PROPOSED RESIDENTIAL DEVELOPMENT

GLEN GARAGE

GLEN ROAD

YORK

YO31 7XZ

DRAINAGE STRATEGY REPORT

24/07/2018

1. INTRODUCTION

This report provides an assessment of the proposed drainage for this development site. It considers the disposal of foul and surface water from the development and provides outline information about how the development can be drained successfully.

2. LOCATION AND SITE

The site is adjacent to Glen Road and Hawthorn Grove, York. An aerial view of the site is shown below.



LOCATION PLAN

A topographical survey has been undertaken for the development site. The topographical survey shows that the site is level with levels varying from about 13.50 to 13.60m AOD.

The pre-development site is wholly impermeable and consists of a garage building and canopy over a concrete external hard-standing area.



The garage, canopy and concrete hard-standings under the canopy are all positively drained and assumed that they all connect with the local sewer network.

Photographs showing the site are shown below.



PRE-DEVELOPMENT SITE PHOTOGRAPH

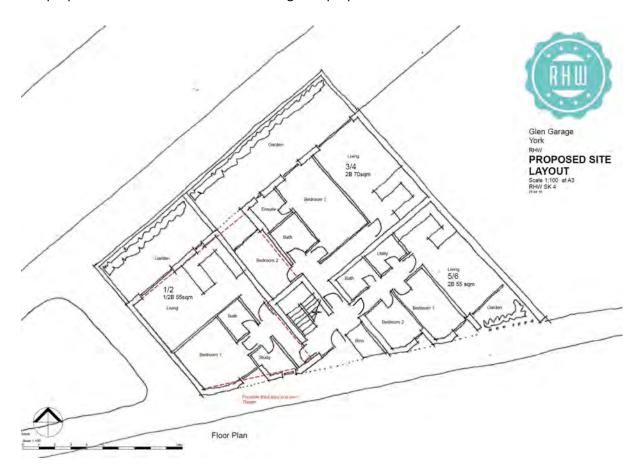


PRE-DEVELOPMENT SITE PHOTOGRAPHS



3. PROPOSALS

The proposals are for new residential building. The proposals are shown below.



PROPOSALS PLAN

The development will use the whole of the site, as per the existing site, but some areas will be garden and so reduce impermeable areas overall and so reduce surface water flows to sewer.

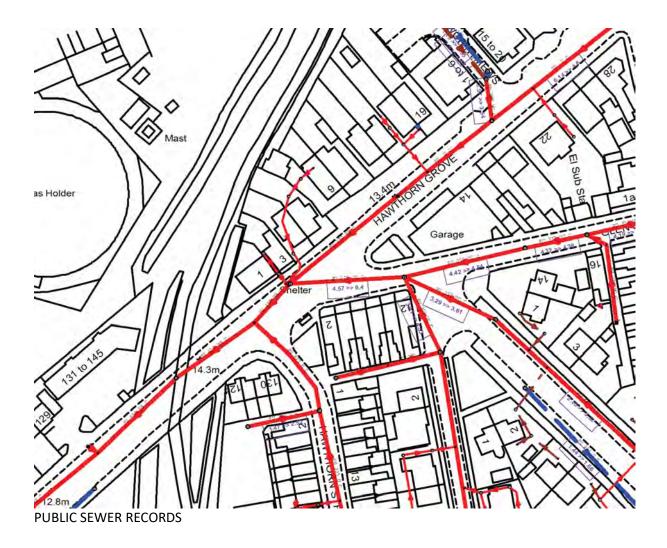
4. PUBLIC SEWER RECORDS

The local public sewer records have been obtained and these are shown below.

A public combined sewer is present within Hawthorne Road and Glen Road adjacent to the development.

No surface water sewers are available on or close to the development site.





No detailed drainage survey has been undertaken. However, it is likely that the whole of the pre-development site drains to the public sewer.

5. FOUL SEWERAGE

Foul sewers from the development will be connected to the combined public sewer within Hawthorne Grove or Glen Road. Preferably using an existing connection on site.

A separate system of foul drainage will be provided on site.

6. SURFACE WATER ASSESSMENT

The surface water from this development should be disposed of through one or more of the following, in this order of priority.

- Discharge to the ground (infiltration).
- Discharge to a surface water body.



- Discharge to a surface water sewer, highway drain or other drain.
- Discharge to a combined sewer.

There is no available space for infiltration on the proposed development. The development is small, urban and so the correct drainage methodology will be to mimic the existing drainage system and discharge flows to the existing public sewers.

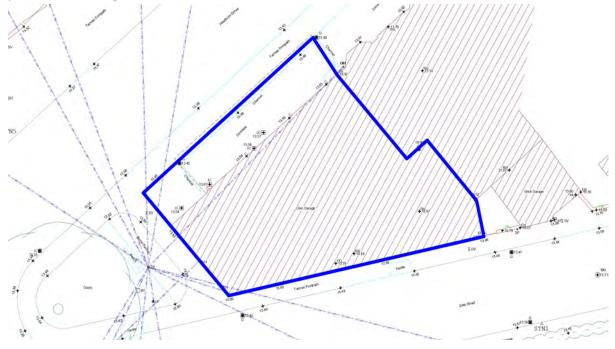
There are no watercourses available on or close to this site.

The existing surface water from the development is discharged to the public sewer network. From site inspection, the roofs and canopy are drained positively through gutters and rainwater pipes and the concrete hard-standing area below the canopy has a drainage channel and gully. Therefore, the post-development surface water drainage will mimic the pre-development site and have an outfall to sewer.

PRE-DEVELOPMENT DISCHARGE TO SEWER

The development site is 318 sq m. The 1 in 1 year discharge rate for this area, taken as 140l/s/hectare is $140 \times 0.0318 = 4.45 l/s$.

For the re-development, the discharge rate to sewer should be reduced by a minimum of 30% and so the post-development discharge rate for all storm events, up to the 1 in 100 year plus climate change storm event should be limited to 4.45l/s minus 30% = 3.1l/s.



PRE-DEVELOPMENT IMPERMEABLE AREAS



POST-DEVELOPMENT DISCHARGE TO SEWER

The post development site will be building with an impermeable area of 255 sq m; and garden areas for the remainder of the site.

To limit flows to 3.1l/s, surface water storage will be required on the proposed surface water drainage system. The Microdrainage program has been used to determine the size of the storage system required, using the following criteria:-

Impermeable area of post-development site = 255 sq m (0.026hectares).

Discharge rate 3.1l/s

Return Period: 1 in 100 year storm event. Climate Change: + 20% added to rainfall.

M5-60 = 19mm

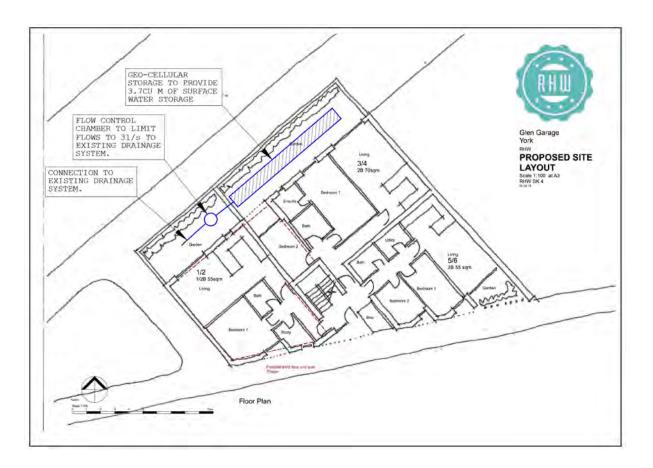
R = 0.400

The Microdrainage calculations are at the rear of this report and show that a surface water storage system constructed from cellular storage blocks and providing 3.7 cu m will be satisfactory for this development.

This could be located under the garden area to the front of the development facing Hawthorn Grove. Existing drainage chambers exist within this area and so likely that existing drainage exists within this area for connection of flows from the development.

A sketch of the location and size of the surface water attenuation features are shown below.



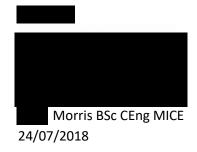


PRELIMINARY SURFACE WATER DRAINAGE DESIGN

7. CONCLUSIONS

- This development site can be drained successfully.
- Foul water and surface water will have separate systems on site.
- Foul water flows will be connected to the public combined sewer, preferably via on site existing drainage.
- Surface water from the development will be disposed of by connection to the combined sewer on site at restricted flow of 3.1l/s.
- Surface water storage (3.7 Cu m) will be supplied by cellular storage under the garden area proposed on the development.
- The surface water storage will cater for all storms up to 1 in 100 year plus 20% climate change.





APPENDIX

MICRODRAINAGE STORAGE CALCULATIONS
 1 in 100 year plus 20% climate change



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Micro Drainage	Source Control 2018.1	

Summary of Results for 100 year Return Period (+20%)

Half Drain Time : 10 minutes.

	Storm Event		Max Level (m)	Max Depth (m)	Max Infiltration (1/s)	Max Control (1/s)	Σ	Max Outflow (1/s)	Max Volume (m³)	Status
15	min	Summer	13.018	0.318	0.0	3.1		3.1	3.0	ОК
30	min	Summer	13.035	0.335	0.0	3.1		3.1	3.2	ОК
60	min	Summer	12.995	0.295	0.0	3.1		3.1	2.8	ОК
120	min	Summer	12.866	0.166	0.0	3.1		3.1	1.6	OK
180	min	Summer	12.772	0.072	0.0	3.1		3.1	0.7	OK
240	min	Summer	12.721	0.021	0.0	3.0		3.0	0.2	OK
360	min	Summer	12.700	0.000	0.0	2.5		2.5	0.0	OK
480	min	Summer	12.700	0.000	0.0	2.0		2.0	0.0	ОК
600	min	Summer	12.700	0.000	0.0	1.7		1.7	0.0	OK
720	min	Summer	12.700	0.000	0.0	1.5		1.5	0.0	O K
960	min	Summer	12.700	0.000	0.0	1.2		1.2	0.0	ОК
1440	min	Summer	12.700	0.000	0.0	0.8		0.8	0.0	O K
2160	min	Summer	12.700	0.000	0.0	0.6		0.6	0.0	OK
2880	min	Summer	12.700	0.000	0.0	0.5		0.5	0.0	OK
4320	min	Summer	12.700	0.000	0.0	0.3		0.3	0.0	OK
5760	min	Summer	12.700	0.000	0.0	0.3		0.3	0.0	OK
7200	min	Summer	12.700	0.000	0.0	0.2		0.2	0.0	OK
8640	min	Summer	12.700	0.000	0.0	0.2		0.2	0.0	O K
10080	min	Summer	12.700	0.000	0.0	0.2		0.2	0.0	O K
15	min	Winter	13.079	0.379	0.0	3.1		3.1	3.6	ОК

	stor	m	Rain	Flooded	Discharge	Time-Peak	
	Even	t	(mm/hr)	Volume	Volume	(mins)	
				(m³)	(m³)		
15	min	Summer	111.940	0.0	5.4	14	
30	min	Summer	73.565	0.0	7.1	23	
60	min	Summer	46.096	0.0	8.8	40	
120	min	Summer	27.939	0.0	10.8	72	
180	min	Summer	20.582	0.0	12.0	100	
240	min	Summer	16.478	0.0	12.8	128	
360	min	Summer	11.961	0.0	14.0	0	
480	min	Summer	9.535	0.0	14.9	0	
600	min	Summer	7.993	0.0	15.6	0	
720	min	Summer	6.916	0.0	16.2	0	
960	min	Summer	5.501	0.0	17.2	0	
1440	min	Summer	3.977	0.0	18.6	0	
2160	min	Summer	2.871	0.0	20.2	0	
2880	min	Summer	2.276	0.0	21.3	0	
4320	min	Summer	1.639	0.0	23.0	0	
5760	min	Summer	1.296	0.0	24.3	0	
7200	min	Summer	1.081	0.0	25.3	0	
8640	min	Summer	0.931	0.0	26.1	0	
0080	min	Summer	0.820	0.0	26.9	0	
15	min	Winter	111.940	0.0	6.2	15	



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Summary of Results for 100 year Return Period (+20%)

	stor	m	Max	Max	Max	Max	Max	Max	Status	
	Even	t	Level	Depth	Infiltration	Control	Σ Outflow	Volume		
			(m)	(m)	(1/s)	(1/s)	(1/s)	(m³)		
30	min	Winter	13.089	0.389	0.0	3.1	3.1	3.7	ОК	
60	min	Winter	13.020	0.320	0.0	3.1	3.1	3.0	OK	
120	min	Winter	12.815	0.115	0.0	3.1	3.1	1.1	OK	
180	min	Winter	12.711	0.011	0.0	3.0	3.0	0.1	O K	
240	min	Winter	12.700	0.000	0.0	2.5	2.5	0.0	O K	
360	min	Winter	12.700	0.000	0.0	1.8	1.8	0.0	OK	
480	min	Winter	12.700	0.000	0.0	1.5	1.5	0.0	O K	
600	min	Winter	12.700	0.000	0.0	1.2	1.2	0.0	OK	
720	min	Winter	12.700	0.000	0.0	1.1	1.1	0.0	OK	
960	min	Winter	12.700	0.000	0.0	0.8	0.8	0.0	OK	
1440	min	Winter	12.700	0.000	0.0	0.6	0.6	0.0	OK	
2160	min	Winter	12.700	0.000	0.0	0.4	0.4	0.0	OK	
2880	min	Winter	12.700	0.000	0.0	0.3	0.3	0.0	OK	
4320	min	Winter	12.700	0.000	0.0	0.3	0.3	0.0	O K	
5760	min	Winter	12.700	0.000	0.0	0.2	0.2	0.0	OK	
7200	min	Winter	12.700	0.000	0.0	0.2	0.2	0.0	OK	
8640	min	Winter	12.700	0.000	0.0	0.1	0.1	0.0	O K	
08001	min	Winter	12.700	0.000	0.0	0.1	0.1	0.0	O K	

Storm		Rain	Flooded	Discharge	Time-Peak	
	Even	t	(mm/hr)	Volume	Volume	(mins)
				(m³)	(m³)	
30	min	Winter	73.565	0.0	8.0	25
60	min	Winter	46.096	0.0	9.9	44
120	min	Winter	27.939	0.0	12.2	74
180	min	Winter	20.582	0.0	13.5	98
240	min	Winter	16.478	0.0	14.4	0
360	min	Winter	11.961	0.0	15.7	0
480	min	Winter	9.535	0.0	16.7	0
600	min	Winter	7.993	0.0	17.5	
720	min	Winter	6.916	0.0	18.1	0
960	min	Winter	5.501	0.0	19.2	0
1440	min	Winter	3.977	0.0	20.8	0
2160	min	Winter	2.871	0.0	22.6	0
2880	min	Winter	2.276	0.0	23.9	0
4320	min	Winter	1.639	0.0	25.8	0
5760	min	Winter	1.296	0.0	27.2	0
7200	min	Winter	1.081	0.0	28.3	0
8640	min	Winter	0.931	0.0	29.3	0
10080	min	Winter	0.820	0.0	30.1	0



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Rainfall Details

Rainfall Model FSR Winter Storms Yes
Return Period (years) 100 Cv (Summer) 0.750
Region England and Wales Cv (Winter) 0.840
M5-60 (mm) 19.000 Shortest Storm (mins) 15
Ratio R 0.400 Longest Storm (mins) 10080
Summer Storms Yes Climate Change % +20

Time Area Diagram

Total Area (ha) 0.026

Time (mins) Area From: To: (ha)

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Micro Drainage	Source Control 2018 1	1

Model Details

Storage is Online Cover Level (m) 13.500

Cellular Storage Structure

Invert Level (m) 12.700 Safety Factor 2.0 Infiltration Coefficient Base (m/hr) 0.00000 Porosity 0.95 Infiltration Coefficient Side (m/hr) 0.00000

Depth	(m)	Area	(m ²)	Inf.	Area	(m ²)	Depth	(m)	Area	(m²)	Inf.	Area	(m²)
0.	000		10.0			10.0	0.	401		0.0			15.1
0.	400		10.0			15.1	7						

Hydro-Brake® Optimum Outflow Control

Unit Reference MD-SHE-0090-3100-0550-3100 Design Head (m) 0.550 Design Flow (1/s) Flush-Florm Calculated Objective Minimise upstream storage Application Surface Sump Available Yes Diameter (mm) 90 Invert Level (m) 12.600 Minimum Outlet Pipe Diameter (mm) 150 Suggested Manhole Diameter (mm) 1200

Control	Points	Head (m)	Flow (1/s)
Design Point	(Calculated)	0.550	3,1
	Flush-Florm	0.168	3.1
	Kick-Flo®	0.383	2.6
Mean Flow ove	r Head Range	-	2.6

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (1/s)	Depth (m) Flo	w (1/s)	Depth (m)	Flow (1/s)	Depth (m)	Flow (1/s)
0.100	2.8	1.200	4.4	3.000	6.8	7.000	10.2
0.200	3.1	1.400	4.8	3.500	7.3	7.500	10.6
0.300	3.0	1.600	5.1	4.000	7.8	8.000	10.9
0.400	2.7	1.800	5.4	4.500	8.3	8.500	11.3
0.500	3.0	2.000	5.6	5.000	8.7	9.000	11.6
0.600	3.2	2.200	5.9	5.500	9.1	9.500	11.9
0.800	3.7	2.400	6.1	6.000	9.5		
1.000	4.1	2.600	6.4	6.500	9.8		

