

**Euro Garages Ltd: High Street, Shirley, Solihull**

**Drainage Strategy Report**


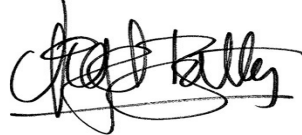
**Client: Euro Garages Ltd**

**Date: 14<sup>th</sup> December 2021**

**Project No: P15588**

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Project Number: PI5588		Signature	Date
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Revision:		Signature	Date
Prepared by:			
Checked by:			
Revision Notes:			

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## 1.0 Introduction

Goodson Associates have been appointed by Euro Garages Ltd to prepare a Drainage Strategy for the proposed commercial re-development of the existing Esso EG Solihull Lodge Garage site at High Street, Shirley, Solihull. The purpose of this report is to describe in principle the design approach for the foul and surface water drainage systems for the development.

## 2.0 Existing Site

### 2.1 General Description

The proposed site is located off High Street in Shirley (Grid Ref: 409631, 278682). Figure 1.0 shows an aerial photograph of the area with the approximate site boundary highlighted in red.

The site is generally bounded by public highway to the north, east and south, with residential properties and associated gardens abutting the western boundary.

### 2.2 Site Topography

As Figure 1.0 shows, the area is a brownfield site which is currently occupied by the operating Esso petrol filling station. The site is of irregular shape and is approximately 0.09 ha in area.

The site falls in an easterly direction with levels ranging from +144.86 AOD on the western boundary to +143.96 AOD on the eastern boundary.



Figure 1.0 - Aerial Photograph showing the approximate site boundary

### 2.3 Existing Natural Drainage Features

There are no natural water courses running through or in close proximity to the site, with the nearest watercourse being the Stratford-upon-Avon Canal located at around 200m to the northeast and beyond that the closest natural watercourse is the River Cole located around 700m to the east.

### 2.4 Existing Drainage Infrastructure

Severn Trent records show that there are foul and surface water public sewers in close proximity to the site. An extract of this information is provided in Figure 2 below and a full copy included in the Section 6 appendices.

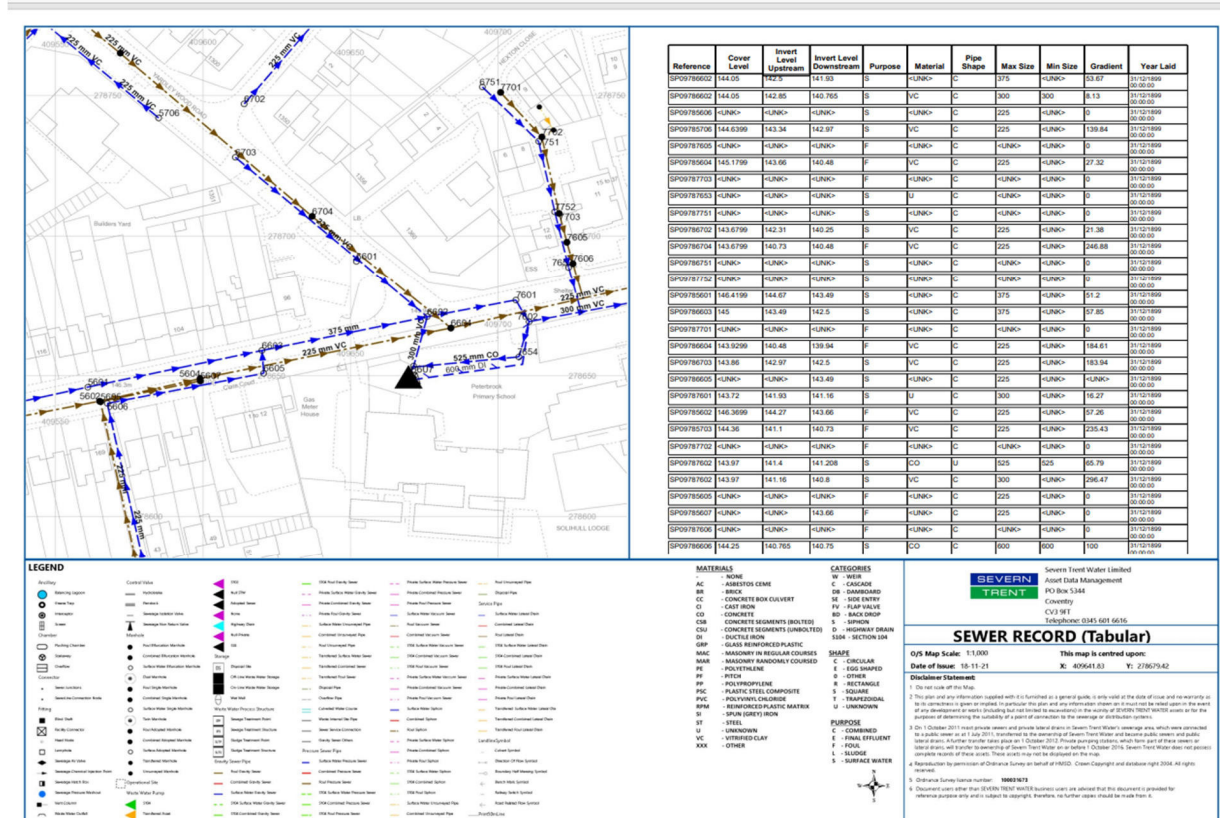


Figure 2.0 – Severn Trent Sewer Record Plan - extract

It is proposed to connect to the existing 375mm diameter surface water sewer located within the High Street to the south of site. Foul flows will drain to the existing 225mm diameter foul sewer also within the High Street. The proposed connections will be via a new junction or utilising an existing drainage connection to the site (subject to a CCTV drainage survey).



### 3.0 Proposed Development

The proposed development is to consist of a convenience store building with associated carparking, access road and landscaping. There will be a total of 13 parking spaces. A copy of the architects proposed layout plan is included in the Section 6 appendices.

### 4.0 Flood Risk Assessment

The possible sources of flooding have been considered for the site and figures 3.0 and 4.0 below show the extent of flooding in the site location for fluvial and surface water flooding. It is indicated in Figure 3.0 that the site is within an area classified as Flood Zone 1, land having a less than 0.001% (1 in 1,000) annual probability of river or sea flooding.

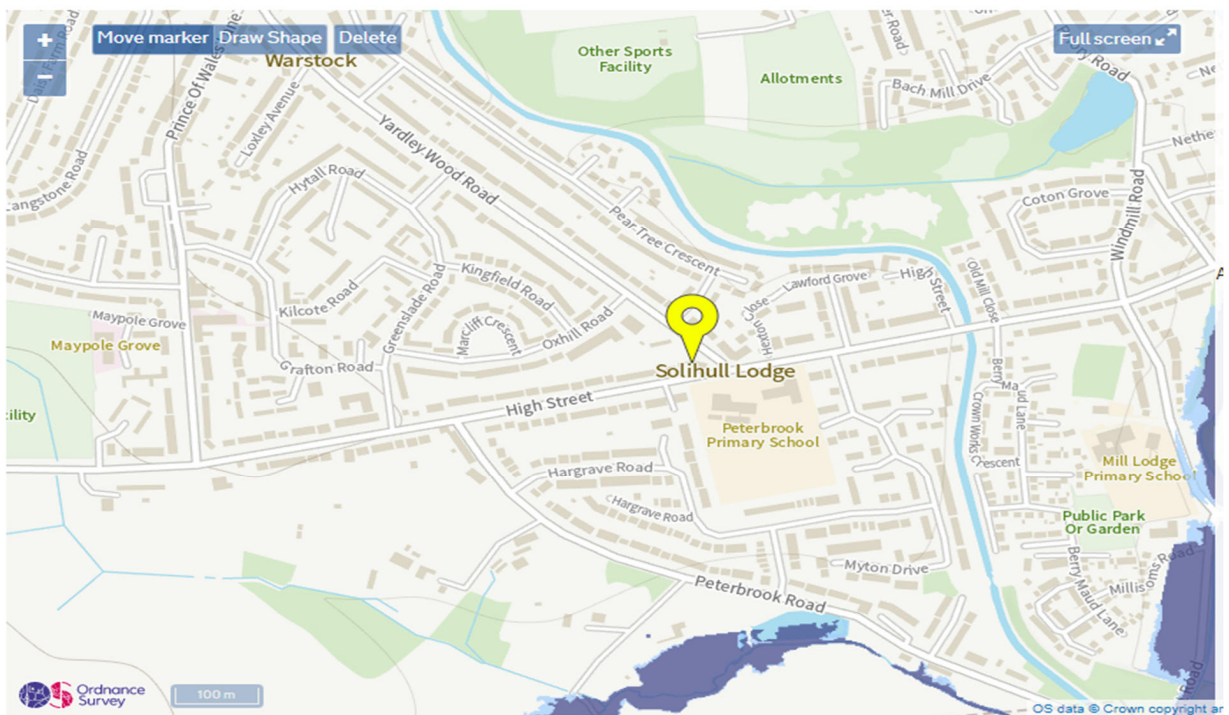


Figure 3.0 Flood Risk from Rivers and the Sea

From Figure 4.0 it appears that the site is at a very low risk of surface water flooding. The proposed development will be designed to current surface water standards and the building will be set at a slightly higher level with external areas falling away from to minimise such flood risk for the new development.

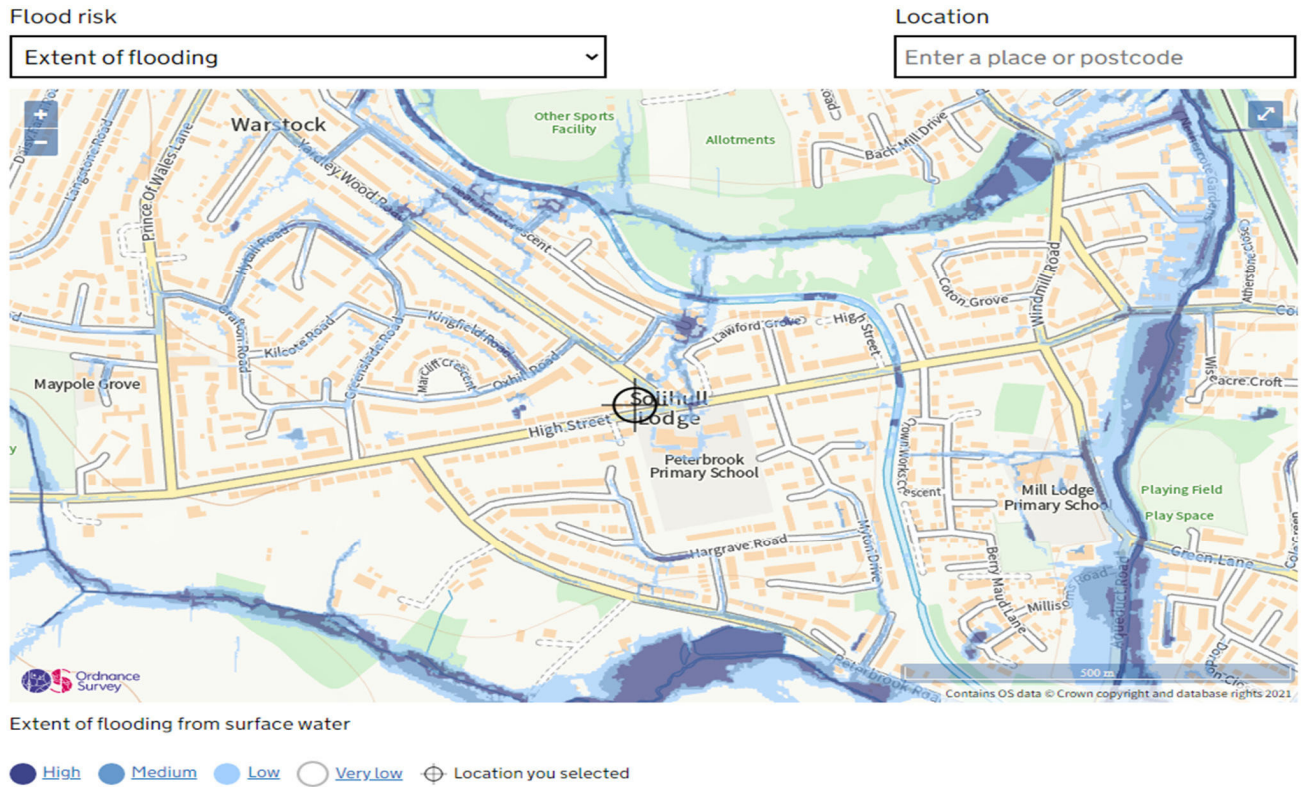


Figure 4.0 Flood Risk from Surface Water

## 5.0 Site Drainage

- The proposed development will have separate foul and surface water drainage systems before connecting into the public foul and surface water sewer located with the High Street, with discharge arrangements proposed as detailed below.
- Drainage layout proposals for both the on-site and off-site drainage are contained in Section 6.0 below

### 5.1 Foul Drainage

- The proposed foul drainage will collectively drain to the south-western corner of the site where it is proposed to discharge this into a combined sewer connection to the Severn Trent adopted combined sewer. A CCTV drainage survey will confirm the presence of any existing connections into site which may be re-used depending on depth and condition.

### 5.2 Surface Water System

- SuDS hierarchy has been used for the surface water design.
- The surface water design flows are calculated on the proposed new development impermeable area of 0.087ha and a design storm intensity of a 100-year return period plus 40% climate change allowance.
- There are no accessible drainage ditches, watercourses or open bodies of water that are suitable to discharge surface water run-off to without crossing third-party owned land.
- Ground records for the area indicate that the soils on the site consist of a mixture of sand and clay. The underlying sand strata may be suitable for soakaway drainage techniques. However, due to the contamination risk associated with the current use as a PFS combined with the presence of underlying clay it is considered that soakaway drainage would provide a risk of spreading known and unknown contamination underground and would therefore not be an appropriate option for this site.
- It is proposed that the surface water from the roof and hardstanding areas will be collected and directed into the proposed surface water drainage network before discharging into the Severn Trent adopted surface water sewer to the south of the site at a discharge rate of 8.3/s based on a 30% reduction in existing surface water run-off – refer to drawing PI5589-501 for details. Severn Trent Pre-development enquiry response can be found in Section 6.0.
- MicroDrainage calculations provided in Section 6.0 determine that 20.5m<sup>3</sup> of cellular storage will be required to achieve the desired discharge rate of 8.3l/s without flooding. A cellular storage tank will provide adequate surface water attenuation to ensure no flooding will occur during a 1 in 100 year + 40% climate change storm event.



## 6.0 Drawings and Calculations

Proposed Site Layout (EG Group)

241121CP-01 Topographical Survey (Chris Partington Land Surveyors)

Correspondence with Severn Trent (Goodson Associates)

Severn Trent Sewer Records

PI5588 Solihull High Street MicroDrainage Calculations

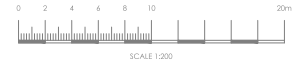
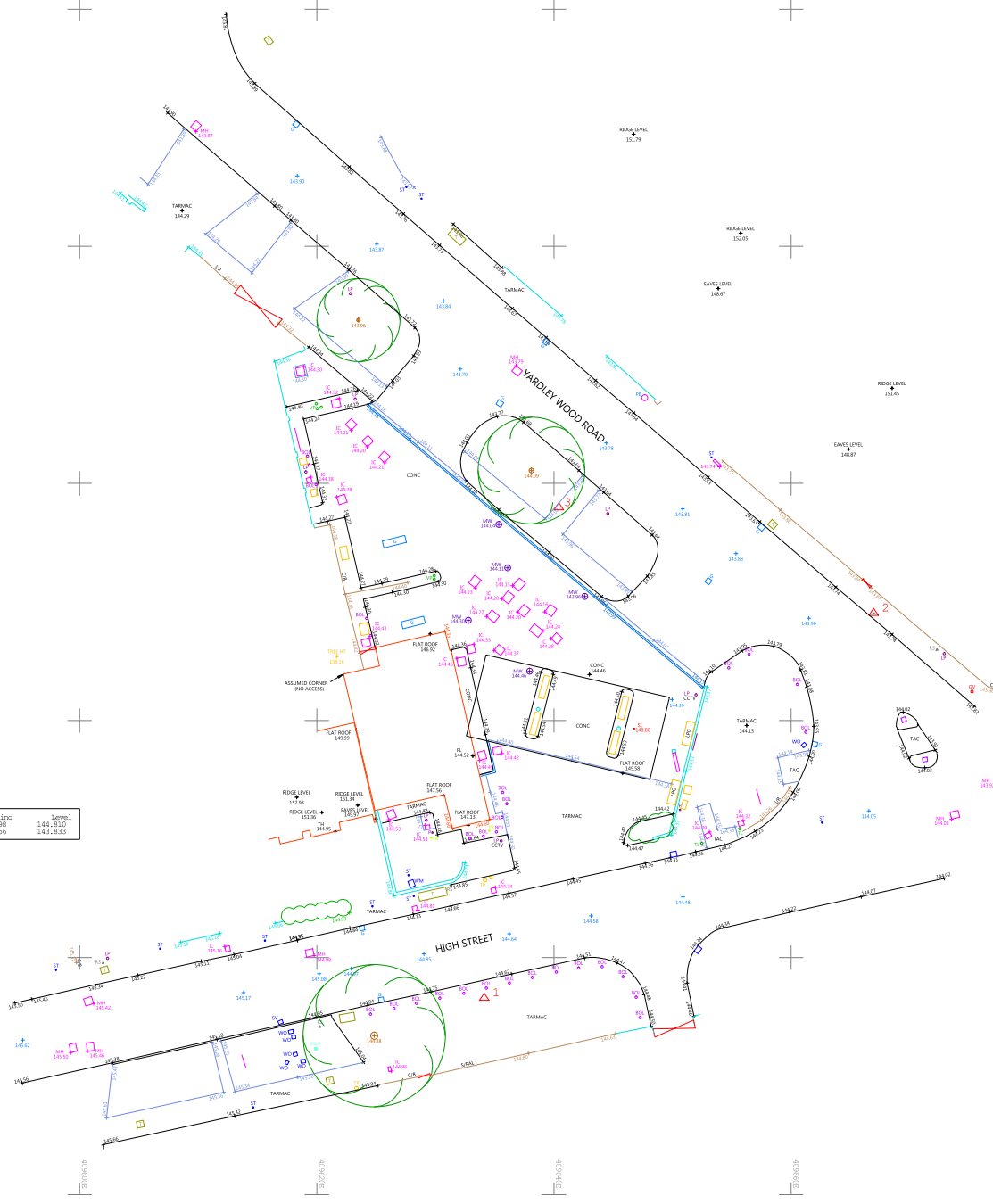
Impermeable Area Plan (Goodson Associates)

Drainage Layout Plan (Goodson Associates)

278740N  
278720N  
278700N  
278680N  
278660N  
278640N  
278620N  
278600N  
278580N  
278560N

278740E  
278720E  
278700E  
278680E  
278660E  
278640E  
278620E  
278600E  
278580E  
278560E

Station	Bearing	Northing	Level
1	409634.114	278656.598	144.810
2	409666.952	278689.056	143.833



**Abbreviations/Symbols (Proposed Buildings Survey)**

CH	Window Ch Height
WH	Window Head Height
BH	Beam Height
DH	Door Height
COL	Column
SVP	Soil Vent Pipe
FL	Floor Level
TL	Threshold Level
FL to Ceiling	Floor to Ceiling Height
VC	Vaulted Ceiling

**Line Types**

---	Hedge Lines
---	Drainage Runs
---	Overhead Electricity Cables
---	Overhead Telephone Cables

**Symbols**

⊗	Tree/Plant
⊗	Grass House
⊗	Control Station
⊗	Obstm
⊗	Schedule
⊗	Tic Hole

**Abbreviations (Topographic Survey)**

AH	Arch Height
AV	As Above
BB	Belted Beacon
EB	Electricity Box, Cables Box, Etc
BDL	Bolton
BTIC	Belted Telecom Inspection Chamber
BS	Bus Stop
BS/TP	Bus Stop Lamp Post
CATV	CATV Inspection Chamber
CCV	Closed Circuit Television
CL	Column
CLP	Column Post
EC	Earth Road
EIC	Electricity Inspection Chamber
EP	Electricity Pole
FL	Flag Pole
FP	Flag Pole
GV	Gas Valve
G	Gully
IC	Inspection Chamber
IO	Iron Outlet
IR	Iron Rod
LB	Ladder Box
LC	Lighting Column
M	Marker
M/R	Manhole
MP	Mooring Post
MS	Man Stone
HTNEX	Hydra Inspection Chamber
O	Overhang
P	Post
PO/IC	Post Office Inspection Chamber
R/S	Road Sign
RE	Rotating Eye
RTW	Rotating Wall
RF	Sign Post
SNP	Street Name Plate
ST	Stop Sign
SV	Stop Valve
TEIC	Telecom Inspection Chamber
TB	Telephone End Box
TL	Threshold Level
TL	Traffic Light
TP	Telephone Pole
TRUCK	Truck
W/O	Water Outlet
W/M	Water Meter

**Fence Descriptions**

B/W	Barbed Wire
C/S	Close Boarded
C/S/BARRER	Cloth Barrier
C/L	Chain Link
C/P	Chain Post
C/P	Chain Post
C/P	Chain Post
IR	Iron Rod
M/C	Manhole
MP	Mooring Post
W	Wire
P/C	Post & Chain
P/CAL	Post & Chain
W/M	Water Meter

**Survey Notes**

Coordinates and Levels related to Ordnance Survey Datum - O.S.D. 1936

Reference	Date	Description



44 Green Lane  
Sole  
Christine  
M33 5PP  
0161 976 1194  
www.opls.co.uk  
osurvey@opls.co.uk

Client  
**Euro Garages**

Project  
**ESSO EG Solihull Lodge  
Site Survey**

Scale	1:200	Surveyed by	C.S.P.	Date	24.11.21
Drawing No.	24112(CP)	Checked by	C.P.S.	Date	24.11.21
Drawn by	J.C.	Date	24.11.21		

# WONDERFUL ON TAP



Goodsons Associates  
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**Severn Trent Water Ltd**  
Leicester Water Centre  
Gorse Hill  
Anstey  
Leicester  
LE7 7GU

F.A.O: phil@goodsons.com

Tel: 0345 266 7930  
[www.stwater.co.uk](http://www.stwater.co.uk)

Ref 1024275  
Email:  
[Network.Solutions@SevernTrent.co.uk](mailto:Network.Solutions@SevernTrent.co.uk)

18<sup>th</sup> November 2021

Dear Sir/Madam,

**Proposed Development: (1 commercial unit) – ESSO Petrol  
Garage 94 High Street, Shirley, Solihull, B90 1JS - 409667,  
278671**

I refer to your 'Development Enquiry Request' in respect of the above named site. Please find enclosed the sewer records that are included in the fee together with the Supplementary Guidance Notes (SGN) which refer to surface water disposal from development sites.

**Protective Strip**

No public sewers shown within site boundary.

Due to a change in legislation on 1 October 2011 there may be former private sewers on the site which have transferred to the responsibility of Severn Trent Water Ltd, which are not shown on the statutory sewer records, but are located in your client's land. These sewers would require protective strips of 3 metres either side of the sewer's centreline that we will not allow to be built over. If such sewers are identified to be present on the site, please contact us for further guidance.

**Foul Water Drainage**

The site is likely to have an existing connection to the public sewer, it might be possible to utilise the existing connection if this is in a convenient location and in good condition.

Alternatively, the 225mm foul sewers on Yardley Wood road or High Street can accommodate gravity foul flows from your development.

A connection is therefore acceptable subject to a S106 submission.

### **Surface Water Drainage**

Under the terms of Section H of the Building Regulations 2000, the disposal of surface water by means of soakaways should be considered as the primary method. If these are found to be unsuitable, satisfactory evidence will need to be submitted. The evidence should be either percolation test results or by the submission of a statement from the SI consultant (extract or a supplementary letter).

Subject to the above, can you please provide further information, to demonstrate how the former impermeable areas on the site are currently drained, if indeed they are positively drained, identifying which impermeable areas drain to which pipeline and the connections/outfalls to the public sewerage system identified. Ideally, a drainage survey of the existing site is required.

On all brownfield site Severn Trent propose at least 30% reduction of surface water flows in comparison to the existing development's discharge. However, it is advised to discuss flow rates with the LLFA as national policy states that all developments should seek to discharge at greenfield rates where practical (5l/s/ha). Please refer to "Severn Trent Surface Water Guidance Notes" submitted with this response for further information.

Note, STW will need to be fully satisfied that all sustainable options have been satisfied before discharge to network is considered, we expect all surface water from the development to be drained in a sustainable way to the nearest watercourse or land drainage channel, subject to the developer discussing all aspects of the developments surface water drainage with the Local Lead Flood Authority (LLFA). Any discharge rate to a watercourse or drainage ditch will be determined by the LLFA / EA.

### **Connections**

For any new connections (including the re-use of existing connections) to the public sewerage system, the developer will need to submit a Section 106 application form. Our Developer Services department are responsible for handling all new connections enquiries and applications. To contact them for an application form

and associated guidance notes please call 0800 7076600 or download from [www.stwater.co.uk](http://www.stwater.co.uk).

Please quote the above reference in any future correspondence (including e-mails) with STW Limited. Please note that Developer Enquiry responses are only valid for 6 months from the date of this letter.


Yours sincerely

A handwritten signature in blue ink, appearing to read 'Belal Ali', is centered below the text 'Yours sincerely'.

Belal Ali  
Network Solutions  
Developer Services





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53 Melville Street Edinburgh EH3 7HL		
Date 13/12/2021 14:58 File P15588 Solihull High Str...	Designed by PhilH Checked by	
XP Solutions		Source Control 2017.1.2

Summary of Results for 100 year Return Period (+40%)

Half Drain Time : 21 minutes.


Storm Event	Max Level (m)	Max Depth (m)	Max Infiltration (l/s)	Max Control (l/s)	Max E Outflow (l/s)	Max Volume (m³)	Status
15 min Summer	0.557	0.557	0.0	8.3	8.3	14.3	O K
30 min Summer	0.677	0.677	0.0	8.3	8.3	17.4	O K
60 min Summer	0.678	0.678	0.0	8.3	8.3	17.4	O K
120 min Summer	0.571	0.571	0.0	8.3	8.3	14.7	O K
180 min Summer	0.432	0.432	0.0	8.3	8.3	11.1	O K
240 min Summer	0.321	0.321	0.0	8.3	8.3	8.2	O K
360 min Summer	0.186	0.186	0.0	8.2	8.2	4.8	O K
480 min Summer	0.140	0.140	0.0	7.4	7.4	3.6	O K
600 min Summer	0.121	0.121	0.0	6.4	6.4	3.1	O K
720 min Summer	0.109	0.109	0.0	5.6	5.6	2.8	O K
960 min Summer	0.095	0.095	0.0	4.5	4.5	2.4	O K
1440 min Summer	0.078	0.078	0.0	3.3	3.3	2.0	O K
2160 min Summer	0.065	0.065	0.0	2.4	2.4	1.7	O K
2880 min Summer	0.057	0.057	0.0	1.9	1.9	1.5	O K
4320 min Summer	0.047	0.047	0.0	1.4	1.4	1.2	O K
5760 min Summer	0.042	0.042	0.0	1.1	1.1	1.1	O K
7200 min Summer	0.038	0.038	0.0	0.9	0.9	1.0	O K
8640 min Summer	0.035	0.035	0.0	0.8	0.8	0.9	O K

Storm Event	Rain (mm/hr)	Flooded Volume (m³)	Discharge Volume (m³)	Time-Peak (mins)
15 min Summer	131.351	0.0	21.4	21
30 min Summer	86.314	0.0	28.1	31
60 min Summer	54.074	0.0	35.3	48
120 min Summer	32.762	0.0	42.7	82
180 min Summer	24.128	0.0	47.2	112
240 min Summer	19.312	0.0	50.4	142
360 min Summer	14.018	0.0	54.9	196
480 min Summer	11.175	0.0	58.3	252
600 min Summer	9.366	0.0	61.1	312
720 min Summer	8.105	0.0	63.4	372
960 min Summer	6.446	0.0	67.3	492
1440 min Summer	4.660	0.0	73.0	734
2160 min Summer	3.364	0.0	79.0	1092
2880 min Summer	2.667	0.0	83.5	1448
4320 min Summer	1.920	0.0	90.2	2200
5760 min Summer	1.519	0.0	95.1	2856
7200 min Summer	1.266	0.0	99.1	3640
8640 min Summer	1.090	0.0	102.4	4360

Summary of Results for 100 year Return Period (+40%)

Storm Event	Max Level (m)	Max Depth (m)	Max Infiltration (l/s)	Max Control (l/s)	Max Σ Outflow (l/s)	Max Volume (m³)	Status
10080 min Summer	0.033	0.033	0.0	0.7	0.7	0.8	O K
15 min Winter	0.645	0.645	0.0	8.3	8.3	16.6	O K
30 min Winter	0.779	0.779	0.0	8.3	8.3	20.0	O K
60 min Winter	0.764	0.764	0.0	8.3	8.3	19.6	O K
120 min Winter	0.595	0.595	0.0	8.3	8.3	15.3	O K
180 min Winter	0.374	0.374	0.0	8.3	8.3	9.6	O K
240 min Winter	0.226	0.226	0.0	8.3	8.3	5.8	O K
360 min Winter	0.133	0.133	0.0	7.0	7.0	3.4	O K
480 min Winter	0.110	0.110	0.0	5.7	5.7	2.8	O K
600 min Winter	0.098	0.098	0.0	4.8	4.8	2.5	O K
720 min Winter	0.089	0.089	0.0	4.1	4.1	2.3	O K
960 min Winter	0.078	0.078	0.0	3.3	3.3	2.0	O K
1440 min Winter	0.065	0.065	0.0	2.4	2.4	1.7	O K
2160 min Winter	0.054	0.054	0.0	1.7	1.7	1.4	O K
2880 min Winter	0.048	0.048	0.0	1.4	1.4	1.2	O K
4320 min Winter	0.040	0.040	0.0	1.0	1.0	1.0	O K
5760 min Winter	0.035	0.035	0.0	0.8	0.8	0.9	O K
7200 min Winter	0.032	0.032	0.0	0.7	0.7	0.8	O K
8640 min Winter	0.030	0.030	0.0	0.6	0.6	0.8	O K


Storm Event	Rain (mm/hr)	Flooded Volume (m³)	Discharge Volume (m³)	Time-Peak (mins)
10080 min Summer	0.961	0.0	105.3	5136
15 min Winter	131.351	0.0	24.0	21
30 min Winter	86.314	0.0	31.5	32
60 min Winter	54.074	0.0	39.5	50
120 min Winter	32.762	0.0	47.9	88
180 min Winter	24.128	0.0	52.9	118
240 min Winter	19.312	0.0	56.4	142
360 min Winter	14.018	0.0	61.5	192
480 min Winter	11.175	0.0	65.3	252
600 min Winter	9.366	0.0	68.4	310
720 min Winter	8.105	0.0	71.1	372
960 min Winter	6.446	0.0	75.4	492
1440 min Winter	4.660	0.0	81.7	738
2160 min Winter	3.364	0.0	88.5	1104
2880 min Winter	2.667	0.0	93.5	1436
4320 min Winter	1.920	0.0	101.0	2204
5760 min Winter	1.519	0.0	106.5	2848
7200 min Winter	1.266	0.0	111.0	3656
8640 min Winter	1.090	0.0	114.7	4304

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Summary of Results for 100 year Return Period (+40%)

Storm Event	Max Level (m)	Max Depth (m)	Max Infiltration (l/s)	Max Control (l/s)	Max Σ Outflow (l/s)	Max Volume (m <sup>3</sup> )	Status
10080 min Winter	0.028	0.028	0.0	0.5	0.5	0.7	O K

Storm Event	Rain (mm/hr)	Flooded Volume (m <sup>3</sup> )	Discharge Volume (m <sup>3</sup> )	Time-Peak (mins)
10080 min Winter	0.961	0.0	117.9	5104

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Rainfall Details


Rainfall Model	FSR	Winter Storms	Yes
Return Period (years)	100	Cv (Summer)	0.750
Region	England and Wales	Cv (Winter)	0.840
M5-60 (mm)	19.100	Shortest Storm (mins)	15
Ratio R	0.400	Longest Storm (mins)	10080
Summer Storms	Yes	Climate Change %	+40

Time Area Diagram

Total Area (ha) 0.087

Time (mins)	Area (ha)	Time (mins)	Area (ha)	Time (mins)	Area (ha)
From:	To:	From:	To:	From:	To:
0	4	4	8	8	12
	0.029		0.029		0.029



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Model Details

Storage is Online Cover Level (m) 2.000

Cellular Storage Structure

Invert Level (m) 0.000 Safety Factor 2.0  
 Infiltration Coefficient Base (m/hr) 0.00000 Porosity 0.95  
 Infiltration Coefficient Side (m/hr) 0.00000

Depth (m)	Area (m <sup>2</sup> )	Inf. Area (m <sup>2</sup> )	Depth (m)	Area (m <sup>2</sup> )	Inf. Area (m <sup>2</sup> )
0.000	27.0	0.0	0.801	0.0	0.0
0.800	27.0	0.0	2.000	0.0	0.0



Hydro-Brake® Optimum Outflow Control

Unit Reference MD-SHE-0137-8300-0800-8300  
 Design Head (m) 0.800  
 Design Flow (l/s) 8.3  
 Flush-Flo™ Calculated  
 Objective Minimise upstream storage  
 Application Surface  
 Sump Available Yes  
 Diameter (mm) 137  
 Invert Level (m) 0.000  
 Minimum Outlet Pipe Diameter (mm) 150  
 Suggested Manhole Diameter (mm) 1200

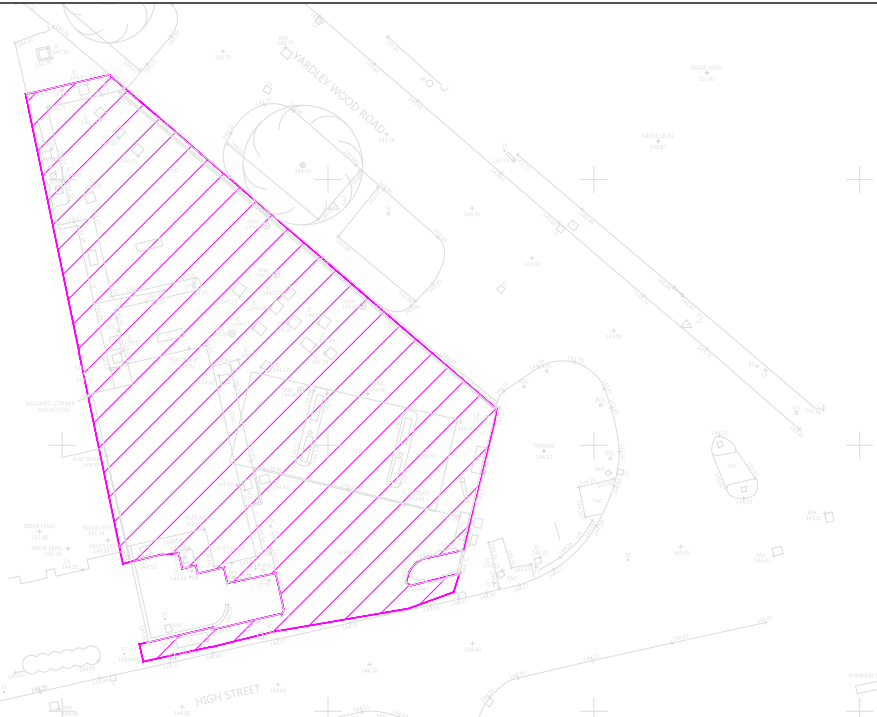
Control Points	Head (m)	Flow (l/s)	Control Points	Head (m)	Flow (l/s)
Design Point (Calculated)	0.800	8.3	Kick-Flo®	0.562	7.0
Flush-Flo™	0.255	8.3	Mean Flow over Head Range	-	7.1

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	4.9	1.200	10.0	3.000	15.5	7.000	23.3
0.200	8.2	1.400	10.8	3.500	16.7	7.500	24.1
0.300	8.3	1.600	11.5	4.000	17.8	8.000	24.8
0.400	8.1	1.800	12.2	4.500	18.8	8.500	25.5
0.500	7.7	2.000	12.8	5.000	19.8	9.000	26.2
0.600	7.3	2.200	13.4	5.500	20.7	9.500	26.9
0.800	8.3	2.400	13.9	6.000	21.6		
1.000	9.2	2.600	14.5	6.500	22.5		

-  EXISTING IMPERMEABLE AREA: 850m<sup>2</sup> (0.085 Ha)  
EXISTING SW RUN-OFF: 2.78 x 0.085 x 50 = 11.8 L/S - 30% = 8.3 L/S
-  PROPOSED IMPERMEABLE AREA: 870m<sup>2</sup> (0.087 Ha)

Station	Easting	Northing	Level
1	409634.114	278656.598	144.810
2	409666.952	278689.056	143.833



Station	Easting	Northing	Level
1	409634.114	278656.598	144.810
2	409666.952	278689.056	143.833



REV.	DATE	REVISION.	BY.	CHK.
-	-	FIRST ISSUE	PH	NB

Euro Garages Ltd

Proposed Convenience Store  
Solihull High Street, Shirley

Impermeable Area Plan

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**PLANNING**

DATE CREATED: Dec '21	SCALE: 1:200 @ A1
CONTRACT No: P15588	DRAWING No: 501
REV: -	

