory testing was generally carried out in accordance with BS1377: 1990, *Methods of Test for Soils for Civil Engineering Purposes*, Parts 1 to 8. The number of tests completed and the test methods used are summarised below. Where non-standard procedures have been undertaken, this is recorded on the report sheet. The results are reported in tabular and/or graphical form and included as Appendix D of this report.

TABLE 3: SUMMARY OF GEOTECHNICAL LABORATORY TESTING			
Number of tests	Test	Test Method	Notes
<b>Classification Tests</b>			
6	Moisture content.	BS1377: Part 2.	
6	Liquid and plastic (Atterberg) limits.	BS1377: Part 2.	
<b>Chemical Tests: Soil</b>			
2	Water soluble sulphate content and pH value.	BRE SD1*.	
3	Water soluble sulphate, total (acid soluble) sulphate and total sulphur contents and pH value.	BRE SD1*.	

Note:

- \* Test(s) carried out to method approved in BRE Special Digest 1.

### 4.2 Contamination

The contamination testing carried out is summarised in the following table. The results are included as Appendix E of this report, and include details of the test method.

TABLE 4: SUMMARY OF CONTAMINATION LABORATORY TESTING*			
Numbers of tests	Description	Notes	
<b>SOIL</b>			
6	SSL HHB Human Assessment suite	Comprises arsenic, cadmium, chromium (total), lead, mercury, selenium, copper, nickel, zinc, speciated polycyclic aromatic hydrocarbons (PAH), total petroleum hydrocarbons (TPHCWG (speciated)), organic matter, soluble sulphate and pH.	

Note:

- \* Tests carried out in accordance with MCERTS/UKAS standards where noted on the results sheets.



## 5 GROUND CONDITIONS

### 5.1 General

The exploratory holes were logged by an engineer and the ground conditions encountered are detailed on the logs contained in Appendix B. The exploratory holes encountered the following general descending sequence of strata:

TABLE 5: SUMMARY OF GROUND CONDITIONS			
Strata	Exploratory holes encountered in	Depth to top of stratum m bgl	Proven Thickness (m)
Made Ground	WS1, WS2, TP1, TP2, TP3, TP4, TP5, TP6	0.00	1.35 - 1.85
Possible Made Ground	WS1	1.85	0.75
Alluvium (Soft Clay)	WS1, WS2	1.35 - 2.60	0.30 - 0.65
Alluvium (Organic Silt)	WS1, WS2	2.00 - 2.90	0.90 - 1.60
River Terrace Deposits (Sands and Gravels)	WS1, WS2	3.60 - 3.80	0.90 - 2.20

The site contained a step of 0.60m, WS1 and TP4 were undertaken on this step, so higher up than the rest of the trial pits and window samples. This is visible on the logs in the thickness variations within the made ground. The ground conditions are summarised in more detail below.

### 5.2 Made Ground and Possible Made Ground

Made ground was encountered in all exploratory holes to proven depths in the window samples of 1.35m to 1.85m and to depths greater than 0.70m to 1.25m in the trial pits. The made ground was variable, comprising concrete and tile over hardstand over uncompact, loose to very loose clays, sands and gravels as well as soft occasionally firm sandy gravelly silt. Anthropologic materials included concrete, brick, charcoal, roof tiles and ceramic tiles.

A layer of possible made ground was encountered in WS1 from 1.85m to 2.60m and comprised soft to very soft sandy gravelly clay.

### 5.3 Alluvium

Beneath the made ground and possible made ground in the window samples, Alluvium of very soft to soft sand, gravel, clay and silt were encountered to 3.60m-3.80m depth. A high organic content was locally recorded in these deposits.



#### **5.4 River Terrace Deposits**

Beneath the Alluvium in the window sample, River Terrace Deposits of medium dense to dense clay, sand and gravel were encountered to final depths of 6.00m and 4.50m.

#### **5.5 Indications of Contamination**

There were no olfactory or visual indications of contamination in any of the exploratory holes.

#### **5.6 Existing Foundations**

Existing foundations were encountered within TP2 & TP4. In TP1, TP5 & TP6, the wall extended below the achievable depth of excavation of the trial pits, with no foundations being encountered. In TP3, a large boulder was encountered, so it is unknown if this is part of the foundations or not.

Within TP2, as shown on the diagram in the log, a step out to a corner foundation was encountered at 0.70m depth. This had a step out of 0.15m from the exterior wall and 0.10m from a demolished interior wall and had a thickness of 0.20m. The foundations were overlying made ground of sandy gravelly clay.

Within TP4, as shown on the diagram in the log, a stepped, stone foundation was encountered at 1.00m depth. It stepped out by 0.20m and was 0.20m thick. At the base of the foundations was what appeared to be lime mortar, as well as the foundations overlying made ground of clayey sandy gravel.

#### **5.7 Groundwater**

Groundwater strikes were encountered in WS1 and WS2 at depths of 3.00m and 1.70m representatively although the recorded depths can be influenced by the drilling technique. Due to the risk of hole collapse, the drilling of the window sample holes were immediately recommenced and therefore standing groundwater levels were not recorded.

No groundwater was encountered in TP1 to TP6 which were terminated at depths above the groundwater table.



## **6 GEOTECHNICAL SITE ASSESSMENT**

### **6.1 Proposed Development**

The proposed development is to reinstate the historic two storey timber framed building, in its original position, with new foundations. The current proposal is to rebuild the timber frame on a new raft foundation, in order to minimize disturbance to any underlying archaeology.

At the rear of the site, a new four storey residential structure is proposed. The higher and more concentrated loads from this structure mean that a raft may not be adequate, and the current proposal is for a raft foundations supported by mini piles.

The purpose of the investigation was to uncover any existing foundations and determine the extent and configuration of the foundations for the existing masonry walls. Secondly, to investigate the extent of contamination, if any on the site, and whether the contamination levels fall within the criteria for residential properties.

### **6.2 Site Preparation and Excavation**

Current proposals are to use raft foundations, supported by mini piles for the new building. No significant depth of excavation is therefore expected under the current proposals, but care should still be taken not to undermine the foundations of the adjacent walls. The trial pits indicate that the walls are founded at least 0.70m, and probably at least 1.00m, below the site level.

The soils encountered at the site are considered suitable for excavation by standard mechanical plant such as a wheeled backhoe excavator. A hydraulic breaker may be required to break out any hard cover, buried foundations or other obstructions that remain following demolition.

Groundwater was encountered 1.70m depth or greater, and so is unlikely to be encountered by excavation for a raft foundation. However, it should be noted that groundwater levels may change due to seasonal or other variations, and also that surface water run-off from rainfall may also enter excavations. Advice on suitable dewatering techniques is given in CIRIA Report C515 *Groundwater Control – design and practice*.

On site works revealed that shallow unsupported excavations are likely to be stable in the short term. However, where water seepage and strikes occur within excavations their stability could be significantly reduced, resulting in collapse. Care should also be taken not to undermine the foundations of the adjacent existing walls.



All excavations should be planned and due consideration should be given to providing temporary support or suitable battering. Excavations should be regularly inspected by a competent person to ensure continued safety. Further advice on the safety of excavations is given in *Health and Safety in Construction*.

Excavations or below ground voids should be checked for the presence of harmful gases and vapours (e.g. hydrocarbons and solvents) prior to personnel entry.

### **6.3 Foundations**

#### **6.3.1 Historic Timber-Framed Building**

The structure is to be rebuilt off a new raft. The underlying made ground is granular, 2.60m thick and very loose. Immediate settlement is to be expected, but the amount is difficult to assess, and would depend to a large extent on the load that the ground had been subjected to in the past by the building on the site. If the newly rebuilt structure is not significantly heavier than the original, then any settlement should be minimal. There is a theoretical risk of significant settlement if the area were flooded and the made ground inundated, assuming that this has not previously occurred.

In any event, some differential settlement between the raft and the surrounding structures is to be expected, and should be allowed for in the design. The raft should be designed in accordance with NHBC Standards.

#### **6.3.2 New building**

The new building is to be built off a raft supported by mini piles.

The following ultimate values for skin friction and end bearing may be used to carry out a preliminary design for bored piles. The soil profile used below is based on WS1 which was drilled in the centre of the new building footprint, supplemented by nearby BGS borehole archive data and our own data from other sites in central Oxford, where ground conditions are very similar.



TABLE 6: PRELIMINARY DESIGN VALUES FOR PILE DESIGN

Depth (m bgl)	Soil Description	Ultimate Unit Skin Friction, kN/m <sup>2</sup>	Ultimate Unit End Bearing, kN/m <sup>2</sup>
0.00 to 1.35	MADE GROUND (Granular, N=0)	Ignore	Not recommended
1.35 to 2.35	Alluvial Clays/Silts (design $c_u = 13\text{kN/m}^2$ )	Ignore	Not recommended
2.35 to 3.60	Alluvial Clays/Silts (design $c_u = 40\text{kN/m}^2$ )	Ignore	Not recommended
3.60 to 5.50	River Terrace Deposits (design N = 40)	20	900 <sup>1</sup>
5.50 to 10.00	Stiff Oxford Clay Formation (design $c_u = 100\text{kN/m}^2$ )	45 <sup>1</sup>	900 <sup>2</sup>
10.00-15.00	Stiff Oxford Clay Formation (design $c_u = 150\text{kN/m}^2$ )	67 <sup>1</sup>	1350 <sup>2</sup>

Notes:

1. Soil adhesion factor,  $\alpha$ , of 4.5 used to derive this value.
2. Bearing capacity factor,  $N_{cs}$ , of 9.0 used to derive this value.
3. Limiting value used to avoid overstressing the underlying stratum.

When calculating the allowable vertically compressive working load of piles for preliminary design purposes a factor of safety of 2.5 should be applied to the above ultimate values for skin friction and end bearing for soils. As the capacity of piles can vary depending on the type and method of installation, it is recommended that the advice of specialist piling contractors be sought with regard to the final design of piles. Consideration should also be given to undertaking loading tests on selected piles.

In practice the final design of any piles may be carried out by the pile designer using Eurocode methods with partial factors applied to loads and soil parameters, as opposed to using the *global* factors of safety recommended above.

#### 6.4 Protection of Buried Concrete

This assessment of the potential for chemical attack on buried concrete is based on current guidance contained in BRE Special Digest 1 ('SD1', 2005) *Concrete in Aggressive Ground Part 1: Assessing the aggressive chemical environment*. Third Edition. The site is classed as *brownfield*, as it conservatively assumed to have been subject to previous industrial development and might contain chemical residues produced by or associated with industrial production. Table C2 in BRE SD1 is therefore used to assess the site. Groundwater is assumed to be *static* above about 1.70m depth. 'Static groundwater' applies to locations where the ground is either



permanently dry, or contains water but has low permeability (i.e. little water movement is possible, permeability generally less than  $10^{-7}$  m/s).

Soil pH values ranging from 8.07 to 10.30 were recorded. From these results a 'Characteristic Value' of 8.08 is derived, which is the mean of the lowest 2 values. The water-soluble sulphate ( $\text{SO}_4$ ) results range from 46mg/l to 1300mg/l, and a 'Characteristic Value' of 795mg/l is derived, which is the mean of the highest 2 values.

It should be noted that the alluvium and Oxford Clay Formation strata may be pyritic. However, buried concrete is unlikely to be exposed to disturbed ground in which pyrite may oxidize to sulphate (e.g. the pyritic strata are too deep, or if piles are used then they will not cause disturbed ground that could oxidise) and so the concrete classification need not be based on the pyrite test results.

It is therefore concluded that for this site the Aggressive Chemical Environment for Concrete (ACEC) class is AC-1 where concrete could be contact with groundwater, and therefore would be applicable to concrete piles, and AC-1s if there is no risk of concrete being in contact with groundwater, which would be applicable to a raft. The designer should utilise these classifications in order to produce the concrete specification.





## 7 GEOENVIRONMENTAL SITE ASSESSMENT

### 7.1 Proposed Development

The proposed development is detailed in Section 6.1 of this report.

#### 7.1.1 Risk to Human Health

##### *General*

To determine whether contaminants are present at levels that may be deemed to pose a significant hazard to human health, measured contamination levels in soil at the site are compared against derived guideline values ('Tier 2' soil screening), either directly or following statistical analysis. Where contaminants are present above the screening values it is probable that site-specific information will be required to further examine the potential risk of harm arising from such contamination.

The background to the assessment is contained in Appendix E and the findings are summarised in the following pages.

The proposed use of the site is a mixture of residential and commercial properties, with no landscaping. The GAC for Human Health – Residential with communal soft landscaping guidelines have been used to assess the results, which are slightly conservative for this situation.

The results have been compared directly to the GACs without the use of the statistics.

##### *Results*

There were no olfactory or visual indications of contamination in any of the holes.

Contaminants assessed against the GAC's are: arsenic, cadmium, chromium, copper, lead, mercury, nickel, selenium, zinc, Polycyclic Aromatic Hydrocarbons (PAH) & Total Petroleum Hydrocarbons (TPH).

All of the individual results for all contaminants were all below the GAC/CLEA SGV's.

##### *Conclusions*

The investigation has shown contaminant levels in the soil to be below the assessment criteria, which indicates that no risks to human health have been identified.



### 7.1.2 Contamination Conclusion

No contamination has been recorded at the site resulting in no complete pollutant linkages being identified. It is therefore considered that the site is fit for the proposed end use without further assessment or remediation.

## 7.2 Off-site Disposal of Surplus Soil

### 7.2.1 General

All excavated material and excess spoil must be classified for waste disposal purposes prior to disposal at landfill. Under the Landfill (England and Wales) Regulations 2002 (as amended), prior to disposal all wastes must be classified as:

- 'inert', or
- 'non-hazardous', or
- 'hazardous'.

The Environment Agency's *Hazardous Waste (Technical Guidance WM2)* document outlines the methodology for classifying wastes.

Currently all wastes may require pre-treatment prior to disposal at landfill.

### 7.2.2 Initial Waste Characterisation

Envirolab have produced an assessment tool, 'Haswaste', that characterises contaminated waste soil by following the guidance within WM2. The 'total solid testing' results from this investigation have been run through this assessment tool to aid potential future off-site disposal of materials. This assessment produces an 'initial' characterisation of the waste which determines if it is hazardous or not (if it is 'not' hazardous, then it may be either inert (insoluble and inorganic) or non-hazardous. However, due to complications with the terminology of 'inert waste' it is best not to refer to it as such until after Waste Acceptance Criteria testing).

The assessment is included in Appendix D. Any samples that are classed as hazardous will have light cells with bold text, in the respective sample columns (assuming results are in black & white, otherwise yellow cells on a colour copy).

The initial waste characterisation indicates that none of the samples tested have been classified as hazardous.



It is important to note that whilst we believe our in-house assessment tool to be an accurate interpretation of the requirements of WM2, thereby producing initial classifications in accordance with it, landfill operators often have their own assessment tools and can often come to a different conclusion. As a result, some landfill operators could even refuse to take apparently suitable waste.



## **8 SUMMARY**

- 8.1** The site is located within the boundaries of 84 St. Aldate's, Oxford. The British National Grid Reference of the site is SP 513 058.
- 8.2** It is understood that the site is to be redeveloped for residential housing consisting of a two story timber framed building and a four story stone clad building.
- 8.3** The site is split into three areas. The eastern section of the site currently has a three story timber framed building, with residential and commercial uses. The central section of the site previously contained a timber framed building, where only the floor slab and external walls remain. The western section of the site is raised by 0.60m and formally contained a garage, which now only contains the external wall to the south.
- 8.4** The British Geological Survey map (sheet 236 Witney, scale 1:50,000 published 1982) shows the site to be underlain by Alluvium deposits and River Terrace Deposits. The solid geology underlying the site is shown as the Oxford Clay Formation and West Walton Formation (undifferentiated).
- 8.5** An intrusive investigation comprising window sampling and hand dug trial pitting was undertaken on 22 April 2014.
- 8.6** Made ground and possible made ground were encountered in all exploratory holes undertaken and extended to a maximum depth of 2.60m in WS1. This was generally underlain by superficial deposits of soft cohesive material and dense gravel.
- 8.7** Groundwater was recorded at a minimum depth within WS2 of 1.70m below ground level.
- 8.8** The soils encountered at the site are considered suitable for excavation by standard mechanical plant such as a wheeled backhoe excavator. A hydraulic breaker may be required to break out any hard cover, buried foundations or other obstructions that remain following demolition.
- 8.9** On site works revealed that shallow unsupported excavations are likely to be stable in the short term. However, where water seepage and strikes occur within excavations their stability could be significantly reduced, resulting in collapse. Care should also be taken not to undermine the foundations of the adjacent existing walls.



- 8.10** The timber framed building is to be rebuilt off a new raft. The underlying ground is granular, 2.60m thick and very loose. Differential settlement between the raft and the surrounding structures is to be expected, and should be allowed for in the design. The raft should be designed in accordance with NHBC standards.
- 8.11** The new building is to be built off a raft supported by mini piles. The competent strata as detailed in Table 6 will offer within the stiff Oxford Clay Formation an ultimate unit end bearing capacity of  $>900\text{kN/m}^2$ , with an ultimate skin friction of  $>45\text{kN/m}^2$ .
- 8.12** According to Table C2 the Aggressive Chemical Environment for Concrete (ACEC) class is AC-1 where concrete could be contact with groundwater, and therefore would be applicable to concrete piles, and AC-1s if there is no risk of concrete being in contact with groundwater, which would be applicable to a raft. The designer should utilise these classifications in order to produce the concrete specification.
- 8.13** The investigation has shown contamination levels in the soil to be below the assessment criteria, which indicates that no risk to human health have been identified.
- 8.14** The initial waste characterisation has indicated that none of the samples tested have been classed as hazardous.

## STRUCTURAL SOILS LIMITED



H Perry BSc (Hons) FGS



B J Simpson MSc (Hons) FGS



## 9 REFERENCES

- 9.1 BS 5930:1999 *Code of Practice for Site Investigation*, including amendment A2 (2010)
- 9.2 BS 10175:2011 *Investigation of potentially contaminated sites: Code of practice*, including amendment A1 (2013)
- 9.3 British Geological Survey sheet 236 Witney, scale 1:50,000 published 1982
- 9.4 British Geological Survey online digital geological map, [www.bgs.ac.uk/data](http://www.bgs.ac.uk/data)
- 9.5 British Geological Survey Lexicon of Named Rock Units, [www.bgs.ac.uk/lexicon](http://www.bgs.ac.uk/lexicon)
- 9.6 Environment Agency website, [www.environment-agency.gov.uk](http://www.environment-agency.gov.uk)
- 9.7 *Health and Safety in Construction*, HSG150, HSE, 1996
- 9.8 CIRIA Report C515 (2000) *Groundwater Control – design and practice*
- 9.9 BS EN ISO 14688-1:2002 *Geotechnical investigation and testing – Identification and classification of soil: Part 1: Identification and description*, including Amendment A1 (2013)
- 9.10 BS EN ISO 14688-2:2004 *Geotechnical investigation and testing – Identification and classification of soil: Part 2: Principles for a classification*, including Amendment A1 (2013)
- 9.11 BS EN ISO 22476-3:2005 (updated February 2007) *Geotechnical Investigation and Testing – Field Testing Part 3: Standard Penetration Test*, including Amendment A1 (2011)
- 9.12 BS 1377:1990 *Methods of Test for Soils for Civil Engineering Purposes*
- 9.13 BRE Special Digest 1 (SD1)(2005) *Concrete in Aggressive Ground Part 1: Assessing the aggressive chemical environment*. Third Edition
- 9.14 Environment Agency Policy. Part IIA – *Detailed Quantitative Assessment of Chronic Risks to Human Health from Contaminated Soils*. Policy Number 199\_04, dated 9 March 2004
- 9.15 *Hazardous Waste: Interpretation of the Definition and Classification of Hazardous Waste*, Environment Agency, WM2 Version 1.0, June 2003
- 9.16 *Landfill (England & Wales) Regulations 2002*

## **APPENDIX A**

- (i) Site Location Plan
- (ii) Exploratory Hole Location Plan
- (iii) Proposed Development Layout Plan



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## STRUCTURAL SOILS

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www.soils.co.uk

CLIENT

Mann Williams

PROJECT

84 St. Aldate's Oxford

TITLE

SITE LOCATION MAP

REV.	DATE	DESCRIPTION	BY	CHKD.	APPR.
00	07.05.2014	-	MW	HP	-

CONTRACT No.

729180

GRID REFERENCE

SP 513 058

SCALE BAR

0 250 500 750 1000m

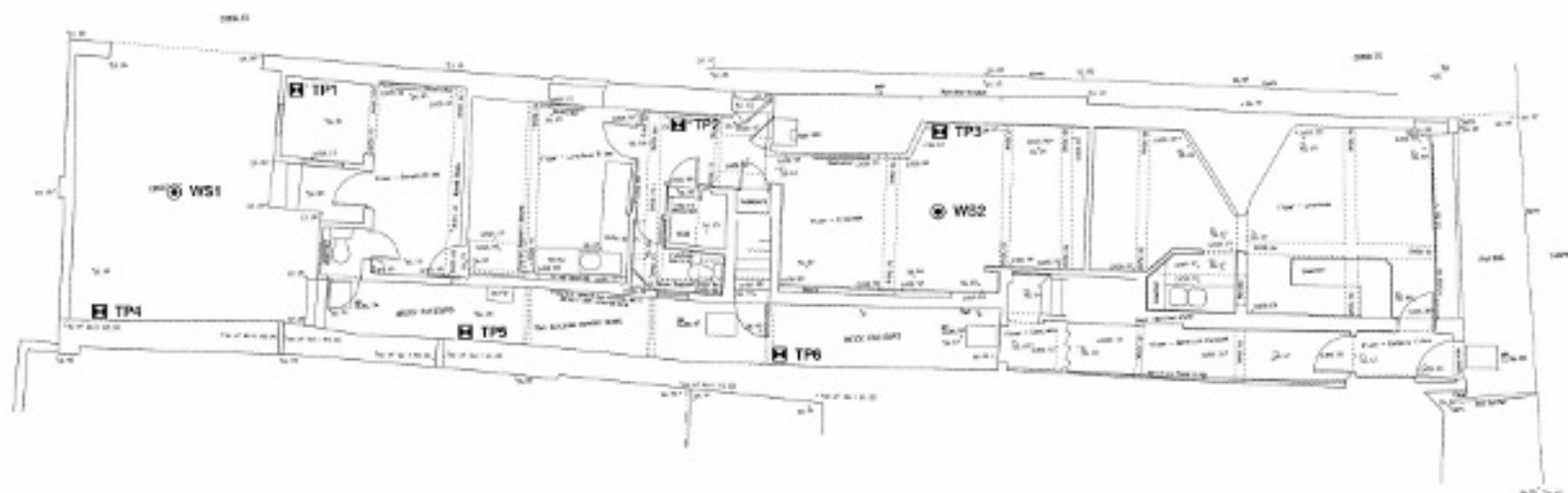
ORIGIN SIZE

A4



FIGURE No

1





LEGEND

-  Trial Pit Location
-  Window Sample Location

REV.	DATE	DESCRIPTION	BY	CHK.	APP.
00	07.05.2014			HW	IP



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NAME	Mann Williams		
PROJECT	64 St. Aidan's Oxford		
DESCRIPTION	EXPLORATORY HOLE LOCATION PLAN		
JOB NO.	729160	ROUND	2
ISSUE DATE		REV.	00

Not To Scale



## Proposed North Elevation



Project  
Scale  
Drawing Title  
Date

84 St Aldanos, Oxford  
1:100 @ A3  
North Elevation  
July 2013

MW Design

Do Not Scale  
All dimensions and details to be checked on site by contractor prior to starting construction. Any discrepancies to be reported to the designer. Please figure to scaled dimensions. This drawing is given without any responsibility on behalf of The Company or their employees.



## **APPENDIX B**

- (i) Key to Exploratory Hole Logs
- (ii) Trial Pit Logs
- (iii) Window Sample Logs

**KEY TO EXPLORATORY HOLE LOGS - SUMMARY OF ABBREVIATIONS****SAMPLING***Sample type codes*

B	=	Bulk disturbed sample.
D	=	Small disturbed sample.
DSPT	=	Small disturbed sample originating from SPT test.
ES	=	Soil sample for environmental testing.

**IN-SITU TESTING**

SPT	=	Standard Penetration Test using split spoon sampler. (SPT <sub>(SM)</sub> indicates 'No Sample Recovery').
HP	=	Hand Penetrometer Test. Value given as shear strength $c_u$ , in kPa.

**ADDITIONAL NOTES**

1. All soil and rock descriptions and legends in general accordance with BS EN ISO 14688-1, 14688-2, 14689-1, and BS5930:1999 including Amendment 2 (2010).
2. Material types divided by a broken line (- - -) indicates an unclear boundary.
3. The data on any sheet within the report showing the AGS icon is available in the AGS format.



### KEY TO EXPLORATORY HOLE LOGS - SUMMARY OF GRAPHIC SYMBOLS

#### WATER COLUMN SYMBOLS



First water strike, second water strike etc.

Standing water level following first strike, standing water level following second strike etc.

Seepage.

Standing water level recorded at documented date.

#### MATERIAL GRAPHIC LEGENDS



CLAY



Gravelly  
clayey  
SAND



Concrete



Clayey  
sandy  
GRAVEL



Gravelly  
SILT



MADE  
GROUND



Possible  
MADE  
GROUND



Sandy  
GRAVEL



Sandy  
gravelly  
SILT



Sandy  
clayey  
SILT



Sandy  
SILT



Clayey  
SILT

#### INSTRUMENTATION SYMBOLS



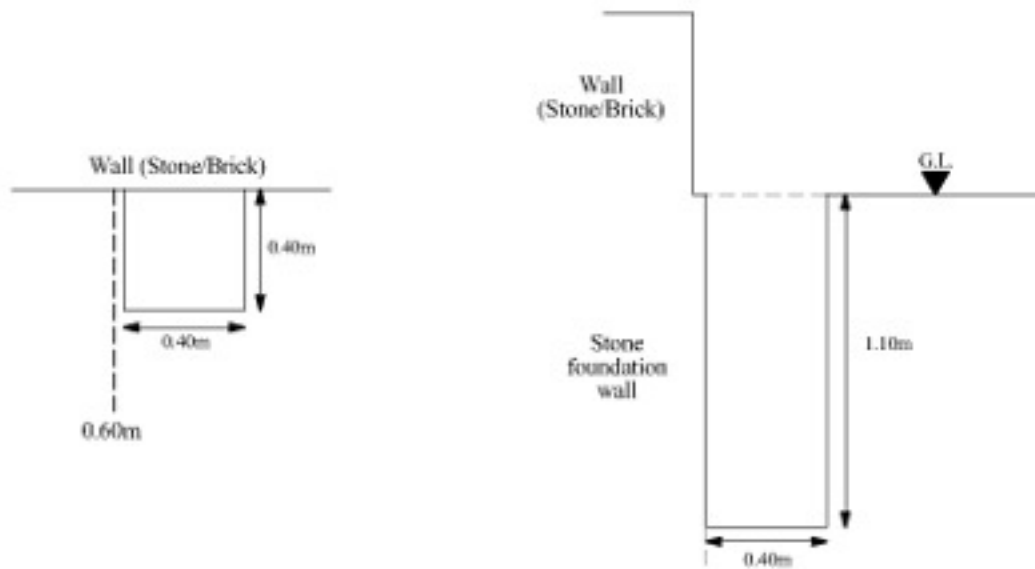
Backfill



Contract: <b>84 St. Aldate's, Oxford</b>		Client: <b>Mann Williams</b>		Trial Pit: <b>TP1</b>	
Contract Ref: <b>729180</b>	Start: <b>22.04.14</b> End: <b>22.04.14</b>	Ground Level: ---	Co-ordinates: ---	Sheet: <b>1 of 1</b>	

Samples and In-situ Tests				Water	Backfill	Description of Strata	Depth (Thickness)	Material Graphic Legend
Depth	No	Type	Results					
0.30-1.10	1	B				MADE GROUND: CONCRETE.	0.05	[Cross-hatched pattern]
						MADE GROUND: Light orangish brown slightly sandy clayey GRAVEL. Gravel is angular medium to coarse of brick. Medium cobble content of brick.	0.30	
0.50	1	ES				MADE GROUND: Greyish brown light brown reddish brown black slightly clayey sandy GRAVEL. Gravel is angular to subangular fine to coarse of brick, charcoal and sandstone.	(-0.80)	
							1.10	

Trial pit terminated at 1.10m depth due to maximum achievable depth of excavation.



Plan (Not to Scale)		General Remarks							
						<ol style="list-style-type: none"> <li>1. Location CAT scanned prior to excavation.</li> <li>2. Hand dug inspection pit to 1.10m depth.</li> <li>3. No groundwater encountered.</li> </ol>			
Method Used: <b>Hand dug</b>		Plant Used: <b>Hand tools</b>		Logged By: <b>HPerry</b>					

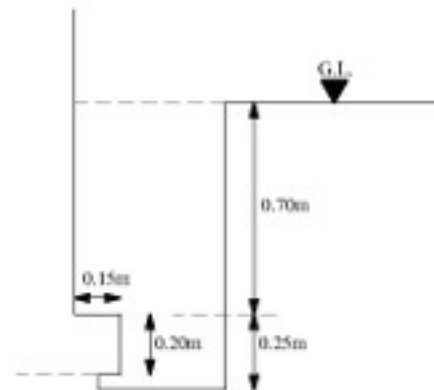
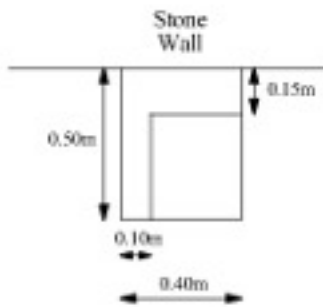




Contract: <b>84 St. Aldate's, Oxford</b>		Client: <b>Mann Williams</b>		Trial Pit: <b>TP2</b>	
Contract Ref: <b>729180</b>	Start: <b>22.04.14</b> End: <b>22.04.14</b>	Ground Level: ---	Co-ordinates: ---	Sheet: <b>1 of 1</b>	

Samples and In-situ Tests				Water	Backfill	Description of Strata	Depth (Thickness)	Material Graphic Legend	
Depth	No	Type	Results						
0.10-0.70	1	B				MADE GROUND: LINO and TILE.	0.05	[Cross-hatch pattern]	
						MADE GROUND: CONCRETE.	0.10		
0.70-0.95	2	D				MADE GROUND: Soft light greyish yellowish brown slightly sandy gravelly CLAY with low cobble content. Gravel is angular fine to coarse of brick, sandstone, limestone and charcoal.	0.60	[Cross-hatch pattern]	
						MADE GROUND: Soft occasionally firm brown greyish brown slightly sandy gravelly CLAY. Gravel is angular fine to coarse sandstone and charcoal.	0.70		
								0.95	

Trial pit terminated at 0.95m depth, when foundations had been proven.



Plan (Not to Scale)



General Remarks

1. Location CAT scanned prior to excavation.
2. Hand dug inspection pit to 0.90m depth.
3. No groundwater encountered.

All dimensions in metres

Scale: **1:25**

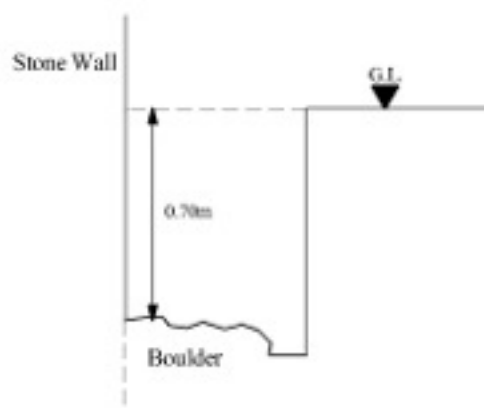
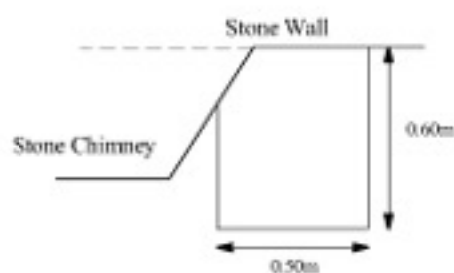
Method Used: <b>Hand dug</b>	Plant Used: <b>Hand tools</b>	Logged By: <b>HPerry</b>	Checked By:	
---------------------------------	----------------------------------	-----------------------------	-------------	--



Contract: <b>84 St. Aldate's, Oxford</b>		Client: <b>Mann Williams</b>		Trial Pit: <b>TP3</b>	
Contract Ref: <b>729180</b>	Start: <b>22.04.14</b> End: <b>22.04.14</b>	Ground Level: <b>---</b>	Co-ordinates: <b>---</b>	Sheet: <b>1 of 1</b>	

Samples and In-situ Tests				Water	Backfill	Description of Strata	Depth (Thickness)	Material Graphic Legend
Depth	No	Type	Results					
0.30-0.70	1	B				MADE GROUND: LINO, TILE and CONCRETE.	0.10	
						MADE GROUND: Lime MORTAR.	0.30	
						MADE GROUND: Soft light yellowish brown slightly sandy gravelly CLAY. Gravel is angular fine to coarse of roof tile and brick.	-(0.40) 0.70	

Trial pit terminated at 0.70m depth on boulder.



Plan (Not to Scale)		General Remarks			
<p>1. Location CAT scanned prior to excavation.                  2. Hand dug inspection pit to 0.70m depth.                  3. No groundwater encountered.</p>		All dimensions in metres		Scale: <b>1:25</b>	
Method Used: <b>Hand dug</b>	Plant Used: <b>Hand tools</b>	Logged By: <b>HPerry</b>	Checked By:		

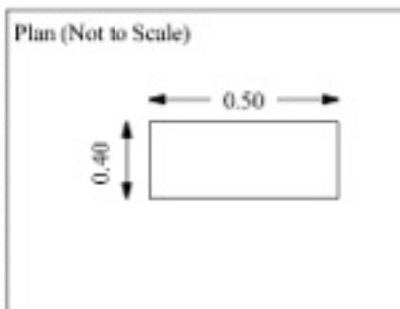
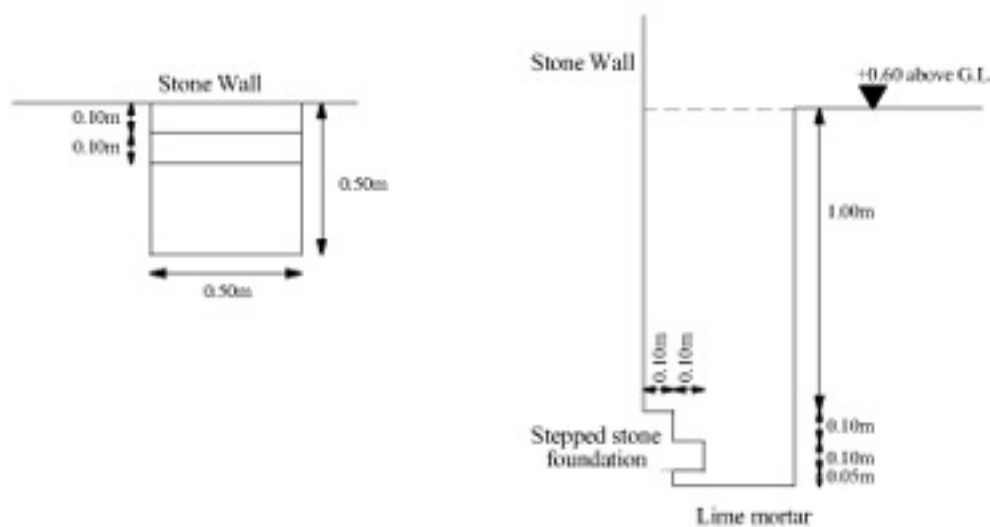




Contract: <b>84 St. Aldate's, Oxford</b>		Client: <b>Mann Williams</b>		Trial Pit: <b>TP4</b>	
Contract Ref: <b>729180</b>	Start: <b>22.04.14</b> End: <b>22.04.14</b>	Ground Level: ---	Co-ordinates: ---	Sheet: <b>1 of 1</b>	

Samples and In-situ Tests				Water	Backfill	Description of Strata	Depth (Thickness)	Material Graphic Legend
Depth	No	Type	Results					
0.50	1	ES				MADE GROUND: CONCRETE.	0.05	
0.50-1.00	1	B				MADE GROUND: Cream grey red brown slightly sandy GRAVEL with high cobble content. Gravel is angular fine to coarse sandstone, limestone, brick, concrete and coal.	(0.45)	
						MADE GROUND: Soft, occasionally firm brown sandy slightly gravelly CLAY. Gravel is angular fine to medium charcoal, slag, sandstone, brick and china plate.	0.50	
							1.00	
1.00-1.25	2	D				MADE GROUND: Light yellowish brown slightly clayey slightly sandy GRAVEL. Gravel is angular fine to coarse of lime mortar.	1.25	

Trial pit terminated at 1.25m depth when foundations had been proven.



**General Remarks**

1. Location CAT scanned prior to excavation.
2. Hand dug inspection pit to 1.25m depth.
3. No groundwater encountered.

All dimensions in metres      Scale: **1:25**

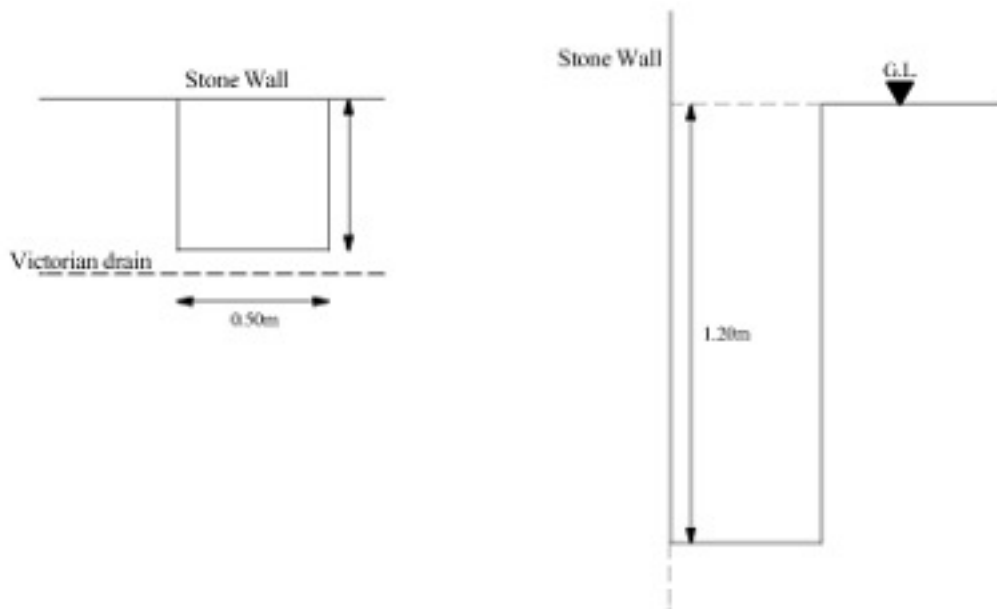
Method Used: <b>Hand dug</b>	Plant Used: <b>Hand tools</b>	Logged By: <b>HPerry</b>	Checked By: <b>AGS</b>
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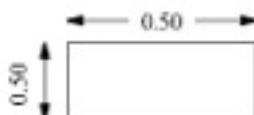
Contract: <b>84 St. Aldate's, Oxford</b>		Client: <b>Mann Williams</b>		Trial Pit: <b>TP5</b>	
Contract Ref: <b>729180</b>		Start: <b>22.04.14</b> End: <b>22.04.14</b>	Ground Level: <b>---</b>	Co-ordinates: <b>---</b>	Sheet: <b>1 of 1</b>

Samples and In-situ Tests				Water	Backfill	Description of Strata	Depth (Thickness)	Material Graphic Legend
Depth	No	Type	Results					
0.07-1.20	1	B				MADE GROUND: BRICK. MADE GROUND: Soft brown greyish brown light brownish orange slightly sandy gravelly CLAY. Gravel is angular fine to coarse of sandstone and brick.  ... at 0.60m a 20mm layer of lime mortar.	0.07          (1.13)          1.20	

Trial pit terminated at 1.20m depth due to maximum achievable depth of excavation.



Plan (Not to Scale)



General Remarks

1. Location CAT scanned prior to excavation.
2. Hand dug inspection pit to 1.20m depth.
3. No groundwater encountered.

All dimensions in metres

Scale: **1:25**

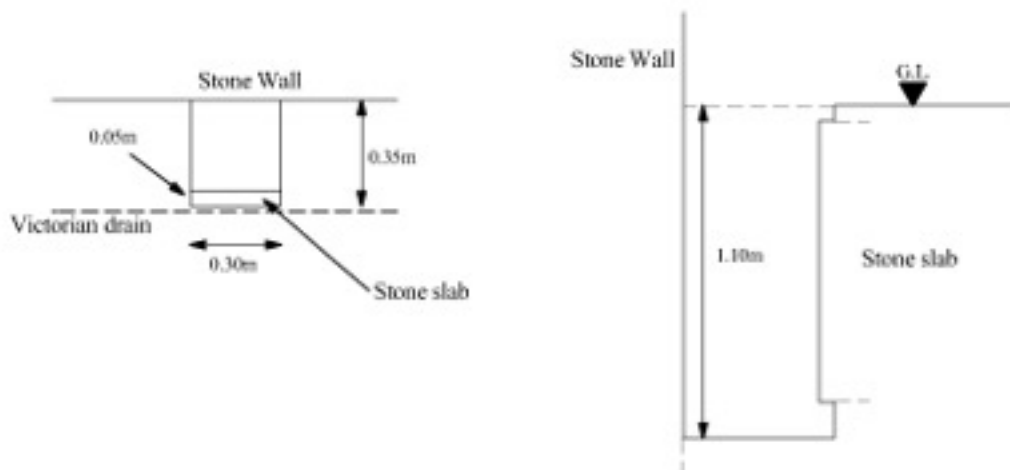
Method Used: <b>Hand dug</b>	Plant Used: <b>Hand tools</b>	Logged By: <b>HPerry</b>	Checked By: <b>HPerry</b>	
---------------------------------	----------------------------------	-----------------------------	------------------------------	--



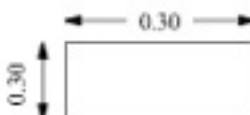
Contract: <b>84 St. Aldate's, Oxford</b>		Client: <b>Mann Williams</b>		Trial Pit: <b>TP6</b>	
Contract Ref: <b>729180</b>	Start: <b>22.04.14</b> End: <b>22.04.14</b>	Ground Level: ---	Co-ordinates: ---	Sheet: <b>1 of 1</b>	

Samples and In-situ Tests				Water	Backfill	Description of Strata	Depth (Thickness)	Material Graphic Legend
Depth	No	Type	Results					
0.07-1.10	1	B				MADE GROUND: BRICK. MADE GROUND: Soft greyish brown gravelly CLAY. Gravel is angular to subangular fine to coarse of sandstone and brick.	0.07 --- (1.03) --- 1.10	

Trial pit terminated at 1.10m depth due to maximum achievable depth of excavation.



Plan (Not to Scale)



General Remarks

1. Location CAT scanned prior to excavation.
2. Hand dug inspection pit to 1.10m depth.
3. No groundwater encountered.

All dimensions in metres

Scale: **1:25**

Method Used: <b>Hand dug</b>	Plant Used: <b>Hand tools</b>	Logged By: <b>HPerry</b>	Checked By: <b>HPerry</b>	
---------------------------------	----------------------------------	-----------------------------	------------------------------	--



Contract: <b>84 St. Aldate's, Oxford</b>		Client: <b>Mann Williams</b>		Window Sample: <b>WS1</b>	
Contract Ref: <b>729180</b>		Start: <b>22.04.14</b>	Ground Level: <b>---</b>	Co-ordinates: <b>---</b>	Sheet: <b>1 of 2</b>
		End: <b>22.04.14</b>			

Progress Window Run	Samples / Tests				Water	Backfill	Description of Strata	Depth (Thickness)	Material Graphic Legend
	Depth	No	Type	Results					
	0.00-0.30	1	B				MADE GROUND: CONCRETE	0.05	
	0.30	1	ES				MADE GROUND: Uncompact light yellowish brown and cream slightly sandy GRAVEL. Gravel is angular fine to coarse of concrete.	0.30	
	0.30-0.70	2	B				MADE GROUND: Uncompact light yellowish brown and cream slightly sandy GRAVEL with a medium cobble content. Gravel is angular fine to coarse of concrete and brick. Cobble of same material.	(0.30) 0.70	
	0.70-1.10	3	B				MADE GROUND: Uncompact brown to reddish brown and brownish black sandy GRAVEL. Gravel is angular to subangular fine to coarse of brick and charcoal.	(0.60)	
	1.00-1.45	1	SPT	N=0			MADE GROUND: Very loose light brownish yellow sandy GRAVEL. Gravel is subround to round fine to coarse of sandstone, quartz and flint.	1.30	
	1.30-1.85	5	D				MADE GROUND: Very loose brown to yellowish brown slightly clayey sandy GRAVEL. Gravel is angular to subround fine to coarse of sandstone, brick and charcoal.	(0.55) 1.85	
	1.85-2.00	6	D				POSSIBLE MADE GROUND: Soft to very soft greyish brown to yellowish brown black slightly sandy slightly gravelly CLAY. Gravel is angular to subrounded fine to medium of charcoal and sandstone.	(0.75)	
	1.90	2	HP	$c_u=25/13/25$					
	2.00-2.45	2	SPT	N=3					
	2.00	8	ES						
	2.00-2.60	8	D				$c_u=25/25/25$	2.60	
	2.00		HP						
	2.00 - 3.00 (87mm dia) 80% rec	2.50	HP	$c_u=25/25/25$			Soft greyish brown mottled orangish brown slightly sandy slightly gravelly CLAY with a medium shell fragment and organic content. Gravel is angular to subrounded fine to medium of charcoal. (ALLUVIUM)	2.90	
	2.60-2.90	9	D						
	2.90-3.00	10	D				Very soft to soft dark grey slightly sandy clayey SILT with a medium shell fragment content. (ALLUVIUM)	(0.50)	
	3.00-3.45	3	SPT	N=3					
	3.00		HP	$c_u=13/25/13$					
	3.00 - 4.00 (78mm dia) 70% rec	3.40-3.80	12	D			Very soft dark brown to black clayey SILT with medium wood/reed content. (ALLUVIUM)	(0.40)	
	3.50		HP	$c_u=0/13/0$					
	3.80-4.00	13	D				Medium dense dark brownish grey gravelly clayey SAND. Gravel is subangular to subrounded fine to medium of sandstone. (RIVER TERRACE DEPOSITS)	(0.80)	
	4.00-4.45	4	SPT	N=16					
	4.00-4.60	15	D						
	4.00 - 5.00 (67mm dia) 100% rec	4.60-6.00	16	D			Description on next sheet		

GINT LIBRARY V8 05.GLB LabVersion v8.05 - Core-Logs-0003 | Log WINDOW SAMPLE LOG | 729180 84 ST ALDATE'S, OXFORD.GPJ - v8.05 06/06/14 - 16:57 | HP.  
 Structural Soils Ltd, Head Office - Bristol: The Old School, Stillhouse Lane, Badminton, Bristol, BS3 4EB, Tel: 0117-947-1000, Fax: 0117-947-1000, Web: www.soils.co.uk, Email: info@soils.co.uk

Drilling Progress and Water Observations						General Remarks
Date	Time	Borehole Depth (m)	Casing Depth (m)	Borehole Diameter (mm)	Water Depth (m)	
22/04/14		3.00	-	87	3.00	1. Location scanned with a CAT prior to and after digging the inspection pit. 2. Inspection pit dug to 1.10m. 3. Ground water strike at 3.00m. 4. Hole collapsed at 6.00m due to gravel. 5. Hole back filled with arising on completion. 6. SPT hammer AC0124-2013 ( $E_s = 70.62\%$ ) used.
All dimensions in metres						
Method Used:	<b>Tracked window sampling</b>		Plant Used:	<b>Archway Competitor</b>		Drilled By: <b>RD</b> Logged By: <b>HPerry</b> Checked By: <b>AGS</b>





Contract: <b>84 St. Aldate's, Oxford</b>		Client: <b>Mann Williams</b>		Window Sample: <b>WS2</b>	
Contract Ref: <b>729180</b>		Start: <b>22.04.14</b>	Ground Level: <b>---</b>	Co-ordinates: <b>---</b>	Sheet: <b>1 of 1</b>
		End: <b>22.04.14</b>			

Progress Window Run	Samples / Tests				Water	Backfill	Description of Strata	Depth (Thickness)	Material Graphic Legend
	Depth	No	Type	Results					
	0.05-0.30	1	B			MADE GROUND: LINO and CERAMIC TILE.	0.05		
						MADE GROUND: CONCRETE	0.10		
	0.30	1	ES			MADE GROUND: Uncompact light yellowish brown slightly sandy GRAVEL. Gravel is angular fine to coarse of concrete.	0.30		
	0.30-0.70	2	B			MADE GROUND: Uncompact light yellowish brown to brown slightly clayey slightly sandy GRAVEL. Gravel is angular fine to coarse of concrete, ceramic tile and brick.	(0.40)		
	0.70-1.00	3	B			MADE GROUND: Very loose greyish yellowish brown to brown and black clayey slightly sandy GRAVEL. Gravel is angular to subangular fine to coarse of brick, concrete and charcoal.	0.70		
	1.00-1.45	1	SPT	N=0			(0.65)		
	1.00-1.35	5	D				1.35		
	1.35-2.00	6	D			Very soft dark brown mottled orangish brown slightly sandy slightly gravelly SILT with medium shell fragment content. Gravel is subround to round fine to medium of sandstone. (ALLUVIUM)	(0.65)		
	1.40		HP	$c_u=13/13/13$			2.00		
	1.50		HP	$c_u=13/13/13$					
	1.60		HP	$c_u=13/25/13$					
	1.70		HP	$c_u=13/0/13$					
	1.80		HP	$c_u=13/13/13$					
	1.90		HP	$c_u=13/13/13$			2.00		
	2.00-2.45	2	SPT	N=5		Soft locally firm dark brownish grey slightly gravelly SILT. Gravel is subround fine to medium of charcoal. (ALLUVIUM)	(0.30)		
	2.00		ES						
	2.00-2.30	8	D				2.30		
	2.20		HP	$c_u=0/0/13$					
	2.30-2.35	9	D			Dark brownish grey slightly sandy GRAVEL. Gravel is subround to round fine to coarse of sandstone, flint and quartz. (ALLUVIUM)	2.35		
	2.35-3.00	10	D			Firm locally stiff dark brownish black slightly sandy clayey SILT with high wood/reed content. (ALLUVIUM)	(1.25)		
	2.50		HP	$c_u=50/63/50$					
	2.70		HP	$c_u=38/50/38$					
	2.90		HP	$c_u=25/38/25$					
	3.00-3.45	3	SPT	N=29					
	3.00-3.60	12	D				3.60		
	3.50		HP	$c_u=50/63/50$					
	3.60-3.90	13	D			Grey to greyish brown slightly clayey sandy GRAVEL. Gravel is angular to subround fine to coarse of sandstone, quartz and flint. (RIVER TERRACE DEPOSITS)	(0.30)		
	3.90-4.00	14	D			Dense orangish brown to yellowish brown slightly clayey sandy GRAVEL. Gravel is angular to subround fine to coarse of sandstone and flint. (RIVER TERRACE DEPOSITS)	(0.60)		
	4.00-4.45	4	SPT	N=43					
	4.00-4.50	16	D				4.50		
						Window sample terminated at 4.50m due to refusal.			

GINT LIBRARY V8 05.GLB.LabVisions v8.05 - Core-Logs.0003 | Log WINDOW SAMPLE LOG | 729180 84 ST ALDATES OXFORD.GPJ - v8.05 06/06/14 - 16:57 | HP. Structural Soils Ltd, Head Office - Bristol: The Old School, Stillhouse Lane, Badminton, Bristol, BS3 4EB. Tel: 0117-947-1000, Fax: 0117-947-1000, Web: www.soils.co.uk, Email: info@soils.co.uk

Drilling Progress and Water Observations						General Remarks
Date	Time	Borehole Depth (m)	Casing Depth (m)	Borehole Diameter (mm)	Water Depth (m)	
22/04/14		2.00	-	102	1.70	1. Location scanned with a CAT prior to and after digging the inspection pit. 2. Inspection pit dug to 1.00m. 3. Ground water strike at 1.70m. 4. Hole terminated at 4.50m due to refusal within the gravels. 5. Hole back filled with arising on completion. 6. SPT hammer AC0124-2013 ( $E_s = 70.62\%$ ) used.
All dimensions in metres						
Method Used:	<b>Tracked window sampling</b>		Plant Used:	<b>Archway Competitor</b>		Drilled By: <b>RD</b>
						Logged By: <b>HPerry</b>
						Checked By: <b>AGS</b>

## APPENDIX C

- (i) Standard Penetration Test (SPT) Summary Sheet
  - (ii) SPT Hammer Calibration Records
  - (iii) SPT N value versus Depth Plot
  - (iv) SPT  $N_{(60)}$  Value versus Depth Plot


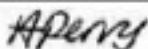
## STANDARD PENETRATION TEST SUMMARY TABLE

Exploratory Position ID	Depth (m)	Hole Dia (mm)	Casing Depth (m)	Water Depth (m)	Seating Drive		Test Drive			Hammer ID	Calibration Date	Energy Ratio (%)	N <sub>60</sub>	Comments
					Blows	Pen (mm)	Blows	R (mm)	Result					
WS1	1.00	300			0,0	150	0,0,0,0		N=0	AC0124-2013	04/10/2013	70.62	0	
	2.00	102			0,0	150	0,0,2,1		N=3	AC0124-2013	04/10/2013	70.62	4	
	3.00	87		3.00	0,0	150	1,1,0,1		N=3	AC0124-2013	04/10/2013	70.62	4	
	4.00	78		3.00	1,2	150	1,2,6,7		N=16	AC0124-2013	04/10/2013	70.62	19	
	5.00	67		3.00	2,7	150	8,7,9,9		N=33	AC0124-2013	04/10/2013	70.62	39	
WS2	1.00	300			0,0	150	0,0,0,0		N=0	AC0124-2013	04/10/2013	70.62	0	
	2.00	102		1.70	0,0	150	0,2,2,1		N=5	AC0124-2013	04/10/2013	70.62	6	
	3.00	87		1.70	0,0	150	11,8,10,10		N=39	AC0124-2013	04/10/2013	70.62	46	
	4.00	78		1.70	1,4	150	10,11,12,10		N=43	AC0124-2013	04/10/2013	70.62	51	

**Notes:**

1. Tests carried out in general accordance with BS EN ISO 22476-3:2005, including amendment A1 (2011).
2. Reported blows are for 75mm penetration unless indicated "+".
3. Where full test drive was not achieved, actual penetration (R) and extrapolated N value (N\*) reported.
4. Tests carried out using a split spoon sampler unless noted as SPT(c) (denotes use of solid cone method) in the comments column.
5. Entries in the water depth column reflects the measured water depth at time of test.

$$N_{60} = (\text{Measured hammer energy ratio} / 60) \times N \text{ value}$$

 <b>STRUCTURAL SOILS</b> The Old School Stillhouse Lane Bedminster Bristol BS3 4EB	Compiled By		Date	Contract Ref:
	 <b>HPERRY</b>		<b>06.06.14</b>	<b>729180</b>
Contract:			Page:	
<b>84 St. Aldate's, Oxford</b>			<b>1 of 1</b>	





www.equipegroup.com

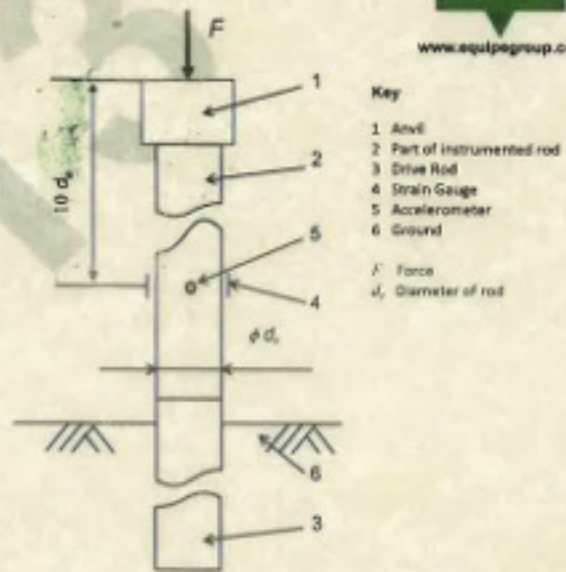
# SPT Calibration Report

## Hammer Energy Measurement Report

Type of Hammer: **COMPETETOR**  
 Client: **STRUCTURAL SOILS**  
 Test No: **EQU908**  
 Test Depth (m): **6.90**  
 Date of Test: **04 October 2013**  
 Valid until: **04 October 2014**  
 Hammer ID: **AC0124**

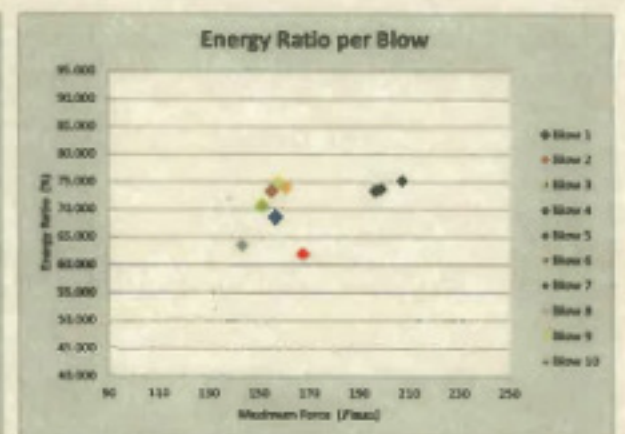
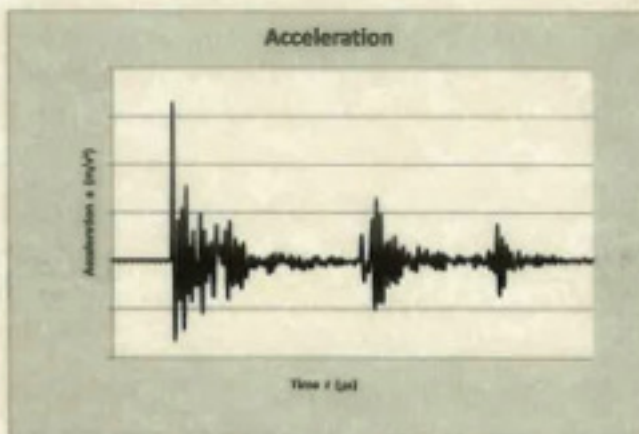
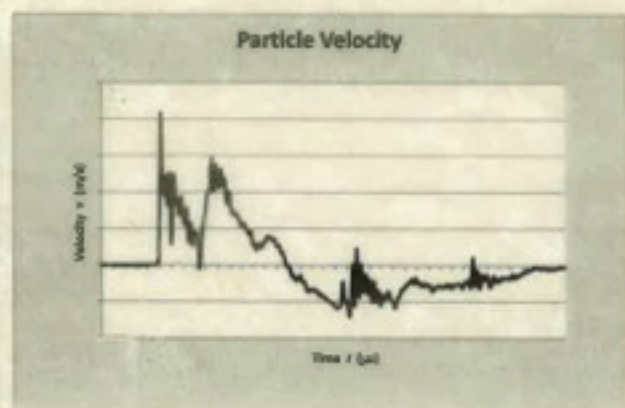
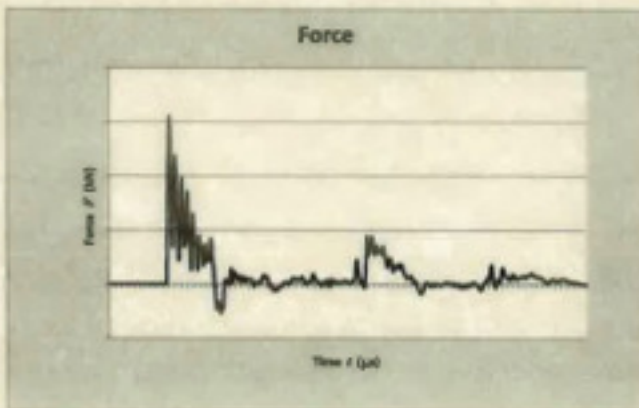
Mass of the hammer  $m = 63.5\text{kg}$   
 Falling height  $h = 0.76\text{m}$   
 $E_{theor} = m \times g \times h = 249\text{J}$

Characteristics of the instrumented rod  
 Diameter  $d_r = 0.052\text{ m}$   
 Length of the instrumented rod  $0.558\text{ m}$   
 Area  $A = 11.61\text{ cm}^2$   
 Modulus  $E_s = 206843\text{ MPa}$



- Key**
- 1 Anvil
  - 2 Part of instrumented rod
  - 3 Drive Rod
  - 4 Strain Gauge
  - 5 Accelerometer
  - 6 Ground
- $F$  Force  
 $d_r$  Diameter of rod

Fig B.1 and B.2 BS EN ISO 22476-3 : 2005 + A1 : 2011



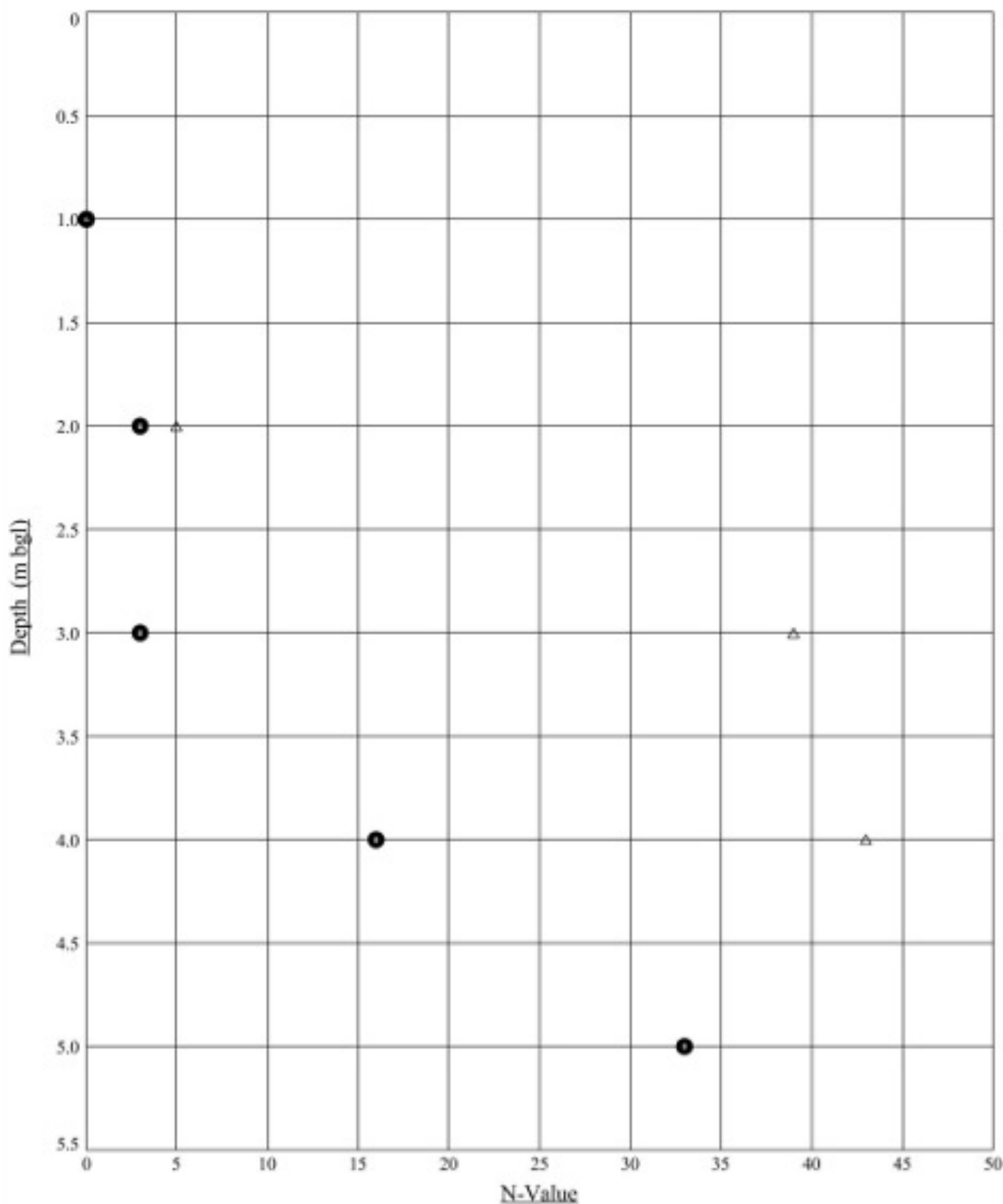
Observations:  
 1.

$E_{meas} = 0.334\text{ kN-m}$   
 $E_{theor} = 0.473\text{ kN-m}$

Energy Ratio =  $\frac{E_{meas}}{E_{theor}} = 70.62\%$


Equipe SPT Analyzer Operators: **KS**  
 Prepared by: *K. Spire* Checked by: *Spire* Date: **07/10/2013**

# STANDARD PENETRATION TEST (SPT N-Value) vs DEPTH




Key: ● = WS1, △ = WS2

GINT\_LIBRARY\_V8\_05.GLB LIBVersion: v8\_05 - L10004 PyVersion: v8\_05 - Case+Logs 0003 | Graph G - PLOTS - SITE - GENERAL | 729180\_84\_ST\_ALDATES\_OXFORD.GPJ - v8\_05 | 04/06/14 - 13:13 | HP

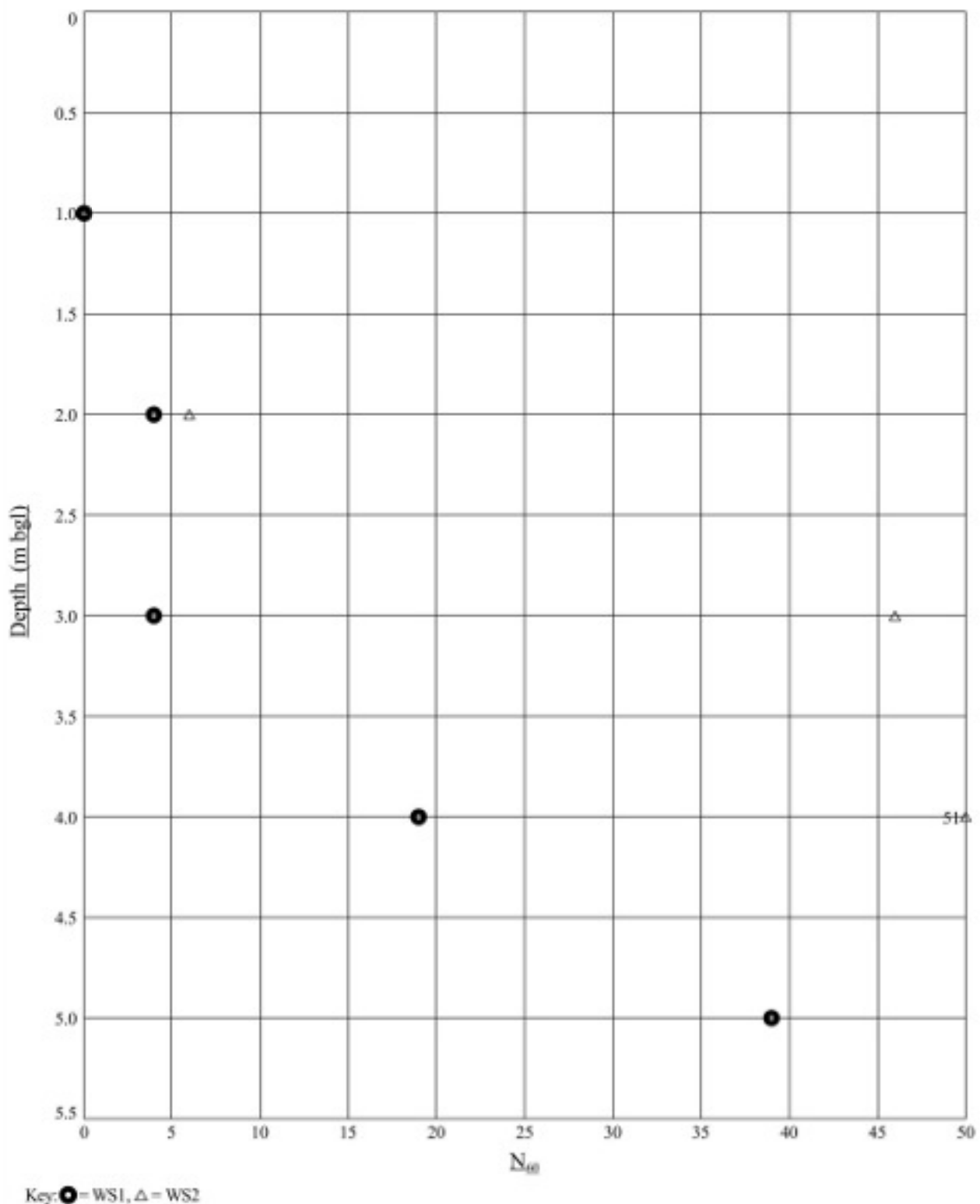


**STRUCTURAL SOILS**  
The Old School  
Stillhouse Lane  
Bedminster  
Bristol BS3 4EB



Contract	<b>84 St. Aldates</b>
Client	<b>Mann Williams</b>

Date	04.06.14	Compiled By	<i>HP</i>
Contract Ref:		729180	

# STANDARD PENETRATION TEST (SPT $N_{60}$ ) vs DEPTH



GINT\_LIBRARY\_V8\_05.GLB LIBVersion: v8\_05 - Case+Logs 0003 | Graph G - PLOTS - SITE - GENERAL | 729180\_84\_ST\_ALDATES\_OXFORD.GPJ - v8\_05 | 04/06/14 - 13:23 | HP

 <b>STRUCTURAL SOILS</b> The Old School Stillhouse Lane Bedminster Bristol BS3 4EB	Contract	Date	Compiled By
	<b>84 St. Aldates</b>	04.06.14	<i>HP</i>
	Client	Contract Ref:	
	<b>Mann Williams</b>	729180 	

## **APPENDIX D**

- (i) Geotechnical Laboratory Test Verification Sheet
- (ii) Geotechnical Laboratory Test Results

# TESTING VERIFICATION CERTIFICATE



1774

The test results included in this report are certified as:-

**ISSUE STATUS: FINAL**

In accordance with Structural Soils Ltd Laboratory Quality Assurance Manual, Issue 6, January 2010 all results sheets and summaries of results issued by the laboratory are checked by an approved signatory. This check will also involve checking of at least 10% of calculations for each test type to ensure that data has been correctly entered into the computer and calculated. The integrity of the test data and results are ensured by control of the computer system employed by the laboratory as part of the Software Verification Program as detailed in the Laboratory Quality Assurance Manual.

This testing verification certificate covers all testing compiled on or before the following datetime: **15/05/2014 14:04:29**.

Testing reported after this date is not covered by this Verification Certificate.

Approved Signatory  
**Justin Barrett (Laboratory Manager)**



**STRUCTURAL SOILS**  
1a Princess Street  
Bedminster  
Bristol  
BS3 4AG

Contract:

**84 St. Aldates**

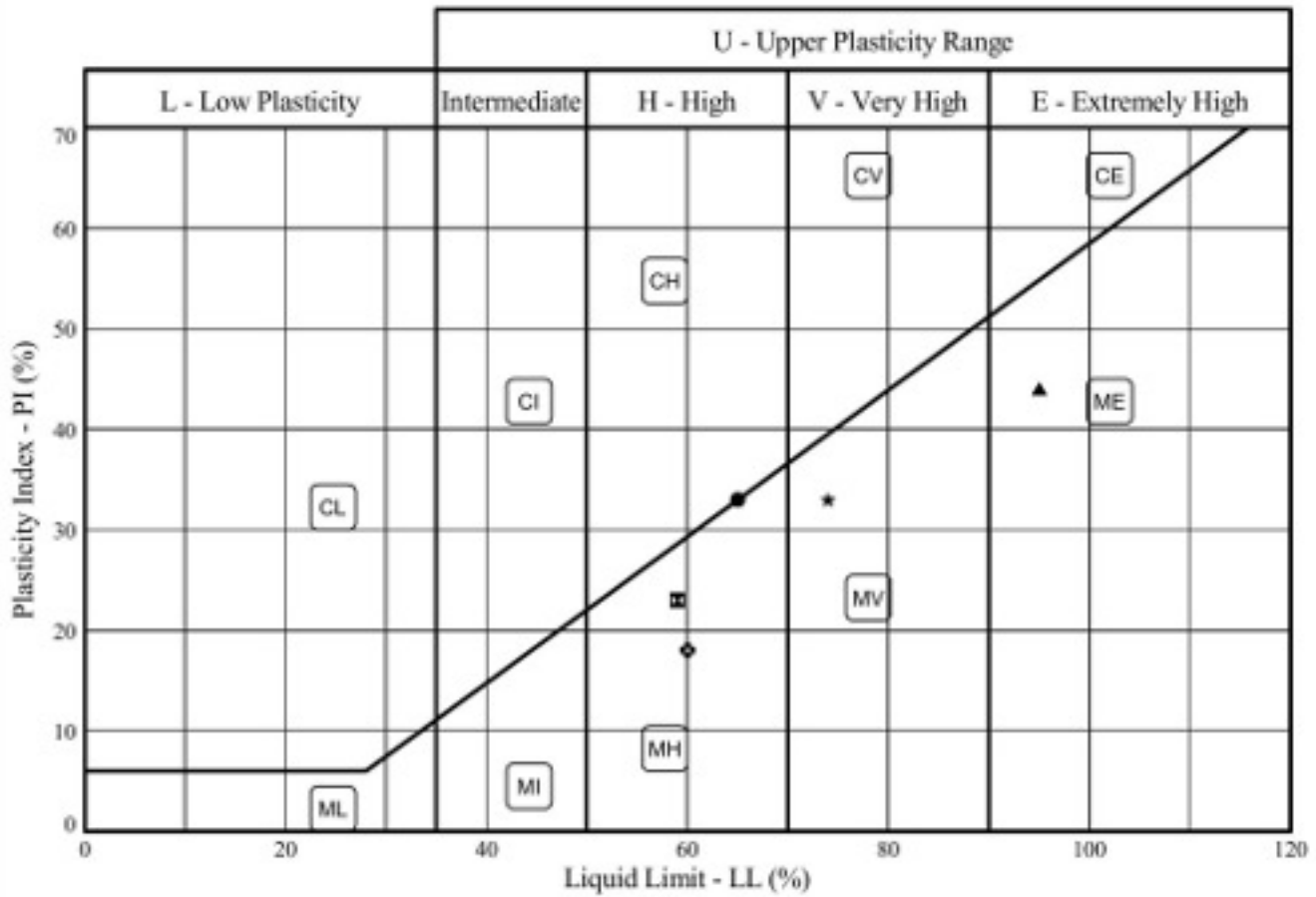
Job No:

**729180**



# PLASTICITY CHART - PI Vs LL

In accordance with clause 42.3 of BS5930:1999  
Testing in accordance with BS1377-2:1990



Sample Identification			BS Test Method #	Preparation Method +	MC %	LL %	PL %	PI %	<425um %	
Exploratory Position ID	Sample	Depth (m)								
●	WS1	9D	2.60	3.2/4.4/5.3/5.4	4.2.4	38	65	32	33	80
■	WS1	11DSPT	3.00	3.2/4.4/5.3/5.4	4.2.4	48	59	36	23	63 *
▲	WS1	12D	3.40	3.2/4.4/5.3/5.4	4.2.4	66	95	51	44	77
★	WS2	6D	1.35	3.2/4.4/5.3/5.4	4.2.4	45	74	41	33	66
	WS2	10D	2.35	3.2/4.4/5.3/5.4	4.2.3	113	197	104	93	83
◆	WS2	12D	3.00	3.2/4.4/5.3/5.4	4.2.4	77	60	42	18	73

# Tested in accordance with the following clauses of BS1377-2:1990.

- 3.2 - Moisture Content
- 4.3 - Cone Penetrometer Method
- 4.4 - One Point Cone Penetrometer Method
- 4.6 - One Point Casagrande Method
- 5.3 - Plastic Limit Method
- 5.4 - Plasticity Index

+ Tested in accordance with the following clauses of BS1377-2:1990.

- 4.2.3 - Natural State
- 4.2.4 - Wet Sieved

Key: \* = Non standard test, NP = Non plastic.

Approved Signatories: J.BARRETT A.FROST M.STOKES S.HANDCOCK S.PHILP



**STRUCTURAL SOILS**  
1a Princess Street  
Bedminster  
Bristol  
BS3 4AG

Compiled By		Date
A.S. Frost		12/05/14
Contract		Contract Ref:
84 St. Aldates		729180



## SUMMARY OF CHEMICAL ANALYSES

Exploratory Position ID	Sample Ref	Sample Type	Depth (m)	Acid Soluble Sulphate (% SO <sub>4</sub> )	Aqueous Extract Sulphate (mg/l SO <sub>4</sub> )	pH	Total Sulphur (%)	Description
WS1	9	D	2.60	0.08	96	8.12	0.03	Greyish brown mottled orangish brown slightly sandy slightly gravelly clayey SILT
WS1	12	D	3.40	0.13	123	8.09	0.29	Dark brown mottled dark grey slightly gravelly SILT with some organic matter
WS1	16	D	4.60		74	8.38		Brown slightly clayey gravelly SAND
WS2	10	D	2.35	0.23	289	8.23	0.80	Dark brown/black slightly sandy slightly gravelly SILT with some organic matter
WS2	16	D	4.00		46	8.73		Brown clayey very sandy GRAVEL

NOTES:- All chemical tests were undertaken by Envirolab.

Approved Signatories: J.BARRETT A.FROST M.STOKES S.HANDCOCK S.PHILP



**STRUCTURAL SOILS**  
1a Princess Street  
Bedminster  
Bristol  
BS3 4AG

Compiled By

*A. J. Frost*

**ALAN FROST**

Date

**12.05.14**

Contract Ref:

**729180**

Contract:

**84 St. Aldates**



## SUMMARY OF SOIL CLASSIFICATION TESTS

In accordance with clauses 3.2,4.3,4.4,5.3,5.4,7.2,8.2,8.3 of BS1377:Part 2:1990

Exploratory Position ID	Sample Ref	Sample Type	Depth (m)	Moisture Content %	Liquid Limit %	Plastic Limit %	Plasticity Index %	% <425um	Description of Sample
WS1	9	D	2.60	38	65	32	33	80	Greyish brown mottled orangish brown slightly sandy slightly gravelly clayey SILT
WS1	11	DSPT	3.00	48	59	36	23	63	Dark grey slightly gravelly sandy SILT
WS1	12	D	3.40	66	95	51	44	77	Dark brown mottled dark grey slightly gravelly SILT with some organic matter
WS2	6	D	1.35	45	74	41	33	66	Dark brown mottled dark grey slightly sandy slightly gravelly SILT
WS2	10	D	2.35	113	197	104	93	83	Dark brown/black slightly sandy slightly gravelly SILT with some organic matter
WS2	12	D	3.00	77	60	42	18	73	Dark grey slightly sandy slightly gravelly SILT with some organic matter



**STRUCTURAL  
SOILS LTD**

Contract:

**84 St. Aldates**

Contract Ref:

**729180**





## **APPENDIX E**

- (i) Contamination Laboratory Test Results
- (ii) Initial Waste Characterisation (Haswaste)
- (iii) Laboratory UKAS Accreditation Certificate
- (iv) RSK Group Generic Assessment Criteria (GAC)

## FINAL ANALYTICAL TEST REPORT

Envirolab Job Number: 14/02063  
Issue Number: 1 Date: 08 May, 2014

Client: Structural Soils Bristol  
The Old School House  
Stillhouse Lane  
Bedminster  
Bristol  
UK  
BS3 4EB

Project Manager: Helen Perry  
Project Name: 84 St. Aldate's  
Project Ref: 729180  
Order No: N/A  
Date Samples Received: 24/04/14  
Date Instructions Received: 24/04/14  
Date Analysis Completed: 08/05/14

Prepared by:

  
Melanie Marshall  
Laboratory Coordinator

Approved by:

  
Liz Oliver  
Client Service Manager

Envirolab Job Number: 14/02063

Client Project Name: 84 St. Aldate's

Client Project Ref: 729180

Lab Sample ID	14/02063/1	14/02063/2	14/02063/3	14/02063/4	14/02063/5	14/02063/6				
Client Sample No	1	1	1	2	1	2				
Client Sample ID	TP1	TP4	WS1	WS1	WS2	WS2				
Depth to Top	0.50	0.50	0.30	2.00	0.30	2.00				
Depth To Bottom										
Date Sampled	22-Apr-14	22-Apr-14	22-Apr-14	22-Apr-14	22-Apr-14	22-Apr-14				
Sample Type	Soil - ES	Soil - ES	Soil - ES	Soil - ES	Soil - ES	Soil - ES				
MCERTS Sample Matrix Code	5AB	4ABE	4A	6A	4A	6A				
									Units	Method ref
% Stones >10mm <sub>s</sub> <sup>†</sup>	11.4	7.1	13.4	8.4	12.9	<0.1			% w/w	A-T-008
pH <sub>s</sub> <sup>††</sup>	10.30	8.07	8.42	8.17	8.33	8.09			pH	A-T-025
Sulphate (water sol 2:1) <sub>s</sub> <sup>†††</sup>	0.26	1.30	0.10	0.05	0.16	0.05			g/l	A-T-026
Organic matter <sub>s</sub> <sup>††††</sup>	1.3	8.6	3.1	3.1	1.3	5.0			% w/w	A-T-028 08
Arsenic <sub>s</sub> <sup>†††††</sup>	26	14	27	12	15	20			mg/kg	A-T-029
Cadmium <sub>s</sub> <sup>†††††</sup>	0.8	0.6	1.0	0.8	0.8	1.0			mg/kg	A-T-029
Copper <sub>s</sub> <sup>†††††</sup>	61	27	20	24	24	18			mg/kg	A-T-029
Chromium <sub>s</sub> <sup>†††††</sup>	13	9	17	20	12	22			mg/kg	A-T-029
Lead <sub>s</sub> <sup>†††††</sup>	128	261	201	146	139	101			mg/kg	A-T-029
Mercury <sub>s</sub>	1.17	0.98	0.92	0.38	0.65	0.39			mg/kg	A-T-029
Nickel <sub>s</sub> <sup>†††††</sup>	13	11	17	16	13	16			mg/kg	A-T-029
Selenium <sub>s</sub> <sup>†††††</sup>	<1	<1	<1	<1	<1	<1			mg/kg	A-T-029
Zinc <sub>s</sub> <sup>†††††</sup>	73	85	104	80	48	74			mg/kg	A-T-029

Envirolab Job Number: 14/02063

Client Project Name: 84 St. Aldate's

Client Project Ref: 729180

Lab Sample ID	14/02063/1	14/02063/2	14/02063/3	14/02063/4	14/02063/5	14/02063/6			
Client Sample No	1	1	1	2	1	2			
Client Sample ID	TP1	TP4	WS1	WS1	WS2	WS2			
Depth to Top	0.50	0.50	0.30	2.00	0.30	2.00			
Depth To Bottom									
Date Sampled	22-Apr-14	22-Apr-14	22-Apr-14	22-Apr-14	22-Apr-14	22-Apr-14			
Sample Type	Soil - ES	Soil - ES	Soil - ES	Soil - ES	Soil - ES	Soil - ES			
MCERTS Sample Matrix Code	5AB	4ABE	4A	5A	4A	5A			
								Units	Method ref
TPH CWG									
All >C5-C6 <sub>s</sub> <sup>f</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-02b
All >C6-C8 <sub>s</sub> <sup>f</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-02b
All >C8-C10 <sub>s</sub> <sup>f</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-02b
All >C10-C12 <sub>s</sub> <sup>f</sup>	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		mg/kg	A-T-02b
All >C12-C16 <sub>s</sub> <sup>f</sup>	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		mg/kg	A-T-02b
All >C16-C21 <sub>s</sub> <sup>f</sup>	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		mg/kg	A-T-02b
All >C21-C35 <sub>s</sub> <sup>f</sup>	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		mg/kg	A-T-02b
Total Aliphatics <sub>s</sub>	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		mg/kg	A-T-02b-2b
Aro >C5-C7 <sub>s</sub> <sup>f</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-02b
Aro >C7-C8 <sub>s</sub> <sup>f</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-02b
Aro >C8-C9 <sub>s</sub> <sup>f</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-02b
Aro >C9-C10 <sub>s</sub> <sup>f</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-02b
Aro >C10-C12 <sub>s</sub> <sup>f</sup>	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		mg/kg	A-T-02b
Aro >C12-C16 <sub>s</sub> <sup>f</sup>	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		mg/kg	A-T-02b
Aro >C16-C21 <sub>s</sub> <sup>f</sup>	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		mg/kg	A-T-02b
Aro >C21-C35 <sub>s</sub> <sup>f</sup>	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		mg/kg	A-T-02b
Total Aromatics <sub>s</sub>	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		mg/kg	A-T-02b-2b
TPH (All & Aro) <sub>s</sub>	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		mg/kg	A-T-02b-2b
BTEX - Benzene <sub>s</sub> <sup>f</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-02b
BTEX - Toluene <sub>s</sub> <sup>f</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-02b
BTEX - Ethyl Benzene <sub>s</sub> <sup>f</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-02b
BTEX - m & p Xylene <sub>s</sub> <sup>f</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-02b
BTEX - o Xylene <sub>s</sub> <sup>f</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-02b
MTBE <sub>s</sub> <sup>f</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-02b

Envirolab Job Number: 14/02063

Client Project Name: 84 St. Aldate's

Client Project Ref: 729180

Lab Sample ID	14/02063/1	14/02063/2	14/02063/3	14/02063/4	14/02063/5	14/02063/6			
Client Sample No	1	1	1	2	1	2			
Client Sample ID	TP1	TP4	WS1	WS1	WS2	WS2			
Depth to Top	0.50	0.50	0.30	2.00	0.30	2.00			
Depth To Bottom									
Date Sampled	22-Apr-14	22-Apr-14	22-Apr-14	22-Apr-14	22-Apr-14	22-Apr-14			
Sample Type	Soil - ES	Soil - ES	Soil - ES	Soil - ES	Soil - ES	Soil - ES			
MCERTS Sample Matrix Code	5AB	4ABE	4A	6A	4A	6A			
PAH 16									
Acenaphthene <sub>16</sub> <sup>MS</sup>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01		mg/kg	A-T-01b
Acenaphthylene <sub>16</sub> <sup>MS</sup>	<0.01	0.01	0.02	<0.01	<0.01	<0.01		mg/kg	A-T-01b
Anthracene <sub>16</sub> <sup>MS</sup>	<0.02	0.03	0.06	<0.02	<0.02	<0.02		mg/kg	A-T-01b
Benzo(a)anthracene <sub>16</sub> <sup>MS</sup>	<0.04	0.14	0.20	<0.04	<0.04	<0.04		mg/kg	A-T-01b
Benzo(a)pyrene <sub>16</sub> <sup>MS</sup>	0.05	0.16	0.16	<0.04	<0.04	<0.04		mg/kg	A-T-01b
Benzo(b)fluoranthene <sub>16</sub> <sup>MS</sup>	0.06	0.22	0.19	<0.05	<0.05	<0.05		mg/kg	A-T-01b
Benzo(ghi)perylene <sub>16</sub> <sup>MS</sup>	<0.05	0.12	0.08	<0.05	<0.05	<0.05		mg/kg	A-T-01b
Benzo(k)fluoranthene <sub>16</sub> <sup>MS</sup>	<0.07	0.10	0.06	<0.07	<0.07	<0.07		mg/kg	A-T-01b
Chrysene <sub>16</sub> <sup>MS</sup>	<0.06	0.17	0.16	<0.06	<0.06	<0.06		mg/kg	A-T-01b
Dibenzo(ah)anthracene <sub>16</sub> <sup>MS</sup>	<0.04	<0.04	<0.04	<0.04	<0.04	<0.04		mg/kg	A-T-01b
Fluoranthene <sub>16</sub> <sup>MS</sup>	<0.06	0.29	0.36	<0.06	<0.06	<0.06		mg/kg	A-T-01b
Fluorene <sub>16</sub> <sup>MS</sup>	<0.01	<0.01	0.03	<0.01	<0.01	<0.01		mg/kg	A-T-01b
Indeno(123-cd)pyrene <sub>16</sub> <sup>MS</sup>	0.04	0.11	0.06	<0.03	<0.03	<0.03		mg/kg	A-T-01b
Naphthalene <sub>16</sub> <sup>MS</sup>	<0.03	<0.03	<0.03	<0.03	<0.03	<0.03		mg/kg	A-T-01b
Phenanthrene <sub>16</sub> <sup>MS</sup>	<0.03	0.11	0.24	<0.03	<0.03	<0.03		mg/kg	A-T-01b
Pyrene <sub>16</sub> <sup>MS</sup>	<0.07	0.23	0.29	<0.07	<0.07	<0.07		mg/kg	A-T-01b
PAH (total 16) <sub>16</sub> <sup>MS</sup>	0.17	1.72	2.01	<0.06	<0.06	<0.06		mg/kg	A-T-01b

## REPORT NOTES

### Notes - Soil chemical analysis

All results are reported as dry weight (<40°C).

For samples with Matrix Codes 1 - 6 natural stones >10mm are removed or excluded from the sample prior to analysis and reported results corrected to a whole sample basis. For samples with Matrix Code 7 the whole sample is dried and crushed prior to analysis.

### Notes - General

This report shall not be reproduced, except in full, without written approval from Envirolab.

Subscript "A" indicates analysis performed on the sample as received. "D" indicates analysis performed on the dried sample, crushed to pass a 2mm sieve, unless asbestos is found to be present in which case all analysis is performed on the sample as received.

All analysis is performed on the dried and crushed sample for samples with Matrix Code 7 and this supercedes any "A" subscripts.

All analysis is performed on the sample as received for soil samples from outside the European Union and this supercedes any "D" subscripts.

Superscript "M" indicates method accredited to MCERTS.

For complex, multi-compound analysis, quality control results do not always fall within chart limits for every compound and we have criteria for reporting in these situations. If results are in italic font they are associated with such quality control failures and may be unreliable.

A deviating samples report is appended and will indicate if samples or tests have been found to be deviating. Any test results affected may not be an accurate record of the concentration at the time of sampling and, as a result, may be invalid.

### TPH analysis of water by method A-T-007

Free and visible oils are excluded from the sample used for analysis so that the reported result represents the dissolved phase only.

### Asbestos in soil

Asbestos in soil analysis is performed on a dried aliquot of the submitted sample and cannot guarantee to identify asbestos if present as discrete fibres/fragments. Stones etc. are not removed from the sample prior to analysis.

Quantification of asbestos is a 3 stage process including visual identification, hand picking and weighing and fibre counting by sedimentation/phase contrast optical microscopy if required. If asbestos is identified a being present but is not in a form that is suitable for analysis by hand picking and weighing (normally if the asbestos is present as free fibres) quantification by sedimentation is performed. Where ACMs are found a percentage asbestos is assigned to each with reference to 'HSG264, Asbestos: The survey guide' and the calculated asbestos content is expressed as a percentage of the dried soil sample aliquot used.

### Predominant Matrix Codes:

1 = SAND, 2 = LOAM, 3 = CLAY, 4 = LOAM/SAND, 5 = SAND/CLAY, 6 = CLAY/LOAM, 7 = OTHER.

Samples with Matrix Code 7 are not predominantly a SAND/LOAM/CLAY mix and are not covered by our MCERTS accreditation.

### Secondary Matrix Codes:

A = contains stones, B = contains construction rubble, C = contains visible hydrocarbons, D = contains glass/metal,

E = contains roots/twigs.

IS indicates Insufficient sample for analysis.

NDP indicates No Determination Possible.

NAD indicates No Asbestos Detected.

N/A indicates Not Applicable.

Superscript # Indicates method accredited to ISO 17025.

Analytical results reflect the quality of the sample at the time of analysis only. Opinions and interpretations expressed are outside the scope of our accreditation.

Please contact us if you need any further information.

HASWASTE v5.2b: Envirolab's Contaminated Land Soil Hazardous Waste Assessment Tool

Envirolab, Sandpits Business Park, Mottram Road, Hyde, Cheshire SK14 3AR.

Site Code and Name									
TFWAS/BH		TP1	TP4	WS1	WS1	WS2	WS2		
Depth (m)		0.00	0.00	0.30	3.00	0.30	3.00		
Envirolab reference		14020031	14020032	14020033	14020034	14020035	14020036		
		mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
% Moisture									
pH (soil)		6.35	6.07	6.42	6.17	6.33	6.08		
pH (leachate)									
Arsenic		25	14	21	12	15	28		
Cadmium		0.8	0.6	1.0	0.8	0.8	1.0		
Copper		61	27	30	24	28	18		
Cr(VI) or Chromium		15	9	11	28	10	22		
Lead		128	261	261	146	118	191		
Mercury		1.17	0.98	0.92	0.38	0.95	0.39		
Nickel		15	11	11	16	15	16		
Selenium		1	1	1	1	1	1		
Zinc		75	58	104	58	45	74		
Beryllium									
Barium									
Cobalt									
Manganese									
Molybdenum									
TPH									
Petrol									
Diesel									
Lube Oil									
White Spirit / Kerosene									
Cresols									
Unknown TPH with ID									
Unknown TPHCWG									
Inseparable TPH Mixtures									
Any									
Any but No Petrol									
White Spirit / Kerosene and Diesel									
Total USEPA 16 PAHs		0.2	1.7	2.0	0.1	0.1	0.1		
Acenaphthene		0.01	0.01	0.01	0.01	0.01	0.01		
Acenaphthylene		0.01	0.01	0.02	0.01	0.01	0.01		
Anthracene		0.02	0.02	0.02	0.02	0.02	0.02		
Benzo[a]anthracene		0.04	0.14	0.20	0.04	0.04	0.04		
Benzo[a]pyrene		0.05	0.18	0.16	0.04	0.04	0.04		
Benzo[b]fluoranthene		0.05	0.22	0.15	0.05	0.05	0.05		
Benzo[g]perylene		0.05	0.12	0.08	0.05	0.05	0.05		
Benzo[k]fluoranthene		0.07	0.18	0.08	0.07	0.07	0.07		
Chrysene		0.06	0.17	0.16	0.06	0.06	0.06		
Di-benz[a,h]anthracene		0.04	0.04	0.04	0.04	0.04	0.04		
Fluoranthene		0.02	0.23	0.20	0.02	0.02	0.02		
Fluorene		0.01	0.01	0.01	0.01	0.01	0.01		
Indeno[1,2,3-cd]pyrene		0.04	0.11	0.08	0.03	0.03	0.03		
Naphthalene		0.03	0.03	0.03	0.03	0.03	0.03		
Phenanthrene		0.03	0.11	0.24	0.03	0.03	0.03		
Pyrene		0.07	0.23	0.29	0.07	0.07	0.07		
Benzene		0.01	0.01	0.01	0.01	0.01	0.01		
Toluene		0.01	0.01	0.01	0.01	0.01	0.01		
Ethylbenzene		0.01	0.01	0.01	0.01	0.01	0.01		
Xylenes		0.01	0.01	0.01	0.01	0.01	0.01		
Trimethylbenzenes		0.010	0.010	0.010	0.010	0.010	0.010		
Chlorobenzene									
1,2-Dichlorobenzene									
1,3-Dichlorobenzene									
1,4-Dichlorobenzene									
1,2,4-Trichlorobenzene									
2-Chlorotoluene									
4-Chlorotoluene									
Trichloroethene (TCE)									
Total Sulphide									
Free Cyanide									
Thiocyanate									
Elemental Free Sulphur									
PCBs Total (eg EC19WD12)									
Phenols Total by HPLC									
Phenol									
Cresols									
Xylenols									
1-Naphthol									
Resorcinol									
2,3,5-Trichlorophenol									
2,4,5-Trichlorophenol									
2,4,6-Trichlorophenol									
2,4-Dichlorophenol									
4-Chloro-3-methylphenol									
Pentachlorophenol									
Bis(2-ethylhexyl)phthalate									
Butylbenzylphthalate									
Di-n-butylphthalate									

HASWASTE v5.2b. EnviroLab's Contaminated Land Soil Hazardous Waste Assessment Tool.  
 EnviroLab, Sandpits Business Park, Mottram Road, Hyde, Cheshire SK14 5AR.

Site Code and Name

TP/WS/BH  
 Depth (m)  
 EnviroLab reference

Asbestos in Soil  
 Asbestos detected in Soil (enter Y or N)  
 Asbestos % Composition in Soil (Matrix Loose Fibres or Microscopic Identifiable Pieces only)  
 Asbestos identifiable Pieces visible with the naked eye detected in the Soil (enter Y or N).

TP1	TP4	WS1	WS1	WS2	WS2		
0.30	0.06	0.30	0.06	0.30	0.06		
14/020631	14/020632	14/020633	14/020634	14/020635	14/020636		
mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
%	%	%	%	%	%	%	%
N	N	N	N	N	N		
N	N	N	N	N	N		

Hazard Codes	Thresholds
Inflam H4	>1%
Inflam H4	>2%
Harmful H5	>20%
Toxic H6	>1%
Toxic H6	>2%
Carcinogenic H7	>0.1%
Carcinogenic H7	>1%
Carcinogenic H7 Unknown TPH with ID	>1,000 mg/kg
Carcinogenic H7 biop marker test (unknown TPH with ID only)	>0.2%
Carcinogenic H7 % Asbestos in Soil (Fibres)	>0.1%
Corrosive H8 (Inflam H4)	>50%+10% >40%+2%
pH Corrosive H8 (Inflam H4) pH (soil or leachate)	H8 <11.5
pH Corrosive H8 (Inflam H4) pH (soil or leachate)	H8 <12
Toxic for Reproduction H10	>0.2%
Toxic for Reproduction H10	>2%
Mutagenic H11	>0.1%
Mutagenic H11 Unknown TPH with ID	>1,000 mg/kg
Mutagenic H11 biop marker test (unknown TPH with ID only)	>0.2%
Mutagenic H11	>1%
Produces Toxic Gases H12 Sulphide	>1,400 mg/kg
Produces Toxic Gases H12 Free Cyanide	>1,200 mg/kg
Produces Toxic Gases H12 Thiocyanate	>2,600 mg/kg
H12 Sensitivity	>1%
Ecotoxic H14	>10
Ecotoxic H14 individual substance specific thresholds	>0.025%
Ecotoxic H14 individual substance specific thresholds	>0.025%

0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.000	0.002	0.004	0.002	0.002	0.002	0.000	0.000
0.002	0.015	0.020	0.025	0.010	0.015	0.000	0.000
0.002	0.0017	0.0021	0.0013	0.0010	0.0011	0.0000	0.0000
0.0040	0.0030	0.0039	0.0047	0.0030	0.0049	0.0000	0.0000
0.0030	0.0028	0.0040	0.0042	0.0027	0.0028	0.0000	0.0000
0.0002	0.0017	0.0020	0.0021	0.0021	0.0021	0.0000	0.0000
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
10.38	0.07	0.42	0.17	0.33	0.08	0.0	0.0
10.38	0.07	0.40	0.17	0.33	0.08	0.0	0.0
0.0280	0.0281	0.0270	0.0148	0.0280	0.0121	0.0000	0.0000
0.0280	0.0281	0.0270	0.0148	0.0280	0.0121	0.0000	0.0000
0.0002	0.0017	0.0020	0.0021	0.0021	0.0021	0.0000	0.0000
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0040	0.0028	0.0040	0.0042	0.0027	0.0028	0.0000	0.0000
0.1547	0.1478	0.1985	0.1548	0.1417	0.1380	0.0000	0.0000
0.00017	0.00172	0.00201	0.00006	0.00008	0.00006	0.00008	0.00000
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000



# United Kingdom Accreditation Service

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## ACCREDITATION CERTIFICATE



**TESTING LABORATORY**  
**No. 1247**

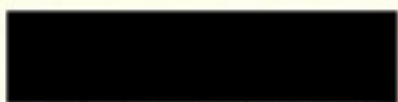
**Envirolab**

is accredited in accordance with the recognised International Standard ISO/IEC 17025:2005  
General Requirements for the competence of testing and calibration laboratories.

This accreditation demonstrates technical competence for a defined scope as detailed in and at the locations specified in the schedule to this certificate, and the operation of a laboratory quality management system (refer joint ISO-ILAC-IAF Communiqué dated January 2009).

The schedule to this certificate is an essential accreditation document and from time to time may be revised and reissued by the United Kingdom Accreditation Service. The most recent issue of the schedule of accreditation, which bears the same accreditation number as this certificate, is available from the UKAS website [www.ukas.com](http://www.ukas.com).

This accreditation is subject to continuing conformity with United Kingdom Accreditation Service requirements. The absence of a schedule on the UKAS website indicates that the accreditation is no longer in force.

  
Accreditation Manager, United Kingdom Accreditation Service

**Initial Accreditation date**  
**2 December 1992**

**This certificate issued on**  
**12 November 2012**

UKAS is appointed as the sole national accreditation body for the UK by The Accreditation Regulations 2009 (SI No 3155/2009) and operates under a Memorandum of Understanding (MoU) with the Department for Business, Innovation and Skills (BIS).



**Table 6**  
Human health generic assessment criteria for residential with communal soft landscaping

Compound	GrAC for groundwater (mg/l)	SAC for soil SOM 1% (mg/kg)	SAC for soil SOM 2.5% (mg/kg)	SAC for soil SOM 6% (mg/kg)
<b>Metals</b>				
Arsenic	-	35	35	35
Cadmium	-	55	85	85
Chromium (III) - oxide	-	3,000	3,000	3,000
Chromium (VI) - hexavalent	-	4.3	4.3	4.3
Copper	-	6,200	6,200	6,200
Lead	-	300	300	300
Elemental Mercury (Hg <sup>0</sup> )	0.0094	0.17	0.42	1.0
Inorganic Mercury (Hg <sup>2+</sup> )	-	240	240	240
Methyl Mercury (Hg <sup>+</sup> )	20	5.4	1.1	1.1
Nickel	-	130	130	130
Selenium	-	600	600	600
Zinc	-	41,000	41,000	41,000
Cyanide	-	110	140	110
<b>Volatile organic compounds</b>				
Benzene	7	0.27	0.49	1.0
Toluene	1,900	610	1,200	2,700
Ethylbenzene	290	170	361	840
Xylene - m	84	55	130	300
Xylene - o	100	50	139	320
Xylene - p	87	53	125	290
Triethylene	84	55	130	300
Methyl tertiary butyl ether (MTBE)	2,200	180	159.55	270
Trichloroethene	1.8	0.11	0.2	0.51
Tetrachloroethene	3.6	1.0	2.3	5.3
1,1,1-Trichloroethane	20	6.3	12.9	29
1,1,1,2-Tetrachloroethane	14	1.1	2.5	5.8
1,1,2,2-Tetrachloroethane	14	2.7	5.58	12
Carbon tetrachloride	0.055	0.02	0.040	0.09
1,2-Dichloroethane	0.30	0.076	0.0763	0.07
Vinyl chloride	0.019	0.0025	0.0007	0.001
1,2,4-Trimethylbenzene	0.075	0.4	0.99	2.3
1,3,5-Trimethylbenzene	0.047	0.5	1.10	2.6
<b>Semi-volatile organic compounds</b>				
Acenaphthene	3.2	2,000 (157)	3,700 (191)	3,500 (240)
Acenaphthylene	4.2	2,000 (198)	3,000 (212)	3,500 (210)
Anthracene	0.001	20,000 (1.2)	22,000	23,000
Benzo[a]anthracene	0.004	3.7	6.2	6.2
Benzo[b]fluoranthene	0.017	7.0	7.3	7.4
Benzo[a,h]perylene	0.0009	47	47	48
Benzo[k]fluoranthene	0.0108	10	10	10
Chrysene	0.002	5.5	9.7	10
Dibenz[a,h]anthracene	0.0006	0.87	0.91	0.93
Fluoranthene	0.23	970	990	1,000
Fluorene	1.0	1,000 (131)	2,500 (277)	2,500 (180)
Indeno[1,2,3-cd]pyrene	0.0003	4.2	4.4	4.4
Phenanthrene	0.53	840 (28)	930	970
Pyrene	0.13	2,300	2,400	2,400
Benzo[e]pyrene	0.004	1.0	1.0	1.0
Naphthalene	15	1.5	3.9	9.2
Phenol	-	310	420	520
<b>Total petroleum hydrocarbons</b>				
Aliphatic hydrocarbons <EC <sub>10</sub> -EC <sub>5</sub>	10	30	65	110
Aliphatic hydrocarbons <EC <sub>10</sub> -EC <sub>9</sub>	5.4	73	180	370
Aliphatic hydrocarbons <EC <sub>10</sub> -EC <sub>8</sub>	0.23	19	45	110
Aliphatic hydrocarbons <EC <sub>10</sub> -EC <sub>7</sub>	0.03	33 (46)	230 (118)	540 (285)
Aliphatic hydrocarbons <EC <sub>10</sub> -EC <sub>6</sub>	0.0048	740 (24)	1,740 (59)	3,540 (14)
Aliphatic hydrocarbons <EC <sub>10</sub> -EC <sub>5</sub>	-	45,000	64,000 (21)	77,000
Aliphatic hydrocarbons <EC <sub>10</sub> -EC <sub>4</sub>	-	45,000	64,000 (21)	77,000
Aromatic hydrocarbons <EC <sub>10</sub> -EC <sub>9</sub> (alkylenes)	7.4	260	627	1,400
Aromatic hydrocarbons <EC <sub>10</sub> -EC <sub>8</sub>	7.4	33	81	190
Aromatic hydrocarbons <EC <sub>10</sub> -EC <sub>7</sub>	21	180	417	870
Aromatic hydrocarbons <EC <sub>10</sub> -EC <sub>6</sub>	5.8	1,300 (170)	1,800 (49)	1,700
Aromatic hydrocarbons <EC <sub>10</sub> -EC <sub>5</sub>	-	1,300	1,900	1,300
Aromatic hydrocarbons <EC <sub>10</sub> -EC <sub>4</sub>	-	1,300	1,900	1,300
Aromatic hydrocarbons <EC <sub>10</sub> -EC <sub>3</sub>	-	1,300	1,900	1,300

**Notes:**

∇ Generic assessment criteria not calculated owing to low volatility of substance and therefore no pathway or an absence of toxicological data.

EC - eqv. alkyl carbon; GrAC - groundwater assessment criteria; SAC - soil assessment criteria.

The SAC for organic compounds are dependent on Soil Organic Matter (SOM) (%) content. To obtain SOM from total organic carbon (TOC) (%) divide by 0.58:  
 1% TOC is 0.58% SOM. (B. Rowell and Ransom, Methods and Applications, Longman, 1988)

SAC for TPH fractions, polycyclic aromatic hydrocarbons, MTBE, BTEX and trimethylbenzene compounds were produced using an attenuation factor for the indoor air inhalation pathway of 10 to reduce conservatism associated with the vapour inhalation pathway, section 10.1.1, SP3.

The SAC has been set as the model calculated SAC with the default on limit shown in brackets.  
 For consistency where the GrAC exceeds the solubility limit, GrAC has been set at the solubility limit. These are highly conservative as concentrations of the chemical are very unlikely to be at sufficient concentration to result in an exceedance of the threshold criteria value at the point of exposure (i.e. indoor air) provided the phase product is stable.