



## DRAINAGE STRATEGY REPORT

76-78 HIGH STREET, TONBRIDGE, KENT TN9 1EE

ON BEHALF OF MCCARTHY & STONE RETIREMENT LIFESTYLES LTD

MAY2021

IDL/1070/DS/001



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# DRAINAGE STRATEGY REPORT

**IDL/1070/DS/001**

REPORT ISSUE

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P01 12/05/2021 Preliminary Issue

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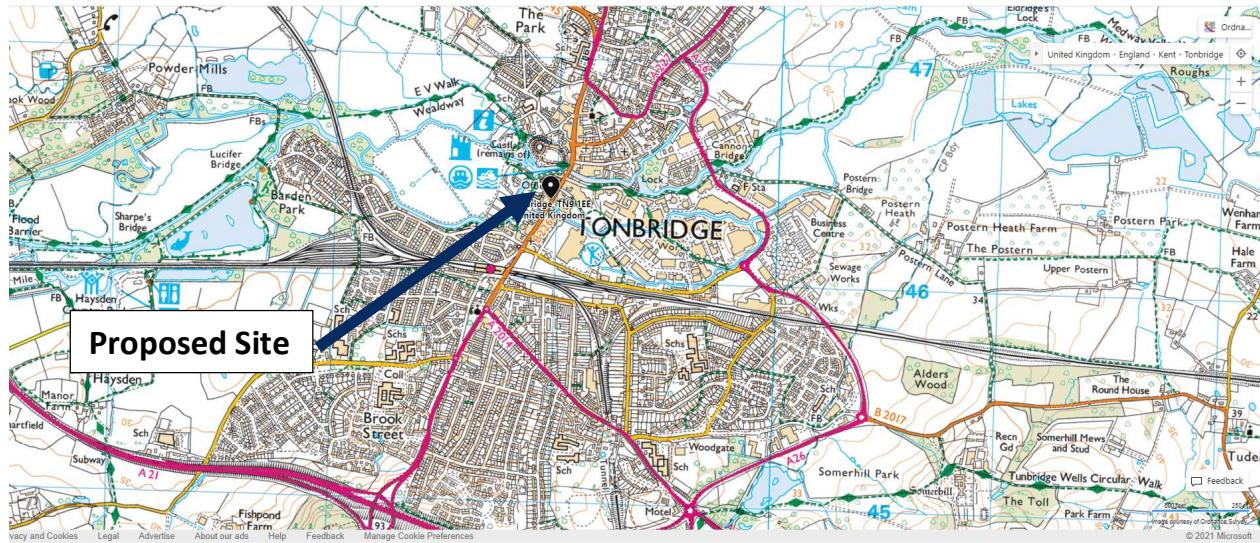
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## 1 INTRODUCTION

- 1.1 Infrastructure Design Ltd has been appointed by **McCarthy & Stone Ltd** to prepare this Foul, Surface Water & SuDS Strategy Report to support their planning application for their proposed retirement living plus accommodation development site.
- 1.2 This report has been prepared in accordance with both national and local planning policy and takes guidance from Ciria 753, The SuDS Manual and The Building Regulations, Approved Document Part H.
- 1.3 The site is located to the northwest of High Street and 90m east of the River Medway. River Walk bounds the west, New Wharf Road to the north, High Street to the east and commercial properties are present to the northeast and south of the site. The development site is centred approximately on the Ordnance Survey (OS) national grid reference 558932mE, 146409mN. Refer to the site location extract in Figure 1 below;

**Figure 1 – Site Location Plan**



1.4 Reference Documents:-

Southern Water asset search.

Topographical Survey carried out by Laser Surveys Ltd dated Dec 2020.

Crossfield Consulting Geotechnical Environmental desk study Report No. CCL03372.CM32 appraisal was carried out in October 2020.

Rosemary White Design Ground Floor Plan SE-2739-02-AC-03 Rev E

- 1.5 Currently site is brownfield. The eastern part of the site is occupied by a two-storey commercial unit (Poundland). The western part of the site comprises a surface level car park, and the commercial unit finish floor level is approximately 22.64m. The car park level is relatively flat. The car park entrance is from River Walk. The northwest corner of the site is (River Walk & New Wharf Road junction) slightly higher than the rest of the site areas. Refer to Appendix C for a copy of the topographical survey.
- 1.6 The proposed development is a construction of retirement living accommodation comprising of four-storey blocks of apartments. The apartment block is associated with car parking areas, vehicular crossover to the car parking areas and external soft and hard landscape areas.
- 1.7 A new vehicle entrance will be constructed leading from New Wharf Road.
- 1.8 The existing site total area is 2010 m<sup>2</sup> (0.201 hectares), and it is a 100% impermeable area. The proposed development's impermeable area is approximately 1720 m<sup>2</sup> (0.172 hectares).
- 1.9 Laser Surveys have carried out a topographical survey and found the below-ground surface water drainage for the existing car park and the front of the commercial unit. It is believed that these surface areas are discharging into Southern Water surface water manhole reference no:9451 located on New Wharf Road. This surface water manhole leads towards the High Street via 150mm diameter surface water sewer. A 150mm diameter foul water sewer is located on New Wharf Road and leads towards High Street. Refer to Appendix C for a copy of the topographic survey and Appendix B for a copy of the Southern Water sewer record plan.
- 1.10 Reference has been made to the British Geological Survey online data, which indicates that the site is underlain by the Turnbridge Wells Sand Formation– Sandstone and Siltstone. Alluvium-clay, silt sand and gravel superficial deposits is recorded. The extract from the BGS site is included in Appendix F.

- 1.11 Crossfield Consulting Limited undertook a desk study appraisal of the site to identify potential constraints and ground conditions. Due to the low permeability strata, groundwater will likely be present at a relatively shallow depth, which is likely to be similar to the nearby river level; it is considered that a soakaway is not a viable option for the surface water drainage outfall. Therefore, it is recommended that an alternative drainage solution is to be identified.
- 1.12 The site is located within source protection zone 1.
- 1.13 Urban Creep has not been considered, as it is not regarded as appropriate for a development of this nature.

## **2 FOUL WATER DRAINAGE**

- 2.1 The proposed foul drainage for the apartment block will be drained through the gravity drainage into the foul adoptable sewer. This gravity-fed drainage via a new manhole will discharge to the Southern Water foul sewer manhole Reference no: 9402.
- 2.2 The drainage strategy layout is included in Appendix D.

### 3 SURFACE WATER DRAINAGE & SUDS

- 3.1 The existing site is brownfield land; the total site area is 2010m<sup>2</sup>(0.201 hectares)
- 3.2 The total site's proposed impermeable area is approximately 1720 m<sup>2</sup>(0.172Ha) from the roofs and the external paved areas. The impermeable area layout is included in Appendix D.
- 3.3 As mentioned in section 1.11, the infiltration technique is not a viable option to discharge the proposed surface water runoff from the site.
- 3.4 The nearest river is not close to the site; therefore discharging the surface water runoff from the site to the watercourse is not considered feasible.
- 3.5 Discharging the proposed surface water runoff to the Southern Water sewer is considered the most feasible option for the site. The existing impermeable area for the car park and Poundland is believed to be discharging into the Southern Water sewer manhole reference no:9451 freely without any flow rate restriction. The pre-development (brownfield land) surface water runoff from the site has been calculated using the Modified Rational Method using the following equation to calculate peak runoff from area:  $Q = 2.78 Cv Cr i A$

2.78 is a conversion factor to address the rainfall unit being in mm/hr

$Cv$  = Volumetric Runoff Coefficient

$Cr$  = Routing Coefficient

$i$  = Rainfall Intensity (mm/hr) based on a 1 hour rainfall event.

$A$  = Area (ha)

- 3.6 The tables below summarise the pre & post-development runoff rates, along with the storage volumes available within each SuDs feature.

**Figure 3** Comparison of pre & post-development runoff rates

Location / Storm Event	Rainfall Intensity (mm) <b>(From FEH 2013 web service)</b>	Existing site Runoff Rate- brownfield site (l/s)	Proposed Runoff Rate (l/s)	Betterment
1 in 2 year	13.1	9.05	2.1	76%
1 in 30 year	37.06	25.5	4.5	82%

1 in 100 year	48.37	33.37	6.1	81%
1 in 100 year (+40%cc)		-	8.2	

**76% to 82% improvement in the runoff rate**

**Figure 4** Storage volumes available within each SuDS feature

LOCATION	SuDS DEVICE	AVAILABLE STORAGE
Roads and Parking areas	Granular subbase /Permeable Paving-1005m <sup>2</sup> x 0.35m x 0.33	116 m <sup>3</sup>
Crate storage	Crate system (113m <sup>2</sup> x 0.8)	91 m <sup>3</sup>

- 3.7 The proposed residential development will incorporate the use of SuDS techniques selected for their suitability given the site layout, topographical levels and geotechnical constraints. Refer to Appendix A to view the SuDS Hierarchy.
- 3.8 To summarise, the following SuDS devices will be implemented on this development;

**Porous Paving with granular sub base**

Ground Floor parking areas. These will be detailed in accordance with Interpaved System C and be lined (no infiltration).

**Crate Attenuation**

Incorporating flow controls on the outlet to accommodate the runoff from all storm events up to and including the peak 1 in 100 years, plus climate changes storm.

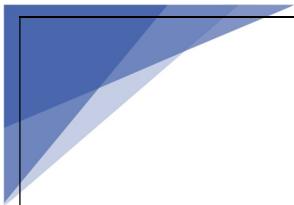
- 3.8 The calculations located in Appendix E demonstrate that where the subbase is laid level, a minimum permeable stone layer of 350mm is required. Permeable Paving with a subbase lined in an impermeable membrane will be used in forming roads and parking areas. This will serve to delay runoff into the ditch outfall slowly and improve water quality in the process.
- 3.10 All of the roof areas will drain through conventional gravity drainage and stored within the crate attenuation tank, located within the car parking areas. The crate attenuation then will discharge to the private surface water pump chamber. Pump fed surface water discharge has been chosen due to not having enough gravity fall in the proposed drainage system to the surface water sewer. The surface water runoff will outfall at a brownfield discharge rate to the existing 150mm diameter surface water sewer located south of New Wharf Road. The sewer connection consent and sewer capacity check to be obtained from Southern Water.
- 3.11 The surface water discharge rate from the new development will be limited to a maximum of 8.2 l/sec for the 1 in 100 years plus climate change (40%) return period. The improvement in the proposed runoff rate compare to the existing site are between 76% to 82%.
- 3.12 Appendix E provides the Flow software results summary for the 1 in 2, 1 in 30 and 1 in 100 years (plus a 40% allowance for climate change) return period events for each of the networks. Refer to Appendix E for the surface water calculations and simulation.

**4 ENCLOSURES**

- 4.1 Appendix A includes the SuDS Hierarchy.
- 4.2 Appendix B includes a copy of the Southern Water asset search.
- 4.3 Appendix C includes a copy of the Topographical Site Survey.
- 4.4 Appendix D includes a copy of the Drainage Strategy Layouts.
- 4.5 Appendix E includes the Surface Water / SuDS calculations and simulation results.
- 4.6 Appendix F BGS Website extract
- 4.7 Appendix G includes the Draft Management & Maintenance Requirements

## APPENDIX A – SUDS HIERARCHY

Most Sustainable	SUDS technique	Flood Reduction	Pollution Reduction	Landscape & Wildlife Benefit	Included in the scheme?	Comments
	<b>Living roofs</b>	✓	✓	✓		The proposed roof finishes preclude the use of green roofs
	<b>Basins and ponds</b>	✓	✓	✓		Given the proposed layout of this site, these SuDS features are not suitable.
	<b>Filter strips and swales</b>	✓	✓	✓		Given the site density and insufficient space exists within the site for these types of SuDS features.
	<b>Infiltration devices</b>	✓	✓	✓		Due to the soil strata and possibility of shallow groundwater it is considered that the infiltration is not a viable option for the surface water drainage outfall
	<b>Permeable surfaces and infiltration blanket</b>	✓	✓		✓	Permeable Paving is proposed to be used within parking areas. This will assist in pollution reduction and the 'delay' of runoff.
Least Sustainable	<b>Tanked systems-Over size Pipes</b>	✓			✓	Crate storage is proposed to store extreme storm events and surface water runoff.



## **APPENDIX B – SOUTHERN WATER ASSET SEARCH**



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Date: 24/11/20

Scale: 1:1250

Map Centre: 558957, 146386

Data updated: 16/11/20

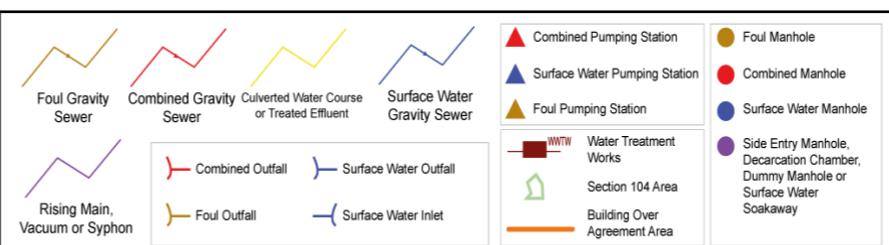
Our Ref: 462012 - 1

Wastewater Plan A3

The positions of pipes shown on this plan are believed to be correct, but Southern Water Services Ltd accept no responsibility in the event of inaccuracy. The actual positions should be determined on site. This plan is produced by Southern Water Services Ltd (c) Crown copyright and database rights 2020 Ordnance Survey 100031673 .This map is to be used for the purposes of viewing the location of Southern Water plant only. Any other uses of the map data or further copies is not permitted.

WARNING: BAC pipes are constructed of Bonded Asbestos Cement.

WARNING: Unknown (UNK) materials may include Bonded Asbestos Cement.



john.duncan@nrswa.net
Tonbridge



from  
Southern Water.

Manhole Reference	Liquid Type	Cover Level	Invert Level	Depth to Invert
0302	F	21.88	20.40	
0303	F	21.83	20.37	
0306	F	22.11	0.00	
0307	F	21.77	19.49	
0308	F	21.95	20.05	
0309	F	21.40	19.53	
030D	F	0.00	0.00	
0310	F	21.80	19.33	
0311	F	22.25	20.96	
0312	F	22.00	19.25	
031D	F	0.00	0.00	
0401	F	22.05	20.42	
0402	F	22.04	20.46	
0403	F	22.14	21.13	
0404	F	22.63	20.56	
0405	F	22.80	20.80	
0407	F	22.47	20.65	
0408	F	0.00	0.00	
040D	F	0.00	0.00	
041D	F	0.00	0.00	
042D	F	0.00	0.00	
043D	F	0.00	0.00	
1301	F	21.89	18.12	
1302	F	22.34	18.45	
1305	F	22.04	18.99	
1306	F	22.17	18.62	
1307	F	22.15	18.38	
1308	F	21.93	18.10	
1310	F	0.00	0.00	
1311	F	0.00	0.00	
1401	F	22.14	19.48	
1402	F	22.15	19.30	
1403	F	22.10	18.94	
1404	F	22.08	19.97	
1405	F	22.18	20.15	
1406	F	0.00	0.00	
1501	F	22.86	20.56	
1502	F	23.39	20.39	
1503	F	23.71	20.26	
2301	F	22.40	17.88	
8204	F	22.47	21.31	
8205	F	22.42	21.61	
820D	F	0.00	0.00	
821D	F	0.00	0.00	
822D	F	0.00	0.00	
823D	F	0.00	0.00	
9204	F	21.82	21.01	
9205	F	22.02	21.26	
9206	F	22.55	21.14	
9208	F	22.75	21.25	

Manhole Reference	Liquid Type	Cover Level	Invert Level	Depth to Invert
9209	F	23.18	21.72	
9301	F	22.56	21.51	
9302	F	22.53	0.00	
9303	F	22.36	21.68	
9304	F	22.48	21.84	
9305	F	22.37	22.08	
9306	F	22.13	0.00	
9307	F	0.00	0.00	
9308	F	0.00	0.00	
9309	F	0.00	0.00	
930D	F	0.00	0.00	
9310	F	0.00	0.00	
9311	F	0.00	0.00	
9312	F	0.00	0.00	
9313	F	0.00	0.00	
9315	F	0.00	0.00	
931D	F	0.00	0.00	
933D	F	0.00	0.00	
934D	F	0.00	0.00	
9401	F	22.82	21.38	
9402	F	22.10	20.93	
9403	F	22.41	0.00	
9404	F	0.00	0.00	
9405	F	0.00	0.00	
940D	F	0.00	0.00	
0252	S	22.54	19.39	
0253	S	22.86	0.00	
0255	S	21.71	19.61	
0352	S	0.00	0.00	
0372	S	0.00	0.00	
0373	S	0.00	0.00	
0451	S	22.18	20.18	
0452	S	22.15	20.59	
0453	S	22.22	20.72	
0455	S	22.40	0.00	
0456	S	22.80	21.20	
0457	S	0.00	0.00	
0458	S	22.30	20.30	
045D	S	0.00	0.00	
046D	S	0.00	0.00	
1350	S	0.00	0.00	
1351	S	0.00	0.00	
1352	S	0.00	0.00	
1353	S	22.19	20.04	
1354	S	22.17	19.95	
1355	S	22.07	0.00	
1356	S	0.00	20.32	
1357	S	22.21	20.12	
1358	S	21.90	20.05	
1359	S	22.03	19.89	

Manhole Reference	Liquid Type	Cover Level	Invert Level	Depth to Invert
1450	S	22.18	20.68	
1451	S	22.24	20.62	
1452	S	22.23	20.19	
8251	S	22.14	21.57	
8252	S	22.12	19.95	
8253	S	21.06	0.00	
9254	S	21.75	0.00	
9255	S	21.85	0.00	
9262	S	0.00	0.00	
9451	S	22.18	0.00	
9452	S	21.95	20.31	



## **APPENDIX C – TOPOGRAPHICAL SITE SURVEY**





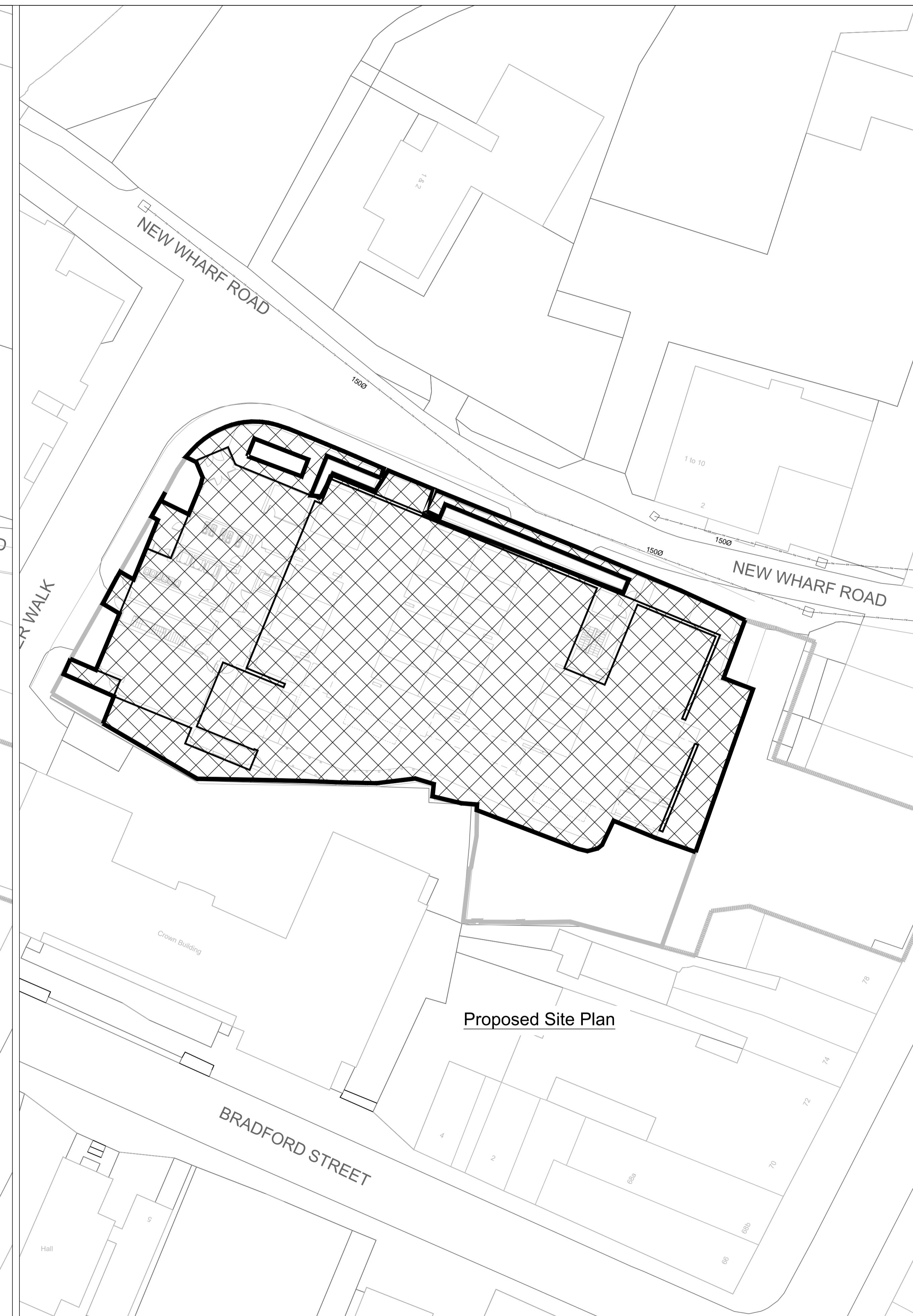


## **APPENDIX D – PROPOSED DRAINAGE STRATEGY LAYOUTS & DRAINAGE AREA PLANS**



# PRELIMINARY

## Notes



## Key

	Existing Impermeable Area Approximately-2010m²
	Proposed Impermeable Area Approximately-1720m²

A Proposed Impermeable area revised 12.05.21  
- First Issue 14.04.21  
Rev Description Date

Status:

## Stage 3

	Scale : 1:200@A1		
Date :	Dec 20	Checked:	Approved:
Drawn :	IDL	BM	PT

## Drainage Areas

Project :  
76-78 High Street, Tonbridge, Surrey

Drg. No: SE-2739-03-DE-100 Rev: File Ref: 1070-07-100.dwg  
A Plot Ref: SE-2739-03-DE-100

33 The Point  
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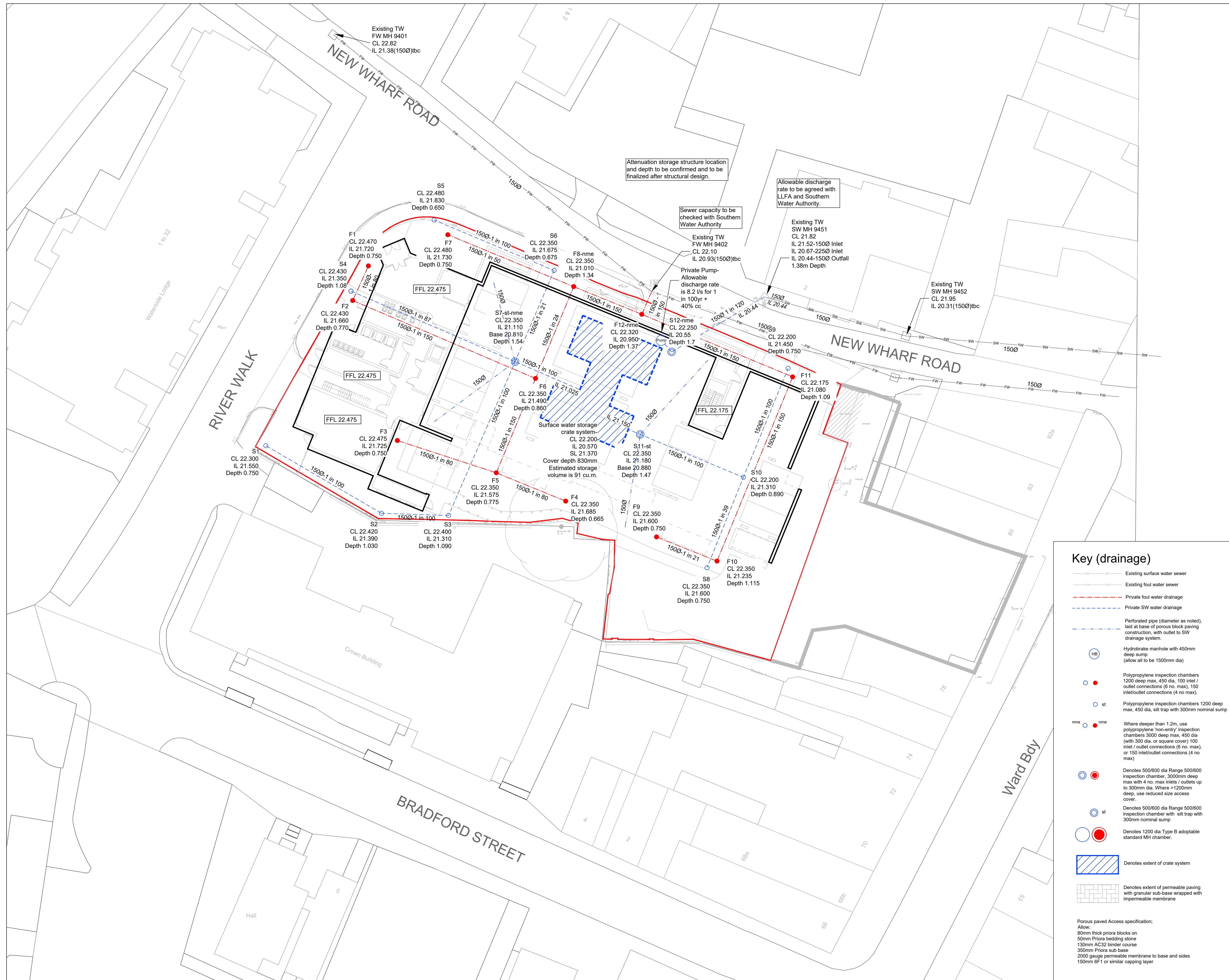
INFRASTRUCTURE DESIGN LIMITED

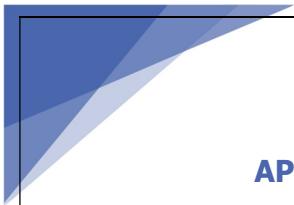
working for

**McCARTHY STONE**  
*life, well lived*

# PRELIMINARY

## Notes





## **APPENDIX E – SURFACE WATER DRAINAGE CALCULATIONS**

### Design Settings

Rainfall Methodology	FEH-13	Minimum Velocity (m/s)	1.00
Return Period (years)	100	Connection Type	Level Soffits
Additional Flow (%)	0	Minimum Backdrop Height (m)	0.200
CV	0.750	Preferred Cover Depth (m)	1.200
Time of Entry (mins)	4.00	Include Intermediate Ground	✓
Maximum Time of Concentration (mins)	30.00	Enforce best practice design rules	✓
Maximum Rainfall (mm/hr)	50.0		

### Nodes

Name	Area (ha)	Cover Level (m)	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
Crate	0.172	22.640	1500	558937.166	146405.239	2.070

### Simulation Settings

Rainfall Methodology	FEH-13	Skip Steady State	x	2 year (l/s)	1.1
Summer CV	0.750	Drain Down Time (mins)	240	30 year (l/s)	2.9
Winter CV	0.840	Additional Storage (m³/ha)	20.0	100 year (l/s)	3.9
Analysis Speed	Normal	Check Discharge Rate(s)	✓	Check Discharge Volume	x

### Storm Durations

15	60	180	360	600	960	2160	4320	7200	10080
30	120	240	480	720	1440	2880	5760	8640	

Return Period (years)	Climate Change (CC %)	Additional Area (A %)	Additional Flow (Q %)
2	0	0	0
30	0	0	0
100	0	0	0
100	40	0	0

### Pre-development Discharge Rate

Site Makeup	Greenfield	Growth Factor 30 year	1.95
Greenfield Method	IH124	Growth Factor 100 year	2.48
Positively Drained Area (ha)	0.201	Betterment (%)	0
SAAR (mm)	675	QBar	1.2
Soil Index	5	Q 1 year (l/s)	
SPR	0.53	Q 30 year (l/s)	
Region	6	Q 100 year (l/s)	
Growth Factor 1 year	0.85		

### Node Crate Online Pump Control

Flap Valve	x	Design Depth (m)	1.600	Switch off depth (m)	0.100
Replaces Downstream Link	✓	Design Flow (l/s)	14.3		
Invert Level (m)	20.570	Switch on depth (m)	0.101		

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.500	5.000	0.700	8.000	2.000	11.000

**Node Crate Carpark Storage Structure**

Base Inf Coefficient (m/hr)	0.00000	Invert Level (m)	20.570	Slope (1:X)	500.0
Side Inf Coefficient (m/hr)	0.00000	Time to half empty (mins)	148	Depth (m)	0.800
Safety Factor	2.0	Width (m)	10.000	Inf Depth (m)	
Porosity	0.95	Length (m)	11.300		

**Other (defaults)**

Entry Loss (manhole)	0.250	Entry Loss (junction)	0.000	Apply Recommended Losses	x
Exit Loss (manhole)	0.250	Exit Loss (junction)	0.000	Flood Risk (m)	0.300

Results for 2 year Critical Storm Duration. Lowest mass balance: 100.00%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
240 minute winter	Crate	172	20.779	0.209	5.9	21.8696	0.0000	OK
<hr/>								
<hr/>								
Link Event (Outflow)	US Node	Link Pump	Outflow (l/s)	Discharge Vol (m³)				
240 minute winter	Crate	Pump	2.1	23.7				

**Results for 30 year Critical Storm Duration. Lowest mass balance: 100.00%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
180 minute winter	Crate	136	21.024	0.454	16.7	49.0132	0.0000	OK
<b>Link Event</b>								
<b>(Outflow)</b>								
180 minute winter	Crate	Pump			4.5		59.7	
<b>Discharge</b>								
<b>(l/s)</b>								
<b>Vol (m³)</b>								

**Results for 100 year Critical Storm Duration. Lowest mass balance: 100.00%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
180 minute winter	Crate	132	21.146	0.576	21.5	62.5267	0.0000	OK
<hr/>								
<hr/>								
Link Event (Outflow)	US Node	Link Pump	Outflow (l/s)	Discharge Vol (m³)				
180 minute winter	Crate	Pump	6.1	77.1				

**Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 100.00%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
180 minute winter	Crate	136	21.363	0.793	30.1	86.6493	0.0000	OK
<b>Link Event</b>								
<b>(Outflow)</b>								
180 minute winter	Crate	Pump			8.2		108.5	Discharge Vol (m³)

## ❖ RAINFALL MODELLING FOR POINT DATA AT 558917,146410

FEH 2013

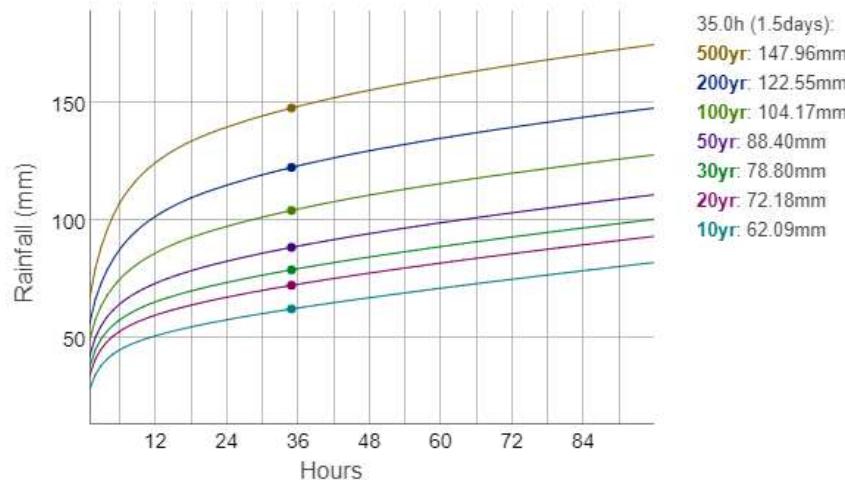
Point rainfall at 558917, 146410

Design Rainfall  Event Rarity

Duration  Hours

Return period  Years

Depth  mm



A design rainfall of 13.1 mm was calculated.

This design rainfall has been calculated for a return period on the annual maximum scale.

Return period options

- Annual maximum  
 Peaks over threshold

Duration options

- Fixed  
 Sliding

## ❖ RAINFALL MODELLING FOR POINT DATA AT 558917,146410

FEH 2013

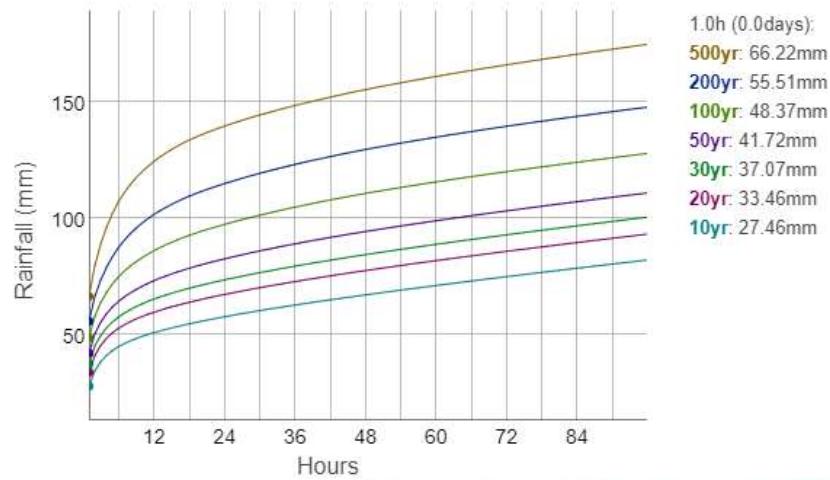
Point rainfall at 558917, 146410

Design Rainfall  Event Rarity

Duration

Return period

Depth  mm



A design rainfall of 37.07 mm was calculated.

This design rainfall has been calculated for a return period on the annual maximum scale.

Return period options

- Annual maximum
- Peaks over threshold

Duration options

- Fixed
- Sliding

## ❖ RAINFALL MODELLING FOR POINT DATA AT 558917,146410

FEH 2013

Point rainfall at 558917, 146410

Design Rainfall  Event Rarity

Duration

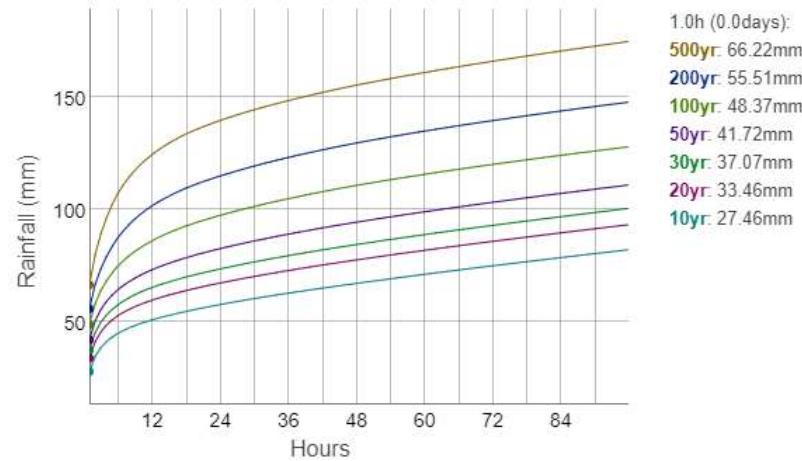
1

Return period

100

Depth

48.37 mm



A design rainfall of 48.37 mm was calculated.

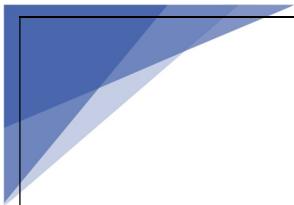
This design rainfall has been calculated for a return period on the annual maximum scale.

Return period options

- Annual maximum  
 Peaks over threshold

Duration options

- Fixed  
 Sliding



## **APPENDIX F – BGS WEBSITE EXTRACT**

# Geology of Britain viewer (classic)



More BGS map viewers

Try the 3D version of the Geology of Britain viewer

Surface

Geology

3D

Models

Borehole

Scans

Earthquake

Timeline

## Surface Geology

Superficial only

Bedrock only

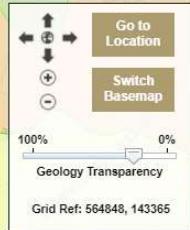
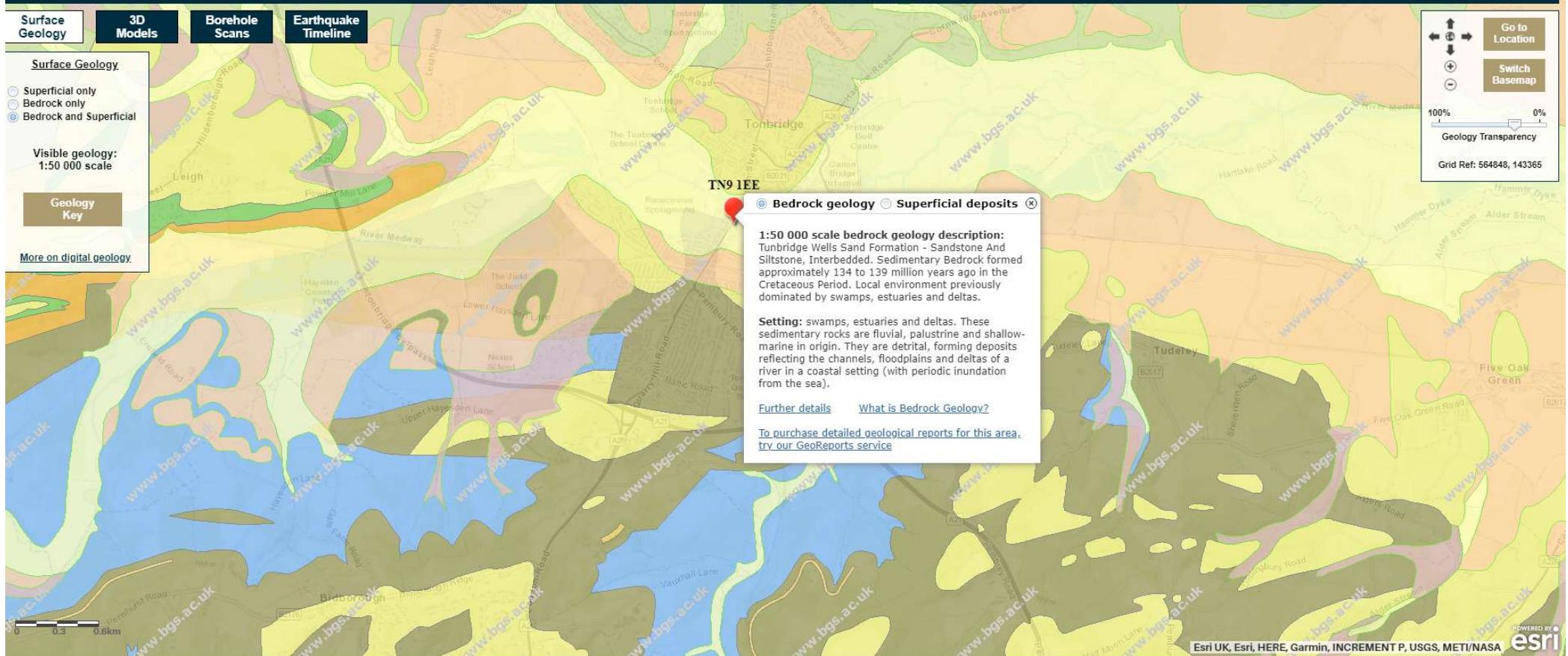
Bedrock and Superficial

Visible geology:  
1:50 000 scale

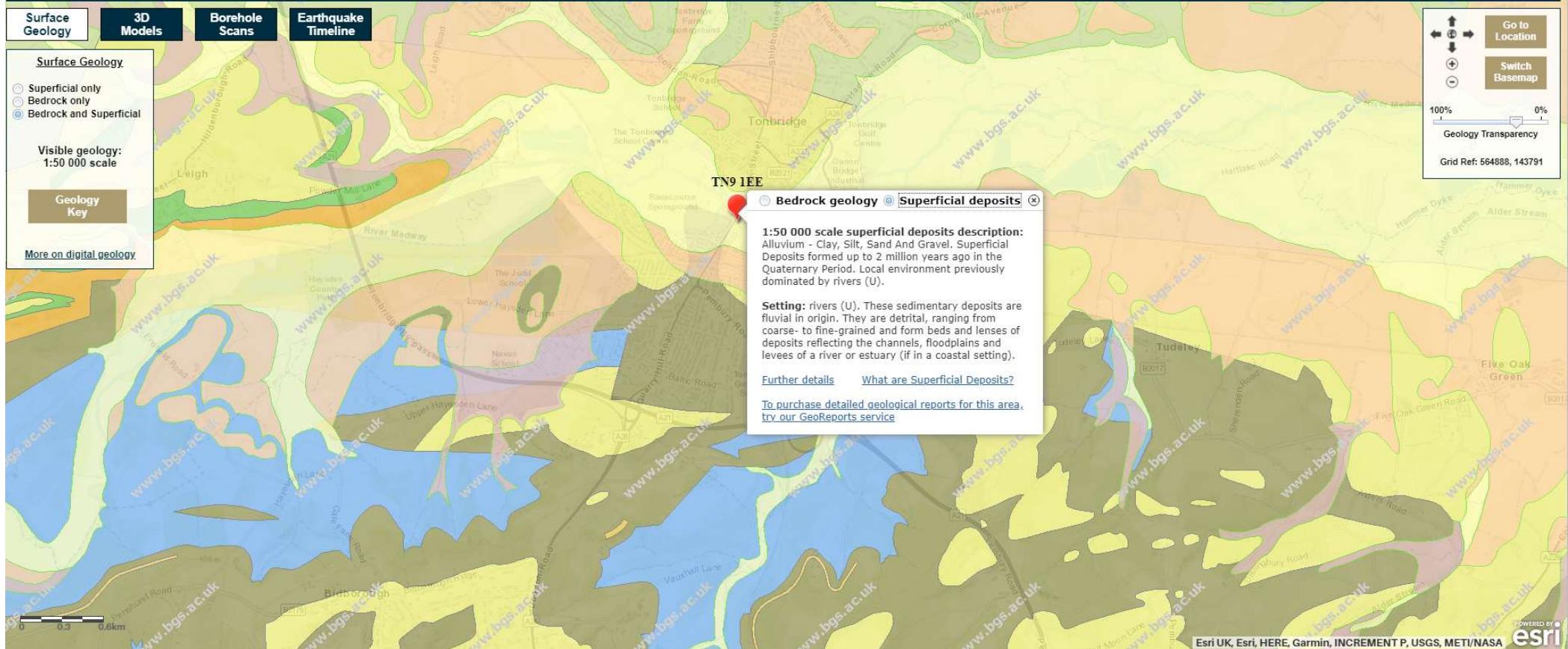
## Geology

Key

More on digital geology



## Geology of Britain viewer (classic)



## **APPENDIX G – MANAGEMENT & MAINTENANCE REGIME**

### **The Management Company**

The responsibility for maintenance of all elements of the development remain with the developers until handed over to the Management Company.

Handover of external works to the Management Company coincides with completion of the final residential unit.

The Management Company employs a specialist Managing Agent to manage the development which includes all aspects of maintenance.

*The Management Company BI registered No. 'tbc' was incorporated in 'tbc' and its directors are currently made up of developers representatives plus an appointment from the Managing Agent.*

*The Managing Agents are 'tbc' who have over 'tbc' years' experience in the industry.*

At handover the Management Company and Managing Agent receive as built information together with operating and maintenance manuals which detail all maintenance protocols.

Approximately 1 year following completion of the final unit the residents will be invited to elect members to become directors of the Management Company, the developer appointed directors at that time resign from the Management Company to be replaced by the elected representatives of the residents.

To ensure continuity and a full understanding of the development and the operation and maintenance of its various components the representative of the Managing Agent remains as a director of the Management Company and the appointment of the Managing Agents is fixed for a minimum period of two years following the date of resignation of the last developer's director.

After that two year period the Management Company have the right to re-tender the Managing Agent services but it is very rare that a change is made as our original appointments provide an excellent service.

Within the first two years from the final unit completion on the development the residents have two ways in which they can report any defects and problems which would include flooding and that is either to our Aftersales department or to the Managing Agents, the residents are issued with telephone numbers for both which include out of hours emergency response.

After two years our Aftersales contacts are normally replaced by members of the Management Company. The residents therefore have the ability to contact them or the Managing Agents which then remains through the life of the development.

## **Crate Attenuation**

The principle means of surface water attenuation/disposal from the development is by way of cellular storage.

The Management Company will ensure that the following measures are undertaken to ensure the longevity of the surface water drainage system;

Inspections to identify any areas not operating correctly, pollution, blocked inlets or outlets, standing water etc.

Collect and remove from site all extraneous rubbish that is detrimental to the operation or detract from the appearance of the site, including paper, bottles, cans and similar debris.

## **Onsite Surface Water Drainage System (generally)**

The Management Company will be responsible for maintaining those private sewers that reside outside of a Freeholders responsibility, are not located within the adopted highway or not otherwise covered under the Section 38/104 Agreements.

The following measures are to be undertaken to ensure the longevity of the surface water drainage system;

**Every 6 months:** Remove silt build up from *all* catchpits and road gullies. Leaf guards should be installed to the rainwater gutters and it should be checked and cleared at the same time with other drainage inspection.

**Annually:** elect approx. 20% of the development's surface water inspection chambers (situated in accessible non-private areas) and inspect for blockages / silt build up. Remove silt and debris. Rotate on a 5 yearly cycle to cover all such chambers over this period.

### **Every 2-5 years (depending on the outcome of aforementioned inspections)**

Commission a CCTV survey and report on condition of the surface water drainage system, check for structural integrity and hydraulic fluidity. Carry out promptly any remedial work as advised by CCTV company.

## **Private surface water Pump Chambers**

Flow control chambers are to be maintained by a Management Company. Their maintenance regime shall be as follows:

Following installation of the Flow Controls any extraneous material i.e. Building materials are removed from the unit and the chamber. After the system is made live, the unit is to be inspected monthly for three months and thereafter at six monthly intervals with hose down if required.

The chambers are to be cleared checked for structural integrity at the six monthly interval. Any damage/problems should be made good as per the original design drawings.

## **Permeable Paving**

External parking areas and access roads are to be constructed in permeable block paving in order to;

- a) Delay the surface water runoff from these areas, and
- b) Enhance the quality of the rainwater prior to discharge into the receiving sewer.

The Management Company will ensure that the following measures are undertaken to ensure the longevity of the pervious pavement;

### **Quarterly**

- i) Inspect the pervious pavement for signs of ponding and ensure there is no migration of soils from adjacent landscaped areas or other deleterious material that may prematurely clog up the jointing stone situated in the gaps between the blocks. Ideally this type of inspection should be undertaken immediately following a heavy rainfall event.
- ii) Commission vacuum sweeping and brushing of the pervious pavement to ensure joints are kept free of silt. Minimum 3 sweeping per year, thus;
  - a) End of Winter (April) – to collect winter debris
  - b) Mid-Summer (July/August) – to collect dust, flower and grass-type deposits.
  - c) After Autumn leaf fall (November)

The company commissioned to carry out this work should ensure that their vacuum equipment is adjusted accordingly to avoid removal of jointing material.

Any lost material should be replaced promptly to avoid the blocks from being dislodged.

### **Last Resort Remedial Action**

- i) Should a portion of the pervious pavement become substantially impervious due to excessive siltation, the following procedure should be followed;
  - a) Lift block paving and laying course
  - b) Break out underlying bitmac base layer and replace with similar compacted depth of coarse aggregate subbase material to BS EN 13242:2002 Type 4/20, wrapped in geotextile as Terram 1000 or similar.
  - c) Renew laying course, replace blocks and renew jointing material

NB. Material removed from the voids or the layers below the surface may contain heavy metals and hydrocarbons and as such may need to be disposed of as 'controlled waste'. Sediment testing should be carried out before disposal to confirm its classification and appropriate disposal methods.