

### **Robin Beattie**

**Project Name:** Beattie CO10 7PW **Address:** 17 CHEQUERS LANE, GLEMSFORD, CO10 7PW

Date Created: 17th February 2022

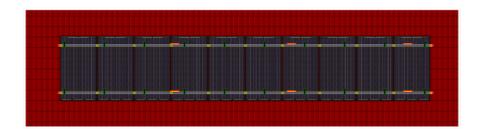
Designer: Joe Pilgrim



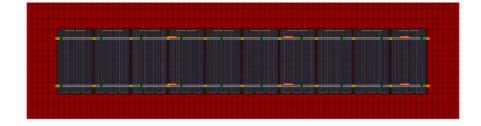
## **Roof Layout**

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Roof 1



### Roof 2





### Structural calculations

### Weight loading calculations

#### Roof 1

For a traditional cut roof with rafters and purlins we recommend also using our rafter calculator to check the load-bearing capacity of the rafters. Even if the increase in loading is more than 15% the rafters may well be able to take the additional weight.

Please note that this method does not calculate the strength of the roof, and if a roof was badly constructed, does not meet existing building regulations, or is in poor condition then it may still not be appropriate to install an array.

Dead load from roof covering	0.44 kN/m <sup>2</sup>
Imposed load	0.75 kN/m <sup>2</sup>
Total loading without solar array	1.19 kN/m <sup>2</sup>
Weight of solar panels and mounting	231.2 kg
Area covered by solar array	19 m <sup>2</sup>
Loading imposed by solar array	0.12 kN/m <sup>2</sup>
Total loading with solar array	1.3 kN/m <sup>2</sup>

### Increase in loading due to solar array: 10.1%

An increase of less than 15% in the load imposed on a roof is not considered to be a significant change (The Building Regulations 2000, Approved Document A).



#### Roof 2

Total loading with solar array	1.3 kN/m <sup>2</sup>
Loading imposed by solar array	0.12 kN/m <sup>2</sup>
Area covered by solar array	19 m <sup>2</sup>
Weight of solar panels and mounting	231.2 kg
Total loading without solar array	1.19 kN/m <sup>2</sup>
	4 40 4 44 2
Imposed load	0.75 kN/m <sup>2</sup>
Dead load from roof covering	0.44 kN/m <sup>2</sup>

# Increase in loading due to solar array: 10.1%

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### Wind loading calculations

The maximum force acting on a solar array from wind loading is given by the following formula in BRE Digest 489:

### $F = q_p \times C_{p net} \times C_a \times C_t \times A_{ref}$

Deef	1
ROOT	т

Pressure	14460N	15906N
Uplift	-18798N	-31813N
	Roof Centre	Roof edge
f		18.95m <sup>2</sup>
When there is no significant topography		
		1
At an altitude of 12m		
		1
Pressure	1	1.1
Uplift	-1.3	-2.2
net	Roof Centre	Roof edge
		763 Pa
	From Fig 34 in Guide to the Installation of Photovoltaic System windzone 1, in urban terrain, at a distance of greater than 20 net Uplift Pressure At an altitude of 12m When there is no significant topography ef Uplift	From Fig 34 in Guide to the Installation of Photovoltaic Systems for a building windzone 1, in urban terrain, at a distance of greater than 20km from the set net of the presence of the set of the se

With 20 roof hooks we should allow for an uplift force per hook in the central zone of **940N**, rising to **1591N** at the edges. If 2 screws are used per roof hook, this equates to **470N**per fixing in the central zone, and **795N** at the edges.

Pan tile roof hooks are fixed with screws that pass through the 5mm plate of the roof hook and are then buried fully into the rafter beneath. So there is approximately 75 mm of thread in the timber. The pull-out force in C16 timber is given by tables and formulae in BS5268 Part 2:

### 17.3 × 1.25 × 75 = **1622N**

The pullout force on the fixings is less than the expected wind loading, even when the fixings are close to the edge of the roof.

#### Roof 2

Qp		763 F
	n of Photovoltaic Systems for a building stance of greater than 20km from the sea	
C <sub>p net</sub>	Roof Centre	Roof ed
Uplift	-1.3	-2
Pressure	1	1
C <sub>a</sub>		
At an altitude of 12m		
C <sub>t</sub>		
When there is no significant topograp	hy	
A <sub>ref</sub>		18.95m
F	Roof Centre	Roof ed
Uplift	-18798N	-31813
Pressure	14460N	15906

With 20 roof hooks we should allow for an uplift force per hook in the central zone of 940N, rising to 1591N at the edges. If 2 screws are used per roof hook, this equates to 470Nper fixing in the central zone, and **795N** at the edges.

Pan tile roof hooks are fixed with screws that pass through the 5mm plate of the roof hook and are then buried fully into the rafter beneath. So there is approximately 75 mm of thread in the timber. The pull-out force in C16 timber is given by tables and formulae in BS5268 Part 2:

### 17.3 x 1.25 x 75 = **1622N**

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