## Jacobs

Bishop Auckland Bus Station and Car Park

DRAINAGE STRATEGY REPORT
BL000034-JAC-XX-XX-RP-C-00001 | P01
16/12/22

Bishop Auckland Bus Station and Car Park

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Contents

1. Introduction ..... 2
2. Site Description ..... 3
3. Soil Conditions ..... 4
4. Flood Risk ..... 5
5. Foul Water Drainage Strategy ..... 6
6. Surface Water Drainage Strategy ..... 7
7. Sustainable Urban Drainage Systems (SUDS) ..... 8
8. Pollution Prevention ..... 9
9. Maintenance. ..... 11
10. Conclusion ..... 13
Appendix A. EA Flood Mapping
Appendix B. Greenfiled Runoff Estimation
Appendix C. Drainage Strategy
Appendix D. Sewer Records
Appendix E. Hydraulic Calculations
Appendix F. AquaTreat Interceptor Certificates
Appendix G. Topo Survey
Appendix H. Scheme Drawings
Appendix I. Maintenance Schedule
Figure 1: Ground Profile ..... 4
Figure 2: Pollution Hazard Indices ..... 9
Figure 3: Pollution Mitigation Indices ..... 9

## 1. Introduction

The purpose of this report is to present the basis of the foul and surface water drainage design proposals associated with a new bus station and car park in Bishop Auckland.

This project forms part of the wider regeneration of Bishop Auckland town centre. The proposed bus station and car park will be constructed in the location of the existing bus station, near the historical town centre. The bus station will provide improved facilities for tourists and locals. The carpark will provide parking provision for an anticipated increase in tourists as a result of several attractions currently under development in the town.

## 2. Site Description

The project site is situated toward the north of Bishop Auckland. The site is bound to the north by Clayton Street, to the east by the existing Newgate shopping centre, to the south by Saddler Street and the A689 to the west.

The existing project site is composed of an external bus station to the north, at grade carpark to the south and pedestrianised area to the east adjacent to the Newgate Centre. The site is predominantly hard paved with a small number of raised planters/tree pits in the pedestrian area close to the shopping centre.

The topographical survey indicates site levels fall significantly from west to east with a level difference across the site of approximately 6 m .
3. Soil Conditions

The following sources of information have been used to provide historical borehole information:
-BGS Geolndex Onshore website

- BGS Maps Portal
- Coal Authority's Interactive Viewer

According to the BGS records, in the area of the proposed car park and bus station building, there are only records of shallow geotechnical investigation information of up to 3 m in depth, undertaken for the purpose of the existing open space car parking and bus station. Therefore, deep exploratory holes located on the east side of the proposed site, namely NZ22NW 174, NZ22NW176 and NZ22NW 177, were mainly used to determine the ground model.

According to BGS (Bedrock geology 1:50:000), the site is underlined by Pennine Middle Coal Measures Formation. It comprises of interbedded grey mudstone, siltstone, pale grey sandstone and commonly coal seams, with a bed of mudstone marine fossils at the base, and several such marine fossil-bearing mudstones in the upper half of the unit. The site surface is covered by superficial deposits according to BGS (superficial geology 1:50:000), described as Devensian Till. All nearby historical boreholes were drilled within this formation proven to be extent up to 26 m depth.

The ground profile below (Figure 1) is mainly derived from the information on borehole log NZ22NW176 since it is the most adjacent to the proposed site works and presents the least favourable profile with the competent boulder clay layer encountered at greater depths. Field and laboratory tests were assessed from the aforementioned boreholes to derive the engineering properties summarized in the table below. The water table was assumed 3.00 m BGL according to the borehole records.

Intrusive soil investigations are to be carried out as part of the preliminary works. These investigations will include infiltration testing and groundwater monitoring to help determine the feasibility and suitability of using infiltration techniques within the overall drainage strategy at detailed design stage.

| Level $(\mathrm{mbgl})$ | Thickness <br> $(\mathrm{m})$ | Unit Weight <br> $\mathrm{kN} / \mathrm{m} 3$ | $\varphi^{\prime}(0)$ | $\mathrm{Cu}(\mathrm{kPa})$ | $\mathrm{E}(\mathrm{MPa})$ |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | From | To |  |  |  |  |  |
| Made Ground | 0.0 | 1.6 |  | 18 | 30 |  | 20 |
| Sand | 1.7 | 8.7 | 7.0 | 19 |  | 40 | 20 |
| Clay | 8.7 | 14.0 | 5.3 | 18 | 30 |  | 20 |
| Sand | 14.0 | 16.0 | 2.0 | 20 |  | 130 | 65 |
| Boulder clay | 16.0 | 22.0 | 6.0 | 19 |  | 100 | 50 |
| Clay | 22.0 | 24.5 | 2.5 | 35 |  | 50 |  |
| Sand | 24.5 | 26.0 | Not Proven | 18 | 35 |  |  |

Figure 1: Ground Profile

## 4. Flood Risk

Fluvial:
In accordance with the Environment Agency's indicative online flood maps, the Site is located within a Flood Zone 1 area, which is classed as having less than 1 in $1000(<0.1 \%)$ chance of river flooding in any one year.

In accordance with Table 3 of the NPPF Technical Guidance all forms of development are considered appropriate within zone 1.

Please refer to Appendix A for EA Flood Map.

## Surface Water:

The George Street/S addler Street junction at the south-eastern corner of the site is susceptible to 'low risk' flooding from surface water according to the Long-Term Flood R isk information available on Gov.uk.

Low risk means that each year this area has a chance of flooding of between $0.1 \%$ and1\%. Flooding from surface water is difficult to predict as rainfall location and volume are difficult to forecast. In addition, local features can greatly affect the chance and severity of flooding.

This is the lowest corner of the site and therefore surface water flooding in this area is unlikely to affect the proposed development, as any surface water flooding will flow overland in a southerly direction along George Street and away from the development.

## Reservoir:

In accordance with the Environment Agency's indicative online flood maps, the Site is not located in an area at risk of flooding from reservoirs.

## Local Drainage System Failure:

As noted in Section 6 of this report, the existing site discharges surface water at uncontrolled rates to the surrounding infrastructure. The proposed development will restrict surface water flows from the new development to equivalent greenfield runoff rates, offering a substantial load reduction on the receiving network and increased capacity downstream.

In the event of total failure of the existing network, overland flows from the site would flow to the lowest point in the southeastern corner towards George Street.

## Ground Water:

According to the Durham County Councils Preliminary Flood Risk Assessment (PRFA) May 2016, no records of groundwater flooding have been found within the County of Durham.

The PFRA reports that in 2004, Defra commissioned J acobs to carry out a detailed investigation into areas of potential 'groundwater emergence' throughout England. This study concluded that there were no areas of predicted groundwater flooding within this area.

The PFRA notes that there is a long history of coal mining within the northeast region, and it is understood that mine dewatering has recently ceased in some areas. This may lead to an increase in groundwater levels within historical mining areas of the County. The PFRA concludes (from strategic perspective) that there is a high level of uncertainty as to the long-term impacts of the cessation of dewatering upon groundwater levels, and there is no evidence that groundwater flooding will ensue.
5. Foul Water Drainage Strategy

## Existing:

The Northumbrian Water asset records indicate an adopted combined sewer network which surrounds the site on all four sides.

The existing foul drainage network within the site is limited. The topographical survey indicates foul connections serving the small building containing facilities for the bus operators, the public toilet block and a small retail outlet which serves food and drinks.

All three of these facilities are shown to discharge to the existing combined sewer network along the northern boundary of the development site adjacent to Clayton Street.

## Proposed:

The proposed bus station building forming part of the redevelopment scheme will contain public toilet facilities, staff toilet facilities and a small retail outlet. It is proposed to discharge foul flows from this building to the combined sewer network in Clayton Street via an indirect connection. (Indirect connection subject to the results of a line, level and condition survey of the existing lateral).

Proposed discharge rates and point of connection are subject to Northumbrian Waters approval.
Please refer to Appendix C for Drainage Strategy Layout

## 6. Surface Water Drainage Strategy

## Existing:

Survey information indicates that the surface water runoff from the existing site is positively drained via surface level gullies and a below ground gravity pipe network. The existing surface water network is shown to fall from west to east eventually discharging to the existing combined sewer network at the corner of Saddler Street/G eorge Street to the south-eastern corner of the site.

There is no indication or evidence of attenuation features or flow control structures in place within the existing surface water network. It is assumed that surface water runoff currently discharges unrestricted to the surrounding infrastructure.

## Proposed:

It is proposed to maintain similar flow paths in line with the existing site. Surface water flows will be conveyed west to east via a below ground gravity piped network and discharge to the existing surface water lateral that serves the existing site.

In accordance with requirements of Durham County Councils Surface Water Management Plan (SWMP), it is proposed to restrict peak flows from the new development to equivalent greenfield runoff rates. Please refer to Appendix B for greenfield runoff estimation calculations

Due to the large level difference across the site, it is proposed to cascade the network with several flow controls and associated below ground attenuation at both the higher parking area to the west and at the bus station turning area to the east.

Peak flows from the proposed development will be restricted to less than or equal to the equivalent greenfield runoff rates for the respective 1 in 1 yr , 1 in 30 yr and 100 yr return period events using a complex control chamber.

Attenuation will be provided to accommodate all storms up to and including the 100 yr RP event with an additional $45 \%$ allowance for climate change.

There are a number of existing road gullies serving Saddler Street carriageway which are assumed to discharge to the existing on-site surface water drainage network. It is therefore proposed to introduce a new highway carrier drain in Saddler Street to serve all of the existing road gullies to separate the highway drainage from the new on-site drainage network.

Proposed discharge rates and points of connection are subject to Northumbrian Waters approval.
Please refer to Appendix C for Drainage Strategy Layout

## 7. Sustainable Urban Drainage Systems (SUDS)

It is proposed to implement a number of SUDS elements into the new surface water drainage scheme as outlined below:

Green Roof:
The roof above the bus station concourse area will utilise a sedum roof construction. R unoff from the green roof will subsequently discharge directly to the rain garden features to the north of the bus station.

## R ainwater Harvesting:

The area of flat roof above the bus station accommodation block will collect and convey water to a rainwater harvesting system for reuse in the bus station facilities.

## R ain Garden:

It is proposed to introduce a rain garden feature to the north of the bus station building. Flows from the green roof, overflow from the rainwater harvesting system, and localised hardstanding areas in the immediate vicinity north of the bus station building will be conveyed into the rain garden. There are also a number of smaller rain gardens to collect and convey runoff to the pedestrian area between the bus station and ground level car parking area. For the purposes of the preliminary design, it has been assumed at this stage that the rain gardens will be tanked with an impermeable liner. Intrusive soil investigations to be carried out as part of the preliminary works will include infiltration testing and groundwater monitoring to help determine the feasibility and suitability of using infiltration techniques within the overall drainage strategy.

## Permeable Paving:

The parking bays to the ground level parking area to the west of the site will be constructed of permeable block paving. For the purposes of the preliminary design, it has been assumed at this stage that the permeable parking bays will be tanked with an impermeable liner. Intrusive soil investigations to be carried out as part of the preliminary works will include infiltration testing and groundwater monitoring to help determine the feasibility and suitability of using infiltration techniques within the overall drainage strategy.

## 8. Pollution Prevention

Compliance with the requirements of the simple index approach to pollution control outlined in Chapter 26 of the CIRIA SUDS Manual C 753 is summarized below:

| Land Use | Pollution Hazard <br> Level | Total Suspended <br> solids (TSS) | Metals | Hydro-Carbons |
| :---: | :---: | :---: | :---: | :---: |
| Commercial yard <br> and delivery areas | Medium | 0.7 | 0.6 | 0.7 |

Figure 2: Pollution Hazard Indices
Due to the size, layout, and topographical profile; the pollution mitigation process will be via a treatment management train formed of several propriety systems.

## Trapped Gully Pots:

Within the access road to the west and bus turning area to the east, surface water will be drained via a series of trapped gully outlets. Trapped gullies will offer mitigation against the first flush and trap sediment/small oil spills within the gully pot. They are easily accessible and readily maintainable. Gully pots alone do not achieve the required mitigation indices in line with the requirements of the SUDS manual for the given land use.

## Permeable Paving (Parking Bays):

All parking bays within the ground level car park are to be formed using permeable block paving. The SUDS Manual (CIRIA, 2015) recognises the effectiveness of concrete block permeable paving in removing pollution. For areas with low to medium pollution hazard level permeable block paving is more than sufficient on its own to provide an adequate pollution mitigation index.

## Catchpits:

The flow control chambers used to limit peak flows to acceptable rates will be formed with a sump to aid sediment removal prior to the attenuation tank system, flow control device and downstream treatment system.

## Oil Separator:

All run-off from the proposed development site will pass through a full retention separator such as the Klargester AquaTreat system or similar approved. The AquaTreat Full R etention GRP surface water treatment separators have been designed for use in SuDS schemes that require a full pollution treatment. This system helps to reduce pollution by removing TSS, Metals \& Hydrocarbons from surface water entering the local watercourse or network.

| Proprietary <br> Treatment System | Total Suspended <br> solids (TSS) | Metals | Hydro-Carbons |
| :---: | :---: | :---: | :---: |
| AquaTreat SWT010 | 0.85 | 0.75 | 0.99 |

Figure 3: Pollution Mitigation Indices
Please refer to Appendix F for AquaTreat Interceptor Mitigation certificates

By incorporating the above measures through a treatment management train approach, the receiving watercourse will be protected from excessive deposits of suspended solids, metals and hydro-carbons.
9. Maintenance

## Management

SUDS management proposals will need to involve a framework for the maintenance of the Site, considering the SUDS, how the Site will change with time, and the operations required to achieve the management aims for the Site, particularly having regard to:

The function of SUDS.
How and why they work on the Site.
Health and safety issues.
Long-term expectations for the SUDS on Site.

## Programme

SUDS maintenance should comprise:
Regular maintenance - for day-to-day care of the SUDS
Litter collection.
Vegetation pruning.
Inspection of inlets, outlets and control structures.
These activities are normally carried out monthly to coincide with regular landscape maintenance.
Occasional tasks - to manage silt and vegetation:
Silt control on hard surfaces, in silt traps and in general SUDS features.
The occasional task activities are to be undertaken on a frequency determined by regular inspection or specification.

Remedial work - to repair unforeseen defects that occur during the design life of the system due to damage or vandalism. Remedial action due to failure or damage will be required on an as necessary basis but should be minimal with good design, maintenance and the control of water flows through the development.

## General

For this scheme, it is assumed that all parts of the drainage system are to be owned and maintained by the Site owner/operator, Durham County Council.

The below-ground surface water drainage system requires regular inspection/clearing to prevent blockages due to accumulation of silt. It is recommended that the following items are initially inspected and cleared by a suitably trained person in accordance with the outline maintenance schedule in Appendix I to establish a longterm inspection/clearing interval appropriate for this site.

Trapped gullies
Drainage channels

Catchpit chambers
Flow Control Devices

Attenuation Tanks
Petrol Interceptors
Rain Gardens

Permeable Paving
Outfall pipes to the public sewers
Inspection/clearing should also be carried out after every major storm event.

## Maintenance Schedule

A preliminary maintenance schedule for this site can be found in Appendix I
This schedule is intended to give an overview of the operation and maintenance for the drainage features included within the proposed drainage strategy. Where proprietary products are specified the manufacturer's instructions and recommendations should be followed.

The recommended operations and frequencies are typical only and should be more frequent initially to ensure that there are no unforeseen issues with the operation of the system. These activities and their frequency can then be adjusted to suit the specific site requirements.
10. Conclusion

In accordance with the Environment Agency's indicative flood map the Site is located within a Flood Zone 1 area, which is classed as having less than 1 in $1000(<0.1 \%)$ chance of river flooding in any one year.

In accordance with Table 3 of the NPPF Technical Guidance all forms of development are considered appropriate within zone 1.

The surface water system to serve the proposed development will follow best practice using sustainable drainage systems (SUDS) to both intercept storm water at source and treat the runoff from roofs, hardstandings and other impermeable areas.

Preliminary soil information as documented in Section 3 of this report indicates a thick band of sand at reasonably shallow depths which may be conducive to infiltration and/or partial infiltration methods for the disposal of surface water runoff. However, the ground profile notes a potential layer of made ground in the near surface formation. Borehole logs also note the possibility of relatively high groundwater levels. F or the purpose of the preliminary hydraulic design and ensuring adequate spacial provisions for SUDS within the scheme design, infiltration methods have not been considered at this stage. Intrusive soil investigations are to be carried out as part of the preliminary works. These investigations will include infiltration testing and groundwater monitoring to help determine the feasibility and suitability of using infiltration techniques within the overall drainage strategy at detailed design stage.

Peak flows from the proposed development will be restricted to less than or equal to the equivalent greenfield runoff rates for the respective 1 in 1 yr , 1 in 30 yr and 100 yr return period events using a complex control chamber. The SUDS systems will be designed to accommodate all storms up to and including the 100 yr RP event with a $45 \%$ allowance for climate change. Unaffected areas within the site planning boundary will remain unchanged and continue to discharge as existing.

By incorporating the above measures, the Proposed Development complies with the requirements of the National Planning Policy Framework by protecting the users of the development and reducing the flood risk to third parties beyond the Site. Appropriate levels of treatment will be provided within the combination of proposed SUDS measures to minimise the risk of contamination to the receiving watercourse.

Appendix A. EA Flood Mapping

# Flood map for planning 

| Your reference | Location (easting/northing) | Created |
| :--- | :--- | :--- |
| Bishop Auckland | 420888/529963 | 13 Dec 2022 9:41 |

## Your selected location is in flood zone 1, an area with a low probability of flooding.

## You will need to do a flood risk assessment if your site is any of the following:

- bigger that 1 hectare (ha)
- In an area with critical drainage problems as notified by the Environment Agency
- identified as being at increased flood risk in future by the local authority's strategic flood risk assessment
- at risk from other sources of flooding (such as surface water or reservoirs) and its development would increase the vulnerability of its use (such as constructing an office on an undeveloped site or converting a shop to a dwelling)


## Notes

The flood map for planning shows river and sea flooding data only. It doesn't include other sources of flooding. It is for use in development planning and flood risk assessments.

This information relates to the selected location and is not specific to any property within it. The map is updated regularly and is correct at the time of printing.

Flood risk data is covered by the Open Government Licence which sets out the terms and conditions for using government data. https://www.nationalarchives.gov.uk/doc/open-governmentlicence/version/3/

Use of the address and mapping data is subject to Ordnance Survey public viewing terms under Crown copyright and database rights 2022 OS 100024198. https://flood-map-for-planning.service.gov.uk/os-terms


[^0]Appendix B. Greenfiled Runoff Estimation

Greenfield runoff rate estimation for sites www.uksuds.com | Greenfield runoff tool Site Details

| Latitude: | $54.66430^{\circ} \mathrm{N}$ |
| :--- | ---: |
| Longitude: | $1.67778^{\circ} \mathrm{W}$ |
|  |  |


| Calculated by: | Stuart Clark |
| :--- | :--- |
| Site name: | Bishop Auckland |
| Site location: | Bishop Auckland |

This is an estimation of the greenfield runoff rates that are used to meet normal bes practice criteria in line with Environment Agency guidance "Rainfall runoff

Reference: management for developments", SC030219 (2013) , the SuDS Manual C753 (Ciria, 2015) and the non-statutory standards for SuDS (Defra, 2015). This information on greenfield Date:

956217831
runoff rates may be the basis for setting consents for the drainage of surface water runoff from sites.

Runoff estimation approach IH124

Site characteristics
Total site area (ha): 0.77

## Methodology

QBAB estimation method:
Calculate from SPR and SAAR
SPR estimation method:
Soil characteristics
Calculate from SOIL type Default Edited

SOIL type:
HOST class:
SPR/SPRHOST:
Hydrological

| 4 | 4 |
| :--- | :---: |
| N/A | N/A |
| 0.47 | 0.47 |
|  | Default | characteristics


| SAAR (mm): | 670 | 670 |
| :---: | :---: | :---: |
| Hydrological region: | 3 | 3 |
| Growth curve factor 1 year. | 0.86 | 0.86 |
| Growth curve factor 30 years: | 1.75 | 1.75 |
| Growth curve factor 100 years: | 2.08 | 2.08 |
| Growth curve factor 200 | 2.37 | 2.37 |

## Notes

(1) Is $Q_{B A R}<2.0 \mathrm{l} / \mathrm{s} / \mathrm{ha}$ ?

When $Q_{B A R}$ is $<2.0 \mathrm{l} / \mathrm{s} /$ ha then limiting discharge rates are set at $2.0 \mathrm{l} / \mathrm{s} / \mathrm{ha}$.
(2) Are flow rates < $5.0 \mathrm{l} / \mathrm{s}$ ?

Where flow rates are less than $5.0 \mathrm{l} / \mathrm{s}$ consent for discharge is usually set at $5.0 \mathrm{l} / \mathrm{s}$ if blockage from vegetation and other materials is possible. Lower consent flow rates may be set where the blockage risk is addressed by using appropriate drainage elements.
(3) Is SPR/SPRHOST $\leq 0.3$ ?

Where groundwater levels are low enough the use of soakaways to avoid discharge offsite would normally be preferred for disposal of surface water runoff.

| Greenfield runoff rates | Default | Edited |
| :---: | :---: | :---: |
| $\mathrm{Q}_{\mathrm{BAR}}(1 / \mathrm{s})$ : | 3.53 | 3.53 |
| 1 in 1 year (1/s): | 3.04 | 3.04 |
| 1 in 30 years (l/s): | 6.18 | 6.18 |
| 1 in 100 year (1/s): | 7.35 | 7.35 |
| 1 in 200 years (l/s): | 8.37 | 8.37 |

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at www.uksuds.com/terms-and-conditions.htm. The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.

Appendix C. Drainage Strategy


Appendix D. Sewer Records

NWG Property Solutions is part of Northumbrian Water Group (NWG)
Northumbrian Water and Essex \& Suffolk Water are also part of NWG

## Site Enquiry

## Plan

We enclose plan(s) showing the location of any Company apparatus in the vicinity of the area of your enquiry.

If your request for plan(s) is part of a C2 enquiry, or relates to development, information about connecting to our water and sewer networks and the protection of existing apparatus, details for further information can be found via the following link https://www.nwl.co.uk/developers.aspx

1. The company is not responsible for private water supply pipes, private drains and sewers that connect the property to the public sewerage system and does not hold details of these.

## General Notes

A copy of the standard conditions for working near Company apparatus is enclosed for your information. If you require any further assistance to identify Company apparatus, then do not hesitate to make contact with the Area Office at the contact number shown in the standard conditions.

Important:- Please ensure this detail is made available to anyone carrying out any works which may affect our apparatus.
From the 1st October 2011 there may be lateral drains and/or public sewers which are not recorded on the public sewer map.

Signed.


On behalf of Northumbrian Water, Essex \& Suffolk Water


Date: 30/MAR/2020
Ref: 1148443

## STANDARD CONDITIONS FOR WORKING NEAR NORTHUMBRIAN WATER APPARATUS

## THE FOLLOWING CONDITIONS WILL APPLY TO ALL WORKS IN THE VICINITY OF COMPANY APPARATUS

1. Contact should be made with the appropriate Company Area Office prior to the commencement of any work. Arrangements can then be made for the local representative to visit the site and assist in the location and protection of any apparatus affected. The Company must be given two working days notice before any works, including trial holes, are carried out within their easements. Contact 03457171100.
2. The information shown on any plan provided by the Company is for general guidance only. The position of apparatus shown should not be relied upon as being precise. No service pipes are shown on plans.
3. The actual position of apparatus must be established by taking trial holes in all cases. No machine excavation will be permitted within 1 metre side of a main. The actual position of any apparatus must be found by hand excavation.
4. Where Company apparatus is exposed by excavation, support and protection measures are to be agreed on site. Where excavations are taken out below the invert of a main, adequate support is to be provided to prevent collapse of the excavation and subsequent undermining of the main. Special attention is to be given to the compaction of selected backfill material under the main and the company may require the use of lean mix concrete to replace inadequately compacted or unsuitable support backfill material. The compaction of selected backfill material under, around and up to a level of 300 mm above the top of any main shall be carried out by hand. Upon completion of operations, any excavation is to be left open until after inspection by Company $i$ s representative.
5. No installation of plant may take place within the Company's easements without the prior consent of the Company and with all special conditions and arrangements being finalised before commencement of work
6. Indiscriminate crossing of the main by heavy construction plant will not be permitted. Where applicable, Crossing Points must be agreed by the Company and any protective measures necessary taken before work begins.
7. Surface boxes and covers should not be removed without obtaining prior consent of the Company. All surface covers to washouts, valves, air valves, hydrants, stopcocks etc., are to be kept clear of obstruction and with free access at all times. If surface boxes or covers have been temporarily removed, positions should be clearly marked.
8. Where the levels of carriageway and footpath surfaces are raised or lowered, then the Company's surface covers must be adjusted as appropriate
9. No pipes or cables are to be laid or structures placed directly over the line of Company apparatus.
10. Where drains, pipes or cables cross over or under any mains, a minimum clearance of 300 mm must be maintained. Where it is necessary for any plant to lay parallel to the pipelines, a minimum distance of 1 metre shall be maintained between the outside of the pipeline and any plant being installed, except in the case of small diameter plant where N.J.U.G 7 dimensions apply. The Company must agree exceptions to these conditions in writing.
11. All crossing of the company's pipelines and easements shall be at right angles where possible. Where skew crossings are necessary, no more than 3 metres of the Company's pipeline shall be exposed at any time.
12. The Company will require three copies of proposal drawings showing the details of any proposed crossing of pipelines above 300 mm diameter. The drawings must show the Company's pipelines in relation to the proposed works, to a scale of no less than 1:500 and no work shall commence until the Company has given approval.
13. Where it is necessary to carry out piling works closer than 6 m to the Company' apparatus, or to carry out works using plant that is likely to damage the integrity of the Company's apparatus, the Company will require a method statement of the works shall be consulted before work commences.
14. Where the Company's pipeline is protected by a cathodic protection system, the Company will require a suitable joint testing programme to be agreed before the application of any cathodic protection scheme proposed by another authority or utility undertaking. If any bond-wires or test leads associated with the Company's cathodic protection system are damaged, disconnected or found to be in poor condition, the Company should be notified so that repairs can be made.
15. In the case of Trunk mains which cross development sites, no development is to take place within an agreed distance either side of the pipeline. A guide showing the easement widths for the various diameters and depths of pipe is available from the RASWA department.
16. No tree planting or landscaping work is done in close proximity to Company apparatus unless otherwise agreed in writing by the Company. A planting guide is available from the RASWA department.
17. In the event of any damage to any of the Company's plant the Company must be informed immediately. Where any damage occurs to Company apparatus, the appropriate remedial work will be carried out by the Company and charged to the promoter of the works.
18. Every effort should be made to secure the site against vandalism of the Company's plant.
19. A copy of these conditions is to be made available to all Contractors or Sub-Contractors working in the vicinity of Company apparatus.


The material contained on this plot has been reproduced from an Ordnance Survey map with permission of the controller of H.M.S.O. Crown Copyright Reserved. Licence No. 100022480 The information shown on this plan should be regarded as approximate and is intended for guidance only. No Liability of any kind whatsoever is accepted by Northumbrian Water, it's Northumbrian Water must be given two working days notice of their intention to excavate trial holes. With effect from 1 October 2011, private lateral drains and sewers automatically transferred to Northumbrian Water under a scheme made by the Secretary of State pursuant to section 105A Water Industry Act 1991. These former private drains and sewers together with existing private connections may not be shown but their presence should be anticipated. WARNING...Where indicated on the plan there could be abandoned asbestos
cement materials or shards of pipe. If excavating in the vicinity of these abandoned asbestos cement materials, the appropriate Health \& Safety precautions should be taken Northumbrian Water accepts no liability in respect of claims, costs, losses or other liabilities which arise as the result of the presence of the pipes or any failure to take adequate precautions

Appendix E. Hydraulic Calculations

| Jacobs Engineering Limited |  | Page 1 |
| :---: | :---: | :---: |
| $\cdot$ | Bishop Auckland <br> Bus Station and Car Park |  |
| Date 13／12／2022 09：26 File BA－Drainage Model＿v19．MDX | Designed by G．Jones Checked by S．Clark | Drainage |
| Innovyze | Network 2020．1．3 |  |

STORM SEWER DESIGN by the Modified Rational Method<br>\section*{Design Criteria for Storm－SIte Network}<br>Pipe Sizes STANDARD Manhole Sizes STANDARD<br>FSR Rainfall Model－England and Wales<br><br>Designed with Level Soffits

## Network Design Table for Storm－SIte Network

« - Indicates pipe capacity < flow

| PN | Length （m） | Fall <br> （m） | Slope $(1: X)$ | I．Area <br> （ha） | $\begin{aligned} & \text { T.E. } \\ & \text { (mins) } \end{aligned}$ | $\begin{gathered} \text { Base } \\ \text { Flow }(1 / s) \end{gathered}$ | $\begin{gathered} \mathbf{k} \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & \text { HYD } \\ & \text { SECT } \end{aligned}$ | $\begin{aligned} & \text { DIA } \\ & (\mathrm{mm}) \end{aligned}$ | Section Type | Auto Design |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S23．000 | 20.267 | 1.043 | 19.4 | 0.018 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 寊 |
| S23．001 | 12.697 | 0.519 | 24.5 | 0.010 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 䍖 |
| S24．000 | 7.855 | 0.530 | 14.8 | 0.000 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | － |
| S25．000 | 3.795 | 0.163 | 23.3 | 0.000 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 畧 |
| S24．001 | 4.650 | 0.289 | 16.1 | 0.000 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 配 |
| S23．002 | 11.512 | 0.248 | 46.4 | 0.000 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 8 |
| S26．000 | 17.550 | 1.111 | 15.8 | 0.000 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 顑 |
| S26．001 | 5.093 | 0.085 | 59.9 | 0.013 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | B |
| S27．000 | 7.855 | 0.642 | 12.2 | 0.000 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 8 |

## Network Results Table

| PN | $\begin{gathered} \text { Rain } \\ (\mathrm{mm} / \mathrm{hr}) \end{gathered}$ | $\begin{aligned} & \text { T.C. } \\ & \text { (mins) } \end{aligned}$ | $\begin{gathered} \text { US / IL } \\ \text { (m) } \end{gathered}$ | $\begin{gathered} \Sigma \text { I.Area } \\ \text { (ha) } \end{gathered}$ | $\begin{gathered} \Sigma \text { Base } \\ \text { Flow }(1 / s) \end{gathered}$ | Foul (1/s) | Add Flow $(1 / s)$ | $\begin{gathered} \mathrm{Vel} \\ (\mathrm{~m} / \mathrm{s}) \end{gathered}$ | $\begin{aligned} & \text { Cap } \\ & (1 / s) \end{aligned}$ | $\begin{aligned} & \text { Flow } \\ & (1 / s) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S23．000 | 50.00 | 4.15 | 100.260 | 0.018 | 0.0 | 0.0 | 0.0 | 2.30 | 40.6 | 3.2 |
| S23．001 | 50.00 | 4.25 | 99.217 | 0.028 | 0.0 | 0.0 | 0.0 | 2.04 | 36.1 | 5.1 |
| S24．000 | 50.00 | 4.05 | 99.517 | 0.000 | 0.0 | 0.0 | 0.0 | 2.63 | 46.5 | 0.0 |
| S25．000 | 50.00 | 4.03 | 99.150 | 0.000 | 0.0 | 0.0 | 0.0 | 2.10 | 37.0 | 0.0 |
| S24．001 | 50.00 | 4.08 | 98.987 | 0.000 | 0.0 | 0.0 | 0.0 | 2.52 | 44.6 | 0.0 |
| S23．002 | 50.00 | 4.38 | 98.698 | 0.028 | 0.0 | 0.0 | 0.0 | 1.48 | 26.2 | 5.1 |
| S26．000 | 50.00 | 4.11 | 99.646 | 0.000 | 0.0 | 0.0 | 0.0 | 2.55 | 45.0 | 0.0 |
| S26．001 | 50.00 | 4.18 | 98.535 | 0.013 | 0.0 | 0.0 | 0.0 | 1.30 | 23.0 | 2.4 |
| S27．000 | 50.00 | 4.05 | 99.409 | 0.000 | 0.0 | 0.0 | 0.0 | 2.90 | 51.2 | 0.0 |


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| － |  |  |
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Network Design Table for Storm－SIte Network

| PN | Length <br> （m） | $\begin{gathered} \text { Fall } \\ \text { (m) } \end{gathered}$ | Slope $(1: X)$ | I．Area <br> （ha） | $\begin{aligned} & \text { T.E. } \\ & \text { (mins) } \end{aligned}$ | $\begin{gathered} \text { Base } \\ \text { Flow }(1 / s) \end{gathered}$ | $\begin{gathered} \mathbf{k} \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & \text { HYD } \\ & \text { SECT } \end{aligned}$ | $\begin{aligned} & \text { DIA } \\ & (\mathrm{mm}) \end{aligned}$ | Section Type | Auto Design |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S27．001 | 4.650 | 0.317 | 14.7 | 0.026 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 8 |
| S23．003 | 26.900 | 1.495 | 18.0 | 0.005 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | － |
| S28．000 | 25.600 | 1.433 | 17.9 | 0.000 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 寊 |
| S28．001 | 4.999 | 0.083 | 60.2 | 0.019 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | B |
| S23．004 | 8.312 | 0.050 | 166.2 | 0.000 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit | 顑 |
| S23．005 | 7.588 | 0.050 | 151.8 | 0.000 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit | 8 |
| S29．000 | 12.550 | 0.209 | 60.0 | 0.000 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 遌 |
| S30．000 | 10.050 | 0.760 | 13.2 | 0.000 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 咀 |
| S29．001 | 4.950 | 0.483 | 10.2 | 0.023 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 8 |
| S31．000 | 10.050 | 0.651 | 15.4 | 0.000 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 囪 |
| S32．000 | 12.550 | 0.263 | 47.7 | 0.000 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 回 |
| S31．001 | 6.750 | 0.113 | 59.7 | 0.040 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 8 |
| S23．006 | 7.397 | 0.050 | 147.9 | 0.000 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit | 8 |
| S23．007 | 6.903 | 0.125 | 55.2 | 0.000 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit |  |
| S33．000 | 12.550 | 0.209 | 60.0 | 0.000 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 咼 |

## Network Results Table

| PN | $\begin{gathered} \text { Rain } \\ (\mathrm{mm} / \mathrm{hr}) \end{gathered}$ | $\begin{aligned} & \text { T.C. } \\ & \text { (mins) } \end{aligned}$ | $\begin{aligned} & \text { US/IL } \\ & \text { (m) } \end{aligned}$ | $\begin{gathered} \Sigma \text { I.Area } \\ \text { (ha) } \end{gathered}$ | $\begin{gathered} \Sigma \text { Base } \\ \text { Flow }(1 / s) \end{gathered}$ | Foul $(1 / s)$ | Add Flow $(1 / s)$ | $\begin{aligned} & \mathrm{Vel} \\ & (\mathrm{~m} / \mathrm{s}) \end{aligned}$ | Cap $(1 / s)$ | $\begin{aligned} & \text { Flow } \\ & (1 / s) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S27．001 | 50.00 | 4.07 | 98.767 | 0.026 | 0.0 | 0.0 | 0.0 | 2.64 | 46.7 | 4.7 |
| S23．003 | 50.00 | 4.57 | 98.450 | 0.072 | 0.0 | 0.0 | 0.0 | 2.39 | 42.2 | 12.9 |
| S28．000 | 50.00 | 4.18 | 99.126 | 0.000 | 0.0 | 0.0 | 0.0 | 2.39 | 42.3 | 0.0 |
| S28．001 | 50.00 | 4.24 | 97.693 | 0.019 | 0.0 | 0.0 | 0.0 | 1.30 | 22.9 | 3.4 |
| S23．004 | 50.00 | 4.68 | 96.805 | 0.091 | 0.0 | 0.0 | 0.0 | 1.22 | 86.0 | 16.4 |
| S23．005 | 50.00 | 4.78 | 96.755 | 0.091 | 0.0 | 0.0 | 0.0 | 1.27 | 90.1 | 16.4 |
| S29．000 | 50.00 | 4.16 | 98.372 | 0.000 | 0.0 | 0.0 | 0.0 | 1.30 | 23.0 | 0.0 |
| S30．000 | 50.00 | 4.06 | 98.923 | 0.000 | 0.0 | 0.0 | 0.0 | 2.79 | 49.2 | 0.0 |
| S29．001 | 50.00 | 4.19 | 98.163 | 0.023 | 0.0 | 0.0 | 0.0 | 3.17 | 55.9 | 4.2 |
| S31．000 | 50.00 | 4.06 | 98.312 | 0.000 | 0.0 | 0.0 | 0.0 | 2.58 | 45.5 | 0.0 |
| S32．000 | 50.00 | 4.14 | 97.924 | 0.000 | 0.0 | 0.0 | 0.0 | 1.46 | 25.8 | 0.0 |
| S31．001 | 50.00 | 4.23 | 97.661 | 0.040 | 0.0 | 0.0 | 0.0 | 1.30 | 23.0 | 7.3 |
| S23．006 | 50.00 | 4.88 | 96.705 | 0.154 | 0.0 | 0.0 | 0.0 | 1.29 | 91.2 | 27.9 |
| S23．007 | 50.00 | 4.93 | 96.655 | 0.154 | 0.0 | 0.0 | 0.0 | 2.12 | 149.9 | 27.9 |
| S33．000 | 50.00 | 4.16 | 99.001 | 0.000 | 0.0 | 0.0 | 0.0 | 1.30 | 23.0 | 0.0 |


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| Date 13/12/2022 09:26 | Designed by G.Jones <br> File BA-Drainage Model_v19.MDX | Checked by S.Clark |

Network Design Table for Storm - SIte Network


## Network Results Table

| PN | $\begin{gathered} \text { Rain } \\ (\mathrm{mm} / \mathrm{hr}) \end{gathered}$ | $\begin{aligned} & \text { T.C. } \\ & \text { (mins) } \end{aligned}$ | $\begin{gathered} \text { US/IL } \\ \text { (m) } \end{gathered}$ | $\Sigma$ I.Area (ha) | $\begin{gathered} \Sigma \text { Base } \\ \text { Flow }(1 / s) \end{gathered}$ | Foul $(1 / s)$ | $\begin{aligned} & \text { Add Flow } \\ & (1 / s) \end{aligned}$ | $\begin{gathered} \mathrm{Vel} \\ (\mathrm{~m} / \mathrm{s}) \end{gathered}$ | $\begin{gathered} \text { Cap } \\ (1 / s) \end{gathered}$ | $\begin{aligned} & \text { Flow } \\ & (1 / s) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S34.000 | 50.00 | 4.04 | 99.916 | 0.000 | 0.0 | 0.0 | 0.0 | 2.91 | 51.5 | 0.0 |
| S33.001 | 50.00 | 4.18 | 98.792 | 0.020 | 0.0 | 0.0 | 0.0 | 3.73 | 65.8 | 3.6 |
| S35.000 | 50.00 | 4.05 | 99.336 | 0.000 | 0.0 | 0.0 | 0.0 | 3.10 | 54.7 | 0.0 |
| S36.000 | 50.00 | 4.16 | 98.607 | 0.000 | 0.0 | 0.0 | 0.0 | 1.30 | 23.0 | 0.0 |
| S35.001 | 50.00 | 4.25 | 98.398 | 0.038 | 0.0 | 0.0 | 0.0 | 1.30 | 22.9 | 6.9 |
| S33.002 | 50.00 | 4.42 | 98.286 | 0.058 | 0.0 | 0.0 | 0.0 | 1.12 | 19.9 | 10.4 |
| S33.003 | 50.00 | 4.49 | 98.140 | 0.058 | 0.0 | 0.0 | 0.0 | 1.13 | 19.9 | 10.4 |
| S33.004 | 50.00 | 4.70 | 98.079 | 0.058 | 0.0 | 0.0 | 0.0 | 1.12 | 19.9 | 10.4 |
| S23.008 | 50.00 | 5.08 | 96.605 | 0.212 | 0.0 | 0.0 | 0.0 | 2.00 | 79.3 | 38.3 |
| S37.000 | 50.00 | 4.13 | 96.400 | 0.000 | 0.0 | 0.0 | 0.0 | 1.17 | 82.6 | 0.0 |
| S37.001 | 50.00 | 4.21 | 96.350 | 0.000 | 0.0 | 0.0 | 0.0 | 1.34 | 94.5 | 0.0 |
| S38.000 | 50.00 | 4.07 | 97.935 | 0.000 | 0.0 | 0.0 | 0.0 | 2.40 | 42.3 | 0.0 |
| S39.000 | 50.00 | 4.13 | 97.690 | 0.000 | 0.0 | 0.0 | 0.0 | 1.61 | 28.4 | 0.0 |
| S38.001 | 50.00 | 4.19 | 97.372 | 0.022 | 0.0 | 0.0 | 0.0 | 1.30 | 23.0 | 4.0 |


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| :--- | :--- | :--- |
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Network Design Table for Storm－SIte Network

| PN | Length <br> （m） | $\begin{gathered} \text { Fall } \\ \text { (m) } \end{gathered}$ | Slope (1:X) | I．Area <br> （ha） | $\begin{aligned} & \text { T.E. } \\ & \text { (mins) } \end{aligned}$ | $\begin{aligned} & \text { Ba: } \\ & \text { Flow } \end{aligned}$ | $(1 / s)$ | $\begin{gathered} \mathbf{k} \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & \text { HYD } \\ & \text { SECT } \end{aligned}$ | $\begin{aligned} & \text { DIA } \\ & (\mathrm{mm}) \end{aligned}$ | Section Type | Auto Design |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S40．000 | 12.550 | 0.383 | 32.8 | 0.000 | 4.00 |  | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | － |
| S41．000 | 10.050 | 0.408 | 24.6 | 0.000 | 4.00 |  | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | － |
| S40．001 | 7.150 | 0.409 | 17.5 | 0.034 | 0.00 |  | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 臬 |
| S37．002 | 7.150 | 0.050 | 143.0 | 0.000 | 0.00 |  | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit | 策 |
| S37．003 | 7.150 | 0.050 | 143.0 | 0.000 | 0.00 |  | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit | 回 |
| S23．009 | 17.700 | 0.525 | 33.7 | 0.000 | 0.00 |  | 0.0 | 0.600 | $\bigcirc$ | 225 | Pipe／Conduit | 酓 |
| S42．000 | 33.267 | 1.865 | 17.8 | 0.000 | 4.00 |  | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | － |
| S42．001 | 4.359 | 0.073 | 59.7 | 0.021 | 0.00 |  | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 合 |
| S23．010 | 7.150 | 0.050 | 143.0 | 0.000 | 0.00 |  | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit | 8 |
| S23．011 | 7.150 | 0.050 | 143.0 | 0.000 | 0.00 |  | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit |  |
| S43．000 | 22.493 | 1.495 | 15.0 | 0.000 | 4.00 |  | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 8 |
| S43．001 | 4.954 | 0.083 | 59.7 | 0.017 | 0.00 |  | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 㦹 |
| S43．002 | 8.607 | 0.895 | 9.6 | 0.000 | 0.00 |  | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 畐 |
| S43．003 | 7.441 | 0.050 | 148.8 | 0.000 | 0.00 |  | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit |  |
| S43．004 | 8.459 | 0.050 | 169.2 | 0.000 | 0.00 |  | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit | 昷 |
| S44．000 | 10.050 | 0.183 | 54.9 | 0.000 | 4.00 |  | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 8 |
| S45．000 | 12.550 | 0.209 | 60.0 | 0.000 | 4.00 |  | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 㚗 |

## Network Results Table

| PN | $\begin{gathered} \text { Rain } \\ (\mathrm{mm} / \mathrm{hr}) \end{gathered}$ | $\begin{aligned} & \text { T.C. } \\ & \text { (mins) } \end{aligned}$ | $\begin{aligned} & \text { US/IL } \\ & \text { (m) } \end{aligned}$ | $\begin{gathered} \Sigma \text { I.Area } \\ \text { (ha) } \end{gathered}$ | $\begin{gathered} \Sigma \text { Base } \\ \text { Flow }(1 / s) \end{gathered}$ | Foul $(1 / s)$ | $\begin{aligned} & \text { Add Flow } \\ & (1 / s) \end{aligned}$ | $\begin{aligned} & \mathrm{Vel} \\ & (\mathrm{~m} / \mathrm{s}) \end{aligned}$ | $\begin{gathered} \text { Cap } \\ (1 / s) \end{gathered}$ | $\begin{aligned} & \text { Flow } \\ & (1 / s) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S40．000 | 50.00 | 4.12 | 97.242 | 0.000 | 0.0 | 0.0 | 0.0 | 1.76 | 31.2 | 0.0 |
| S41．000 | 50.00 | 4.08 | 97.267 | 0.000 | 0.0 | 0.0 | 0.0 | 2.04 | 36.0 | 0.0 |
| S40．001 | 50.00 | 4.17 | 96.859 | 0.034 | 0.0 | 0.0 | 0.0 | 2.42 | 42.8 | 6.1 |
| S37．002 | 50.00 | 4.31 | 96.300 | 0.056 | 0.0 | 0.0 | 0.0 | 1.31 | 92.8 | 10.1 |
| S37．003 | 50.00 | 4.40 | 96.250 | 0.056 | 0.0 | 0.0 | 0.0 | 1.31 | 92.8 | 10.1 |
| S23．009 | 50.00 | 5.21 | 96.200 | 0.268 | 0.0 | 0.0 | 0.0 | 2.26 | 89.9 | 48.4 |
| S42．000 | 50.00 | 4.23 | 98.403 | 0.000 | 0.0 | 0.0 | 0.0 | 2.40 | 42.3 | 0.0 |
| S42．001 | 50.00 | 4.29 | 96.538 | 0.021 | 0.0 | 0.0 | 0.0 | 1.30 | 23.0 | 3.8 |
| S23．010 | 50.00 | 5.30 | 95.600 | 0.289 | 0.0 | 0.0 | 0.0 | 1.31 | 92.8 | 52.1 |
| S23．011 | 50.00 | 5.39 | 95.550 | 0.289 | 0.0 | 0.0 | 0.0 | 1.31 | 92.8 | 52.1 |
| S43．000 | 50.00 | 4.14 | 98.223 | 0.000 | 0.0 | 0.0 | 0.0 | 2.61 | 46.1 | 0.0 |
| S43．001 | 50.00 | 4.21 | 96.728 | 0.017 | 0.0 | 0.0 | 0.0 | 1.30 | 23.0 | 3.0 |
| S43．002 | 50.00 | 4.25 | 96.645 | 0.017 | 0.0 | 0.0 | 0.0 | 3.27 | 57.8 | 3.0 |
| S43．003 | 50.00 | 4.35 | 95.600 | 0.017 | 0.0 | 0.0 | 0.0 | 1.29 | 90.9 | 3.0 |
| S43．004 | 50.00 | 4.46 | 95.550 | 0.017 | 0.0 | 0.0 | 0.0 | 1.21 | 85.2 | 3.0 |
| S44．000 | 50.00 | 4.12 | 96.982 | 0.000 | 0.0 | 0.0 | 0.0 | 1.36 | 24.0 | 0.0 |
| S45．000 | 50.00 | 4.16 | 97.008 | 0.000 | 0.0 | 0.0 | 0.0 | 1.30 | 23.0 | 0.0 |


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| :---: | :---: | :---: |
| － | Bishop Auckland <br> Bus Station and Car Park |  |
| Date 13／12／2022 09：26 <br> File BA－Drainage Model＿v19．MDX | Designed by G．Jones <br> Checked by S．Clark | Drainage |

Network Design Table for Storm－SIte Network

| PN | Length <br> （m） | $\begin{gathered} \text { Fall } \\ (\mathrm{m}) \end{gathered}$ | Slope $(1: X)$ | I．Area <br> （ha） | $\begin{aligned} & \text { T.E. } \\ & \text { (mins) } \end{aligned}$ | $\begin{gathered} \text { Base } \\ \text { Flow }(1 / s) \end{gathered}$ | $\begin{gathered} \mathbf{k} \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & \text { HYD } \\ & \text { SECT } \end{aligned}$ | $\begin{aligned} & \text { DIA } \\ & (\mathrm{mm}) \end{aligned}$ | Section Type | Auto Design |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S44．001 | 4.350 | 0.373 | 11.7 | 0.024 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | 畧 |
| S23．012 | 7.150 | 0.050 | 143.0 | 0.000 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit | 量 |
| S46．000 | 16.100 | 0.468 | 34.4 | 0.000 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | B |
| S47．000 | 16.750 | 0.279 | 60.0 | 0.000 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | － |
| S23．013 | 4.649 | 0.050 | 93.0 | 0.052 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit | 臬 |
| S48．000 | 9.722 | 0.162 | 60.0 | 0.000 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 150 | Pipe／Conduit | － |
| S23．014 | 9.249 | 0.642 | 14.4 | 0.010 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 225 | Pipe／Conduit | 易 |
| S23．015 | 15.498 | 0.050 | 310.0 | 0.000 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 450 | Pipe／Conduit |  |
| S23．016 | 19.976 | 0.050 | 399.5 | 0.000 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 450 | Pipe／Conduit |  |
| S49．000 | 22.165 | 0.261 | 84.9 | 0.028 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 225 | Pipe／Conduit |  |
| S49．001 | 13.389 | 0.423 | 31.7 | 0.011 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 225 | Pipe／Conduit | － |
| S49．002 | 13.275 | 0.191 | 69.5 | 0.007 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 225 | Pipe／Conduit | g |
| S49．003 | 16.968 | 0.160 | 106.0 | 0.004 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 225 | Pipe／Conduit |  |
| S49．004 | 12.740 | 0.082 | 155.4 | 0.000 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 225 | Pipe／Conduit | ） |
| S50．000 | 15.503 | 0.103 | 150.5 | 0.109 | 4.00 | 0.0 | 0.600 | $\bigcirc$ | 225 | Pipe／Conduit | 8 |
| S50．001 | 12.033 | 0.060 | 200.6 | 0.068 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit | 0 |
| S50．002 | 8.731 | 0.044 | 200.0 | 0.000 | 0.00 | 0.0 | 0.600 | $\bigcirc$ | 300 | Pipe／Conduit | 8 |

## Network Results Table

| PN | $\underset{(\mathrm{mm} / \mathrm{hr})}{\mathrm{Rain}}$ | $\begin{aligned} & \text { T.C. } \\ & \text { (mins) } \end{aligned}$ | $\begin{gathered} \text { US /IL } \\ \text { (m) } \end{gathered}$ | $\begin{gathered} \Sigma \text { I.Area } \\ \text { (ha) } \end{gathered}$ | $\begin{gathered} \Sigma \text { Base } \\ \text { Flow }(1 / s) \end{gathered}$ | Foul <br> （1／s） | Add Flow $(1 / s)$ | $\begin{gathered} \mathrm{Vel} \\ (\mathrm{~m} / \mathrm{s}) \end{gathered}$ | $\begin{aligned} & \text { Cap } \\ & (1 / s) \end{aligned}$ | $\begin{aligned} & \text { Flow } \\ & (1 / s) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S44．001 | 50.00 | 4.19 | 96.799 | 0.024 | 0.0 | 0.0 | 0.0 | 2.97 | 52.4 | 4.4 |
| S23．012 | 50.00 | 5.48 | 95.500 | 0.330 | 0.0 | 0.0 | 0.0 | 1.31 | 92.8 | 59.5 |
| S46．000 | 50.00 | 4.16 | 96.844 | 0.000 | 0.0 | 0.0 | 0.0 | 1.72 | 30.4 | 0.0 |
| S47．000 | 50.00 | 4.21 | 96.434 | 0.000 | 0.0 | 0.0 | 0.0 | 1.30 | 23.0 | 0.0 |
| S23．013 | 50.00 | 5.53 | 95.450 | 0.382 | 0.0 | 0.0 | 0.0 | 1.63 | 115.3 | 69.0 |
| S48．000 | 50.00 | 4.12 | 96.194 | 0.000 | 0.0 | 0.0 | 0.0 | 1.30 | 23.0 | 0.0 |
| S23．014 | 50.00 | 5.57 | 95.400 | 0.392 | 0.0 | 0.0 | 0.0 | 3.47 | 137.8 | 70.7 |
| S23．015 | 50.00 | 5.80 | 94.533 | 0.392 | 0.0 | 0.0 | 0.0 | 1.15 | 182.8 | 70.7 |
| S23．016 | 50.00 | 6.13 | 94.483 | 0.392 | 0.0 | 0.0 | 0.0 | 1.01 | 160.8 | 70.7 |
| S49．000 | 50.00 | 4.26 | 95.550 | 0.028 | 0.0 | 0.0 | 0.0 | 1.42 | 56.5 | 5.1 |
| S49．001 | 50.00 | 4.36 | 95.289 | 0.040 | 0.0 | 0.0 | 0.0 | 2.33 | 92.8 | 7.2 |
| S49．002 | 50.00 | 4.50 | 94.866 | 0.046 | 0.0 | 0.0 | 0.0 | 1.57 | 62.5 | 8.4 |
| S49．003 | 50.00 | 4.72 | 94.675 | 0.051 | 0.0 | 0.0 | 0.0 | 1.27 | 50.5 | 9.2 |
| S49．004 | 50.00 | 4.92 | 94.515 | 0.051 | 0.0 | 0.0 | 0.0 | 1.05 | 41.6 | 9.2 |
| S50．000 | 50.00 | 4.24 | 94.715 | 0.109 | 0.0 | 0.0 | 0.0 | 1.06 | 42.3 | 19.7 |
| S50．001 | 50.00 | 4.42 | 94.537 | 0.177 | 0.0 | 0.0 | 0.0 | 1.11 | 78.2 | 32.0 |
| S50．002 | 50.00 | 4.56 | 94.477 | 0.177 | 0.0 | 0.0 | 0.0 | 1.11 | 78.3 | 32.0 |



Network Results Table

| PN | $\underset{(\mathrm{mm} / \mathrm{hr})}{\mathrm{Rain}}$ | $\begin{aligned} & \text { T.C. } \\ & \text { (mins) } \end{aligned}$ | $\begin{gathered} \text { US / IL } \\ (\mathrm{m}) \end{gathered}$ | $\Sigma$ I.Area (ha) | $\begin{gathered} \Sigma \text { Base } \\ \text { Flow }(1 / s) \end{gathered}$ | $\begin{aligned} & \text { Foul } \\ & (1 / s) \end{aligned}$ | Add Flow $(1 / s)$ | $\begin{aligned} & \text { Vel } \\ & (\mathrm{m} / \mathrm{s}) \end{aligned}$ | $\begin{gathered} \text { Cap } \\ (1 / s) \end{gathered}$ | $\begin{aligned} & \text { Flow } \\ & (1 / s) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S23.017 | 50.00 | 6.22 | 94.433 | 0.620 | 0.0 | 0.0 | 0.0 | 1.01 | 17.8< | 111.9 |
| S23.018 | 50.00 | 6.39 | 94.374 | 0.620 | 0.0 | 0.0 | 0.0 | 1.01 | 17.8<< | 111.9 |
| S23.019 | 50.00 | 6.49 | 94.270 | 0.620 | 0.0 | 0.0 | 0.0 | 0.86 | 15.3<< | 111.9 |


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| :---: | :---: | :---: |
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Manhole Schedules for Storm - SIte Network

| $\begin{gathered} \text { MH } \\ \text { Name } \end{gathered}$ | $\begin{gathered} \mathrm{MH} \\ \mathrm{CL} \quad(\mathrm{~m}) \end{gathered}$ |  | MH <br> Connection | $\underset{\substack{\text { MH } \\(\mathrm{mm})}}{\mathrm{Diam}, \mathrm{~L} \star \mathrm{~W}}$ | PN | Pipe Out Invert Level (m) | $\begin{aligned} & \text { Diameter } \\ & (\mathrm{mm}) \end{aligned}$ | PN | $\begin{aligned} & \text { Pipes In } \\ & \text { Invert } \\ & \text { Level (m) } \end{aligned}$ | $\begin{aligned} & \text { Diameter } \\ & (\mathrm{mm}) \end{aligned}$ | Backdrop $(\mathrm{mm})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SWP-1 | 101.310 | 1.050 | Open Manhole | 1200 | S23.000 | 100.260 | 150 |  |  |  |  |
| SWP-2 | 100.271 | 1.054 | Open Manhole | 1200 | S23.001 | 99.217 | 150 | S23.000 | 99.217 | 150 |  |
| SWP-3 | 100.123 | 0.606 | Junction |  | S24.000 | 99.517 | 150 |  |  |  |  |
| SWP-4 | 100.200 | 1.050 | Open Manhole | 1200 | S25.000 | 99.150 | 150 |  |  |  |  |
| SWP-5 | 100.043 | 1.056 | Open Manhole | 1200 | S24.001 | 98.987 | 150 | S24.000 | 98.987 | 150 |  |
|  |  |  |  |  |  |  |  | S25.000 | 98.987 | 150 |  |
| SWP-6 | 99.998 | 1.300 | Open Manhole | 1200 | S23.002 | 98.698 | 150 | S23.001 | 98.698 | 150 |  |
|  |  |  |  |  |  |  |  | S24.001 | 98.698 | 150 |  |
| SWP-7 | 100.296 | 0.650 | Junction |  | S26.000 | 99.646 | 150 |  |  |  |  |
| SWP-8 | 99.835 | 1.300 | Open Manhole | 600 | S26.001 | 98.535 | 150 | S26.000 | 98.535 | 150 |  |
| SWP-9 | 100.015 | 0.606 | Junction |  | S27.000 | 99.409 | 150 |  |  |  |  |
| SWP-10 | 99.917 | 1.150 | Open Manhole | 600 | S27.001 | 98.767 | 150 | S27.000 | 98.767 | 150 |  |
| SWP-11 | 99.790 | 1.340 | Open Manhole | 1200 | S23.003 | 98.450 | 150 | S23.002 | 98.450 | 150 |  |
|  |  |  |  |  |  |  |  | S26.001 | 98.450 | 150 |  |
|  |  |  |  |  |  |  |  | S27.001 | 98.450 | 150 |  |
| SWP-12 | 99.776 | 0.650 | Junction |  | S28.000 | 99.126 | 150 |  |  |  |  |
| SWP-13 | 98.977 | 1.284 | Open Manhole | 600 | S28.001 | 97.693 | 150 | S28.000 | 97.693 | 150 |  |
| SWP-14 | 98.879 | 2.074 | Open Manhole | 1200 | S23.004 | 96.805 | 300 | S23.003 | 96.955 | 150 |  |
|  |  |  |  |  |  |  |  | S28.001 | 97.610 | 150 | 655 |
| SWP-TANK 1 | 98.959 | 2.204 | Junction |  | S23.005 | 96.755 | 300 | S23.004 | 96.755 | 300 |  |
| SWP-16 | 99.033 | 0.661 | Junction |  | S29.000 | 98.372 | 150 |  |  |  |  |
| SWP-17 | 99.622 | 0.699 | Junction |  | S30.000 | 98.923 | 150 |  |  |  |  |
| SWP-18 | 99.388 | 1.225 | Open Manhole | 600 | S29.001 | 98.163 | 150 | S29.000 | 98.163 | 150 |  |
|  |  |  |  |  |  |  |  | S30.000 | 98.163 | 150 |  |
| SWP-19 | 98.989 | 0.677 | Junction |  | S31.000 | 98.312 | 150 |  |  |  |  |
| SWP-20 | 98.586 | 0.662 | Junction |  | S32.000 | 97.924 | 150 |  |  |  |  |
| SWP-21 | 98.819 | 1.158 | Open Manhole | 600 | S31.001 | 97.661 | 150 | S31.000 | 97.661 | 150 |  |
|  |  |  |  |  |  |  |  | S32.000 | 97.661 | 150 |  |
| SWP-22 | 99.135 | 2.430 | Open Manhole | 1200 | S23.006 | 96.705 | 300 | S23.005 | 96.705 | 300 |  |
|  |  |  |  |  |  |  |  | S29.001 | 97.680 | 150 | 825 |
|  |  |  |  |  |  |  |  | S31.001 | 97.548 | 150 | 693 |
| SWP-TANK 2 | 99.299 | 2.644 | Junction |  | S23.007 | 96.655 | 300 | S23.006 | 96.655 | 300 |  |
| SWP-24 | 99.669 | 0.668 | Junction |  | S33.000 | 99.001 | 150 |  |  |  |  |
| SWP-25 | 100.479 | 0.563 | Junction |  | S34.000 | 99.916 | 150 |  |  |  |  |
| SWP-26 | 100.197 | 1.405 | Open Manhole | 600 | S33.001 | 98.792 | 150 | S33.000 | 98.792 | 150 |  |
|  |  |  |  |  |  |  |  | S34.000 | 99.292 | 150 | 500 |
| SWP-27 | 99.973 | 0.637 | Junction |  | S35.000 | 99.336 | 150 |  |  |  |  |
| SWP-28 | 99.269 | 0.662 | Junction |  | S36.000 | 98.607 | 150 |  |  |  |  |
| SWP-29 | 99.658 | 1.260 | Open Manhole | 600 | S35.001 | 98.398 | 150 | S35.000 | 98.398 | 150 |  |
|  |  |  |  |  |  |  |  | S36.000 | 98.398 | 150 |  |
| SWP-30 | 99.974 | 1.688 | Open Manhole | 1200 | S33.002 | 98.286 | 150 | S33.001 | 98.286 | 150 |  |
|  |  |  |  |  |  |  |  | S35.001 | 98.286 | 150 |  |
| SWP-31 | 100.381 | 2.241 | Open Manhole | 1200 | S33.003 | 98.140 | 150 | S33.002 | 98.140 | 150 |  |
| SWP-32 | 99.994 | 1.915 | Open Manhole | 1200 | S33.004 | 98.079 | 150 | S33.003 | 98.079 | 150 |  |
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## Manhole Schedules for Storm - SIte Network

| MH Name | $\underset{\mathrm{CL}}{\mathrm{MH}}(\mathrm{~m})$ | MH Depth (m) | MH Connection | $\underset{\substack{\text { Diam. , } \mathrm{L} * \mathrm{~W} \\(\mathrm{~mm})}}{\mathrm{MH}}$ | PN | Pipe Out Invert Level (m) | $\underset{(\mathrm{mm})}{\text { Diameter }}$ | PN | $\begin{aligned} & \text { Pipes In } \\ & \text { Invert } \\ & \text { Level ( } \mathrm{m} \text { ) } \end{aligned}$ | $\underset{(\mathrm{mm})}{\text { Diameter }}$ | $\underset{(\mathrm{mm})}{\text { Backdrop }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |



| Jacobs Engineering Limited |  | Page 9 |
| :---: | :---: | :---: |
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## Manhole Schedules for Storm - SIte Network

| $\begin{gathered} \text { MH } \\ \text { Name } \end{gathered}$ | $$ |  | MH <br> Connection | $\begin{gathered} \mathrm{MH} \\ \text { Diam. , L*W } \\ (\mathrm{mm}) \end{gathered}$ | PN | Pipe Out Invert Level (m) | $\begin{aligned} & \text { Diameter } \\ & (\mathrm{mm}) \end{aligned}$ | PN | Pipes In Invert Level (m) | $\begin{aligned} & \text { Diameter } \\ & \text { (mm) } \end{aligned}$ | $\begin{gathered} \text { Backdrop } \\ (\mathrm{mm}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SWP-TANK 7 | 96.394 | 1.911 | Junction |  | S23.016 | 94.483 | 450 | S23.015 | 94.483 | 450 |  |
| SWP-65 | 97.337 | 1.787 | Open Manhole | 600 | S49.000 | 95.550 | 225 |  |  |  |  |
| SWP-66 | 96.750 | 1.461 | Open Manhole | 600 | S49.001 | 95.289 | 225 | S49.000 | 95.289 | 225 |  |
| SWP-67 | 96.359 | 1.493 | Open Manhole | 600 | S49.002 | 94.866 | 225 | S49.001 | 94.866 | 225 |  |
| SWP-68 | 96.115 | 1.440 | Open Manhole | 600 | S49.003 | 94.675 | 225 | S49.002 | 94.675 | 225 |  |
| SWP-69 | 96.532 | 2.017 | Open Manhole | 1200 | S49.004 | 94.515 | 225 | S49.003 | 94.515 | 225 |  |
| SWP-70 | 96.174 | 1.459 | Open Manhole | 1200 | S50.000 | 94.715 | 225 |  |  |  |  |
| SWP-71 | 95.990 | 1.453 | Open Manhole | 1200 | S50.001 | 94.537 | 300 | S50.000 | 94.612 | 225 |  |
| SWP-72 | 96.266 | 1.789 | Open Manhole | 1200 | S50.002 | 94.477 | 300 | S50.001 | 94.477 | 300 |  |
| SWP-CC1 | 96.346 | 1.913 | Open Manhole | 2400 | S23.017 | 94.433 | 150 | S23.016 | 94.433 | 450 |  |
|  |  |  |  |  |  |  |  | S49.004 | 94.433 | 225 |  |
|  |  |  |  |  |  |  |  | S50.002 | 94.433 | 300 |  |
| SWP-PI | 96.248 | 1.874 | Junction |  | S23.018 | 94.374 | 150 | S23.017 | 94.374 | 150 |  |
| SWP-75 | 95.960 | 1.690 | Open Manhole | 1200 | S23.019 | 94.270 | 150 | S23.018 | 94.270 | 150 |  |
| SWP-EXTG | 95.780 | 1.545 | Open Manhole | 0 |  | OUTFALL |  | S23.019 | 94.235 | 150 |  |


| MH <br> Name | Manhole Easting (m) | Manhole <br> Northing (m) | Intersection Easting (m) | Intersection Northing (m) | Manhole <br> Access | Layout <br> (North) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SWP -1 | 420798.397 | 529957.316 | 420798.397 | 529957.316 | Required |  |
| SWP-2 | 420816.281 | 529966.851 | 420816.281 | 529966.851 | Required |  |
| SWP-3 | 420821.559 | 529962.703 |  |  | No Entry |  |
| SWP-4 | 420829.751 | 529959.702 | 420829.751 | 529959.702 | Required |  |
| SWP - 5 | 420829.376 | 529963.479 | 420829.376 | 529963.479 | Required |  |
| SWP-6 | 420828.916 | 529968.106 | 420828.916 | 529968.106 | Required |  |
| SWP-7 | 420821.224 | 529972.317 |  |  | No Entry |  |
| SWP-8 | 420838.688 | 529974.052 | 420838.688 | 529974.052 | Required |  |
| SWP-9 | 420833.015 | 529963.841 |  |  | No Entry |  |
| SWP-10 | 420840.832 | 529964.617 | 420840.832 | 529964.617 | Required |  |
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| $\begin{gathered} \text { MH } \\ \text { Name } \end{gathered}$ | Manhole Easting (m) | Manhole <br> Northing <br> (m) | Intersection Easting (m) | Intersection Northing (m) | Manhole <br> Access | Layout <br> (North) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SWP-11 | 420840.372 | 529969.245 | 420840.372 | 529969.245 | Required |  |
| SWP-12 | 420841.873 | 529974.368 |  |  | No Entry |  |
| SWP-13 | 420867.347 | 529976.899 | 420867.347 | 529976.899 | Required |  |
| SWP-14 | 420867.140 | 529971.904 | 420867.140 | 529971.904 | Required |  |
| SWP-TANK 1 | 420867.962 | 529963.632 |  |  | No Entry |  |
| SWP-16 | 420862.546 | 529968.081 |  |  | No Entry |  |
| SWP-17 | 420864.780 | 529945.592 |  |  | No Entry |  |
| SWP-18 | 420863.786 | 529955.593 | 420863.786 | 529955.593 | Required |  |
| SWP-19 | 420876.423 | 529946.749 |  |  | No Entry |  |
| SWP-20 | 420874.188 | 529969.238 |  |  | No Entry |  |
| SWP-21 | 420875.429 | 529956.749 | 420875.429 | 529956.749 | Required |  |
| SWP-22 | 420868.712 | 529956.082 | 420868.712 | 529956.082 | Required |  |
| SWP-TANK 2 | 420869.443 | 529948.721 |  |  | No Entry |  |
| SWP-24 | 420845.927 | 529966.430 |  |  | No Entry |  |
| SWP-25 | 420847.915 | 529946.429 |  |  | No Entry |  |
| SWP-26 | 420847.168 | 529953.942 | 420847.168 | 529953.942 | Required |  |
| SWP-27 | 420858.610 | 529944.979 |  |  | No Entry |  |
| SWP-28 | 420856.376 | 529967.468 |  |  | No Entry |  |
| SWP-29 | 420857.617 | 529954.979 | 420857.617 | 529954.979 | Required |  |
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| :--- | :--- | :--- |
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| Fate 13/12/2022 09:26 BA-Drainage Model_v19.MDX | Network 2020.1.3 |  |
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| Jacobs Engineering Limited | Page 12 |  |
| :--- | :--- | :--- |
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| Jacobs Engineering Limited | Page 13 |  |
| :--- | :--- | :--- |
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| • | Designed by G.Jones <br> Fate 13/12/2022 09:26 <br> File BA-Drainage Model_v19.MDX | Network 2020.1.3 |


| MH <br> Name | Manhole Easting (m) | Manhole Northing (m) | Intersection Easting (m) | Intersection Northing (m) | Manhole <br> Access | Layout <br> (North) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SWP-68 | 420963.161 | 529991.824 | 420963.161 | 529991.824 | Required |  |
| SWP-69 | 420966.272 | 529975.144 | 420966.272 | 529975.144 | Required |  |
| SWP-70 | 420954.479 | 529951.395 | 420954.479 | 529951.395 | Required |  |
| SWP-71 | 420969.906 | 529952.927 | 420969.906 | 529952.927 | Required |  |
| SWP-72 | 420968.716 | 529964.902 | 420968.716 | 529964.902 | Required |  |
| SWP-CC1 | 420960.028 | 529964.039 | 420960.028 | 529964.039 | Required |  |
| SWP-PI | 420960.608 | 529958.199 |  |  | No Entry |  |
| SWP-75 | 420961.632 | 529947.898 | 420961.632 | 529947.898 | Required |  |
| SWP-EXTG | 420960.014 | 529943.461 |  |  | No Entry |  |


| Jacobs Engineering Limited |  | Page 14 |
| :--- | :--- | :--- |
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## Area Summary for Storm - SIte Network

| Pipe | PIMP | PIMP | PIMP | Gross | Imp. | e Total <br> (ha) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Number | Type | Name | (\%) | Area (ha) | Area (ha) |  |
| 23.000 | Classification | Soft Landscape | 50 | 0.008 | 0.004 | 0.004 |
|  | Classification | Soft Landscape | 50 | 0.013 | 0.007 | 0.011 |
|  | Classification | Hard Landscape | 100 | 0.007 | 0.007 | 0.018 |
| 23.001 | Classification | Roof | 100 | 0.006 | 0.006 | 0.006 |
|  | Classification | Soft Landscape | 50 | 0.005 | 0.002 | 0.009 |
|  | Classification | Soft Landscape | 50 | 0.003 | 0.002 | 0.010 |
| 24.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 25.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 24.001 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 23.002 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 26.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 26.001 | Classification | Soft Landscape | 50 | 0.009 | 0.005 | 0.005 |
|  | Classification | Permeable Paving | 100 | 0.009 | 0.009 | 0.013 |
| 27.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 27.001 | Classification | Permeable Paving | 100 | 0.011 | 0.011 | 0.011 |
|  | Classification | Soft Landscape | 50 | 0.005 | 0.003 | 0.013 |
|  | Classification | Road | 100 | 0.013 | 0.013 | 0.026 |
| 23.003 | Classification | Hard Landscape | 100 | 0.005 | 0.005 | 0.005 |
| 28.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 28.001 | Classification | Permeable Paving | 100 | 0.014 | 0.014 | 0.014 |
|  | Classification | Soft Landscape | 50 | 0.009 | 0.005 | 0.019 |
| 23.004 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 23.005 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 29.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 30.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 29.001 | Classification | Permeable Paving | 100 | 0.013 | 0.013 | 0.013 |
|  | Classification | Soft Landscape | 50 | 0.003 | 0.002 | 0.014 |
|  | Classification | Road | 100 | 0.005 | 0.005 | 0.019 |
|  | Classification | Road | 100 | 0.005 | 0.005 | 0.023 |
| 31.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 32.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 31.001 | Classification | Permeable Paving | 100 | 0.012 | 0.012 | 0.012 |
|  | Classification | Road | 100 | 0.028 | 0.028 | 0.040 |
| 23.006 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 23.007 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 33.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 34.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 33.001 | Classification | Permeable Paving | 100 | 0.011 | 0.011 | 0.011 |
|  | Classification | Soft Landscape | 50 | 0.010 | 0.005 | 0.016 |
|  | Classification | Road | 100 | 0.004 | 0.004 | 0.020 |
| 35.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 36.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 35.001 | Classification | Permeable Paving | 100 | 0.012 | 0.012 | 0.012 |
|  | Classification | Road | 100 | 0.025 | 0.025 | 0.038 |
| 33.002 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 33.003 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 33.004 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 23.008 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 37.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 37.001 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 38.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 39.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 38.001 | Classification | Permeable Paving | 100 | 0.013 | 0.013 | 0.013 |
|  | Classification | Soft Landscape | 50 | 0.003 | 0.001 | 0.014 |
|  | Classification | Road | 100 | 0.004 | 0.004 | 0.018 |
|  | Classification | Road | 100 | 0.004 | 0.004 | 0.022 |
| 40.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 41.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 40.001 | Classification | Permeable Paving | 100 | 0.010 | 0.010 | 0.010 |


| Jacobs Engineering Limited |  | Page 15 |
| :---: | :---: | :---: |
|  | Bishop Auckland <br> Bus Station and Car Park |  |
| Date 13/12/2022 09:26 <br> File BA-Drainage Model_v19.MDX | Designed by G.Jones <br> Checked by S.Clark | Drainage |

## Area Summary for Storm - SIte Network

| Pipe <br> Number | PIMP Type | PIMP <br> Name | PIMP <br> (\%) | Gross <br> Area (ha) | $\begin{gathered} \text { Imp. } \\ \text { Area (ha) } \end{gathered}$ | $\begin{gathered} \text { Pipe Total } \\ \text { (ha) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Classification | Road | 100 | 0.024 | 0.024 | 0.034 |
| 37.002 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 37.003 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 23.009 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 42.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 42.001 | Classification | Permeable Paving | 100 | 0.019 | 0.019 | 0.019 |
|  | Classification | Soft Landscape | 50 | 0.004 | 0.002 | 0.021 |
| 23.010 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 23.011 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 43.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 43.001 | Classification | Permeable Paving | 100 | 0.012 | 0.012 | 0.012 |
|  | Classification | Soft Landscape | 50 | 0.009 | 0.004 | 0.017 |
| 43.002 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 43.003 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 43.004 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 44.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 45.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 44.001 | Classification | Permeable Paving | 100 | 0.010 | 0.010 | 0.010 |
|  | Classification | Soft Landscape | 50 | 0.002 | 0.001 | 0.011 |
|  | Classification | Road | 100 | 0.009 | 0.009 | 0.020 |
|  | Classification | Road | 100 | 0.004 | 0.004 | 0.024 |
| 23.012 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 46.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 47.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 23.013 | Classification | Permeable Paving | 100 | 0.017 | 0.017 | 0.017 |
|  | Classification | Soft Landscape | 50 | 0.003 | 0.002 | 0.018 |
|  | Classification | Road | 100 | 0.034 | 0.034 | 0.052 |
| 48.000 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 23.014 | Classification | Hard Landscape | 100 | 0.006 | 0.006 | 0.006 |
|  | Classification | Hard Landscape | 100 | 0.003 | 0.003 | 0.010 |
| 23.015 | - | Hard | 100 | 0.000 | 0.000 | 0.000 |
| 23.016 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 49.000 | Classification | Roof | 100 | 0.015 | 0.015 | 0.015 |
|  | Classification | Hard Landscape | 100 | 0.013 | 0.013 | 0.028 |
| 49.001 | Classification | Hard Landscape | 100 | 0.010 | 0.010 | 0.010 |
|  | Classification | Soft Landscape | 50 | 0.004 | 0.002 | 0.011 |
| 49.002 | Classification | Hard Landscape | 100 | 0.005 | 0.005 | 0.005 |
|  | Classification | Soft Landscape | 50 | 0.002 | 0.001 | 0.007 |
| 49.003 | Classification | Hard Landscape | 100 | 0.003 | 0.003 | 0.003 |
|  | Classification | Soft Landscape | 50 | 0.002 | 0.001 | 0.004 |
| 49.004 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 50.000 | Classification | Road | 100 | 0.109 | 0.109 | 0.109 |
| 50.001 | Classification | Road | 100 | 0.068 | 0.068 | 0.068 |
| 50.002 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 23.017 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 23.018 | - | - | 100 | 0.000 | 0.000 | 0.000 |
| 23.019 | - | - | 100 | 0.000 | 0.000 | 0.000 |
|  |  |  |  | Total | Total | Total |
|  |  |  |  | 0.667 | 0.620 | 0.620 |


| Jacobs Engineering Limited |  | Page 16 |
| :--- | :--- | :--- |
| $\cdot$ | Bishop Auckland <br> Bus Station and Car Park |  |
| • |  |  |
| Date 13/12/2022 09:26 | Designed by G.Jones <br> File BA-Drainage Model_v19.mDx | Checked by S.Clark |

Network Classifications for Storm - SIte Network

| PN | USMH <br> Name | Pipe Dia (mm) | Min Cover Depth (m) | Max Cover Depth (m) | Pipe Type | MH <br> Dia <br> (mm) |  | MH Ring Depth (m) | MH Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S23.000 | SWP-1 | 150 | 0.715 | 0.904 | Unclassified | 1200 | 0 | 0.900 | Unclassified |
| S23.001 | SWP-2 | 150 | 0.904 | 1.150 | Unclassified | 1200 | 0 | 0.904 | Unclassified |
| S24.000 | SWP-3 | 150 | 0.456 | 0.906 | Unclassified |  |  |  | Junction |
| S25.000 | SWP-4 | 150 | 0.851 | 0.906 | Unclassified | 1200 | 0 | 0.900 | Unclassified |
| S24.001 | SWP-5 | 150 | 0.906 | 1.150 | Unclassified | 1200 | 0 | 0.906 | Unclassified |
| S23.002 | SWP-6 | 150 | 1.150 | 1.200 | Unclassified | 1200 | 0 | 1.150 | Unclassified |
| S26.000 | SWP-7 | 150 | 0.500 | 1.150 | Unclassified |  |  |  | Junction |
| S26.001 | SWP-8 | 150 | 1.150 | 1.190 | Unclassified | 600 | 0 | 1.150 | Unclassified |
| S27.000 | SWP-9 | 150 | 0.456 | 1.000 | Unclassified |  |  |  | Junction |
| S27.001 | SWP-10 | 150 | 1.000 | 1.190 | Unclassified | 600 | 0 | 1.000 | Unclassified |
| S23.003 | SWP-11 | 150 | 1.190 | 1.774 | Unclassified | 1200 | 0 | 1.190 | Unclassified |
| S28.000 | SWP-12 | 150 | 0.500 | 1.134 | Unclassified |  |  |  | Junction |
| S28.001 | SWP-13 | 150 | 1.119 | 1.134 | Unclassified | 600 | 0 | 1.134 | Unclassified |
| S23.004 | SWP-14 | 300 | 1.738 | 1.904 | Unclassified | 1200 | 0 | 1.774 | Unclassified |
| S23.005 | SWP-TANK 1 | 300 | 1.904 | 2.130 | Unclassified |  |  |  | Junction |
| S29.000 | SWP-16 | 150 | 0.511 | 1.075 | Unclassified |  |  |  | Junction |
| S30.000 | SWP-17 | 150 | 0.549 | 1.075 | Unclassified |  |  |  | Junction |
| S29.001 | SWP-18 | 150 | 1.075 | 1.305 | Unclassified | 600 | 0 | 1.075 | Unclassified |
| S31.000 | SWP-19 | 150 | 0.527 | 1.008 | Unclassified |  |  |  | Junction |
| S32.000 | SWP-20 | 150 | 0.512 | 1.008 | Unclassified |  |  |  | Junction |
| S31.001 | SWP-21 | 150 | 1.008 | 1.437 | Unclassified | 600 | 0 | 1.008 | Unclassified |
| S23.006 | SWP-22 | 300 | 2.130 | 2.344 | Unclassified | 1200 | 0 | 2.130 | Unclassified |
| S23.007 | SWP-TANK 2 | 300 | 2.344 | 2.480 | Unclassified |  |  |  | Junction |
| S33.000 | SWP-24 | 150 | 0.518 | 1.255 | Unclassified |  |  |  | Junction |
| S34.000 | SWP-25 | 150 | 0.413 | 0.755 | Unclassified |  |  |  | Junction |
| S33.001 | SWP-26 | 150 | 1.255 | 1.538 | Unclassified | 600 | 0 | 1.255 | Unclassified |
| S35.000 | SWP-27 | 150 | 0.487 | 1.110 | Unclassified |  |  |  | Junction |
| S36.000 | SWP-28 | 150 | 0.512 | 1.110 | Unclassified |  |  |  | Junction |
| S35.001 | SWP-29 | 150 | 1.110 | 1.538 | Unclassified | 600 | 0 | 1.110 | Unclassified |
| S33.002 | SWP-30 | 150 | 1.538 | 2.091 | Unclassified | 1200 | 0 | 1.538 | Unclassified |
| S33.003 | SWP-31 | 150 | 1.765 | 2.091 | Unclassified | 1200 | 0 | 2.091 | Unclassified |
| S33.004 | SWP-32 | 150 | 1.140 | 1.765 | Unclassified | 1200 | 0 | 1.765 | Unclassified |
| S23.008 | SWP-HB1 | 225 | 1.901 | 2.366 | Unclassified | 1500 | 0 | 2.366 | Unclassified |
| S37.000 | SWP-34 | 300 | 1.482 | 1.589 | Unclassified | 1200 | 0 | 1.521 | Unclassified |
| S37.001 | SWP-TANK 3 | 300 | 1.589 | 1.689 | Unclassified |  |  |  | Junction |
| S38.000 | SWP-36 | 150 | 0.549 | 0.999 | Unclassified |  |  |  | Junction |
| S39.000 | SWP-37 | 150 | 0.507 | 0.999 | Unclassified |  |  |  | Junction |
| S38.001 | SWP-38 | 150 | 0.843 | 0.999 | Unclassified | 600 | 0 | 0.999 | Unclassified |
| S40.000 | SWP-39 | 150 | 0.504 | 0.956 | Unclassified |  |  |  | Junction |
| S41.000 | SWP-40 | 150 | 0.584 | 0.956 | Unclassified |  |  |  | Junction |
| S40.001 | SWP-41 | 150 | 0.956 | 1.689 | Unclassified | 600 | 0 | 0.956 | Unclassified |
| S37.002 | SWP-42 | 300 | 1.689 | 1.810 | Unclassified | 1200 | 0 | 1.689 | Unclassified |
| S37.003 | SWP-TANK 4 | 300 | 1.810 | 1.872 | Unclassified |  |  |  | Junction |
| S23.009 | SWP-HB2 | 225 | 1.539 | 1.901 | Unclassified | 1500 | 0 | 1.901 | Unclassified |
| S42.000 | SWP-45 | 150 | 0.558 | 0.889 | Unclassified |  |  |  | Junction |
| S42.001 | SWP-46 | 150 | 0.824 | 0.889 | Unclassified | 600 | 0 | 0.889 | Unclassified |
| S23.010 | SWP-47 | 300 | 1.528 | 1.575 | Unclassified | 1200 | 0 | 1.539 | Unclassified |
| S23.011 | SWP-TANK 6 | 300 | 1.575 | 1.672 | Unclassified |  |  |  | Junction |
| S43.000 | SWP-49 | 150 | 0.495 | 1.135 | Unclassified |  |  |  | Junction |
| S43.001 | SWP-50 | 150 | 1.084 | 1.135 | Unclassified | 600 | 0 | 1.135 | Unclassified |
| S43.002 | SWP-51 | 150 | 1.084 | 1.653 | Unclassified | 1200 | 0 | 1.084 | Unclassified |
| S43.003 | SWP-52 | 300 | 1.612 | 1.653 | Unclassified | 1200 | 0 | 1.653 | Unclassified |
| S43.004 | SWP-TANK 5 | 300 | 1.627 | 1.672 | Unclassified |  |  |  | Junction |
| S44.000 | SWP-54 | 150 | 0.521 | 0.784 | Unclassified |  |  |  | Junction |
| S45.000 | SWP-55 | 150 | 0.504 | 0.784 | Unclassified |  |  |  | Junction |
| S44.001 | SWP-56 | 150 | 0.784 | 0.896 | Unclassified | 600 | 0 | 0.784 | Unclassified |
| S23.012 | SWP-57 | 300 | 1.354 | 1.672 | Unclassified | 1200 | 0 | 1.672 | Unclassified |



## Network Classifications for Storm - SIte Network

| PN | USMH <br> Name | Pipe Dia (mm) | Min Cover Depth (m) | Max Cover Depth (m) | Pipe Type | $\begin{aligned} & \text { MH } \\ & \text { Dia } \\ & (\mathrm{mm}) \end{aligned}$ |  | MH Ring Depth (m) | MH Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S46.000 | SWP-58 | 150 | 0.364 | 0.578 | Unclassified |  |  |  | Junction |
| S47.000 | SWP-59 | 150 | 0.514 | 0.799 | Unclassified |  |  |  | Junction |
| S23.013 | SWP-60 | 300 | 1.354 | 1.505 | Unclassified | 1200 | 0 | 1.354 | Unclassified |
| S48.000 | SWP-61 | 150 | 0.880 | 0.930 | Unclassified | 600 | 0 | 0.920 | Unclassified |
| S23.014 | SWP-HB3 | 225 | 1.487 | 1.705 | Unclassified | 1500 | 0 | 1.487 | Unclassified |
| S23.015 | SWP-63 | 450 | 1.461 | 1.705 | Unclassified | 1500 | 0 | 1.705 | Unclassified |
| S23.016 | SWP-TANK 7 | 450 | 1.455 | 1.468 | Unclassified |  |  |  | Junction |
| S49.000 | SWP-65 | 225 | 1.236 | 1.562 | Unclassified | 600 | 0 | 1.562 | Unclassified |
| S49.001 | SWP-66 | 225 | 1.236 | 1.421 | Unclassified | 600 | 0 | 1.236 | Unclassified |
| S49.002 | SWP-67 | 225 | 1.215 | 1.440 | Unclassified | 600 | 0 | 1.268 | Unclassified |
| S49.003 | SWP-68 | 225 | 1.215 | 1.792 | Unclassified | 600 | 0 | 1.215 | Unclassified |
| S49.004 | SWP-69 | 225 | 1.688 | 1.792 | Unclassified | 1200 | 0 | 1.792 | Unclassified |
| S50.000 | SWP-70 | 225 | 1.153 | 1.234 | Unclassified | 1200 | 0 | 1.234 | Unclassified |
| S50.001 | SWP-71 | 300 | 1.153 | 1.489 | Unclassified | 1200 | 0 | 1.153 | Unclassified |
| S50.002 | SWP-72 | 300 | 1.489 | 1.654 | Unclassified | 1200 | 0 | 1.489 | Unclassified |
| S23.017 | SWP-CC1 | 150 | 1.724 | 1.763 | Unclassified | 2400 | 0 | 1.763 | Unclassified |
| S23.018 | SWP-PI | 150 | 1.540 | 1.724 | Unclassified |  |  |  | Junction |
| S23.019 | SWP-75 | 150 | 1.395 | 1.673 | Unclassified | 1200 | 0 | 1.540 | Unclassified |

Free Flowing Outfall Details for Storm - SIte Network


Volumetric Runoff Coeff 1.000 Additional Flow - \% of Total Flow 0.000
Areal Reduction Factor 1.000 MADD Factor * $10 \mathrm{~m}^{3} /$ ha Storage 2.000 Hot Start (mins) 0 Inlet Coeffiecient 0.800
Hot Start Level (mm) 0 Flow per Person per Day (l/per/day) 0.000
Manhole Headloss Coeff (Global) $0.500 \quad$ Run Time (mins) 60 Foul Sewage per hectare (l/s) $0.000 \quad$ Output Interval (mins) 1

Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 3 Number of Online Controls 4 Number of Storage Structures 20 Number of Real Time Controls 0

## Synthetic Rainfall Details

| Rainfall Model | FSR | Profile Type | Summer |
| ---: | ---: | ---: | ---: |
| Return Period (years) | 100 | $C v$ (Summer) | 1.000 |
| Region England and Wales | Cv (Winter) | 0.840 |  |
| M5-60 (mm) | 17.000 | Storm Duration (mins) | 30 |
| Ratio R | 0.336 |  |  |


| Jacobs Engineering Limited |  | Page 18 |
| :---: | :---: | :---: |
|  | Bishop Auckland <br> Bus Station and Car Park |  |
| Date 13/12/2022 09:26 <br> File BA-Drainage Model_v19.MDX | Designed by G.Jones <br> Checked by S.Clark | Drainage |
| Innovyze | Network 2020.1.3 |  |

Hydro-Brake® Optimum Manhole: SWP-HB1, DS/PN: S23.008, Volume (m ${ }^{3}$ ): 5.2

| Unit Reference MD-SHE-0097-4500-1250-4500 |  |
| ---: | ---: |
| Design Head (m) | 1.250 |
| Design Flow (l/s) | 4.5 |
| Flush-Flo | Calculated |
| Objective | Minimise upstream storage |
| Application | Surface |
| Sump Available | Yes |
| Diameter (mm) | 97 |
| Invert Level (m) | 96.605 |
| Pipe Diameter (mm) | 150 |
| Dianhole Diameter (mm) | 1200 |



The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

| Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 0.100 | 3.1 | 0.800 |  | 3.7 | 2.000 | 5.6 | 4.000 | 7.8 | 7.000 | 10.1 |
| 0.200 | 4.2 | 1.000 | 4.1 | 2.200 | 5.9 | 4.500 | 8.2 | 7.500 | 10.4 |  |
| 0.300 | 4.5 | 1.200 | 4.4 | 2.400 | 6.1 | 5.000 | 8.6 | 8.000 | 10.8 |  |
| 0.400 | 4.5 | 1.400 | 4.7 | 2.600 | 6.3 | 5.500 | 9.0 | 8.500 | 11.1 |  |
| 0.500 | 4.4 | 1.600 | 5.0 | 3.000 | 6.8 | 6.000 | 9.4 | 9.000 | 11.4 |  |
| 0.600 | 4.3 | 1.800 | 5.3 | 3.500 | 7.3 | 6.500 | 9.8 | 9.500 | 11.7 |  |

Hydro-Brake® Optimum Manhole: SWP-HB2, DS/PN: S23.009, Volume (m³): 4.8

| Unit Reference | MD-SHE-0097-4000-0850-4000 |
| ---: | ---: |
| Design Head (m) | 0.850 |
| Design Flow (l/s) | 4.0 |
| Flush-Flo | Calculated |
| Objective | Minimise upstream storage |
| Application | Surface |
| Sump Available | Yes |
| Diameter (mm) | 97 |
| Invert Level (m) | 96.200 |
| Minimum Outlet Pipe Diameter (mm) | 150 |
| Suggested Manhole Diameter (mm) | 1200 |



The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brakeß Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m) Flow (l/s) Depth (m) Flow (l/s)| Depth (m) Flow (1/s)|Depth (m) Flow (l/s) Depth (m) Flow (l/s)
0.100

| 4.0 | 0.500 |
| :--- | :--- |
| 3.9 | 0.600 |


| 3.6 | 0.800 |
| :--- | :--- |
| 3.4 | 1.000 |

3.9
4.3
1.200
1.400

| 0.200 | 4.0 | 0.400 | 3.9 | 0.600 | 3.4 | 1.000 | 4.3 | 1.400 | 5.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Jacobs Engineering Limited |  |  |  |  | Page 19 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - |  | Bishop Auckland <br> Bus Station and Car Park |  |  | Micro Drainage |  |
| Date 13/12/2022 09:26File BA-Drainage Model_v19.MDX |  | Designed by G.Jones Checked by S.Clark |  |  |  |  |
| Innovyze Network 2020.1.3 |  |  |  |  |  |  |
| Hydro-Brake® Optimum Manhole: SWP-HB2, DS/PN: S23.009, Volume (m³): 4.8 |  |  |  |  |  |  |
| Depth (m) Flow (1/s) | Depth (m) Flow (1/s) | Depth (m) Flow (1/s) | Depth (m) Flow (1/s) | Depth (m) | m) Flow | (1/s) |
| 1.600 5.4 | $2.400 \quad 6.5$ | 4.0008 .2 | 6.00010 .0 | 8.000 |  | 11.5 |
| 1.800 5.7 | $2.600 \quad 6.7$ | 4.5008 .7 | $6.500 \quad 10.4$ | 8.500 |  | 11.8 |
| $2.000 \quad 6.0$ | $3.000 \quad 7.2$ | $5.000 \quad 9.2$ | 7.00010 .8 | 9.000 |  | 12.1 |
| $2.200 \quad 6.2$ | $3.500 \quad 7.7$ | $5.500 \quad 9.6$ | 7.50011 .1 | 9.500 |  | 12.4 |

Hydro-Brake® Optimum Manhole: SWP-HB3, DS/PN: S23.014, Volume (m³): 3.4

| Unit Reference | MD-SHE-0107-5000-0900-5000 |
| ---: | ---: |
| Design Head (m) | 0.900 |
| Design Flow (l/s) | 5.0 |
| Flush-Flo | Calculated |
| Objective | Minimise upstream storage |
| Application | Surface |
| Sump Available | Yes |
| Diameter (mm) | 107 |
| Invert Level (m) | 95.400 |
| Minimum Outlet Pipe Diameter (mm) | 150 |
| Suggested Manhole Diameter (mm) |  |



The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

| Depth (m) | Flow (1/s) | Depth (m) | Flow (1/s) | Depth (m) | Flow (1/s) | Depth (m) | Flow (1/s) | Depth (m) | Flow | (1/s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.100 | 3.6 | 0.800 | 4.7 | 2.00 | 7.2 | 4.000 | 10.1 | 7.000 |  | 13.1 |
| 0.200 | 4.9 | 1.000 | 5.2 | 2.20 | 7.6 | 4.500 | 10.6 | 7.500 |  | 13.6 |
| 0.300 | 5.0 | 1.200 | 5.7 | 2.40 | 7.9 | 5.000 | 11.2 | 8.000 |  | 14.0 |
| 0.400 | 4.9 | 1.400 | 6.1 | 2.60 | 8.2 | 5.500 | 11.7 | 8.500 |  | 14.4 |
| 0.500 | 4.6 | 1.600 | 6.5 | 3.00 | 8.8 | 6.000 | 12.2 | 9.000 |  | 14.8 |
| 0.600 | 4.1 | 1.800 | 6.9 | 3.50 | 9.4 | 6.500 | 12.7 | 9.500 |  | 15.2 |

Complex Manhole: SWP-CC1, DS/PN: S23.017, Volume (m³): 12.6

## Hydro-Brake® Optimum

| Unit Reference MD-SHE-0090-3000-0500-3000 |  |
| ---: | ---: |
| Design Head (m) | 0.500 |
| Design Flow (l/s) | 3.0 |
| Flush-Flo |  |
| Objective | Minimise upstream storage |
| Application | Calculated |
| Sump Available | Surface |
| Diameter (mm) | Yes |
| Invert Level (m) | 90 |
| Minimum Outlet Pipe Diameter (mm) | 94.433 |
| Suggested Manhole Diameter (mm) | 150 |


| Control Points | Head (m) Flow (1/s) | Control Points Head (m) Flow (1/s) |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Design Point (Calculated) | 0.500 | 3.0 | Flush-Flo |  |
| TM | 0.157 | 3.0 |  |  |



The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

| Depth (m) Flow (l/s) | Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) |  |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 0.100 | 2.8 | 0.800 |  | 3.7 | 2.000 | 5.7 | 4.000 | 7.9 | 7.000 | 10.4 |
| 0.200 | 3.0 | 1.000 | 4.1 | 2.200 | 6.0 | 4.500 | 8.4 | 7.500 | 10.7 |  |
| 0.300 | 2.8 | 1.200 | 4.5 | 2.400 | 6.2 | 5.000 | 8.8 | 8.000 | 11.1 |  |
| 0.400 | 2.7 | 1.400 | 4.8 | 2.600 | 6.4 | 5.500 | 9.2 | 8.500 | 11.4 |  |
| 0.500 | 3.0 | 1.600 | 5.1 | 3.000 | 6.9 | 6.000 | 9.6 | 9.000 | 11.8 |  |
| 0.600 | 3.3 | 1.800 | 5.4 | 3.500 | 7.4 | 6.500 | 10.0 | 9.500 | 12.1 |  |

## Orifice

Diameter (m) 0.054 Discharge Coefficient 0.600 Invert Level (m) 94.933

| Jacobs Engineering Limited |  | Page 21 |
| :---: | :---: | :---: |
|  | Bishop Auckland <br> Bus Station and Car Park |  |
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| Innovyze | Network 2020.1.3 |  |



Porous Car Park Manhole: SWP-18, DS/PN: S29.001

| Infiltration Coefficient Base (m/hr) | 0.00000 | Width (m) | 5.0 |
| ---: | ---: | ---: | ---: | ---: |
| Membrane Percolation (mm/hr) | 1000 | Length (m) | 25.0 |
| Max Percolation (l/s) | 34.7 | Slope (1:X) | 58.8 |
| Safety Factor | 2.0 | Depression Storage (mm) | 5 |
| Porosity | 0.30 | Evaporation (mm/day) | 3 |
| Invert Level (m) | 98.912 | Cap Volume Depth (m) | 0.200 |

Porous Car Park Manhole: SWP-21, DS/PN: S31.001

| Infiltration Coefficient Base (m/hr) | 0.00000 | Width (m) | 5.0 |
| ---: | ---: | ---: | ---: | ---: |
| Membrane Percolation (mm/hr) | 1000 | Length (m) | 25.0 |
| Max Percolation (l/s) | 34.7 | Slope (1:X) | 36.2 |
| Safety Factor | 2.0 | Depression Storage (mm) | 5 |
| Porosity | 0.30 | Evaporation (mm/day) | 3 |
| Invert Level (m) | 98.381 | Cap Volume Depth (m) | 0.200 |


| Jacobs Engineering Limited |  | Page 22 |
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Cellular Storage Manhole: SWP-TANK 2, DS/PN: S23.007

| Invert Level (m) | 96.655 | Safety Factor | 2.0 |
| ---: | ---: | ---: | ---: | ---: |
| Infiltration Coefficient Base (m/hr) | 0.00000 | Porosity | 0.95 |
| Infiltration Coefficient Side (m/hr) | 0.00000 |  |  |


| Depth (m) | Area ( $\mathrm{m}^{2}$ ) | Inf. Area (m²) | Depth (m) | Area ( $\mathrm{m}^{2}$ ) | Inf. Area (m²) | Depth (m) | Area | $\left(\mathrm{m}^{2}\right)$ | Inf. Area | $\left(\mathrm{m}^{2}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.000 | 40.0 | 40.0 | 1.200 | 40.0 | 73.6 | 1.201 |  | 0.0 |  | 73.6 |

Porous Car Park Manhole: SWP-26, DS/PN: S33.001

| Infiltration Coefficient Base (m/hr) | 0.0000 | Width (m) | 5.0 |
| ---: | ---: | ---: | ---: | ---: |
| Membrane Percolation (mm/hr) | 1000 | Length (m) | 22.5 |
| Max Percolation (l/s) | 31.3 | Slope (1:X) | 34.4 |
| Safety Factor | 2.0 | Depression Storage (mm) | 5 |
| Porosity | 0.30 | Evaporation (mm/day) | 3 |
| Invert Level (m) | 99.601 | Cap Volume Depth (m) | 0.200 |

Porous Car Park Manhole: SWP-29, DS/PN: S35.001

| Infiltration Coefficient Base (m/hr) | 0.0000 | Width (m) | 5.0 |
| ---: | ---: | ---: | ---: | ---: |
| Membrane Percolation (mm/hr) | 1000 | Length (m) | 25.0 |
| Max Percolation (l/s) | 34.7 | Slope (1:X) | 38.8 |
| Safety Factor | 2.0 | Depression Storage (mm) | 5 |
| Porosity | 0.30 | Evaporation (mm/day) | 3 |
| Invert Level (m) | 99.166 | Cap Volume Depth (m) | 0.200 |

Cellular Storage Manhole: SWP-TANK 3, DS/PN: S37.001

Invert Level (m) 96.350 Safety Factor 2.0
Infiltration Coefficient Base (m/hr) 0.00000 Porosity 0.95
Infiltration Coefficient Side (m/hr) 0.00000


Porous Car Park Manhole: SWP-38, DS/PN: S38.001

$$
\begin{aligned}
& \text { Infiltration Coefficient Base (m/hr) } 0.00000 \text { Width (m) } 5.0 \\
& \text { Membrane Percolation (mm/hr) } 1000 \text { Length (m) } 25.0 \\
& \text { Max Percolation (l/s) } 34.7 \quad \text { Slope (1:X) } 24.7 \\
& \text { Safety Factor } 2.0 \text { Depression Storage (mm) } 5 \\
& \text { Porosity } 0.30 \text { Evaporation (mm/day) } 3 \\
& \text { Invert Level (m) } 98.092 \text { Cap Volume Depth (m) } 0.200 \\
& \text { Porous Car Park Manhole: SWP-41, DS/PN: S40.001 } \\
& \text { Infiltration Coefficient Base (m/hr) } 0.00000 \\
& \text { Membrane Percolation (mm/hr) } 1000 \\
& 1000 \quad \text { Width (m) } \quad 5.0 \\
& \text { Max Percolation (l/s) } 27.8 \\
& \text { Safety Factor } 2.0 \text { Depression Storage (mm) } 5 \\
& \text { Porosity } 0.30 \text { Evaporation (mm/day) } 3 \\
& \text { Invert Level (m) } 97.579 \text { Cap Volume Depth (m) } 0.200
\end{aligned}
$$

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| :--- | :--- | :--- |
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| Innovyze |  |  |

Cellular Storage Manhole: SWP-TANK 4, DS/PN: S37.003

| Invert Level (m) | 96.250 | Safety Factor | 2.0 |  |
| :--- | ---: | ---: | ---: | ---: |
| Infiltration Coefficient Base (m/hr) | 0.00000 | Porosity | 0.95 |  |
| Infiltration Coefficient Side | $(\mathrm{m} / \mathrm{hr})$ | 0.00000 |  |  |



Porous Car Park Manhole: SWP-46, DS/PN: S42.001

| Infiltration Coefficient Base (m/hr) | 0.0000 | Width (m) | 5.0 |
| ---: | ---: | ---: | ---: | ---: |
| Membrane Percolation (mm/hr) | 1000 | Length (m) | 35.0 |
| Max Percolation (l/s) | 48.6 | Slope (1:X) | 18.8 |
| Safety Factor | 2.0 | Depression Storage (mm) | 5 |
| Porosity | 0.30 | Evaporation (mm/day) | 3 |
| Invert Level (m) | 97.258 | Cap Volume Depth (m) | 0.200 |

Cellular Storaqe Manhole: SWP-TANK 6, DS/PN: S23.011

| Invert Level (m) | 95.550 | Safety Factor | 2.0 |
| ---: | ---: | ---: | ---: | ---: |
| Infiltration Coefficient Base $(\mathrm{m} / \mathrm{hr})$ | 0.00000 | Porosity | 0.95 |
| Infiltration Coefficient Side $(\mathrm{m} / \mathrm{hr})$ | 0.00000 |  |  |

Depth ( m ) Area ( $\mathrm{m}^{2}$ ) Inf. Area ( $\mathrm{m}^{2}$ ) Depth ( m ) Area ( $\mathrm{m}^{2}$ ) Inf. Area ( $\mathrm{m}^{2}$ ) Depth (m) Area ( $\mathrm{m}^{2}$ ) Inf. Area ( $\mathrm{m}^{2}$ )

| 0.000 | 40.0 | 40.0 | 0.800 | 40.0 | 62.4 | 0.801 | 0.0 | 62.4 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Porous Car Park Manhole: SWP-50, DS/PN: S43.001

| Infiltration Coefficient Base (m/hr) | 0.00000 | Width (m) | 5.0 |
| ---: | ---: | ---: | ---: | ---: | ---: |
| Membrane Percolation (mm/hr) | 1000 | Length (m) | 32.0 |
| Max Percolation (l/s) | 44.4 | Slope (1:X) | 31.8 |
| Safety Factor | 2.0 | Depression Storage (mm) | 5 |
| Sorosity | 0.30 | Evaporation (mm/day) | 3 |
| Invert Level (m) | 97.690 | Cap Volume Depth (m) | 0.200 |

Cellular Storage Manhole: SWP-TANK 5, DS/PN: S43.004

| Invert Level (m) | 95.550 | Safety Factor | 2.0 |
| ---: | ---: | ---: | ---: | ---: |
| Infiltration Coefficient Base (m/hr) | 0.00000 | Porosity 0.95 |  |

Infiltration Coefficient Side (m/hr) 0.00000
Depth (m) Area ( $\mathrm{m}^{2}$ ) Inf. Area ( $\mathrm{m}^{2}$ ) Depth (m) Area ( $\mathrm{m}^{2}$ ) Inf. Area ( $\mathrm{m}^{2}$ ) Depth (m) Area ( $\mathrm{m}^{2}$ ) Inf. Area ( $\mathrm{m}^{2}$ )

| 0.000 | 48.0 | 48.0 | 0.800 | 48.0 | 73.6 | 0.801 | 0.0 | 73.6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Porous Car Park Manhole: SWP-56, DS/PN: S44.001

| Infiltration Coefficient Base (m/hr) | 0.00000 | Width (m) | 5.0 |
| ---: | ---: | ---: | ---: | ---: |
| Membrane Percolation (mm/hr) | 1000 | Length (m) | 20.0 |
| Max Percolation (l/s) | 27.8 | Slope (1:X) | 35.7 |
| Safety Factor | 2.0 | Depression Storage (mm) | 5 |
| Porosity | 0.30 | Evaporation (mm/day) | 3 |
| Invert Level (m) | 97.364 | Cap Volume Depth (m) | 0.200 |


| Jacobs Engineering Limited | Page 24 |  |
| :--- | :--- | :--- |
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| Innovyze |  |  |

Porous Car Park Manhole: SWP-60, DS/PN: S23.013

| Infiltration Coefficient Base (m/hr) | 0.00000 | Width (m) | 5.0 |
| ---: | ---: | ---: | ---: | ---: | ---: |
| Membrane Percolation (mm/hr) | 1000 | Length (m) | 34.2 |
| Max Percolation (l/s) | 47.5 | Slope (1:X) | 33.1 |
| Safety Factor | 2.0 | Depression Storage (mm) | 5 |
| Porosity | 0.30 | Evaporation (mm/day) | 3 |
| Invert Level (m) | 96.772 | Membrane Depth (mm) | 0 |

Cellular Storage Manhole: SWP-TANK 7, DS/PN: S23.016

Invert Level (m) 94.483 Safety Factor 2.0
Infiltration Coefficient Base (m/hr) 0.00000 Porosity 0.95 Infiltration Coefficient Side (m/hr) 0.00000

| Depth (m) | Area (m²) | Inf. Area (m²) | Depth (m) | Area (m²) | Inf. Area (m²) | Depth (m) | Area (m²) | Inf. | Area | $\left(m^{2}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.000 | 312.0 | 312.0 | 0.800 | 312.0 | 371.2 | 0.801 | 0.0 |  |  | 371.2 |


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| :---: | :---: | :---: |
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| Innovyze | Network 2020.1.3 |  |
| 1 year Return Period Summary | ical Results by Maximum L SIte Network | for storm - |

Simulation Criteria<br>Areal Reduction Factor 1.000 Additional Flow - of Total Flow 0.000 Hot Start (mins) $0 \quad$ MADD Factor * $10 \mathrm{~m}^{3} /$ ha Storage 2.000 Hot Start Level (mm) Inlet Coeffiecient 0.800 Manhole Headloss Coeff (Global) 0.500 Flow per Person per Day (l/per/day) 0.000 Foul Sewage per hectare (l/s) 0.000

Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 3 Number of Online Controls 4 Number of Storage Structures 20 Number of Real Time Controls 0

Synthetic Rainfall Details
Rainfall Model FSR M5-60 (mm) 17.000 Cv (Summer) 1.000
Region England and Wales Ratio R 0.336 Cv (Winter) 1.000

Margin for Flood Risk Warning (mm) 300.0
Analysis Timestep 2.5 Second Increment (Extended)
DTS Status ON
DVD Status ON
Inertia Status ON
Profile(s)
Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960, 1440
Return Period(s) (years)
Climate Change (\%)

| US/MH <br> Name |  | Storm | Return <br> Period | Climate Change | First (X) <br> Surcharge | $\begin{gathered} \text { First (Y) } \\ \text { Flood } \end{gathered}$ | First (Z) Overflow | Overflow Act. | Water <br> Level <br> (m) | Surcharged Depth <br> (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SWP-1 | 15 | Summer | 1 | +45\% |  |  |  |  | 100.293 | -0.117 |
| SWP-2 | 15 | Summer | 1 | +45\% |  |  |  |  | 99.259 | -0.108 |
| SWP-3 | 15 | Summer | 1 | +45\% |  |  |  |  | 99.517 | -0.150 |
| SWP-4 | 15 | Summer | 1 | +45\% |  |  |  |  | 99.150 | -0.150 |
| SWP-5 | 15 | Summer | 1 | +45\% |  |  |  |  | 98.987 | -0.150 |
| SWP-6 | 15 | Summer | 1 | +45\% | 100/15 Summer |  |  |  | 98.749 | -0.099 |
| SWP-7 | 15 | Summer | 1 | +45\% |  |  |  |  | 99.646 | -0.150 |
| SWP-8 | 15 | Summer | 1 | +45\% | 100/15 Summer |  |  |  | 98.575 | -0.110 |
| SWP-9 | 15 | Summer | 1 | +45\% |  |  |  |  | 99.409 | -0.150 |
| SWP-10 | 15 | Summer | 1 | +45\% | 100/15 Summer |  |  |  | 98.803 | -0.114 |
| SWP-11 | 15 | Summer | 1 | +45\% | 100/15 Summer |  |  |  | 98.508 | -0.092 |
| SWP-12 | 15 | Summer | 1 | +45\% |  |  |  |  | 99.126 | -0.150 |
| SWP-13 | 15 | Summer | 1 | +45\% | 100/240 Summer |  |  |  | 97.741 | -0.102 |
| SWP-14 | 120 | Summer | 1 | +45\% | 30/15 Summer |  |  |  | 96.933 | -0.172 |
| SP-TANK 1 | 120 | Summer | 1 | +45\% | 30/15 Summer |  |  |  | 96.932 | -0.123 |
| SWP-16 | 15 | Summer | 1 | +45\% |  |  |  |  | 98.372 | -0.150 |
| SWP-17 | 15 | Summer | 1 | +45\% |  |  |  |  | 98.923 | -0.150 |
| SWP-18 | 15 | Summer | 1 | +45\% |  |  |  |  | 98.195 | -0.118 |
| SWP-19 | 15 | Summer | 1 | +45\% |  |  |  |  | 98.312 | -0.150 |
| SWP-20 | 15 | Summer | 1 | +45\% |  |  |  |  | 97.924 | -0.150 |
| SWP-21 | 15 | Summer | 1 | +45\% | 30/15 Summer |  |  |  | 97.723 | -0.088 |
| SWP-22 | 120 | Summer | 1 | +45\% | 30/15 Summer |  |  |  | 96.931 | -0.074 |
| SPP-TANK 2 | 120 | Summer | 1 | +45\% | 30/15 Summer |  |  |  | 96.929 | -0.026 |
| SWP-24 | 15 | Summer | 1 | +45\% |  |  |  |  | 99.001 | -0.150 |
| SWP-25 | 15 | Summer | 1 | +45\% |  |  |  |  | 99.916 | -0.150 |
| SWP-26 | 15 | Summer | 1 | +45\% | 100/15 Summer |  |  |  | 98.823 | -0.119 |
| SWP-27 | 15 | Summer | 1 | +45\% |  |  |  |  | 99.336 | -0.150 |
| SWP-28 | 15 | Summer | 1 | +45\% |  |  |  |  | 98.607 | -0.150 |
| SWP-29 | 15 | Summer | 1 | +45\% | 30/15 Summer |  |  |  | 98.458 | -0.090 |

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| PN | US/MH <br> Name | Flooded <br> Volume <br> ( $\mathrm{m}^{3}$ ) | $\begin{gathered} \text { Flow / } \\ \text { Cap. } \end{gathered}$ | Overflow (1/s) | Half Drain Time (mins) | Pipe <br> Flow <br> (1/s) | Status | Level <br> Exceeded |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S23.000 | SWP-1 | 0.000 | 0.11 |  |  | 4.1 | OK |  |
| S23.001 | SWP-2 | 0.000 | 0.18 |  |  | 5.9 | OK |  |
| S24.000 | SWP-3 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S25.000 | SWP-4 | 0.000 | 0.00 |  |  | 0.0 | OK |  |
| S24.001 | SWP -5 | 0.000 | 0.00 |  |  | 0.0 | OK |  |
| S23.002 | SWP-6 | 0.000 | 0.25 |  |  | 5.9 | OK |  |
| S26.000 | SWP-7 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S26.001 | SWP-8 | 0.000 | 0.12 |  | 7 | 2.2 | OK |  |
| S27.000 | SWP-9 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S27.001 | SWP-10 | 0.000 | 0.13 |  | 9 | 4.5 | OK |  |
| S23.003 | SWP-11 | 0.000 | 0.32 |  |  | 12.9 | OK |  |
| S28.000 | SWP-12 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S28.001 | SWP-13 | 0.000 | 0.18 |  | 7 | 3.2 | OK |  |
| S23.004 | SWP-14 | 0.000 | 0.15 |  |  | 9.0 | OK |  |
| S23.005 | SWP-TANK 1 | 0.000 | 0.07 |  | 55 | 4.5 | OK* |  |
| S29.000 | SWP-16 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S30.000 | SWP-17 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S29.001 | SWP-18 | 0.000 | 0.09 |  | 8 | 4.1 | OK |  |
| S31.000 | SWP-19 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S32.000 | SWP-20 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S31.001 | SWP-21 | 0.000 | 0.36 |  | 8 | 7.0 | OK |  |
| S23.006 | SWP-22 | 0.000 | 0.16 |  |  | 10.0 | OK |  |
| S23.007 | SWP-TANK 2 | 0.000 | 0.05 |  | 73 | 4.4 | OK* |  |
| S33.000 | SWP-24 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S34.000 | SWP-25 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S33.001 | SWP-26 | 0.000 | 0.08 |  | 8 | 3.4 | OK |  |
| S35.000 | SWP-27 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S36.000 | SWP-28 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S35.001 | SWP-29 | 0.000 | 0.34 |  | 8 | 6.6 | OK |  |



| PN | US/MH <br> Name | Storm | Return <br> Period | Climate <br> Change | First (X) Surcharge | $\begin{gathered} \text { First (Y) } \\ \text { Flood } \end{gathered}$ | First (Z) Overflow | Overflow Act. | Water <br> Level <br> (m) | Surcharged Depth (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S33.002 | SWP-30 | 15 Summer | 1 | +45\% | 30/15 Summer |  |  |  | 98.367 | -0.069 |
| S33.003 | SWP-31 | 15 Summer | 1 | +45\% | 30/15 Summer |  |  |  | 98.230 | -0.060 |
| S33.004 | SWP-32 | 15 Summer | 1 | +45\% | 30/15 Summer |  |  |  | 98.160 | -0.069 |
| S23.008 | SWP-HB1 | 120 Summer | 1 | +45\% | 1/15 Summer |  |  |  | 96.936 | 0.106 |
| S37.000 | SWP-34 | 360 Summer | 1 | +45\% | $30 / 240$ Summer |  |  |  | 96.483 | -0.217 |
| S37.001 | SWP-TANK 3 | 360 Summer | 1 | +45\% | $30 / 240$ Summer |  |  |  | 96.483 | -0.167 |
| S38.000 | SWP-36 | 15 Summer | 1 | +45\% |  |  |  |  | 97.935 | -0.150 |
| S39.000 | SWP-37 | 15 Summer | 1 | +45\% |  |  |  |  | 97.690 | -0.150 |
| S38.001 | SWP-38 | 15 Summer | 1 | +45\% |  |  |  |  | 97.422 | -0.100 |
| S40.000 | SWP-39 | 15 Summer | 1 | +45\% |  |  |  |  | 97.242 | -0.150 |
| S41.000 | SWP-40 | 15 Summer | 1 | +45\% |  |  |  |  | 97.267 | -0.150 |
| S40.001 | SWP-41 | 15 Summer | 1 | +45\% | 100/960 Summer |  |  |  | 96.899 | -0.110 |
| S37.002 | SWP-42 | 360 Summer | 1 | +45\% | 30/120 Winter |  |  |  | 96.483 | -0.117 |
| S37.003 | SWP-TANK 4 | 360 Summer | 1 | +45\% | $30 / 120$ Summer |  |  |  | 96.483 | -0.067 |
| S23.009 | SWP-HB2 | 360 Summer | 1 | +45\% | 1/120 Summer |  |  |  | 96.483 | 0.058 |
| S42.000 | SWP-45 | 15 Summer | 1 | +45\% |  |  |  |  | 98.403 | -0.150 |
| S42.001 | SWP-46 | 30 Summer | 1 | +45\% |  |  |  |  | 96.584 | -0.104 |
| S23.010 | SWP-47 | 360 Summer | 1 | +45\% | 30/60 Summer |  |  |  | 95.724 | -0.176 |
| S23.011 | SWP-TANK 6 | 360 Summer | 1 | +45\% | 30/30 Winter |  |  |  | 95.722 | -0.128 |
| S43.000 | SWP-49 | 15 Summer | 1 | +45\% |  |  |  |  | 98.223 | -0.150 |
| S43.001 | SWP-50 | 30 Summer | 1 | +45\% |  |  |  |  | 96.771 | -0.107 |
| S43.002 | SWP-51 | 30 Summer | 1 | +45\% |  |  |  |  | 96.667 | -0.128 |
| S43.003 | SWP-52 | 360 Summer | 1 | +45\% | 30/60 Summer |  |  |  | 95.718 | -0.182 |
| S43.004 | SWP-TANK 5 | 360 Summer | 1 | +45\% | 30/60 Summer |  |  |  | 95.718 | -0.132 |
| S44.000 | SWP-54 | 15 Summer | 1 | +45\% |  |  |  |  | 96.982 | -0.150 |
| S45.000 | SWP-55 | 15 Summer | 1 | +45\% |  |  |  |  | 97.008 | -0.150 |
| S44.001 | SWP-56 | 15 Summer | 1 | +45\% |  |  |  |  | 96.832 | -0.117 |
| S23.012 | SWP-57 | 360 Summer | 1 | +45\% | 30/15 Summer |  |  |  | 95.723 | -0.077 |
| S46.000 | SWP-58 | 15 Summer | 1 | +45\% |  |  |  |  | 96.844 | -0.150 |
| S47.000 | SWP-59 | 15 Summer | 1 | +45\% |  |  |  |  | 96.434 | -0.150 |
| S23.013 | SWP-60 | 360 Summer | 1 | +45\% | 30/15 Summer |  |  |  | 95.726 | -0.024 |
| S48.000 | SWP-61 | 15 Summer | 1 | +45\% | 100/240 Summer |  |  |  | 96.194 | -0.150 |
| S23.014 | SWP-HB3 | 360 Summer | 1 | +45\% | 1/15 Summer |  |  |  | 95.726 | 0.101 |
| S23.015 | SWP-63 | 960 Summer | 1 | +45\% | $30 / 360$ Summer |  |  |  | 94.860 | -0.123 |
| S23.016 | SWP-TANK 7 | 960 Summer | 1 | +45\% | 30/240 Summer |  |  |  | 94.859 | -0.074 |
| S49.000 | SWP-65 | 60 Summer | 1 | +45\% |  |  |  |  | 95.569 | -0.206 |
| S49.001 | SWP-66 | 60 Summer | 1 | +45\% |  |  |  |  | 95.312 | -0.202 |
| S49.002 | SWP-67 | 60 Summer | 1 | +45\% | 30/960 Winter |  |  |  | 94.899 | -0.192 |
| S49.003 | SWP-68 | 960 Summer | 1 | +45\% | 30/15 Summer |  |  |  | 94.859 | -0.041 |
| S49.004 | SWP-69 | 960 Summer | 1 | +45\% | 1/240 Summer |  |  |  | 94.857 | 0.117 |
| S50.000 | SWP-70 | 960 Summer | 1 | +45\% | 30/15 Summer |  |  |  | 94.859 | -0.081 |
| S50.001 | SWP-71 | 960 Summer | 1 | +45\% | 1/960 Summer |  |  |  | 94.858 | 0.021 |
| S50.002 | SWP-72 | 960 Summer | 1 | +45\% | 1/360 Summer |  |  |  | 94.857 | 0.080 |
| S23.017 | SWP-CC1 | 960 Summer | 1 | +45\% | 1/15 Summer |  |  |  | 94.857 | 0.274 |
| S23.018 | SWP-PI | 1440 Winter | 1 | +45\% |  |  |  |  | 94.415 | -0.109 |
| S23.019 | SWP-75 | 1440 Summer | 1 | +45\% |  |  |  |  | 94.321 | -0.099 |



| Jacobs Engineering Limited |  | Page 4 |
| :---: | :---: | :---: |
|  | Bishop Auckland <br> Bus Station and Car Park | Micro Drainage |
| Date 13/12/2022 09:28 <br> File BA-Drainage Model_v19.MDX | Designed by G.Jones Checked by S.Clark |  |
| Innovyze | Network 2020.1.3 |  |
| 1 year Return Period Summary | ical Results by Maximum Lever | for Storm - |


| PN | Flooded |  |  |  | Half Drain | Pipe |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | US/MH <br> Name | Volume $\left(\mathrm{m}^{3}\right)$ | Flow / Cap. | $\begin{aligned} & \text { Overflow } \\ & (1 / s) \end{aligned}$ |  | $\begin{aligned} & \text { Flow } \\ & (1 / s) \end{aligned}$ | Status | Level <br> Exceeded |
| S37.000 | SWP-34 | 0.000 | 0.00 |  |  | 0.0 | OK |  |
| S37.001 | SWP-TANK 3 | 0.000 | 0.03 |  | 58 | 1.6 | OK* |  |
| S38.000 | SWP-36 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S39.000 | SWP-37 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S38.001 | SWP-38 | 0.000 | 0.22 |  | 8 | 3.8 | OK |  |
| S40.000 | SWP-39 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S41.000 | SWP-40 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S40.001 | SWP-41 | 0.000 | 0.16 |  | 7 | 5.8 | OK |  |
| S37.002 | SWP-42 | 0.000 | 0.04 |  |  | 2.5 | OK |  |
| S37.003 | SWP-TANK 4 | 0.000 | 0.05 |  | 77 | 3.3 | OK* |  |
| S23.009 | SWP-HB2 | 0.000 | 0.05 |  |  | 3.9 | SURCHARGED |  |
| S42.000 | SWP-45 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S42.001 | SWP-46 | 0.000 | 0.20 |  | 8 | 3.5 | OK |  |
| S23.010 | SWP-47 | 0.000 | 0.08 |  |  | 4.9 | OK |  |
| S23.011 | SWP-TANK 6 | 0.000 | 0.10 |  | 178 | 6.2 | OK* |  |
| S43.000 | SWP-49 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S43.001 | SWP-50 | 0.000 | 0.15 |  | 8 | 2.8 | OK |  |
| S43.002 | SWP-51 | 0.000 | 0.05 |  |  | 2.7 | OK |  |
| S43.003 | SWP-52 | 0.000 | 0.01 |  |  | 0.8 | OK |  |
| S43.004 | SWP-TANK 5 | 0.000 | 0.04 |  | 179 | 2.6 | OK* |  |
| S44.000 | SWP-54 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S45.000 | SWP-55 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S44.001 | SWP-56 | 0.000 | 0.11 |  | 7 | 4.2 | OK |  |
| S23.012 | SWP-57 | 0.000 | 0.11 |  |  | 6.8 | OK |  |
| S46.000 | SWP-58 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S47.000 | SWP-59 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S23.013 | SWP-60 | 0.000 | 0.09 |  | 164 | 5.8 | OK |  |
| S48.000 | SWP-61 | 0.000 | 0.00 |  |  | 0.0 | OK |  |
| S23.014 | SWP-HB3 | 0.000 | 0.04 |  |  | 5.0 | SURCHARGED |  |
| S23.015 | SWP-63 | 0.000 | 0.04 |  |  | 5.0 | OK |  |
| S23.016 | SWP-TANK 7 | 0.000 | 0.03 |  | 516 | 4.5 | OK* |  |
| S49.000 | SWP-65 | 0.000 | 0.02 |  |  | 0.9 | OK |  |
| S49.001 | SWP-66 | 0.000 | 0.02 |  |  | 1.8 | OK |  |
| S49.002 | SWP-67 | 0.000 | 0.05 |  |  | 2.7 | OK |  |
| S49.003 | SWP-68 | 0.000 | 0.03 |  |  | 1.2 | OK |  |
| S49.004 | SWP-69 | 0.000 | 0.03 |  |  | 1.1 | SURCHARGED |  |
| S50.000 | SWP-70 | 0.000 | 0.08 |  |  | 2.9 | OK |  |
| S50.001 | SWP-71 | 0.000 | 0.08 |  |  | 4.7 | SURCHARGED |  |
| S50.002 | SWP-72 | 0.000 | 0.08 |  |  | 4.6 | SURCHARGED |  |
| S23.017 | SWP-CC1 | 0.000 | 0.20 |  |  | 3.0 | SURCHARGED |  |
| S23.018 | SWP-PI | 0.000 | 0.17 |  |  | 3.0 | OK* |  |
| S23.019 | SWP-75 | 0.000 | 0.26 |  |  | 3.0 | OK |  |


| Jacobs Engineering Limited |  | Page 5 |
| :---: | :---: | :---: |
| $\cdot$ | Bishop Auckland <br> Bus Station and Car Park |  |
| Date 13/12/2022 09:28 <br> File BA-Drainage Model_v19.MDX | Designed by G.Jones Checked by S.Clark | Drainage |
| Innovyze | Network 2020.1.3 |  |
| 30 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm - |  |  |
|  | SIte Network |  |

Simulation Criteria<br>Areal Reduction Factor 1.000 Additional Flow - \% of Total Flow 0.000 Hot Start (mins) $0 \quad$ MADD Factor * $10 \mathrm{~m}^{3} /$ ha Storage 2.000 Hot Start Level (mm) Inlet Coeffiecient 0.800 Manhole Headloss Coeff (Global) 0.500 Flow per Person per Day (l/per/day) 0.000 Foul Sewage per hectare (l/s) 0.000

Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 3 Number of Online Controls 4 Number of Storage Structures 20 Number of Real Time Controls 0

Synthetic Rainfall Details
Rainfall Model FSR M5-60 (mm) 17.000 CV (Summer) 1.000
Region England and Wales Ratio R 0.336 Cv (Winter) 1.000

Margin for Flood Risk Warning (mm) 300.0
Analysis Timestep 2.5 Second Increment (Extended)
DTS Status ON
DVD Status ON
Inertia Status ON
Profile(s)
Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960,1440
Return Period(s) (years)
Climate Change (\%)

| US/MH <br> Name | Storm | Return <br> Period | Climate Change | First (X) <br> Surcharge | $\begin{gathered} \text { First (Y) } \\ \text { Flood } \end{gathered}$ | First (Z) Overflow | Overflow Act. | Water <br> Level <br> (m) | Surcharged Depth (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SWP-1 | 15 Summer | 30 | +45\% |  |  |  |  | 100.312 | -0.098 |
| SWP-2 | 15 Summer | 30 | +45\% |  |  |  |  | 99.290 | -0.077 |
| SWP-3 | 15 Summer | 30 | +45\% |  |  |  |  | 99.517 | -0.150 |
| SWP-4 | 15 Summer | 30 | +45\% |  |  |  |  | 99.150 | -0.150 |
| SWP-5 | 15 Summer | 30 | +45\% |  |  |  |  | 98.987 | -0.150 |
| SWP-6 | 15 Summer | 30 | +45\% | 100/15 Summer |  |  |  | 98.789 | -0.059 |
| SWP-7 | 15 Summer | 30 | +45\% |  |  |  |  | 99.646 | -0.150 |
| SWP-8 | 15 Summer | 30 | +45\% | 100/15 Summer |  |  |  | 98.602 | -0.083 |
| SWP-9 | 15 Summer | 30 | +45\% |  |  |  |  | 99.409 | -0.150 |
| SWP-10 | 15 Summer | 30 | +45\% | 100/15 Summer |  |  |  | 98.834 | -0.083 |
| SWP-11 | 15 Summer | 30 | +45\% | 100/15 Summer |  |  |  | 98.574 | -0.026 |
| SWP-12 | 15 Summer | 30 | +45\% |  |  |  |  | 99.126 | -0.150 |
| SWP-13 | 15 Summer | 30 | +45\% | 100/240 Summer |  |  |  | 97.776 | -0.067 |
| SWP-14 | 240 Summer | 30 | +45\% | 30/15 Summer |  |  |  | 97.513 | 0.408 |
| WP-TANK 1 | 240 Summer | 30 | +45\% | 30/15 Summer |  |  |  | 97.512 | 0.457 |
| SWP-16 | 15 Summer | 30 | +45\% |  |  |  |  | 98.372 | -0.150 |
| SWP-17 | 15 Summer | 30 | +45\% |  |  |  |  | 98.923 | -0.150 |
| SWP-18 | 15 Summer | 30 | +45\% |  |  |  |  | 98.219 | -0.094 |
| SWP-19 | 15 Summer | 30 | +45\% |  |  |  |  | 98.312 | -0.150 |
| SWP-20 | 15 Summer | 30 | +45\% |  |  |  |  | 97.924 | -0.150 |
| SWP-21 | 15 Summer | 30 | +45\% | 30/15 Summer |  |  |  | 97.844 | 0.033 |
| SWP-22 | 240 Summer | 30 | +45\% | 30/15 Summer |  |  |  | 97.512 | 0.507 |
| WP-TANK 2 | 240 Summer | 30 | +45\% | 30/15 Summer |  |  |  | 97.510 | 0.555 |
| SWP-24 | 15 Summer | 30 | +45\% |  |  |  |  | 99.001 | -0.150 |
| SWP-25 | 15 Summer | 30 | +45\% |  |  |  |  | 99.916 | -0.150 |
| SWP-26 | 15 Summer | 30 | +45\% | 100/15 Summer |  |  |  | 98.843 | -0.099 |
| SWP-27 | 15 Summer | 30 | +45\% |  |  |  |  | 99.336 | -0.150 |
| SWP-28 | 15 Summer | 30 | +45\% |  |  |  |  | 98.757 | 0.000 |
| SWP-29 | 15 Summer | 30 | +45\% | 30/15 Summer |  |  |  | 98.881 | 0.333 |

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| Jacobs Engineering Limited |  | Page 6 |
| :---: | :---: | :---: |
|  | Bishop Auckland <br> Bus Station and Car Park | Micro Drainage |
| Date 13/12/2022 09:28 <br> File BA-Drainage Model_v19.MDX | Designed by G.Jones Checked by S.Clark |  |
| Innovyze | Network 2020.1.3 |  |
| 30 year Return Period Summary | ical Results by Maximum | for Storm |


| PN | US/MH Name | Flooded Volume (m ${ }^{3}$ ) | $\begin{gathered} \text { Flow / } \\ \text { Cap. } \end{gathered}$ | $\begin{aligned} & \text { Overflow } \\ & \text { (1/s) } \end{aligned}$ | Half Drain Time (mins) | Pipe <br> Flow <br> (l/s) | Status | Level <br> Exceeded |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S23.000 | SWP-1 | 0.000 | 0.26 |  |  | 10.0 | OK |  |
| S23.001 | SWP-2 | 0.000 | 0.48 |  |  | 15.7 | OK |  |
| S24.000 | SWP-3 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S25.000 | SWP-4 | 0.000 | 0.00 |  |  | 0.0 | OK |  |
| S24.001 | SWP-5 | 0.000 | 0.00 |  |  | 0.0 | OK |  |
| S23.002 | SWP-6 | 0.000 | 0.67 |  |  | 15.8 | OK |  |
| S26.000 | SWP-7 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S26.001 | SWP-8 | 0.000 | 0.41 |  | 4 | 7.5 | OK |  |
| S27.000 | SWP-9 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S27.001 | SWP-10 | 0.000 | 0.41 |  | 4 | 14.5 | OK |  |
| S23.003 | SWP-11 | 0.000 | 1.00 |  |  | 40.1 | OK |  |
| S28.000 | SWP-12 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S28.001 | SWP-13 | 0.000 | 0.59 |  | 4 | 10.6 | OK |  |
| S23.004 | SWP-14 | 0.000 | 0.23 |  |  | 13.9 | SURCHARGED |  |
| S23.005 | SWP-TANK 1 | 0.000 | 0.05 |  | 179 | 2.8 | SURCHARGED* |  |
| S29.000 | SWP-16 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S30.000 | SWP-17 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S29.001 | SWP-18 | 0.000 | 0.30 |  | 4 | 13.1 | OK |  |
| S31.000 | SWP-19 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S32.000 | SWP-20 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S31.001 | SWP-21 | 0.000 | 1.14 |  | 3 | 22.4 | SURCHARGED |  |
| S23.006 | SWP-22 | 0.000 | 0.15 |  |  | 9.2 | SURCHARGED |  |
| S23.007 | SWP-TANK 2 | 0.000 | 0.05 |  | 191 | 4.6 | SURCHARGED* |  |
| S33.000 | SWP-24 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S34.000 | SWP-25 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S33.001 | SWP-26 | 0.000 | 0.25 |  | 4 | 11.1 | OK |  |
| S35.000 | SWP-27 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S36.000 | SWP-28 | 0.000 | 0.10 |  |  | 2.4 | SURCHARGED* |  |
| S35.001 | SWP-29 | 0.000 | 0.83 |  | 3 | 16.2 | SURCHARGED |  |



| PN | US/MH <br> Name | Storm | Return <br> Period | Climate Change | First (X) <br> Surcharge | $\begin{gathered} \text { First (Y) } \\ \text { Flood } \end{gathered}$ | $\begin{gathered} \text { First (Z) } \\ \text { Overflow } \end{gathered}$ | Overflow Act. | Water <br> Level <br> (m) | Surcharged Depth (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S33.002 | SWP-30 | 15 Summer | 30 | +45\% | 30/15 Summer |  |  |  | 98.800 | 0.364 |
| S33.003 | SWP-31 | 15 Summer | 30 | +45\% | 30/15 Summer |  |  |  | 98.518 | 0.228 |
| S33.004 | SWP-32 | 15 Summer | 30 | +45\% | 30/15 Summer |  |  |  | 98.363 | 0.134 |
| S23.008 | SWP-HB1 | 240 Summer | 30 | +45\% | 1/15 Summer |  |  |  | 97.513 | 0.683 |
| S37.000 | SWP-34 | 960 Summer | 30 | +45\% | $30 / 240$ Summer |  |  |  | 96.869 | 0.169 |
| S37.001 | SWP-TANK 3 | 960 Summer | 30 | +45\% | $30 / 240$ Summer |  |  |  | 96.869 | 0.219 |
| S38.000 | SWP-36 | 15 Summer | 30 | +45\% |  |  |  |  | 97.935 | -0.150 |
| S39.000 | SWP-37 | 15 Summer | 30 | +45\% |  |  |  |  | 97.690 | -0.150 |
| S38.001 | SWP-38 | 15 Summer | 30 | +45\% |  |  |  |  | 97.467 | -0.055 |
| S40.000 | SWP-39 | 15 Summer | 30 | +45\% |  |  |  |  | 97.242 | -0.150 |
| S41.000 | SWP-40 | 15 Summer | 30 | +45\% |  |  |  |  | 97.267 | -0.150 |
| S40.001 | SWP-41 | 15 Summer | 30 | +45\% | 100/960 Summer |  |  |  | 96.935 | -0.074 |
| S37.002 | SWP-42 | 960 Summer | 30 | +45\% | 30/120 Winter |  |  |  | 96.869 | 0.269 |
| S37.003 | SWP-TANK 4 | 960 Summer | 30 | +45\% | $30 / 120$ Summer |  |  |  | 96.869 | 0.319 |
| S23.009 | SWP-HB2 | 960 Summer | 30 | +45\% | 1/120 Summer |  |  |  | 96.869 | 0.444 |
| S42.000 | SWP-45 | 15 Summer | 30 | +45\% |  |  |  |  | 98.403 | -0.150 |
| S42.001 | SWP-46 | 15 Summer | 30 | +45\% |  |  |  |  | 96.630 | -0.058 |
| S23.010 | SWP-47 | 360 Summer | 30 | +45\% | 30/60 Summer |  |  |  | 96.157 | 0.257 |
| S23.011 | SWP-TANK 6 | 360 Summer | 30 | +45\% | 30/30 Winter |  |  |  | 96.155 | 0.305 |
| S43.000 | SWP-49 | 15 Summer | 30 | +45\% |  |  |  |  | 98.223 | -0.150 |
| S43.001 | SWP-50 | 15 Summer | 30 | +45\% |  |  |  |  | 96.805 | -0.073 |
| S43.002 | SWP-51 | 15 Summer | 30 | +45\% |  |  |  |  | 96.688 | -0.107 |
| S43.003 | SWP-52 | 360 Summer | 30 | +45\% | 30/60 Summer |  |  |  | 96.152 | 0.252 |
| S43.004 | SWP-TANK 5 | 360 Summer | 30 | +45\% | 30/60 Summer |  |  |  | 96.152 | 0.302 |
| S44.000 | SWP-54 | 15 Summer | 30 | +45\% |  |  |  |  | 96.982 | -0.150 |
| S45.000 | SWP-55 | 15 Summer | 30 | +45\% |  |  |  |  | 97.008 | -0.150 |
| S44.001 | SWP-56 | 15 Summer | 30 | +45\% |  |  |  |  | 96.861 | -0.088 |
| S23.012 | SWP-57 | 360 Summer | 30 | +45\% | 30/15 Summer |  |  |  | 96.160 | 0.360 |
| S46.000 | SWP-58 | 15 Summer | 30 | +45\% |  |  |  |  | 96.844 | -0.150 |
| S47.000 | SWP-59 | 15 Summer | 30 | +45\% |  |  |  |  | 96.434 | -0.150 |
| S23.013 | SWP-60 | 360 Summer | 30 | +45\% | 30/15 Summer |  |  |  | 96.172 | 0.422 |
| S48.000 | SWP-61 | 15 Summer | 30 | +45\% | 100/240 Summer |  |  |  | 96.194 | -0.150 |
| S23.014 | SWP-HB3 | 360 Summer | 30 | +45\% | 1/15 Summer |  |  |  | 96.172 | 0.547 |
| S23.015 | SWP-63 | 1440 Winter | 30 | +45\% | 30/360 Summer |  |  |  | 95.113 | 0.130 |
| S23.016 | SWP-TANK 7 | 1440 Winter | 30 | +45\% | 30/240 Summer |  |  |  | 95.111 | 0.178 |
| S49.000 | SWP-65 | 30 Summer | 30 | +45\% |  |  |  |  | 95.580 | -0.195 |
| S49.001 | SWP-66 | 60 Summer | 30 | +45\% |  |  |  |  | 95.323 | -0.191 |
| S49.002 | SWP-67 | 1440 Winter | 30 | +45\% | 30/960 Winter |  |  |  | 95.116 | 0.025 |
| S49.003 | SWP-68 | 1440 Winter | 30 | +45\% | 30/15 Summer |  |  |  | 95.117 | 0.217 |
| S49.004 | SWP-69 | 1440 Winter | 30 | +45\% | 1/240 Summer |  |  |  | 95.122 | 0.382 |
| S50.000 | SWP-70 | 15 Summer | 30 | +45\% | 30/15 Summer |  |  |  | 95.462 | 0.522 |
| S50.001 | SWP-71 | 15 Summer | 30 | +45\% | 1/960 Summer |  |  |  | 95.226 | 0.389 |
| S50.002 | SWP-72 | 1440 Winter | 30 | +45\% | 1/360 Summer |  |  |  | 95.121 | 0.344 |
| S23.017 | SWP-CC1 | 1440 Winter | 30 | +45\% | 1/15 Summer |  |  |  | 95.123 | 0.540 |
| S23.018 | SWP-PI | 1440 Winter | 30 | +45\% |  |  |  |  | 94.433 | -0.091 |
| S23.019 | SWP-75 | 1440 Winter | 30 | +45\% |  |  |  |  | 94.345 | -0.075 |



| Jacobs Engineering Limited |  | Page 8 |
| :---: | :---: | :---: |
|  | Bishop Auckland <br> Bus Station and Car Park |  |
| Date 13/12/2022 09:28 <br> File BA-Drainage Model_v19.MDX | Designed by G.Jones Checked by S.Clark | Drainage |
| Innovyze | Network 2020.1.3 |  |
| 30 vear Return Period Summary | cal Results by Maximum I | for Storm - |


| PN | US/MH <br> Name | Flooded <br> Volume (m ${ }^{3}$ ) | $\begin{gathered} \text { Flow / } \\ \text { Cap. } \end{gathered}$ | $\begin{aligned} & \text { Overflow } \\ & (1 / s) \end{aligned}$ | Half Drain Time (mins) | Pipe Flow (l/s) | Status | Level <br> Exceeded |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S37.000 | SWP-34 | 0.000 | 0.00 |  |  | 0.0 | SURCHARGED |  |
| S37.001 | SWP-TANK 3 | 0.000 | 0.03 |  | 315 | 2.0 | SURCHARGED* |  |
| S38.000 | SWP-36 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S39.000 | SWP-37 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S38.001 | SWP-38 | 0.000 | 0.72 |  | 4 | 12.5 | OK |  |
| S40.000 | SWP-39 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S41.000 | SWP-40 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S40.001 | SWP-41 | 0.000 | 0.52 |  | 4 | 18.9 | OK |  |
| S37.002 | SWP-42 | 0.000 | 0.03 |  |  | 2.1 | SURCHARGED |  |
| S37.003 | SWP-TANK 4 | 0.000 | 0.06 |  | 341 | 3.7 | SURCHARGED* |  |
| S23.009 | SWP-HB2 | 0.000 | 0.05 |  |  | 4.0 | SURCHARGED |  |
| S42.000 | SWP-45 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S42.001 | SWP-46 | 0.000 | 0.69 |  | 4 | 11.7 | OK |  |
| S23.010 | SWP-47 | 0.000 | 0.10 |  |  | 5.9 | SURCHARGED |  |
| S23.011 | SWP-TANK 6 | 0.000 | 0.11 |  |  | 6.6 | SURCHARGED* |  |
| S43.000 | SWP-49 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S43.001 | SWP-50 | 0.000 | 0.52 |  | 4 | 9.4 | OK |  |
| S43.002 | SWP-51 | 0.000 | 0.19 |  |  | 9.4 | OK |  |
| S43.003 | SWP-52 | 0.000 | 0.03 |  |  | 1.8 | SURCHARGED |  |
| S43.004 | SWP-TANK 5 | 0.000 | 0.04 |  |  | 2.5 | SURCHARGED* |  |
| S44.000 | SWP-54 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S45.000 | SWP-55 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S44.001 | SWP-56 | 0.000 | 0.36 |  | 4 | 13.6 | OK |  |
| S23.012 | SWP-57 | 0.000 | 0.14 |  |  | 8.3 | SURCHARGED |  |
| S46.000 | SWP-58 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S47.000 | SWP-59 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S23.013 | SWP-60 | 0.000 | 0.11 |  |  | 6.5 | SURCHARGED |  |
| S48.000 | SWP-61 | 0.000 | 0.00 |  |  | 0.0 | OK |  |
| S23.014 | SWP-HB3 | 0.000 | 0.04 |  |  | 5.0 | SURCHARGED |  |
| S23.015 | SWP-63 | 0.000 | 0.04 |  |  | 5.0 | SURCHARGED |  |
| S23.016 | SWP-TANK 7 | 0.000 | 0.04 |  | 970 | 6.6 | SURCHARGED* |  |
| S49.000 | SWP-65 | 0.000 | 0.04 |  |  | 2.2 | OK |  |
| S49.001 | SWP-66 | 0.000 | 0.06 |  |  | 4.6 | OK |  |
| S49.002 | SWP-67 | 0.000 | 0.02 |  |  | 1.2 | SURCHARGED |  |
| S49.003 | SWP-68 | 0.000 | 0.03 |  |  | 1.3 | SURCHARGED |  |
| S49.004 | SWP-69 | 0.000 | 0.04 |  |  | 1.3 | SURCHARGED |  |
| S50.000 | SWP-70 | 0.000 | 1.46 |  |  | 54.5 | SURCHARGED |  |
| S50.001 | SWP-71 | 0.000 | 1.44 |  |  | 88.3 | SURCHARGED |  |
| S50.002 | SWP-72 | 0.000 | 0.08 |  |  | 4.6 | SURCHARGED |  |
| S23.017 | SWP-CC1 | 0.000 | 0.39 |  |  | 5.8 | SURCHARGED |  |
| S23.018 | SWP-PI | 0.000 | 0.33 |  |  | 5.8 | OK* |  |
| S23.019 | SWP-75 | 0.000 | 0.49 |  |  | 5.8 | OK |  |



Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 3 Number of Online Controls 4 Number of Storage Structures 20 Number of Real Time Controls 0

Synthetic Rainfall Details
Rainfall Model FSR M5-60 (mm) 17.000 CV (Summer) 1.000
Region England and Wales Ratio R 0.336 Cv (Winter) 1.000

Margin for Flood Risk Warning (mm) 300.0
Analysis Timestep 2.5 Second Increment (Extended)
DTS Status ON
DVD Status ON
Inertia Status ON
Profile(s)
Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960, 1440
Return Period(s) (years)
Climate Change (\%)

| US/MH <br> Name | Storm | Return <br> Period | Climate Change | First (X) <br> Surcharge | $\begin{gathered} \text { First (Y) } \\ \text { Flood } \end{gathered}$ | First (Z) Overflow | Overflow Act. | Water <br> Level <br> (m) | Surcharged Depth (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SWP-1 | 15 Summer | 100 | +45\% |  |  |  |  | 100.320 | -0.090 |
| SWP-2 | 15 Summer | 100 | +45\% |  |  |  |  | 99.302 | -0.065 |
| SWP-3 | 15 Summer | 100 | +45\% |  |  |  |  | 99.517 | -0.150 |
| SWP-4 | 15 Summer | 100 | +45\% |  |  |  |  | 99.150 | -0.150 |
| SWP -5 | 15 Summer | 100 | +45\% |  |  |  |  | 98.989 | -0.148 |
| SWP-6 | 15 Summer | 100 | +45\% | 100/15 Summer |  |  |  | 98.991 | 0.143 |
| SWP-7 | 15 Summer | 100 | +45\% |  |  |  |  | 99.646 | -0.150 |
| SWP-8 | 15 Summer | 100 | +45\% | 100/15 Summer |  |  |  | 98.877 | 0.192 |
| SWP-9 | 15 Summer | 100 | +45\% |  |  |  |  | 99.409 | -0.150 |
| SWP-10 | 15 Summer | 100 | +45\% | 100/15 Summer |  |  |  | 98.921 | 0.004 |
| SWP-11 | 15 Summer | 100 | +45\% | 100/15 Summer |  |  |  | 98.860 | 0.260 |
| SWP-12 | 15 Summer | 100 | +45\% |  |  |  |  | 99.126 | -0.150 |
| SWP-13 | 240 Winter | 100 | +45\% | 100/240 Summer |  |  |  | 97.880 | 0.037 |
| SWP-14 | 240 Winter | 100 | +45\% | 30/15 Summer |  |  |  | 97.879 | 0.774 |
| P-TANK 1 | 240 Winter | 100 | +45\% | 30/15 Summer |  |  |  | 97.877 | 0.822 |
| SWP-16 | 15 Summer | 100 | +45\% |  |  |  |  | 98.372 | -0.150 |
| SWP-17 | 15 Summer | 100 | +45\% |  |  |  |  | 98.923 | -0.150 |
| SWP-18 | 15 Summer | 100 | +45\% |  |  |  |  | 98.228 | -0.085 |
| SWP-19 | 15 Summer | 100 | +45\% |  |  |  |  | 98.312 | -0.150 |
| SWP-20 | 15 Summer | 100 | +45\% |  |  |  |  | 97.931 | -0.143 |
| SWP-21 | 15 Summer | 100 | +45\% | 30/15 Summer |  |  |  | 97.942 | 0.131 |
| SWP-22 | 240 Winter | 100 | +45\% | 30/15 Summer |  |  |  | 97.884 | 0.879 |
| WP-TANK 2 | 240 Winter | 100 | +45\% | 30/15 Summer |  |  |  | 97.856 | 0.901 |
| SWP-24 | 15 Summer | 100 | +45\% |  |  |  |  | 99.035 | -0.116 |
| SWP-25 | 15 Summer | 100 | +45\% |  |  |  |  | 99.916 | -0.150 |
| SWP-26 | 15 Summer | 100 | +45\% | 100/15 Summer |  |  |  | 99.080 | 0.138 |
| SWP-27 | 15 Summer | 100 | +45\% |  |  |  |  | 99.336 | -0.150 |
| SWP-28 | 15 Summer | 100 | +45\% |  |  |  |  | 98.757 | 0.000 |
| SWP-29 | 15 Summer | 100 | +45\% | 30/15 Summer |  |  |  | 99.182 | 0.634 |

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| :--- | :--- | :--- |
| $\cdot$ | Bishop Auckland <br> Bus Station and Car Park |  |
| • |  |  |
| Date 13/12/2022 09:28 |  |  |
| File BA-Drainage Model_v19.MDX | Designed by G.Jones <br> Checked by S.Clark |  |
| Innovyze | Network 2020.1.3 |  |
| 100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm - |  |  |

SIte Network

| PN | US/MH Name | Flooded <br> Volume ( $\mathrm{m}^{3}$ ) | $\begin{gathered} \text { Flow / } \\ \text { Cap. } \end{gathered}$ | Overflow (1/s) | $\begin{gathered} \text { Half Drain } \\ \text { Time } \\ \text { (mins) } \end{gathered}$ | Pipe <br> Flow <br> (1/s) | Status | Level <br> Exceeded |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S23.000 | SWP-1 | 0.000 | 0.34 |  |  | 12.9 | OK |  |
| S23.001 | SWP-2 | 0.000 | 0.62 |  |  | 20.3 | OK |  |
| S24.000 | SWP-3 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S25.000 | SWP-4 | 0.000 | 0.00 |  |  | 0.0 | OK |  |
| S24.001 | SWP-5 | 0.000 | 0.00 |  |  | 0.0 | OK |  |
| S23.002 | SWP-6 | 0.000 | 0.75 |  |  | 17.7 | SURCHARGED |  |
| S26.000 | SWP-7 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S26.001 | SWP-8 | 0.000 | 0.44 |  | 2 | 8.1 | SURCHARGED |  |
| S27.000 | SWP-9 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S27.001 | SWP-10 | 0.000 | 0.51 |  | 2 | 18.1 | SURCHARGED |  |
| S23.003 | SWP-11 | 0.000 | 1.08 |  |  | 43.5 | SURCHARGED |  |
| S28.000 | SWP-12 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S28.001 | SWP-13 | 0.000 | 0.14 |  | 32 | 2.5 | SURCHARGED |  |
| S23.004 | SWP-14 | 0.000 | 0.19 |  |  | 11.7 | SURCHARGED |  |
| S23.005 | SWP-TANK 1 | 0.000 | 0.07 |  | 212 | 4.5 | SURCHARGED* |  |
| S29.000 | SWP-16 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S30.000 | SWP-17 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S29.001 | SWP-18 | 0.000 | 0.39 |  | 4 | 16.9 | OK |  |
| S31.000 | SWP-19 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S32.000 | SWP-20 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S31.001 | SWP-21 | 0.000 | 1.47 |  | 3 | 28.8 | SURCHARGED |  |
| S23.006 | SWP-22 | 0.000 | 0.13 |  |  | 8.1 | SURCHARGED |  |
| S23.007 | SWP-TANK 2 | 0.000 | 0.05 |  | 230 | 4.6 | SURCHARGED* |  |
| S33.000 | SWP-24 | 0.000 | 0.02 |  |  | 0.4 | OK* |  |
| S34.000 | SWP-25 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S33.001 | SWP-26 | 0.000 | 0.30 |  | 3 | 13.5 | SURCHARGED |  |
| S35.000 | SWP-27 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S36.000 | SWP-28 | 0.000 | 0.14 |  |  | 3.2 | SURCHARGED* |  |
| S35.001 | SWP-29 | 0.000 | 1.06 |  | 5 | 20.7 | SURCHARGED |  |



| PN | US/MH <br> Name | Storm | Return <br> Period | Climate Change | First (X) <br> Surcharge | $\begin{gathered} \text { First (Y) } \\ \text { Flood } \end{gathered}$ | $\begin{gathered} \text { First (Z) } \\ \text { Overflow } \end{gathered}$ | Overflow Act. | Water Level (m) | Surcharged Depth <br> (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S33.002 | SWP-30 | 15 Summer | 100 | +45\% | 30/15 Summer |  |  |  | 99.063 | 0.627 |
| S33.003 | SWP-31 | 15 Summer | 100 | +45\% | 30/15 Summer |  |  |  | 98.670 | 0.380 |
| S33.004 | SWP-32 | 15 Summer | 100 | +45\% | 30/15 Summer |  |  |  | 98.474 | 0.245 |
| S23.008 | SWP-HB1 | 240 Winter | 100 | +45\% | 1/15 Summer |  |  |  | 97.896 | 1.066 |
| S37.000 | SWP-34 | 960 Winter | 100 | +45\% | $30 / 240$ Summer |  |  |  | 97.079 | 0.379 |
| S37.001 | SWP-TANK 3 | 960 Winter | 100 | +45\% | $30 / 240$ Summer |  |  |  | 97.078 | 0.428 |
| S38.000 | SWP-36 | 15 Summer | 100 | +45\% |  |  |  |  | 97.935 | -0.150 |
| S39.000 | SWP-37 | 15 Summer | 100 | +45\% |  |  |  |  | 97.690 | -0.150 |
| S38.001 | SWP-38 | 15 Summer | 100 | +45\% |  |  |  |  | 97.486 | -0.036 |
| S40.000 | SWP-39 | 15 Summer | 100 | +45\% |  |  |  |  | 97.242 | -0.150 |
| S41.000 | SWP-40 | 15 Summer | 100 | +45\% |  |  |  |  | 97.267 | -0.150 |
| S40.001 | SWP-41 | 960 Winter | 100 | +45\% | 100/960 Summer |  |  |  | 97.088 | 0.079 |
| S37.002 | SWP-42 | 960 Winter | 100 | +45\% | 30/120 Winter |  |  |  | 97.091 | 0.491 |
| S37.003 | SWP-TANK 4 | 960 Winter | 100 | +45\% | $30 / 120$ Summer |  |  |  | 97.051 | 0.501 |
| S23.009 | SWP-HB2 | 960 Winter | 100 | +45\% | 1/120 Summer |  |  |  | 97.114 | 0.689 |
| S42.000 | SWP-45 | 15 Summer | 100 | +45\% |  |  |  |  | 98.403 | -0.150 |
| S42.001 | SWP-46 | 15 Summer | 100 | +45\% |  |  |  |  | 96.648 | -0.040 |
| S23.010 | SWP-47 | 360 Winter | 100 | +45\% | 30/60 Summer |  |  |  | 96.527 | 0.627 |
| S23.011 | SWP-TANK 6 | 480 Winter | 100 | +45\% | 30/30 Winter |  |  |  | 96.351 | 0.501 |
| S43.000 | SWP-49 | 15 Summer | 100 | +45\% |  |  |  |  | 98.223 | -0.150 |
| S43.001 | SWP-50 | 15 Summer | 100 | +45\% |  |  |  |  | 96.818 | -0.060 |
| S43.002 | SWP-51 | 15 Summer | 100 | +45\% |  |  |  |  | 96.695 | -0.100 |
| S43.003 | SWP-52 | 360 Winter | 100 | +45\% | 30/60 Summer |  |  |  | 96.523 | 0.623 |
| S43.004 | SWP-TANK 5 | 480 Winter | 100 | +45\% | 30/60 Summer |  |  |  | 96.351 | 0.501 |
| S44.000 | SWP-54 | 15 Summer | 100 | +45\% |  |  |  |  | 96.982 | -0.150 |
| S45.000 | SWP-55 | 15 Summer | 100 | +45\% |  |  |  |  | 97.008 | -0.150 |
| S44.001 | SWP-56 | 15 Summer | 100 | +45\% |  |  |  |  | 96.870 | -0.079 |
| S23.012 | SWP-57 | 360 Winter | 100 | +45\% | 30/15 Summer |  |  |  | 96.523 | 0.723 |
| S46.000 | SWP-58 | 15 Summer | 100 | +45\% |  |  |  |  | 96.844 | -0.150 |
| S47.000 | SWP-59 | 360 Winter | 100 | +45\% |  |  |  |  | 96.520 | -0.064 |
| S23.013 | SWP-60 | 360 Winter | 100 | +45\% | 30/15 Summer |  |  |  | 96.520 | 0.770 |
| S48.000 | SWP-61 | 360 Winter | 100 | +45\% | 100/240 Summer |  |  |  | 96.518 | 0.174 |
| S23.014 | SWP-HB3 | 360 Winter | 100 | +45\% | 1/15 Summer |  |  |  | 96.518 | 0.893 |
| S23.015 | SWP-63 | 1440 Winter | 100 | +45\% | 30/360 Summer |  |  |  | 95.229 | 0.246 |
| S23.016 | SWP-TANK 7 | 1440 Winter | 100 | +45\% | 30/240 Summer |  |  |  | 95.227 | 0.294 |
| S49.000 | SWP-65 | 60 Summer | 100 | +45\% |  |  |  |  | 95.585 | -0.190 |
| S49.001 | SWP-66 | 60 Summer | 100 | +45\% |  |  |  |  | 95.329 | -0.185 |
| S49.002 | SWP-67 | 1440 Winter | 100 | +45\% | 30/960 Winter |  |  |  | 95.231 | 0.140 |
| S49.003 | SWP-68 | 1440 Winter | 100 | +45\% | 30/15 Summer |  |  |  | 95.233 | 0.333 |
| S49.004 | SWP-69 | 1440 Winter | 100 | +45\% | 1/240 Summer |  |  |  | 95.238 | 0.498 |
| S50.000 | SWP-70 | 15 Summer | 100 | +45\% | 30/15 Summer |  |  |  | 95.821 | 0.881 |
| S50.001 | SWP-71 | 15 Summer | 100 | +45\% | 1/960 Summer |  |  |  | 95.447 | 0.610 |
| S50.002 | SWP-72 | 1440 Winter | 100 | +45\% | 1/360 Summer |  |  |  | 95.237 | 0.460 |
| S23.017 | SWP-CC1 | 1440 Winter | 100 | +45\% | 1/15 Summer |  |  |  | 95.238 | 0.655 |
| S23.018 | SWP-PI | 1440 Winter | 100 | +45\% |  |  |  |  | 94.438 | -0.086 |
| S23.019 | SWP-75 | 1440 Winter | 100 | +45\% |  |  |  |  | 94.352 | -0.068 |


| PN | US/MH Name | Flooded <br> Volume ( $\mathrm{m}^{3}$ ) | $\begin{gathered} \text { Flow / } \\ \text { Cap. } \end{gathered}$ | $\begin{aligned} & \text { Overflow } \\ & (1 / s) \end{aligned}$ | Half Drain Time (mins) | Pipe Flow (1/s) | Status | Level <br> Exceeded |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S33.002 | SWP-30 | 0.000 | 1.63 |  |  | 29.3 | SURCHARGED |  |
| S33.003 | SWP-31 | 0.000 | 1.85 |  |  | 28.6 | SURCHARGED |  |
| S33.004 | SWP-32 | 0.000 | 1.55 |  |  | 28.3 | SURCHARGED |  |
| S23.008 | SWP-HB1 | 0.000 | 0.06 |  |  | 4.5 | SURCHARGED |  |


| Jacobs Engineering Limited |  | Page 12 |
| :---: | :---: | :---: |
|  | Bishop Auckland <br> Bus Station and Car Park |  |
| Date 13/12/2022 09:28 <br> File BA-Drainage Model_v19.MDX | Designed by G.Jones Checked by S.Clark | Drainage |
| Innovyze | Network 2020.1.3 |  |
| 100 year Return Period Summary | ical Results by Maximum | for Storm - |


| PN | US/MH <br> Name | Flooded <br> Volume ( $\mathrm{m}^{3}$ ) | $\begin{gathered} \text { Flow / } \\ \text { Cap. } \end{gathered}$ | $\begin{aligned} & \text { Overflow } \\ & (1 / s) \end{aligned}$ | $\begin{gathered} \text { Half Drain } \\ \text { Time } \\ \text { (mins) } \end{gathered}$ | Pipe Flow (1/s) | Status | Level <br> Exceeded |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S37.000 | SWP-34 | 0.000 | 0.00 |  |  | 0.1 | SURCHARGED |  |
| S37.001 | SWP-TANK 3 | 0.000 | 0.04 |  | 391 | 2.5 | SURCHARGED* |  |
| S38.000 | SWP-36 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S39.000 | SWP-37 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S38.001 | SWP-38 | 0.000 | 0.93 |  | 5 | 16.1 | OK |  |
| S40.000 | SWP-39 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S41.000 | SWP-40 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S40.001 | SWP-41 | 0.000 | 0.04 |  | 132 | 1.6 | SURCHARGED |  |
| S37.002 | SWP-42 | 0.000 | 0.05 |  |  | 3.0 | SURCHARGED |  |
| S37.003 | SWP-TANK 4 | 0.000 | 0.06 |  | 434 | 3.8 | SURCHARGED* |  |
| S23.009 | SWP-HB2 | 0.000 | 0.05 |  |  | 4.0 | SURCHARGED |  |
| S42.000 | SWP-45 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S42.001 | SWP-46 | 0.000 | 0.89 |  | 4 | 15.1 | OK |  |
| S23.010 | SWP-47 | 0.000 | 0.09 |  |  | 5.6 | SURCHARGED |  |
| S23.011 | SWP-TANK 6 | 0.000 | 0.10 |  |  | 6.2 | SURCHARGED* |  |
| S43.000 | SWP-49 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S43.001 | SWP-50 | 0.000 | 0.67 |  | 4 | 12.1 | OK |  |
| S43.002 | SWP-51 | 0.000 | 0.24 |  |  | 12.1 | OK |  |
| S43.003 | SWP-52 | 0.000 | 0.02 |  |  | 1.5 | SURCHARGED |  |
| S43.004 | SWP-TANK 5 | 0.000 | 0.04 |  |  | 2.3 | SURCHARGED* |  |
| S44.000 | SWP-54 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S45.000 | SWP-55 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S44.001 | SWP-56 | 0.000 | 0.46 |  | 4 | 17.5 | OK |  |
| S23.012 | SWP-57 | 0.000 | 0.12 |  |  | 7.6 | SURCHARGED |  |
| S46.000 | SWP-58 | 0.000 | 0.00 |  |  | 0.0 | OK* |  |
| S47.000 | SWP-59 | 0.000 | 0.01 |  |  | 0.1 | OK* |  |
| S23.013 | SWP-60 | 0.000 | 0.10 |  |  | 6.4 | SURCHARGED |  |
| S48.000 | SWP-61 | 0.000 | 0.01 |  |  | 0.1 | SURCHARGED |  |
| S23.014 | SWP-HB3 | 0.000 | 0.05 |  |  | 5.5 | SURCHARGED |  |
| S23.015 | SWP-63 | 0.000 | 0.04 |  |  | 5.0 | SURCHARGED |  |
| S23.016 | SWP-TANK 7 | 0.000 | 0.05 |  | 1113 | 7.5 | SURCHARGED* |  |
| S49.000 | SWP-65 | 0.000 | 0.06 |  |  | 3.0 | OK |  |
| S49.001 | SWP-66 | 0.000 | 0.07 |  |  | 6.0 | OK |  |
| S49.002 | SWP-67 | 0.000 | 0.03 |  |  | 1.5 | SURCHARGED |  |
| S49.003 | SWP-68 | 0.000 | 0.04 |  |  | 1.7 | SURCHARGED |  |
| S49.004 | SWP-69 | 0.000 | 0.04 |  |  | 1.6 | SURCHARGED |  |
| S50.000 | SWP-70 | 0.000 | 1.92 |  |  | 71.5 | SURCHARGED |  |
| S50.001 | SWP-71 | 0.000 | 1.87 |  |  | 115.0 | SURCHARGED |  |
| S50.002 | SWP-72 | 0.000 | 0.10 |  |  | 6.0 | SURCHARGED |  |
| S23.017 | SWP-CC1 | 0.000 | 0.46 |  |  | 6.8 | SURCHARGED |  |
| S23.018 | SWP-PI | 0.000 | 0.38 |  |  | 6.8 | OK* |  |
| S23.019 | SWP-75 | 0.000 | 0.58 |  |  | 6.8 | OK |  |

Appendix F. AquaTreat Interceptor Certificates

## Klargester

## Stormwater Treatment Device Performance Declaration

Stormwater Treatment Devices compliant with Chapter 26 of the CIRIA SuDS manual

Testing carried out according to DIBt Stormwater Treatment Systems Approval Requirements Part 1: "Systems for connection of motor vehicle circulation areas with a surface of max. $2000 \mathrm{~m}^{2}$ for subsequent infiltration into ground and water course"

Treatment Device Tested: AquaTreat SWT010 stormwater treatment device

General description: A device for the collection and retention of hydrocarbons, particulate and metals.

E nvisaged application: Surface water runoff for trafficked areas for subsequent infiltration into ground and water course.

Pollutant(s) captured: Hydrocarbons, particulate, zinc and copper

| P arameter | Value |
| :--- | :--- |
| Treatment device capacity: | 2,450 I |
| Particulate storage capacity: | 1,000 I |
| Hydrocarbons storage capacity: | 100 I |
| Treatment flow rate: | $10 \mathrm{I} / \mathrm{s}$ |
| Connectable area: | $1,000 \mathrm{~m} 2$ |
| Hydrocarbon retention | $99.65 \%$ |
| Particulate retention efficiency | $85.5 \%$ |
| Zinc retention efficiency* | $64 \%$ |
| Copper retention efficiency* | $64 \%$ |

*R eduction of heavy metals by collecting and retaining suspended solids is assumed as $75 \%$.

# Certificate 

## Kingspan Environmental Ltd.

College Rd North, Aston Clinton, Aylesbury Bucks, HP225EW, Great Britian
Approval principles of DIBt
„Zulassungsgrundsätze für Niederschlagswasserbehandlungsanlagen Teil ${ }^{\text {" }}$
Version November 2017
AquaTreat SWT010
Connected surface area: $1,000 \mathrm{~m}^{2}$
PIA2020-NW-1911-1066

Particle retention (Millisil W4) $\quad 85.50 \%$

Hydro carbon retention $99.65 \%$

Performance tested by:
PIA - Prüfinstitut für Abwassertechnik GmbH
Hergenrather Weg 30
52074 Aachen
Germany

This document does not replace the test report.


## Appendix G. Topo Survey



Appendix H. Scheme Drawings



| PRIVATE SURFACE WATER Network |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Manhole Name | $\begin{array}{\|c} \text { Cover Level } \\ (\mathrm{m}) \end{array}$ | $\underset{\substack{\text { MH Deprt } \\(m)}}{\substack{\text { m }}}$ | Manhole Dia (mm) | Chamber Tye | Pipe Out Invert Level ( $m$ ) | $\begin{array}{\|c} \substack{\text { Pipe out } \\ \text { Diamenter } \\ (m m)} \end{array}$ |  | $\begin{gathered} \text { Pipes in } \\ \text { Ivert Level } \\ \left(\begin{array}{l} m \end{array}\right) \end{gathered}$ |  | $\begin{gathered} \text { Pipesing } \\ \substack{\text { Bacachlop } \\ \text { (nmm) }} \end{gathered}$ | cover Grade col |
| SwP-1 | 101.31 | 1.05 | 1200 | ${ }^{\text {PCCRING }}$ | 100.26 | ${ }^{150}$ | 19.4 |  |  |  | D400 |
| swP-2 | 100271 | 1.054 | 1200 | pecring | 99.217 | ${ }^{150}$ | 24.5 | 99.217 | 150 |  | 0400 |
| swp 3 | ${ }^{100.123}$ | 0.606 | 150 | Roodmg eve | 99.517 | 150 | 14.8 |  |  |  |  |
| swP4 | 100.2 | 1.05 | 1200 | pering | 99.15 | ${ }^{150}$ | ${ }^{23,3}$ |  |  |  | D4400 |
| swe. 5 | 100.033 | ${ }_{1} 1.056$ | 1200 | ${ }_{\text {PCCRING }}$ | 98.887 | ${ }^{150}$ | 16.1 | 98.887 | 150 |  | D400 |
|  |  |  |  |  |  |  |  | 98.88 | 150 |  |  |
| swp. 6 | 99.988 | 1.3 | 1200 | PCRING | 98.688 | 150 | ${ }^{46.4}$ | 98.68 | 150 |  | 0400 |
|  |  |  |  |  |  |  |  | 98.988 | 150 |  |  |
| sw.7 | 100296 | 0.65 | 150 | Roodmg eve | 99.646 | 150 | 15.8 |  |  |  |  |
| sw. 8 | 99.835 | ${ }^{1.3}$ | 600 | PPIC | 98.335 | ${ }^{150}$ | 59.9 | 98.535 | 150 |  | 0400 |
| sw. 9 | 1000.015 | 0.606 | 150 | Rooding eve | 99,09 | ${ }_{150}$ | ${ }^{12.2}$ |  |  |  |  |
| SwP-10 | 99.97 | 1.15 | 600 | PPIC | 98.767 | ${ }^{150}$ | ${ }^{14.7}$ | 98.767 | 150 |  | D4400 |
| SwP-11 | 99.79 | ${ }^{1.34}$ | 1200 | ${ }^{\text {PCCRING }}$ | 98.45 | 150 | 18 | 98.45 | 150 |  | D4400 |
|  |  |  |  |  |  |  |  | 98.45 | 150 |  |  |
|  |  |  |  |  |  |  |  | 98.45 | 150 |  |  |
| ${ }_{\text {swp }}$-12 | 99.776 | 0.65 | 150 | Rooding ye | 99.126 | ${ }_{150}$ | 17.9 |  |  |  |  |
| swp-13 | 98.97 | 1.284 | 600 | Palc | 97.93 | 150 | 60.2 | 97.63 | 150 |  | D400 |
| SwP-14 | 98.879 | 2.074 | 1200 | ${ }^{\text {PCR RING }}$ | 96.805 | 300 | 16.2 | 96.95 | 150 |  | 0400 |
|  |  |  |  |  |  |  |  | 97.61 | 150 | 655 |  |
| SwP-TANK 1 | 98.59 | 2204 |  | crates | 96.75 | 300 | 151.8 | 96.75 | 300 |  |  |
| swp.16 | 99.033 | 0.661 | 150 | Roodme eve | 98.372 | 150 | 60 |  |  |  |  |
| SWP-17 | 99.62 | 0.699 | 150 | Rooding ye | 98.93 | 150 | 13.2 |  |  |  |  |
| swp-18 | 99.388 | 1.225 | 600 | PPIC | 98.163 | 150 | 10.2 | 98.163 | 150 |  | 040 |
|  |  |  |  |  |  |  |  | 98.163 | 150 |  |  |
| SwP-19 | 98.889 | 0.677 | 150 | Roodme eve | 98.312 | 150 | 15.4 |  |  |  |  |
| SWP-20 | 98.586 | 0.662 | 150 | Rooding eve | 97.24 | 150 | 47.7 |  |  |  |  |
| SwP-21 | 98.819 | 1.158 | 600 | PPIC | 97.661 | 150 | 59.7 | 97.661 | 150 |  | D400 |
|  |  |  |  |  |  |  |  | 97.61 | ${ }^{150}$ |  |  |
| swp-22 | 99.135 | 2.43 | 1200 | ${ }^{\text {PC R RNG }}$ | 96.75 | 300 | 147.9 | 96.75 | 300 |  | 0400 |
|  |  |  |  |  |  |  |  | 97.68 | 150 | 825 |  |
|  |  |  |  |  |  |  |  | 97.548 | 150 | 693 |  |
| SwneTaNK 2 | 99.29 | 2.644 |  | CRates | 96.655 | 300 | 55.2 | 96.655 | 300 |  |  |
| swp 24 | 99.669 | 0.668 | 150 | Roodmg eve | 99.001 | 150 | 60 |  |  |  |  |
| SWP-25 | 100479 | 0.563 | 150 | Rooding eve | 99.96 | ${ }^{150}$ | ${ }^{12.1}$ |  |  |  |  |
| ${ }_{\text {swp-26 }}$ | 100.197 | 1.405 | 600 | P9IC | 98.792 | 150 | 7.4 | 98.792 | 150 |  | 0400 |
|  |  |  |  |  |  |  |  | 99.292 | 150 | 500 |  |
| SwP-27 | 99.973 | 0.637 | ${ }^{150}$ | Roodmg eve | 99.336 | ${ }^{150}$ | 10.7 |  |  |  |  |
| swp 28 | 99.26 | 0.662 | 150 | Roodng eve | 98.67 | 150 | 60.1 |  |  |  |  |
| SwP-29 | 99.55 | 1.26 | 600 | PPIC | 98.388 | 150 | 60.3 | 98.388 | 150 |  | 0400 |
|  |  |  |  |  |  |  |  | 98.388 | ${ }^{150}$ |  |  |
| swr-30 | 99.94 | 1.688 | 1200 | PC RING | 98.286 | 150 | 80 | 98.286 | 150 |  | 0400 |
|  |  |  |  |  |  |  |  | 98.286 | 150 |  |  |
| swp-31 | 100381 | 2.241 | 1200 | ${ }^{\text {PC R ING }}$ | 98.14 | 150 | ${ }^{79.6}$ | 98.14 | 150 |  | D400 |
| swp 32 | 99.94 | 1.915 | 1200 | ${ }^{\text {PCCRING }}$ | 98.09 | 150 | 80 | 98.09 | 150 |  | D400 |
| SWP-HE1 | 99.196 | 2.666 | 1500 | PC RING | 96.605 | 225 | ${ }^{43.2}$ | 99.53 | 300 |  | D400 |
|  |  |  |  |  |  |  |  | 97.06 | 150 | ${ }^{1226}$ |  |
| SwP 34 | 98.168 | 1.818 | 1200 | PC Ring | 96.35 | 300 | 180 |  |  |  | 0400 |
| SWP-TANK 3 | 98.239 | 1.939 |  | Crates | 96.35 | 300 | 138 | 96.3 | 300 |  |  |
| swp-36 | 98.63 | 0.69 | 150 | Rooonge eve | 97.35 | 150 | 17.9 |  |  |  |  |
| swp-37 | 98.377 | 0.557 | 150 | Rooong eve | 97.69 | 150 | 39.5 |  |  |  |  |
| SWP-38 | 98.521 | 1.149 | 600 | PPIC | 97.372 | 150 | 59.9 | 97.372 | 150 |  | D4400 |
|  |  |  |  |  |  |  |  | 97.32 | 150 |  |  |
| swe-39 | 97.896 | 0.554 | 150 | Roodmg eve | 97.242 | 150 | 32.8 |  |  |  |  |
| SwP-40 | 98.01 | 0.734 | 150 | Roodime ye | 97.267 | 150 | 24.6 |  |  |  |  |
| SwP-41 | 97.95 | 1.106 | 600 | PPIC | 96.859 | 150 | 17.5 | 96.859 | 150 |  | 0400 |
|  |  |  |  |  |  |  |  | 96.859 | 150 |  |  |
| SwP-42 | 98,289 | 1.989 | 1200 | ${ }^{\text {PCRING }}$ | 96.3 | 300 | ${ }^{143}$ | ${ }_{\text {96,3 }} 9$ | 300 150 |  | D400 |
|  |  |  |  |  |  |  |  | ${ }_{96,45}^{97.26}$ | $\begin{aligned} & 150 \\ & \hline 150 \end{aligned}$ | ${ }^{846}$ |  |
| SWP-TANK 4 | 9836 | 2.11 |  | ${ }^{\text {crates }}$ | 96.25 | 300 | ${ }_{143}$ | 96,45 96.25 | 150 300 |  |  |
| SWP-HB2 | ${ }_{98,366}$ | ${ }^{2.126}$ | 1500 | ${ }^{\text {ç }}$ Ring | 96.2 | ${ }^{325}$ | ${ }_{3,7}$ | 96.2 | ${ }^{325}$ |  | D400 |
|  |  |  |  |  |  |  |  | 96.2 | 300 |  |  |
| SwP-45 | 99.13 | 0.727 | 150 | Roodmg eve | 98.403 | ${ }^{150}$ | 17.8 |  |  |  |  |
| swp-46 | 97.57 | 1.039 | 600 | PPIC | 96.538 | 150 | 59.7 | 96.538 | 150 |  | D400 |
| SwP-47 | 97.439 | 1.839 | 1200 | PCRING | 95.6 | 300 | 143 | 95.675 | 225 |  | ${ }^{2000}$ |
|  |  |  |  |  |  |  |  | 96.455 | 150 | 715 |  |
| SWPTANK 6 | 97.42 | 1.875 |  | Crates | 95.55 | 300 | ${ }^{143}$ | 95.55 | 300 |  |  |
| swp-49 | 98.868 | 0.645 | 150 | Roodng eve | ${ }_{98223}$ | 150 | 15 |  |  |  |  |
| swe-50 | 98.013 | 1.285 | 600 | P9FIC | 96.72 | 150 | 59.7 | 96.728 | 150 |  | D400 |


| PRIVATE FOUL WATER NETWORK |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Manhol Name | $\begin{aligned} & \text { Cover Level } \\ & \text { (m) } \end{aligned}$ | MH Depth (m) | Manhole Dia (mm) | Chamber Tye | Pipe Out Invert Level ( m ) | $\underset{\substack{\text { Pipe out } \\ \text { Dimener } \\(m m)}}{ }$ | $\begin{gathered} \text { Pipe out } \\ \substack{\text { Pandien } \\ \text { nain }} \end{gathered}$ | $\begin{array}{\|c} \substack{\text { Pipes in } \\ \text { nvene tevel } \\ (\mathrm{m})} \end{array}$ | $\begin{array}{\|c\|c\|c\|c\|c\|c\|c\|} \substack{\text { Diamester } \\ (m m)} \end{array}$ | $\begin{gathered} \text { Pipes In } \\ \substack{\text { Backichop } \\ \text { (nmm }} \end{gathered}$ | cover $\begin{gathered}\text { corade } \\ \text { crat }\end{gathered}$ |
| fwP-1 | 97.317 | 1.982 | 1200 | ${ }^{\text {PCR RING }}$ | 95.185 | 150 | 80.1 |  |  |  | 0400 |
| fw-2 | 98.058 | 1.008 | 600 | PPIC | 96.9 | ${ }^{150}$ | 59.9 |  |  |  | 0400 |
| fwe. 3 | 97.65 | ${ }^{2.48}$ | 1200 | PC RIMG | 95.02 | ${ }^{150}$ | 80.8 | 95.02 | ${ }^{150}$ |  | 0400 |
|  |  |  |  |  |  |  |  | ${ }^{96.685}$ | ${ }^{150}$ | 1665 | 0400 |
| fw-4 | 97.313 | 2.263 | 1200 | PCRING | 94.9 | ${ }^{150}$ | ${ }_{80}$ | 94.9 | 150 |  | 0400 |
| fw. 5 | 96.726 | твс | 1200 | ${ }^{\text {PCCRING }}$ | ourfall | ${ }^{150}$ | твС | тв | ${ }^{150}$ |  | 0400 |


| ADOPTED SURFACE WATER NETWORK |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Manhole Name | ${ }_{\substack{\text { Cover } \\ \text { ( } \mathrm{m})}}^{\text {evel }}$ | $\begin{aligned} & \text { MH Depth } \\ & \text { (m) } \end{aligned}$ | Manhole Dia | Chamber Type | $\begin{gathered} \text { Pipe Out Invert } \\ \text { Level (m) } \end{gathered}$ |  | $\begin{gathered} \text { Pipe Out } \\ \text { Gradient } \\ \text { (1 in } X) \end{gathered}$ | $\begin{aligned} & \text { Pipes In } \\ & \text { Invert Level } \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \text { Pipes In } \\ & \text { Diameter } \\ & (\mathrm{mm}) \end{aligned}$ | $\begin{aligned} & \text { Pipes In } \\ & \text { Backdrop } \\ & (\mathrm{mm}) \end{aligned}$ | couer <br> Grade |
| HW-MH-1 | 101372 | 1.397 | 1200 | ${ }^{\text {PCCRING }}$ | 99.150 | 225 | 20.9 | 99.150 | 150 |  | 0400 |
| HWMH-2 | 99.25 | 1.425 | 1200 | pering | 98.25 | 225 | ${ }_{25} 25$ | 97.825 | 225 |  | 0400 |
| HW-MH.3 | 96.98 | 1.343 | 1200 | PC RING | 97.825 | 225 | 16.2 | 95.575 | 225 |  | 0400 |


| PRIVATE SURFACE WATER NETWORK - flow controls |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Manhole Name | Fow Rate | Design Head | Storm Event | Control T yee |
| SWP-H61 | 4.5//s | ${ }^{1.250 m}$ | 100\%rat 4 \%ec | Vortex |
| swp-H182 | 4.01/5 | ${ }^{0.850 m}$ | 100\%rats\%ect | vortex |
| swp-H33 | 5.01/ | 0.900 m | 100yras\%ec | vortex |
| sw. CC1 | 3/5 | 0.500 m |  | Vortex |
|  | 7/s | 0.800m | 100vrat 5 \%ec | Orifice |




TYPICAL MANHOLE DETAIL
Depth from cover level to soffit of pipe $1.5 \mathrm{~m}-3.0 \mathrm{~m}$









PERMEABLE PAVING STORAGE
PARKING BAY TYPICAL SECTION
 PERMEABLE PAVING STORAGE
COLLECTOR DRAIN TYPICAL SECTION
 BLOO0034-JAC-ZZ-ZZ-DR-C-10004

Appendix I. Maintenance Schedule

The following maintenance schedules are based on the recommended guidance for operation and maintenance of drainage assets in accordance with The Suds Manual - CIRIA C753, 2015.

## Drainage Channels and Gullies

| Maintenance Schedule | Required Action | Typical Frequency |
| :--- | :--- | :--- |
| Monitoring (to be undertaken <br> more regularly within the first year <br> of operation and adjusted as <br> required). | Initial Inspection including channel <br> outlet boxes. | Half yearly and after large storms. |
| Regular Maintenance/Inspection | Litter and debris removal | Monthly or as required. |
|  | Check and remove large <br> vegetation growth near channel <br> runs. | Monthly or as required |
|  | Inspect for evidence of poor <br> operation and/or weed growth. If <br> required, take remedial action. <br> Inspect silt accumulation rates and <br> establish appropriate brushing <br> frequencies. Silt can also be caused <br> by adjacent landscaping areas <br> which should be re-profiled to <br> provide a flat area or berm <br> adjacent to the paving. | 3-monthly, 48 hours after large <br> storms. |
| Remedial Action | Inspect access/outlet boxes and <br> rod through poorly performing <br> channels and outlets as initial <br> remediation. | As required. |

## Pipes and Manholes

| Maintenance Schedule | Required Action | Typical Frequency |
| :--- | :--- | :--- |
| Monitoring (to be undertaken <br> more regularly withhin the first year <br> of operation and adjusted as <br> required) | lnitial inspection should be <br> provided as post construction <br> CCTV survey. | Once, upon completion of <br> development |
|  | Inspect for evidence of poor <br> operation via water level in <br> chambers. If required take <br> remedial action. | 3-monthly, 48 hours after large <br> storms. |
| Occasional Maintenance | Check and remove large <br> vegetation growth near pipe runs. | 6 monthly |
| Remedial actions | Rod through poorly performing <br> runs as initial remediation. | As required |
|  | If continued poor performance jet <br> and CCTV survey poorly <br> performing runs. | As required |
|  | Seek advice as to remediation <br> techniques suitable for the type of <br> performance issue and location. | As required If above does not <br> improve performance. |

## Green Roofs

| Maintenance Schedule | Required Action | Typical Frequency |
| :---: | :---: | :---: |
| Regular inspections | Inspect all components including soil substrate, vegetation, drains, irrigation systems (if applicable), membranes and roof structure for proper operation, integrity of waterproofing and structural stability | Annually and after severe storms |
|  | Inspect soil substrate for evidence of erosion channels and identify any sediment sources | Annually and after severe storms |
|  | Inspect drain inlets to ensure unrestricted runoff from the drainage layer to the conveyance or roof drain system | Annually and after severe storms |
|  | Inspect underside of roof for evidence of leakage | Annually and after severe storms |
| Regular maintenance | Remove debris and litter to prevent clogging of inlet drains and interference with plant growth | Six monthly and annually or as required |
|  | During establishment (ie year one), replace dead plants as required | Monthly (but usually responsibility of manufacturer) |
|  | Post establishment, replace dead plants as required (where $>5 \%$ of coverage) | Annually (in autumn) |
|  | Remove fallen leaves and debris from deciduous plant foliage | Six monthly or as required |
|  | Remove nuisance and invasive vegetation, including weeds | Six monthly or as required |
|  | Mow grasses, prune shrubs and manage other planting (if appropriate) as required clippings should be removed and not allowed to accumulate | Six monthly or as required |
| Remedial actions | If erosion channels are evident, these should be stabilised with extra soil substrate similar to the original material, and sources of erosion damage should be identified and controlled | As required |
|  | If drain inlet has settled, cracked or moved, investigate and repair as appropriate | As required |

## Rainwater Harvesting System

| Maintenance Schedule | Required Action | Typical Frequency |
| :--- | :--- | :--- |
| Regular maintenance | Inspection of the tank for debris <br> and sediment build-up, <br> inlets/outlets / withdrawal devices, <br> overflow areas, pumps, filters | Annually (and following poor <br> performance) |
|  | Cleaning of tank, inlets, outlets, <br> gutters, withdrawal devices and <br> roof drain filters of silts and other <br> debris | Annually (and following poor <br> performance) |
| Occasional maintenance | Cleaning and/or replacement of <br> any filters | Three monthly (or as required) |
| Remedial actions | Repair of overflow erosion damage <br> or damage to tank | As required |
| Pump repairs | As required |  |

## Attenuation Tanks

| Maintenance Schedule | Required Action | Typical Frequency |
| :--- | :--- | :--- |
| Regular maintenance | Inspect and identify any areas that <br> are not operating correctly. If <br> required, take remedial action | Monthly for 3 months, then <br> annually |
|  | Remove debris from the <br> catchment surface (where it may <br> cause risks to performance) | Monthly |
|  | Remove sediment from pre- <br> treatment structures and/or <br> internal forebays | Annually, or as required |
| Remedial actions | Repair/ rehabilitate inlets, outlet, <br> overflows and vents | As required |
| Monitoring | Inspect/ check all inlets, outlets, <br> vents and overflows to ensure that <br> they are in good condition and <br> operating as designed | Annually |
|  | Suvey inside of tank for sediment <br> build-up and remove if necessary | Every 5 years or as required |

## Permeable Concrete Block Paving

| Maintenance Schedule | Required Action | Typical Frequency |
| :---: | :---: | :---: |
| Regular maintenance | Brushing and vacuuming (standard cosmetic sweep over whole surface) | Once a year, after autumn leaf fall, or reduced frequency as required, based on site-specific observations of clogging or manufacturer's recommendations - pay particular attention to areas where water runs onto pervious surface from adjacent impermeable areas as this area is most likely to collect the most sediment |
| Occasional maintenance | Stabilise and mow contributing and adjacent areas | As required |
|  | Removal of weeds or management using glyphospate applied directly into the weeds by an applicator rather than spraying | As required - once per year on less frequently used pavements |
| Remedial Actions | Remediate any landscaping which, through vegetation maintenance or soil slip, has been raised to within 50 mm of the level of the paving | As required |
|  | Remedial work to any depressions, rutting and cracked or broken blocks considered detrimental to the structural performance or a hazard to users, and replace lost jointing material | As required |
|  | Rehabilitation of surface and upper substructure by remedial sweeping | Every 10 to 15 years or as required (if infiltration performance is reduced due to significant clogging) |
| Monitoring | Initial inspection | Monthly for three months after installation |
|  | Inspect for evidence of poor operation and/ or weed growth - if required, take remedial action | Three-monthly, 48h after large storms in first six months |
|  | Inspect silt accumulation rates and establish appropriate brushing frequencies | Annually |
|  | Monitor inspection chambers | Annually |

## Flow Control Chambers

| Maintenance Schedule | Required Action | Typical Frequency |
| :--- | :--- | :--- |
| Monitoring (to be undertaken <br> more regularly within the first year <br> of operation and adjusted as <br> required). | Inspect inlets for blockages, and <br> clear if required. If faults persist <br> jetting and CCTV survey may be <br> required. | Monthly and after large storms. |
| Regular maintenance \inspection | Inspect and identify any areas that <br> are not operating correctly. If <br> required, take remedial action. | Monthly for 3 months, then six <br> monthly. |
|  | Debris removal from catchment <br> surface (where may cause <br> blockage/risk to performance) | Monthly |
|  | Remove sediment from pre- <br> treatment structures and flow <br> control chambers. | Annually (or as required after <br> heavy rainfall events) |
| Remedial Actions | Repair/rehabilitation of inlets. | As required. |

## Oil/Petrol Separator

| Maintenance Schedule | Required Action | Typical Frequency |
| :--- | :--- | :--- |
| Routine maintenance | Remove litter and debris and <br> inspect for sediment, oil and <br> grease accumulation | Six monthly |
|  | Change the filter media | As recommended by manufacturer |
|  | Remove sediment, oil, grease and <br> floatables | As necessary - indicated by system <br> inspections or immediately <br> following significant spill |
| Remedial actions | Replace malfunctioning parts or <br> structures | As required |
| Monitoring Inspect for evidence of poor <br> operation <br>  Inspect filter media and establish <br> appropriate replacement <br> frequencies | Six monthly |  |
|  | Inspect sediment accumulation <br> rates and establish appropriate <br> removal frequencies | Monthly during first half year of <br> operation, then every six months |

## Raingardens

| Maintenance Schedule | Required Action | Typical Frequency |
| :---: | :---: | :---: |
| Regular inspections | Inspect infiltration surfaces for silting and ponding, record dewatering time of the facility and assess standing water levels in underdrain (if appropriate) to determine if maintenance is necessary | Quarterly |
|  | Check operation of underdrains by inspection of flows after rain | Annually |
|  | Assess plants for disease infection, poor growth, invasive species etc and replace as necessary | Quarterly |
|  | Inspect inlets and outlets for blockage | Quarterly |
| Regular maintenance | Remove litter and surface debris and weeds | Quarterly (or more frequently for tidiness or aesthetic reasons) |
|  | Replace any plants, to maintain planting density | As required |
|  | Remove sediment, litter and debris build-up from around inlets or from forebays | Quarterly to biannually |
| Occasional maintenance | Infill any holes or scour in the filter medium, improve erosion protection if required | As required |
|  | Repair minor accumulations of silt by raking away surface mulch, scarifying surface of medium and replacing mulch | As required |
| Remedial actions | Remove and replace filter medium and vegetation above | As required but likely to be $>20$ years |


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