Structural Civil Geo-Environmental

**Barrington Road, Bedlington** 

Flood Risk Assessment

for

Mr Harjit Singh Deol



consulting engineers





Report Ref	Issue	Prepared by	Date	Reviewed by	Date
P21-484-3E-ZZ-XX-RP-C-9000	1	J Foster	22.04.22	M Pearse	22.04.22

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#### Barrington Road, Bedlington

#### Drainage Statement including Flood Risk Assessment

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#### **1 INTRODUCTION**

1.1 3e Consulting Engineers Ltd (3e) were commissioned by George F White on behalf of Mr Harjit Singh Deol to carry out a Flood Risk Assessment for a proposed development north of Barrington Road, Bedlington, which includes the construction of 12 properties as indicated on the site layout plan included in **Appendix C**.

1.2 The objective of this assessment is to identify any potential risk of flooding to the proposed site and adjacent properties as a result of the development in accordance with the requirements of the current National Planning Policy Framework (NPPF) and Northumberland County Council's requirements. It will also assess the proposed surface water and foul water drainage proposals in order that the proposed development does not exacerbate flooding elsewhere. It will also provide comments on proposed options for Sustainable Urban Drainage (SUD's) techniques in line with current Ciria guidance.

1.3 This report is based on information received from Northumbrian Water together with the review of the Environment Agency's (EA) online flood maps and Northumberland County Council's SFRA. A topographical survey has also been provided and a Phase 2 Geo-Environmental Assessment has also been undertaken by ERGO Environmental LTD.

1.4 This report presents the factual information available during this appraisal, interpretation of the data obtained and recommendations relevant to the scope of works.

1.5 This report has been prepared for the sole use of Mr Harjit Singh Deol and their appointed consultants. No other third party may rely upon or reproduce the contents of this report without the written approval of 3e. If any unauthorised third party comes into possession of this report, they rely on it entirely at their own risk and 3e do not owe them any Duty of Care or Skill.

#### 2 THE SITE

#### **Location and Description**

2.1 The site, centred on National Grid Reference 426975, 583351, is located north of Bedlington and east of Choppington, Northumberland and is accessed via Barrington Road. A site location plan is included as **Appendix A**.



#### **Site Location**

- 2.2 The site is currently greenfield land and falls northerly from Barrington Road.
- 2.3 The adjacent land use is as follows:
  - North: Car breaker/scrapyard
  - South: Barrington Road
  - East: Car breaker/scrapyard
  - West: Access road to two residential properties

2.4 A topographical survey has been undertaken which shows that levels vary across the site with a high point of 27.360mAOD at the south eastern corner of the site boundary, and a low point of 25.025mAOD on the north-eastern corner of the site boundary. Within Barrington Road, there is a high point of 27.454mAOD along the southern edge, the road itself is cambered, with relation to the site approximately <sup>3</sup>/<sub>4</sub> falls from east to west, with the other <sup>1</sup>/<sub>4</sub> falling in the opposite direction.

2.5 A copy of the topographical survey is attached in **Appendix B.** 

#### **3 EXISTING WATERCOURSES AND DRAINAGE**

3.1 The nearest watercourse to the site is an unnamed watercourse approximately 100m west of the site, just west of Barrington Cottage. This ultimately connects to Sleek Burn, which is located approximately 440m north of the site. Sleek Burn flows east under the A1147 and ultimately discharges into River Blyth approximately 3.15km east of the site.

3.2 A 225mm diameter public combined sewer is shown to be located within the site, running from east to west, before heading north. This is shown as approximately 2.28m depth at this location.

3.3 For copies of the NWL sewer record plans see **Appendix E**.

#### 4 FLOOD FLOW PATHS AND ZONES

#### **Fluvial Flooding**

4.1 Online flood maps, provided by the Environment Agency (EA), have been reviewed and these indicate that both the unnamed watercourse to the west, as well as Sleek Burn to the north are subject to fluvial flooding. However these do not affect the proposed development.

4.2 It is therefore considered that the site is at low risk of fluvial flooding.

#### **Coastal Flooding**

4.3 EA's online Costal Flood Risk Maps have been reviewed and these show that the site is not at risk from coastal waters.

#### **Pluvial Flooding**

4.4 The EA 'Surface Water Flood Risk Maps' have been reviewed online. These maps are undertaken to highlight potential areas at risk of flooding from surface water flows running across land which cannot enter the ground or drainage systems.

4.5 These maps show an area of surface water flooding risk at the western boundary of the site, as well as in the north-eastern boundary of the site. However, from review of the topographical survey information it is considered the areas shown is due to the localised low lying areas within the site, that will be designed out with the proposed level design.

4.6 A positive drainage system is being provided and controlled therefore reducing the potential risk of overland flows within and beyond the development site. An overland flow route plan has been provided, see **Appendix D**.

4.7 Permeable paving has been shown to assist with SuDS on the site, the flow routes are to be directed over the private permeable shared drives.

4.8 The new surface water drainage system within the site will be designed to accommodate a 1 in 100 year +40%CC storm event within the drainage network below ground. Any flooding occurring from a storm event in excess of this will be retained where possible with no flooding occurring to any of the proposed buildings. 4.9 It is considered that the site is at low risk of Pluvial flooding.

#### **Flooding from Artificial Sources**

4.10 Online ordnance survey data maps have been reviewed to determine whether there are any artificial sources such as reservoirs or canals in the vicinity of the site which if failed could affect the proposed development site.

4.11 This review confirmed there are no such sources which could impact the site.

#### **Ground Water Flooding**

4.12 Another potential risk of flooding to be considered is from rising groundwater within the underlying strata. A Phase 2 Geo-Environmental Assessment has been undertaken on site.

4.13 The Geo-Environmental Assessment which utilised groundwater monitoring to complete their assessment has found water in 1 out of 5 trial pits, 0 of 3 boreholes, and 2 out of 5 window samples. Water was encountered at depths of: 1.9m (Seepage), and 3m (Seepage), 5m (Strike).

4.14 It is considered there is low risk to the development as a result of ground water flooding.

#### **Overland Flow Routes**

4.15 As this is a greenfield site, the level design has been undertaken in order to best maintain the existing topography and flow routes. The site access from Barrington Road initially rises in level in order to keep Barrington Road's overland flows from entering the site.

4.16 OS mapping has been reviewed for area adjacent land beyond the extent of the topographical survey. This shows contours that fall away from the site. It is considered there is low risk of overland flow entering the site from neighbouring areas.

#### Sewer Flooding

4.17 Northumbrian Water has been consulted to obtain a copy of their sewer records.

4.18 An existing 225mm diameter public combined sewer is located within the site, running from east to west, before heading northwards off-site. This sewer will be diverted within the development.

4.19 The new surface water drainage system within the site will be designed to accommodate a 1 in 100 year +40%CC storm event within the drainage network below ground. Any flooding occurring from a storm event in excess of this will be retained on site where possible with no flooding occurring to any of the proposed buildings.

4.20 It is considered there is low risk to the development as a result of sewer flooding.

4.21 Northumbrian Waters sewer records are included in **Appendix E**.

#### SURFACE WATER AND FOUL WATER DRAINAGE

#### Surface Water Drainage

4.22 The proposed surface water drainage scheme should seek to meet the current National Planning Policy Framework (NPPF) and North Tyneside Council's requirements.

4.23 Consideration should be given firstly to infiltration techniques (to ground), to watercourse and then to sewer. Sustainable Urban Drainage Systems (SuDS) should also be used wherever possible to mimic as far as practicable the natural run-off regime, improve water quality and attenuate peak flows. These should be designed in accordance with the current guidance Ciria C753 'The SuDs Manual' Version 1.

4.24 In line with the current National Planning Policy Framework (NPPF), the implementation of SuDS to restrict flows and improve water quality has been considered. It is proposed to utilise porous paving within the parking bays. The porous surface and granular stone sub base under the parking bays will provide 2 levels of treatment.

4.25 The results from the Geo-Environmental site investigation and infiltration tests indicated the cohesive drift deposits have poor soakage potential and failed to soakaway. Due to the significant volumes of low permeability clay on the site, it was concluded that soakaway drainage is not suitable for the proposed development.

4.26 A pre-development enquiry has been submitted to NWL and their response dated 7<sup>th</sup> January 2022, states that surface water flows should discharge to directly to the watercourse to the west of Barrington Cottage. Due to the complications highlighted above, we shall go back to NWL seeking an agreed discharge rate and connection. See **Appendix E**.

4.27 The nearest watercourse to the site is an unnamed watercourse approximately 100m west of the site, just west of Barrington Cottage that ultimately connects to Sleek Burn. However, connection to this existing watercourse would cut across 3 different land ownerships and as a result has been ruled out.

4.28 An existing public surface water sewer is shown inland to the south of the site and currently connects to the aforementioned watercourse was also identified as a possible option. However, connection to this sewer would require going below both an adopted road and an active railway line, which would require a bored connection in coordination with the railway

authority. Due to the significant complexity in achieving this connection and land ownership issues, this option was ruled out.

4.29 It has therefore been proposed to go back to NWL seeking agreement on discharging surface water flows to the existing public combined sewer.

4.30 It is proposed that surface water drainage will connect to the diverted public combined sewer, before connecting to the existing public combined manhole 9304 west of the site.

4.31 The IH124 Method has been used to calculate the anticipated Qbar greenfield flow rate from the site using HR Wallingford, see **Appendix D**. The proposed drained impermeable area of the site will be in the order of 0.267ha which will result in a proposed greenfield flow rate for the development of 1.21 l/s.

4.32 Due to the size of the proposed development and to achieve the minimum acceptable orifice size of 75mm, it is proposed to restrict surface water flows from development to a maximum discharge rate of 3.4 l/s. This is for maintenance issues with any smaller sized orifices required to meet lower discharge rates. This results in attenuation being required within the site. The attenuation will be accommodated within oversized pipes.

4.33 The drainage will be designed to accommodate a 1 in 100 year + 40% climate change storm with no flooding.

#### Shared and private driveways (Pollution Hazard Level – Medium)

4.34 The shared and private driveways have been classified as individual property driveways in accordance with Table 26.2 of the SuDS Manual (C753). This states the pollution hazard indices as follows:

Pollution Hazard	Total Suspended Solids(TSS)	Metals	Hydro carbons		
Low	0.5	0.4	0.4		

4.35 The shared and private driveways will drain via porous paving with underlying filtration stone and will be collected via a perforated under drain. In line with Table 26.3 of the SuDS manual (C753) this will provide the following mitigation indices.

Type of SuDS	TSS	Metals	Hydro carbons
component			
Permeable Pavement	0.7	0.6	0.7

4.36 These indices meet the requirements of the pollution hazard indices and therefore provide sufficient treatment from driveways/shared driveways.

4.37 A preliminary drainage layout has been included within **Appendix D.** 

4.38 Details of the porous paving has been included within **Appendix D.** 

4.39 For copies of the proposed surface water calculations refer to **Appendix D.** 

4.40 All private surface water drainage should be designed in accordance with the current Building Regulation. All private drainage will be maintained by the occupier in accordance with the maintenance schedule attached in **Appendix D**.

#### Foul Water Drainage

5.23 A pre development enquiry has been submitted to Northumbrian Water to determine the proposed connection point for foul water drainage from the site. Their response dated 7<sup>th</sup> January 2022 confirms that foul water flows from the site can discharge to the public sewer.

4.41 It is proposed that foul water drainage will connect to the diverted public combined sewer, before connecting to existing public combined manhole 9304 west of the site.

5.24 All private foul water drainage should be designed in accordance with the current Building Regulation. All private drainage will be maintained by the occupier in accordance with the maintenance schedule attached in **Appendix D**.

5.25 A preliminary drainage layout plan has been included within **Appendix D.** 

#### CONCLUSIONS AND RECOMMENDATIONS

6.1 The site has been reviewed in relation to all potential sources of flooding and it is considered that the site is at low risk of flooding from all sources.

6.2 Pluvial flooding across the development isn't an existing issue, a flood flow path has been provided through the site over permeable paving.

6.3 The proposed development will therefore not exacerbate flooding elsewhere.

6.4 Existing public combined sewer to be diverted within development.

6.5 Surface water from the site will discharge to the diverted public combined sewer, before connecting to existing public combined manhole 9304 west of the site in accordance with NWL's requirements. Flows are to be restricted to a maximum flow rate of 3.4 l/s with attenuation being provided using oversized pipes.

6.6 Sustainable Urban Drainage techniques have been considered to improve the water quality of the discharge of surface water flows from the development. This will be in the form of porous paving.

6.7 Foul water flows from the site will discharge to the diverted public combined sewer, before connecting to existing public combined manhole 9304 west of site.

Appendix A



Appendix **B** 



Appendix C



Appendix D



# Greenfield runoff rate estimation for sites

Calculated by:	James Foster
Site name:	P21-484
Site location:	Barrington Road, Bedlington

This is an estimation of the greenfield runoff rates that are used to meet normal best practice criteria in line with Environment Agency guidance "Rainfall runoff management for developments", SC030219 (2013), the SuDS Manual C753 (Ciria, 2015) and the non-statutory standards for SuDS (Defra, 2015). This information on greenfield runoff rates may be the basis for setting consents for the drainage of surface water runoff from sites.

Site Details	
Latitude:	55.14531° N
Longitude:	1.59353° W
Reference:	3631848204
Date:	Jan 06 2022 14:27

www.uksuds.com | Greenfield runoff tool

#### Runoff estimation approach IH124 Site characteristics

Site characteristics					Notes			
Total site area (ha): 0.2	665012				(1) Is $O_{222} < 20$ 1/s/ba2			
Methodology					(1) 13  GBAR < 2.0  is sima:			
Q <sub>BAR</sub> estimation method	Calc	ulate fi	rom SPR a	and SAAR	When $Q_{BAR}$ is < 2.0 l/s/ha then limiting discharge rates are s			
SPR estimation method:	Calc	ulate fi	rom SOIL	type	at 2.0 l/s/ha.			
Soil characteristics	Defau	ılt	Edite	ed				
SOIL type:	4 4		4		(2) Are flow rates < 5.0 l/s?			
HOST class:	N/A	N/A			Where flow rates are less than 5.0.1/a concept for discharge is			
SPR/SPRHOST:	0.47	0.47 0.47			usually set at 5.0 l/s if blockage from vegetation and other			
Hydrological charact	eristics	C	efault	Edited	materials is possible. Lower consent flow rates may be set where the blockage risk is addressed by using appropriate			
SAAR (mm):		666	3	666	drainage elements.			
Hydrological region:		3		3	(3) IS SED/SEDHOST $< 0.32$			
Growth curve factor 1 ye	xar:	0.8	6	0.86				
Growth curve factor 30 y	Growth curve factor 30 years:		5	1.75	Where groundwater levels are low enough the use of			
Growth curve factor 100	years:	2.0	8	2.08	soakaways to avoid discharge offsite would normally be preferred for disposal of surface water runoff.			
Growth curve factor 200	years:	2.3	7	2.37				

#### Edited Default Greenfield runoff rates Q<sub>BAR</sub> (I/s): 1.21 1.21 1 in 1 year (l/s): 1.04 1.04 1 in 30 years (l/s): 2.12 2.12 1 in 100 year (l/s): 2.52 2.52 1 in 200 years (l/s): 2.88 2.88

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at www.uksuds.com/terms-and-conditions.htm. The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.



#### Design Settings

Rainfall Methodology	FSR	Maximum Time of Concentration (mins)	30.00
Return Period (years)	1	Maximum Rainfall (mm/hr)	50.0
Additional Flow (%)	0	Minimum Velocity (m/s)	1.00
FSR Region	England and Wales	Connection Type	Level Soffits
M5-60 (mm)	17.000	Minimum Backdrop Height (m)	0.200
Ratio-R	0.300	Preferred Cover Depth (m)	1.200
CV	0.750	Include Intermediate Ground	$\checkmark$
Time of Entry (mins)	5.00	Enforce best practice design rules	$\checkmark$

#### <u>Nodes</u>

Name	Area (ha)	T of E (mins)	Cover Level (m)	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
2	0.091	5.00	26.965	1200	426951.996	583351.894	1.350
1	0.104	5.00	26.470	2400	426991.512	583357.595	3.250
3			26.100	2400	426955.589	583366.457	2.955
4	0.044	5.00	25.860	2400	426943.453	583369.451	2.740
C3			26.000	1500	426929.476	583375.098	2.970
9304			25.480	1200	426925.683	583382.778	2.505
0302		5.00	27.100	1200	427012.972	583334.143	1.425
C1			26.360	1200	427010.277	583353.648	1.925
C2			26.450	1200	426989.186	583360.368	2.150

<u>Links</u>

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)
2.000	1	3	37.000	0.600	23.220	23.145	0.075	493.3	1500	5.32	39.4
2.001	3	4	12.500	0.600	23.145	23.120	0.025	500.0	1500	5.43	39.1
2.002	4	C3	15.075	0.600	23.120	23.030	0.090	167.5	225	5.68	38.3
3.000	2	3	15.000	0.600	25.615	24.495	1.120	13.4	150	5.09	40.1
1.003	C3	9304	8.566	0.600	23.030	22.975	0.055	155.7	225	6.14	37.1
1.000	0302	C1	19.690	0.600	25.675	24.435	1.240	15.9	225	5.10	40.0
1.001	C1	C2	22.136	0.600	24.435	24.300	0.135	164.0	225	5.46	39.0
1.002	C2	C3	61.500	0.600	24.300	23.030	1.270	48.4	225	6.01	37.5

Name	Vel	Сар	Flow	US	DS	Σ Area	Σ Add	Pro	Pro
	(m/s)	(I/s)	(I/s)	Depth	Depth	(ha)	Inflow	Depth	Velocity
				(m)	(m)		(I/s)	(mm)	(m/s)
2.000	1.924	3400.0	11.1	1.750	1.455	0.104	0.0	60	0.462
2.001	1.911	3377.1	20.7	1.455	1.240	0.195	0.0	82	0.556
2.002	1.007	40.0	24.9	2.515	2.745	0.240	0.0	129	1.061
3.000	2.767	48.9	9.9	1.200	1.455	0.091	0.0	46	2.184
1.003	1.045	41.5	24.1	2.745	2.280	0.240	0.0	123	1.084
1.000	3.300	131.2	0.0	1.200	1.700	0.000	0.0	0	0.000
1.001	1.018	40.5	0.0	1.700	1.925	0.000	0.0	0	0.000
1.002	1.884	74.9	0.0	1.925	2.745	0.000	0.0	0	0.000

CAU	AUSEWAY 🛟			Consultir	ng Engineers	gineers Ltd File: P21-484 - Barrington Roac Network: Storm Network James Foster 08/04/2022			bac Pa P2 Ba	Page 2 P21-484 Barrington Road, Bedlington			
					<u> </u>	Pipeline S	chedule						
	Link	Length	Slope	Dia	Link	US CL	US IL	US Depth	DS C	L DS	IL DS	Depth	
		(m)	(1:X)	(mm)	Туре	(m)	(m)	(m)	(m)	(n	n)	(m)	
	2.000	37.000	493.3	1500	Circular	26.470	23.220	1.750	26.10	0 23.	145	1.455	
	2.001	12.500	500.0	1500	Circular	26.100	23.145	1.455	25.86	0 23.	120	1.240	
	2.002	15.075	167.5	225	Circular	25.860	23.120	2.515	26.00	0 23.	030	2.745	
	3.000	15.000	13.4	150	Circular	26.965	25.615	1.200	26.10	0 24.	495	1.455	
	1.003	8.566	155.7	225	Circular	26.000	23.030	2.745	25.48	0 22.	975	2.280	
	1.000	19.690	15.9	225	Circular	27.100	25.675	1.200	26.36	0 24.	435	1.700	
	1.001	22.136	164.0	225	Circular	26.360	24.435	1.700	26.45	0 24.	300	1.925	
	1.002	61.500	48.4	225	Circular	26.450	24.300	1.925	26.00	0 23.	030	2.745	
		Link	US Node	Dia (mm)	Node	MH Type	DS Node	Dia (mm)	Node Type		MH Type		
		2 000	1	2400	Manhole	Adontah	le 3	2400	Manho	le Ado	ontable		
		2.000	т २	2400	Manhole	Adontah	le 4	2400	Manho	le Ada	ontable		
		2.001	4	2400	Manhole	Adontah		1500	Manho	le Ada	ontable		
		3,000	2	1200	Manhole	Adontah	le 3	2400	Manho	le Adu	ontable		
		1 003	 	1500	Manhole	Adontah	10 0 10 0304	1200	Manho	le Ad	ntahle		
		1 000	0302	1200	Manhole	Adoptab	ile C1	1200	Manho	le Ada	ontable		
		1 001	C1	1200	Manhole	Adontah		1200	Manho	le Ad	ntahle		
		1.001	C2	1200	Manhole	Adoptab	le C3	1500	Manho	le Ado	optable		
					<u>1</u>	Manhole	<u>Schedule</u>						
	Node	Eastin (m)	g ľ	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connect	ions	Link	IL (m)	Dia (mm)	
	2	426951.	996 58	33351.89	4 26.965	1.350	1200						
									0	3.000	25.615	150	
	1	426991.	512 58	33357.59	5 26.470	3.250	2400	0 <					
									0	2.000	23.220	1500	
	3	426955.	589 58	3366.45	7 26.100	2.955	2400		1	3.000	24.495	150	
								0 < > 2	2	2.000	23.145	1500	
								1	0	2.001	23.145	1500	
	4	426943.	453 58	3369.45	1 25.860	2.740	2400		1	2.001	23.120	1500	

0 2.002 23.120 225 C3 2.970 2.002 426929.476 583375.098 26.000 1500 1 23.030 225 2 225 1.002 23.030 0 1.003 23.030 225 9304 426925.683 583382.778 25.480 2.505 1200 1 1.003 22.975 225 0302 427012.972 583334.143 27.100 1.425 1200 T 0 1.000 25.675 225



#### Node 4 Online Hydro-Brake<sup>®</sup> Control

Flap Valve	х	Objective	(HE) Minimise upstream storage
Downstream Link	2.002	Sump Available	$\checkmark$
Replaces Downstream Link	$\checkmark$	Product Number	CTL-SHE-0075-3400-2000-3400
Invert Level (m)	23.120	Min Outlet Diameter (m)	0.100
Design Depth (m)	2.000	Min Node Diameter (mm)	1200
Design Flow (I/s)	3.4		



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#### Results for 1 year Critical Storm Duration. Lowest mass balance: 99.48%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
15 minute winter	2	10	25.662	0.047	9.9	0.1172	0.0000	ОК
120 minute winter	1	90	23.447	0.227	4.2	1.1747	0.0000	ОК
120 minute winter	3	94	23.448	0.303	6.1	1.3687	0.0000	ОК
120 minute winter	4	94	23.448	0.328	4.0	1.5878	0.0000	SURCHARGED
120 minute winter	C3	94	23.069	0.039	2.6	0.0692	0.0000	ОК
120 minute winter	9304	94	23.013	0.038	2.6	0.0000	0.0000	ОК
15 minute winter	0302	1	25.675	0.000	0.0	0.0000	0.0000	ОК
15 minute winter	C1	1	24.435	0.000	0.0	0.0000	0.0000	ОК
15 minute winter	C2	1	24.300	0.000	0.0	0.0000	0.0000	ОК

Link Event	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
15 minute winter	2	3.000	3	9.8	2.115	0.200	0.0694	
120 minute winter	1	2.000	3	2.6	0.168	0.001	7.7798	
120 minute winter	3	2.001	4	2.5	0.150	0.001	3.3540	
120 minute winter	4	Hydro-Brake <sup>®</sup>	C3	2.6				
120 minute winter	C3	1.003	9304	2.6	0.571	0.062	0.0384	28.1
15 minute winter	0302	1.000	C1	0.0	0.000	0.000	0.0000	
15 minute winter	C1	1.001	C2	0.0	0.000	0.000	0.0000	
15 minute winter	C2	1.002	C3	0.0	0.000	0.000	0.1405	



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#### Results for 30 year +40% CC Critical Storm Duration. Lowest mass balance: 99.48%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
15 minute winter	2	10	25.714	0.099	33.7	0.2452	0.0000	ОК
240 minute winter	1	232	24.272	1.052	8.9	5.4338	0.0000	ОК
240 minute winter	3	232	24.272	1.127	10.2	5.0987	0.0000	ОК
240 minute winter	4	232	24.272	1.152	5.2	5.5838	0.0000	SURCHARGED
240 minute winter	C3	232	23.070	0.040	2.6	0.0702	0.0000	ОК
240 minute winter	9304	232	23.013	0.038	2.6	0.0000	0.0000	ОК
15 minute winter	0302	1	25.675	0.000	0.0	0.0000	0.0000	ОК
15 minute winter	C1	1	24.435	0.000	0.0	0.0000	0.0000	ОК
15 minute winter	C2	1	24.300	0.000	0.0	0.0000	0.0000	ОК

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (I/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m <sup>3</sup> )
15 minute winter	2	3.000	3	33.4	2.844	0.683	0.1760	
240 minute winter	1	2.000	3	2.4	0.177	0.001	50.6867	
240 minute winter	3	2.001	4	2.4	0.157	0.001	17.9465	
240 minute winter	4	Hydro-Brake <sup>®</sup>	C3	2.6				
240 minute winter	C3	1.003	9304	2.6	0.576	0.064	0.0393	67.1
15 minute winter	0302	1.000	C1	0.0	0.000	0.000	0.0000	
15 minute winter	C1	1.001	C2	0.0	0.000	0.000	0.0000	
15 minute winter	C2	1.002	C3	0.0	0.000	0.000	0.1417	



P21-484 Barrington Road, Bedlington

Page 6

#### Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 99.48%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
15 minute winter	2	10	25.737	0.122	43.4	0.3040	0.0000	ОК
240 minute winter	1	232	25.166	1.946	11.6	10.0496	0.0000	SURCHARGED
240 minute winter	3	232	25.167	2.022	13.8	9.1455	0.0000	SURCHARGED
240 minute winter	4	232	25.167	2.047	6.4	9.9201	0.0000	SURCHARGED
240 minute winter	C3	232	23.075	0.045	3.4	0.0803	0.0000	ОК
240 minute winter	9304	232	23.018	0.043	3.4	0.0000	0.0000	ОК
15 minute winter	0302	1	25.675	0.000	0.0	0.0000	0.0000	ОК
15 minute winter	C1	1	24.435	0.000	0.0	0.0000	0.0000	ОК
15 minute winter	C2	1	24.300	0.000	0.0	0.0000	0.0000	ОК

Link Event	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
15 minute winter	2	3.000	3	42.8	2.941	0.876	0.2181	
240 minute winter	1	2.000	3	3.6	0.189	0.001	65.1379	
240 minute winter	3	2.001	4	4.1	0.158	0.001	22.0060	
240 minute winter	4	Hydro-Brake <sup>®</sup>	C3	3.4				
240 minute winter	C3	1.003	9304	3.4	0.621	0.083	0.0474	77.4
15 minute winter	0302	1.000	C1	0.0	0.000	0.000	0.0000	
15 minute winter	C1	1.001	C2	0.0	0.000	0.000	0.0000	
15 minute winter	C2	1.002	C3	0.0	0.000	0.000	0.1416	





SW DRAINS & MANHOLES	TO BE MAINTAINED BY DEVELOPER UNTIL ADOPTED BY NWL				
MAINTENANCE SCHEDULE	REQUIRED ACTION	FREQUENCY			
REGULAR MAINTENANCE	INSPECT AND IDENTIFY ANY AREAS THAT ARE NOT OPERATING CORRECTLY. IF REQUIRED TAKE REMEDIAL ACTION	MONTHLY FOR 3 MONTHS THEN ANNUALLY			
OCCASIONAL MAINTENANCE	SURVEY INSIDE OF OUTLET PIPES TO CHECK FOR SEDIMENT BUILD UP AND REMOVE IF NECESSARY	EVERY 5 YEARS OR AS REQUIRED			
REMEDIAL ACTIONS	REPAIR PHYSICAL DAMAGE IF NECESSARY	AS REQUIRED			
DENOTES LOCATION OF HYDROBRAKE FLOW RESTRICTION UNIT					

SW DRAINS & MANHOLES	TO BE MAINTAINED BY PROPER INITIAL INSPECTION TO INFORM FUTURE MA SCHEDULE AND FREQUENCY OF REQUIRED	RTY OWNER. INTENANCE ACTIONS.
MAINTENANCE SCHEDULE	REQUIRED ACTION	FREQUENCY
REGULAR MAINTENANCE	INSPECT AND IDENTIFY ANY AREAS THAT ARE NOT OPERATING CORRECTLY. IF REQUIRED TAKE REMEDIAL ACTION	MONTHLY FOR 3 MONTHS THEN ANNUALLY
OCCASIONAL MAINTENANCE	SURVEY INSIDE OF OUTLET PIPES TO CHECK FOR SEDIMENT BUILD UP AND REMOVE IF NECESSARY	EVERY 5 YEARS OR AS REQUIRED
REMEDIAL ACTIONS	REPAIR PHYSICAL DAMAGE IF NECESSARY	AS REQUIRED

HIGHWAY GULLIES	TO BE MAINTAINED BY DEVELOPER UNTIL ADOPTED BY . COMPANY
MAINTENANCE SCHEDULE	REQUIRED ACTION
	INSPECT ACCESS POINTS FOR SILT ACCUMULATION TO ESTABLISH SILT REMOVAL FREQUENCIES
REGULAR MAINTENANCE	INSPECT FOR PONDING ON ROAD CHANNEL — MAY BE CAUSED BY OBSTRUCTION IN KERB DRAIN. REMOVE BY RODDING/JETTING FROM ACCESS POINT OR FROM KERB APERTURE
OCCASIONAL MAINTENANCE	SURVEY INSIDE OUTLET PIPES TO CHECK FOR SEDIMENT BUILD UP AND REMOVE IF NECESSARY
REMEDIAL ACTIONS	REPAIR PHYSICAL DAMAGE IF NECESSARY

MAINTENANCE SCHEDULE       REQUIRED ACTION         MAINTENANCE SCHEDULE       INSPECT ACCESS POINTS FOR SILT ACCUMULATION TO ESTABLISH SILT         REGULAR MAINTENANCE       INSPECT FOR PONDING ON ROAD CHANNEL – MAY BE CAUSED BY OBSTRUCTION IN KERB DRAIN. REMOVE BY RODDING/JETTING FROM ACCESS POINT OR FROM KERB APERTURE         OCCASIONAL MAINTENANCE       SURVEY INSIDE OUTLET PIPES TO CHECK FOR SEDIMENT BUILD UP AND REMOVE IF NECESSARY         REMEDIAL ACTIONS       REPAIR PHYSICAL DAMAGE IF NECESSARY	PRIVATE GULLIES & ACO CHANNELS	TO BE MAINTAINED BY PROPERTY OWNER. INITIAL INSPECTION TO INFORM FUTURE MAINTENANCE SCHEDULE AND FREQUE ACTIONS.
MAINTENANCE SCHEDULE       REQUIRED ACTION         REGULAR MAINTENANCE       INSPECT ACCESS POINTS FOR SILT ACCUMULATION TO ESTABLISH SILT         REGULAR MAINTENANCE       INSPECT FOR PONDING ON ROAD CHANNEL – MAY BE CAUSED BY OBSTRUCTION IN KERB DRAIN. REMOVE BY RODDING/JETTING FROM ACCESS POINT OR FROM KERB APERTURE         OCCASIONAL MAINTENANCE       SURVEY INSIDE OUTLET PIPES TO CHECK FOR SEDIMENT BUILD UP AND REMOVE IF NECESSARY         REMEDIAL ACTIONS       REPAIR PHYSICAL DAMAGE IF NECESSARY	<b>D</b>	
REGULAR MAINTENANCE       INSPECT ACCESS POINTS FOR SILT ACCUMULATION TO ESTABLISH SILT         REGULAR MAINTENANCE       INSPECT FOR PONDING ON ROAD CHANNEL – MAY BE CAUSED BY OBSTRUCTION IN KERB DRAIN. REMOVE BY RODDING/JETTING FROM ACCESS POINT OR FROM KERB APERTURE         OCCASIONAL MAINTENANCE       SURVEY INSIDE OUTLET PIPES TO CHECK FOR SEDIMENT BUILD UP AND REMOVE IF NECESSARY         REMEDIAL ACTIONS       REPAIR PHYSICAL DAMAGE IF NECESSARY	MAINTENANCE SCHEDULE	REQUIRED ACTION
REGULAR MAINTENANCE       INSPECT FOR PONDING ON ROAD CHANNEL – MAY BE CAUSED BY OBSTRUCTION IN KERB DRAIN. REMOVE BY RODDING/JETTING FROM ACCESS POINT OR FROM KERB APERTURE         OCCASIONAL MAINTENANCE       SURVEY INSIDE OUTLET PIPES TO CHECK FOR SEDIMENT BUILD UP AND REMOVE IF NECESSARY         REMEDIAL ACTIONS       REPAIR PHYSICAL DAMAGE IF NECESSARY		INSPECT ACCESS POINTS FOR SILT ACCUMULATION TO ESTABLISH SILT REMOVAL FREQUENCIES
OCCASIONAL MAINTENANCE       SURVEY INSIDE OUTLET PIPES TO CHECK FOR SEDIMENT BUILD UP AND REMOVE IF NECESSARY         REMEDIAL ACTIONS       REPAIR PHYSICAL DAMAGE IF NECESSARY	REGULAR MAINTENANCE	INSPECT FOR PONDING ON ROAD CHANNEL – MAY BE CAUSED BY OBSTRUCTION IN KERB DRAIN. REMOVE BY RODDING/JETTING FROM ACCESS POINT OR FROM KERB APERTURE
REMEDIAL ACTIONS REPAIR PHYSICAL DAMAGE IF NECESSARY	OCCASIONAL MAINTENANCE	SURVEY INSIDE OUTLET PIPES TO CHECK FOR SEDIMENT BUILD UP AND REMOVE IF NECESSARY
	REMEDIAL ACTIONS	REPAIR PHYSICAL DAMAGE IF NECESSARY

		PERMEABLE PAVING	TO BE MAINTAINED BY PROPERTY OWNER. INITIAL INSPECTION TO INFORM FUTURE MAINTENANCE SCHEDULE AND FREQUENCY OF REQUIRED ACTIONS.		
		MAINTENANCE SCHEDULE	REQUIRED ACTION	FREQUENCY	
-		REGULAR MAINTENANCE BRUSHING AND VACUUMING (STANDARD COSMETIC SWEEP OVER WHOLE SURFACE)			
		OCCASIONAL MAINTENANCE	STABILISE AND MOW CONTRIBUTING AND ADJACENT AREAS.	AS REQUIRED	
			REMOVAL/MANAGEMENT OF WEEDS USING GLYPHOSPATE APPLIED DIRECTLY INTO THE WEEDS BY AN APPLICATOR RATHER THAN SPRAYING	AS REQUIRED. ONCE PER YEA ON INFREQUEN USED PAVEMEN	
			REMEDIATE ANY LANDSCAPING WHICH HAS BEEN RAISED TO WITHIN 50MM OF THE LEVEL OF THE PAVING.	AS REQUIRED	
-		REMEDIAL ACTIONS	REMEDIAL WORK TO ANY DEPRESSIONS, RUTTING AND CRACKED/BROKEN BLOCKS CONSIDERED DETRIMENTAL TO THE STRUCTURAL PERFORMANCE OR A HAZARD TO USERS AND REPLACE LOST JOINTING MATERIAL.	AS REQUIRED	
			REHABILLITATION OF SURFACE AND UPPER SUBSTRUCTURE BY REMEDIAL SWEEPING	EVERY 10–15 YEARS OR AS REQUIRED.	

CATCHPITS	TO INITIAI SCHEI
MAINTENANCE SCHEDULE	REQU
REGULAR MAINTENANCE	INSPE ACCU REMO
OCCASIONAL MAINTENANCE	REMO
REMEDIAL ACTIONS	REPAI





CLASS S BEDDING	CLASS Z BEDDING		
NOMINAL SIZE OF PIPE DN(mm)	RECOMMENDED OVERALL TRENCH WIDTH Bd(m)	PIPE BEDDING REQUIREMENT (mm)	
150	0.60	10 OR 14 NOM. SINGLE SIZE OR 14 TO 5 GRADED	
225	0.70	10, 14 OR 20 NOM. SINGLE SIZE OR 14 TO 5 GRADED	
300	0.85	OR 20 TO 5 GRADED	



#### NOTES -CONT....

12. Where two pipelines cross with less than 300mm cover, surround each pipe with a full concrete bed and surround (class Z detail) for not less than 1m centered on the crossing and extended as required to within 150mm of the nearest flexible joint.

- 13. Selected backfill material shall consist of uniform soil, free from stones larger than 40mm, clay lumps larger than 75mm, tree roots, contaminated material. Selected backfill material is to be placed in layers not exceeding 150mm thickness. Should the excavated material be unsuitable or weather conditions affect the materials stability, then a suitable hard granular material shall be used.
- 14. No mechanical compaction of fill material shall be permitted within 300mm above the barrel/crown of the pipe.
- 15. General backfill to drainage trenches in vehicular trafficked areas above the pipe bedding detail, shall be suitably selected material (in accordance with BS: 8301 clause 5.7.6.1.) and be placed in layers not exceeding 225mm, each layer compacted to form a stable trench backfill, should the material be unsuitable or weather conditions affect the materials stability, then a hard granular material shall be used up to formation level.
- 16. All separators shall be in accordance with the environment agency document PPG3.
- 17. All below ground plastic/grp tanks shall be installed in accordance with the manufacturers instructions. They shall be provided with sufficient concrete surround to counter floatation and shall have a wall thickness adequate to resist the highest ground water level which could be encountered at their location.
- 18. All excavations in areas of high water tables and granular materials with high sand/silt contents shall be wrapped with a suitable geotechnical filter membrane to prevent migration of sands/silts. Full height clay stanks across trenches and/or at manhole locations at 25m intervals to restrict water movement along the excavation shall be provided.
- 19. Where utility/land drainage trenches etc cross over drainage trenches, the contractor shall construct an impermeable barrier to prevent groundwater infiltrating into the drainage trench.
- 20. Non-man entry access chambers shall comply with the relevant provisions of BS:EN 752-3.

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that which a competent contractor should be aware.

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Contractors should refer to the residual risks contained in the CDM Pre Construction Information before carrying out any site operations and should not issue parts of this drawing without including the CDM notes and references. This information will include details of the SIGNIFICANT risks which 3E have considered beyond

NOTES -

- This drawing is to be read in conjunction with all relevant 3E, architect and M&E consultants drawings and project specifications.
- 2. All building drainage works shall be carried out in accordance with the relevant parts of BS EN:752 'Drains and Sewer Systems Outside Buildings', the current building regulations and the local authority building control specifications and requirements.
- All insitu and precast concrete products shall comply with class DS1 requirements for sulphate exposure in accordance with BRE Special Digest 1, Concrete in Aggressive Ground (2001) Part 1: Table 2.
- All precast concrete products shall comply with the relevant provisions of BS:5911 and be Kitemarked. All precast concrete pipes shall be class 120 and comply with the requirements of note 3 above.
- All vitrified clay pipes and fittings shall comply with the relevant provisions of BS EN:295 and BS 65 respectively and be Kitemarked, all pipes shall be extra strength to BS 65 or equivalent BS EN:295 pipe crushing strength and be of a sleeved system.
- All u-PVC pipes and fittings shall comply with WIS 4-35-01 and shall be kitemarked.
- Manhole covers and frames shall comply with the relevant provisions of BS EN:124, have 675x675 clear openings unless otherwise specified and be of non-rocking design without cushion inserts and be Kitemarked. Load class D400 in trafficked areas and load class B125 in footways, landscaped and pedestrian areas. where required, covers shall be recessed to receive the architects specified finish.
- B. Gully grates and frames shall comply with the relevant provisions of BS EN:124 and be of non-rocking design with captive hinge access and be Kitemarked. Load class D400 in industrial estate roads and areas carrying regular heavy traffic and load class C250 in estate roads and car parking areas. In all road locations, the grate shall be hinged on the side of the traffic direction (left hand opening).
- 9. All external rigid pipework shall be laid with a class S pipe bedding detail with 1.2m minimum cover to the pipe barrel under vehicular trafficked areas, 0.9m cover under fields and 0.6m cover under footways/gardens. Where cover is less than that stated, a class A pipe bedding detail shall be used on pipes 225dia and larger, for pipes less than 225dia use a class Z pipe bedding detail. Under buildings a class S pipe bedding detail shall be used. Where there is less than 300mm between the barrel of the pipe and the underside of the structural floor slab, the pipe shall be cast integral with the floor slab with 150mm minimum concrete surround with vertical reinforcement tied into the slab.
- 10. All u-PVC pipework shall be laid with a class T pipe bedding detail with 1.2m minimum cover to the pipe barrel under vehicular trafficked areas, 0.9m cover under fields and 0.6m cover under footways/gardens. Where cover is less than that stated a class Q pipe bedding detail shall be used.
- Where concrete protection is required to pipework, the concrete shall be discontinued at each pipe joint over the full cross section of the concrete by means of a shaped compressible filler.

ES	CLASS B ENGINEERING BRICKS (2No. COURSES MIN 4 COURSES MAX), SET IN CLASS 1 MORTOR								
	PRECAST CONCRETE SLAB	25/01/22 Date	Revisions	F	PRELIMINARY	(ISSUE		JF Drawn	P1 Rev.
	1260Ø WITH 600 X 600MM OPENING	Purpose of	Issue	PRE	LIMIN	IARY		Drawing Sta	tus
	GAP BETWEEN SLAB AND RESTRICTOR CAP TO BE FOAMED FILLED	6 Bento Bennet Horbur Wakefi t 0192	on Office Parl t Ave, y, eld 24 240 420	k	2		Sir Bobby Newcas	2 Esh F Robson Great tle upon NE13	Plaza Way Park Tyne 9BA
	RESTRICTOR CAP 6D930 WITH 350MM OPENING AND SEALING RING 5000TW117	wakefie WW De 8 Devo Londor	eld@3econsu evonshire, nshire Squar	ult.com re	consulting	g engineers	t 0 newcastle@3	191 230 : Seconsult	2993 .com
	-SILT TRAP SHAFT	EC2M t 0750 london	4PL 00 121 181 @3econsult.c	com	www.sec	onsuit.com			
	150Ø INLET PIPE	Client	MR HAF	RJIT S	SINGH	DEOL			
	ч <sup>2</sup> т ч <sup>2</sup> т ч	Project	BARRIN BEDLIN	IGTO IGTO	N ROA N	D			
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AP / SUMP		Scale 1:2	20	Author	JF	Checked MP	Date J/	AN 2022	
ETAIL		Job Number	er 6-001-	Originator <b>3E -</b>	Zone Level	Type F	Role Drawing N	o. Rev ) <b>1 - P</b>	1

![](_page_31_Figure_0.jpeg)

### NOTES -CONT ...

- 11. Where concrete protection is required to pipework, the concrete shall be discontinued at each pipe joint over the full cross section of the concrete by means of a shaped compressible filler.
- 12. Where two pipelines cross with less than 300mm cover, surround each pipe with a full concrete bed and surround (class Z detail) for not less than 1m centered on the crossing and extended as required to within 150mm of the nearest flexible joint.
- 13. Selected backfill material shall consist of uniform soil, free from stones larger than 40mm, clay lumps larger than 75mm, tree roots, contaminated material. Selected backfill material is to be placed in layers not exceeding 150mm thickness. Should the excavated material be unsuitable or weather conditions affect the materials stability, then a suitable hard granular material shall be used.
- 14. No mechanical compaction of fill material shall be permitted within 300mm above the barrel/crown of the pipe.
- 15. General backfill to drainage trenches in vehicular trafficked areas above the pipe bedding detail, shall be suitably selected material (in accordance with BS 8301 clause 5.7.6.1.) and be placed in layers not exceeding 225mm, each layer compacted to form a stable trench backfill, should the material be unsuitable or weather conditions affect the materials stability, then a hard granular material shall be used up to formation level.
- 16. All separators shall be in accordance with the environment agency document PPG3.
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- 19. Where utility/land drainage trenches etc cross over drainage trenches, the contractor shall construct an impermeable barrier to prevent groundwater infiltrating into the drainage trench.
- 20. Non-man entry access chambers shall comply with the relevant provisions of BS EN:752-3.

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before carrying out any site operations and should not issue parts of this drawing without including the CDM notes and references. This information will include details of the SIGNIFICANT risks which 3E have considered beyond that which a competent contractor should be aware.

#### NOTES

- . This drawing is to be read in conjunction with all relevant 3E, architect and M&E consultants drawings and project specifications.
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- All vitrified clay pipes and fittings shall comply with the relevant provisions of BS EN:295 and BS 65 respectively and be Kitemarked, all pipes shall be extra strength to BS 65 or equivalent BS EN:295 pipe crushing strength and be of a sleeved system.
- All u-PVC pipes and fittings shall comply with WIS 4-35-01 and shall be kitemarked.
- Manhole covers and frames shall comply with the relevant provisions of BS EN:124, have 675x675 clear openings unless otherwise specified and be of non-rocking design without cushion inserts and be Kitemarked. Load class D400 in trafficked areas and load class B125 in footways, landscaped and pedestrian areas. where required, covers shall be recessed to receive the architects specified finish.
- . Gully grates and frames shall comply with the relevant provisions of BS EN:124 and be of non-rocking design with captive hinge access and be Kitemarked. Load class D400 in industrial estate roads and areas carrying regular heavy traffic and load class C250 in estate roads and car parking areas. In all road locations, the grate shall be hinged on the side of the traffic direction (left hand opening). All grates to have pedestrian covers.
- 9. All external rigid pipework shall be laid with a class S pipe bedding detail with 1.2m minimum cover to the pipe barrel under vehicular trafficked areas, 0.9m cover under fields and 0.6m cover under footways/gardens. Where cover is less than that stated, a class A pipe bedding detail shall be used on pipes 225dia and larger, for pipes less than 225dia use a class Z pipe bedding detail. Under buildings a class S pipe bedding detail shall be used. Where there is less than 300mm between the barrel of the pipe and the underside of the structural floor slab, the pipe shall be cast integral with the floor slab with 150mm minimum concrete surround with vertical reinforcement tied into the slab.
- 10. All u-PVC pipework shall be laid with a class T pipe bedding detail with 1.2m minimum cover to the pipe barrel under vehicular trafficked areas, 0.9m cover under fields and 0.6m cover under footways/gardens. Where cover is less than that stated a class Q pipe bedding detail shall be used.

25/01/22	PRELIMINARY ISSUE	JF	P1	
Date Purpose of		Drawn Drawing Sta	Rev. atus	
	PRELIMINARY	-		
6 Benton Office Park Bennett Ave, Horbury, Wakefield □ t 01924 240 420 wakefield@3econsult.com WW Devonshire, 8 Devonshire Square London EC2M 4PL □ t 07500 121 181 Iondon@3econsult.com				
Client MR HARJIT SINGH DEOL				
Project BARRINGTON ROAD BEDLINGTON				
TITE PERMEABLE PAVING CONSTRUCTION DETAILS				
Scale 1:2	20 Author Checked Date JF JA	N 2022		
Job Number Originator Zone Level Type Role Drawing No. Rev P21-484-3E - ZZ-XX-DR-C-1202-P1				

POROUS PAVING BEDDING AND JOINTING LAYER SPECIFICATION (2/6.3 TO BS7533-13:2009

SIEVE SIZE (mm)	PERCENTAGE PASSING
14	100
10	90-100
6.3	80-99
2.0	0-20
1.0	0-5

THE MATERIAL SHOULD ALSO MEET DURABILITY REQUIREMENTS IN BS 7533-13:2009

AL GRADING REQUIREMENTS FOR POROUS PAVING BASE AGGREGATES (COARSE AGGREGATE 4/20)				
SIEVE SIZE (mm)	PERCENT PASSING			
80	-			
63	-			
40	100			
31.5	98-100			
20	90-99			
10	25-70			
4	0-15			
2	0-5			
1	_			

Appendix E

![](_page_33_Picture_0.jpeg)

Northumbrian Water Developer Services Leat House Pattinson Road Washington NE38 8LB

 Ext:
 96646

 Direct Line:
 0191 419 6646

 Email:
 developmentenquiries@nwl.co.uk

 Our Ref:
 212811410054

Friday, 07 January 2022

3E Consulting Engineers 2 Esh Plaza Sir Bobby Robson Way Great Park Newcastle upon Tyne NE13 9BA

Dear Matthew,

#### Re: Pre-Planning Enquiry – Barrington Road, Choppington, Northumberland NE22 7AP

Further to the Point of Connection Application for the above site, received January 4<sup>th</sup> 2022, we are now able to provide the following response.

We have based our response on the information in your application and accompanying correspondence. Therefore, should any of the information now be different, then you must ensure that you inform us of any changes as further Network Modelling may be required and our response may also change, leading to this response being invalid.

Northumbrian Water assesses the impact of the proposed development on our assets and assesses the capacity within our network's to accommodate and treat the anticipated flows arising from the development. We do not therefore offer comment on aspects of planning applications that are outside of our area of control.

Enclosed in this response is a scaled plan showing the **approximate** position of the water and sewerage networks within the vicinity of this site.

We have changed the way contractors and developers can access our assets.

Historically only our own staff and framework contractors could access our sewerage network. As of 1st January 2018, we are allowing third party contractors to access our sewer network on a site by site basis, subject to certain conditions.

Further information (including how to apply) is available from our web site - <u>https://www.nwl.co.uk/services/developers/developer-sewerage-services/</u>

Also enclosed is our extract showing locations within the approximate vicinity of this site that have, from our records, experienced flooding. This has been provided to demonstrate the known flood risks within the vicinity which have been considered as part of our assessment on this enquiry.

We have also carried out a review of your application and can confirm the following:

![](_page_33_Picture_16.jpeg)

#### Sewerage and Sewage Treatment

Northumbrian Water would ask that you please separate the foul and surface water flows in accordance with Part H of the Building Regulations prior to the final connection to the public sewer.

All new connections to the public sewerage system must first be approved through the Section 106 of the Water Industry Act 1991 process prior to construction.

Should you decide to proceed with this development, a fully completed Sewer Connection application form will be required. These are available to download from the following link:

https://www.nwl.co.uk/services/developers/developer-sewerage-services/new-sewer-connectionss106/

• Foul Water Discharge

The foul flows can discharge without restriction into the **225mm** diameter **combined** public sewer to the western boundary of the site via manhole **9303.** 

• Surface Water Discharge

No surface water flow from the proposed development will be allowed to connect into the existing public sewerage system unless it is proven that the alternative options which are listed within Part H of the Building Regulations 2003 are not available:

Rainwater from a system provided pursuant to sub-paragraphs (1) or (2) shall discharge to one of the following, listed in order of priority –

(a) an adequate soakaway or some other adequate infiltration system; or, where that is not reasonably practicable,

(b) a watercourse; or, where that is not reasonably practicable,

(c) a sewer.

In this instance we have identified that the surface water flow should discharge directly to the watercourse to the west of Barrington Cottage. We therefore suggest that you contact either the Environment Agency or Lead Local Flood Authority, as appropriate, to discuss this in further detail.

Written approval for all individual connections (direct or indirect) to the public sewerage system should be obtained through the Section 106 process, following completion of the detailed drainage design and before the commencement of any drainage works on site.

• Protection of Existing Sewerage Assets

We wish to draw your attention to the existing sewer which passes through the site. This sewer could be diverted, protected or accommodated within your site layout with an appropriate easement.

Part H of the Building Regulations also details the reasons why Northumbrian Water does not permit buildings to be built over or near to its sewerage network:

- Undue risk in the event of failure of the drain or sewer
- Maintaining access
- Protection of the drain or sewer during construction
- Protection from settlement
- Protection against piling

To discuss the diversion of this asset in further detail, please contact:

Graeme Telford 0191 419 6620 graeme.telford@nwl.co.uk

To discuss the protection of this asset in further detail, please contact:

Niki Mather 0191 419 6603 07764 359220

• Sewage Treatment Capacity

The Sewage Treatment Works to which this development finally discharges to is able to accept the additional flows.

Please note that this response is valid for 1 year only and you should resubmit your proposals should this period lapse prior to your development beginning.

Should you require any further assistance or information, then please do not hesitate to contact me at <u>developmentenquiries@nwl.co.uk</u> or alternatively on 0191 419 6646, please quote our reference number above in any future correspondence.

Yours sincerely,

S. Roberts

Laura Roberts Technical Support Advisor Developer Services

![](_page_36_Figure_0.jpeg)

![](_page_37_Figure_0.jpeg)

#### Company Information

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