

Former Women's Institute, Newton-By-The-Sea Alnwick

Drainage Strategy

Report Ref: JCC23-111-C-01 Revision: 00, August 2023

Civil Engineering Structural Engineering Geo-Environmental Engineering

DOCUMENT CONTROL SHEET



Former Women's Institute, Newton-By-The-Sea, Alnwick

DRAINAGE STRATEGY

Client:	Mr Jonathan Sutherland / George F. White
Client Address:	4-6 Market Street Alnwick Northumberland NE66 1TL
Project Reference:	JCC23-111
Report Reference:	JCC23-111-C-01-00
Status:	Planning
Author:	R Jones

Revision Record:

Rev.	Date	Status	Prepared	Signed	Checked	Signed	Approved	Signed
00	04/08/23	Planning	R Jones		A Short		T Holland	

-		NTS PAGE	~
C	JNIEN	ITS PAGE	0
1	INT	RODUCTION	1
0	1.1 1.2	BRIEF REPORT SCOPE	1
2	REL	EVANT POLICIES, LEGISLATION AND GUIDANCE	
	2.1 2.2 2.3	OVERVIEW NATIONAL PLANNING POLICY FRAMEWORK PLANNING PRACTICE GUIDANCE	2
3	2.4 SITI	NON-STATUTORY TECHNICAL STANDARDS FOR SUSTAINABLE DRAINAGE SYSTEMS E AND SURROUNDINGS	4
4	3.1 Suf	SITE LOCATION AND PROPOSED DEVELOPMENT DESCRIPTION RFACE WATER DRAINAGE STRATEGY	
	4.1 4.2	METHODOLOGY SURFACE WATER DISCHARGE METHOD	
	4.2	GREENFIELD RUN-OFF RATE CALCULATION	
	4.4	POST DEVELOPMENT ATTENUATION	
	4.5	SUDS SUITABILITY ASSESSMENT	
	4.6	WATER QUALITY MANAGEMENT	8
	4.7	SURFACE WATER MAINTENANCE ISSUES	
	4.8	SURFACE WATER SAFETY ISSUES	9
	4.9	SURFACE WATER DRAINAGE SUMMARY1	
5	FOl	UL WATER DRAINAGE STRATEGY1	1
	5.1	METHODOLOGY1	
	5.2	FOUL DRAINAGE DISCHARGE METHOD	
	5.3	FOUL WATER MAINTENANCE ISSUES	
,	5.4	FOUL WATER SAFETY ISSUES	
6		NCLUSION1	
7	LIST	T OF APPENDICES1	3

1 INTRODUCTION

1.1 BRIEF

JC Consulting Ltd (JCC) have been commissioned by George F.White on behalf of Jonathan Sutherland to undertake a Drainage Strategy to support a detailed planning application. The planning application consists of two residential properties, with associated hard and soft landscaping.

The development site is located at Ordnance Survey (OS) Grid Reference: NU 23700 25196 (E423702, N625198), as shown in Figure 1.1.



Figure 1.1 - Ordnance Survey Map - Site Location

As a new development, Sustainable Drainage Systems (SuDS), surface and foul water drainage must be considered. This report gives an overview of the methodology used, summarises the options investigated and the drainage proposals for the development.

1.2 REPORT SCOPE

The principal objectives of this Drainage Strategy are as follows:

To establish the appropriate design standards and guidance that will assist the design of the Drainage Strategy.

To establish the existing site constraints and drainage features.

To determine a Drainage Strategy for the discharge of surface water flows from the site.

To determine a suitable Drainage Strategy for the discharge of foul water flows from the site.

2 RELEVANT POLICIES, LEGISLATION AND GUIDANCE

2.1 OVERVIEW

This Drainage Strategy will be in accordance with the following legislation and guidance:

National Planning Policy Framework

Planning Practice Guidance

Non-Statutory Technical Standards for Sustainable Drainage Systems

This Drainage Strategy will be designed using the standards:

BS EN 725:2017 – Drain and sewer systems outside buildings.

BS EN 12056-2 2000 – Gravity drainage systems inside buildings.

SuDS Manual (CIRIA C753)

Building Regulations Approved Document Part H 2010 Drainage and waste disposal (2015 Edition)

PPG3 – Use and design of oil separators in surface water drainage systems.

National Building Specification

Civil Engineering Specification for the Water Industry (7th Edition)

SSG Appendix C - Design and construction guidance for foul and surface water sewers offered for adoption under the Code for adoption agreements for water and sewerage companies operating wholly or mainly in England ("the Code"). Approved Version 2.0. 10 March 2020

2.2 NATIONAL PLANNING POLICY FRAMEWORK

The NPPF published in July 2018 and updated in February 2019, is a key part of the government's reform to make the planning system less complex and more accessible; to protect the environment and to promote sustainable growth.

In relation to drainage, the NPPF states that 'Major Developments' should incorporate sustainable drainage systems unless there is clear evidence that this would be inappropriate. The systems used should:

Take account of advice from the Lead Local Flood Authority.

Have appropriate proposed minimum operational standards.

Have maintenance arrangements in place to ensure an acceptable standard of operation for the lifetime of the development.

Where possible provide multifunctional benefits.

2.3 PLANNING PRACTICE GUIDANCE

The Planning Practice Guidance (2014) reiterates the government's expectation that sustainable drainage systems are provided in new developments wherever appropriate. It states that the government expect decisions based on incorporated policies, relating to 'Major Developments' (developments of 10 dwellings

or more, or equivalent non-residential developments) to ensure that sustainable drainage systems for the management of run-off are put in place, unless demonstrated otherwise.

2.4 NON-STATUTORY TECHNICAL STANDARDS FOR SUSTAINABLE DRAINAGE SYSTEMS

The 'Non-Statutory Technical Standards for Sustainable Drainage Systems' states that for greenfield developments, the peak run-off rate and run-off volume from the development to any drain, sewer, or surface water body for the 1 in 1-year rainfall event and the 1 in 100-year, 6-hour rainfall event should never exceed the peak greenfield run-off rate and volume for the same event.

For previously developed sites, the peak run-off rate and volume from the development to any drain, sewer or surface water body for the 1 in 1-year rainfall event and the 1 in 100-year, 6-hour rainfall event must be as close as reasonably possible to the greenfield run-off rate and volume from the development at the same rainfall event but should never exceed the rate of discharge or run-off volume from the development prior to re-development for that event.

Where it is not reasonably practicable to constrain volume of run-off, the volume must be discharged at a rate that does not affect flood risk.

Where the drainage system discharges to a surface water body that can accommodate uncontrolled surface water discharges without any impact on flood risk from that surface water body, the peak flow standards and volume control standards need not apply.

The drainage system must be designed so that flooding does not occur on any part of the site for a 1 in 30year rainfall event, unless there is an area of the site dedicated for compensatory storage.

The drainage system must also be designed so that flooding does not occur during a 1 in 100-year rainfall event in any part of the building or any utility plant on-site.

The design of the proposed development must ensure that flows resulting from excess rainfall for a 1 in 100-year event are managed in exceedance routes that minimise the risks to people and properties.

Components of the drainage network must be designed to ensure the structural integrity of the network is maintained throughout its design life. Materials, products, or fittings must be of a suitable standard for intended use.

Pumping should only be used to facilitate drainage for parts of the site where it is not practicable to drain water via gravity.

The construction of any communication with an existing sewer or drainage system must be such that the making of the communication would not damage the structural integrity or functionality of the sewerage system. Damage to the drainage system must be minimised, if unavoidable, and must be rectified prior to completion of the system.

3 SITE AND SURROUNDINGS

3.1 SITE LOCATION AND PROPOSED DEVELOPMENT DESCRIPTION

The proposed development site is situated at Newton-by-the-Sea, Alnwick; see Appendix A for the Proposed Site Plan. The proposed development site is centred at OS Grid Reference NU 23700 25196 (E423702, N625198).

This Drainage Strategy has been produced to support the planning application of a development site, which consists of 2 residential properties, with associated hard and soft landscaping.

The site at Newton-by-the-Sea is an irregular shaped parcel of land and encompasses an area of approximately 0.0596 ha (596²), comprising of an existing non-residential structure, and an area of external hard and soft landscaping used as an access road for the building. The site is bounded by residential properties to the north, and by the main road to the west. To the east and south, the site is bound by land for agricultural use.

A topographical survey has been provided for the site by Project North Geomatics, see Appendix B for the Topography Survey.

4 SURFACE WATER DRAINAGE STRATEGY

4.1 METHODOLOGY

The following methodology was used to produce a surface water Drainage Strategy for the site:

Determine a suitable method for surface water discharge.

Calculate pre-development/greenfield run-off rate, using the method outlined in the Interim Code of Practice for Sustainable Drainage Systems (ICP SuDS).

Calculate the required post development attenuation/storage required for the critical storm with a return period of 30 years in line with the National Planning Policy Framework (NPPF).

Test the sensitivity of the site by investigating the volume of runoff produced during storms with a return period of 100 year plus 40% allowance for climate change in line with the NPPF.

Test the sites suitability for the use of Sustainable Drainage Systems.

Test the sites post development water quality & outline any mitigation procedures.

Outline the maintenance procedures for the proposed drainage network and determine who will be responsible for the maintenance of the network, in accordance with 'CIRIA - The SuDS Manual C753'.

Outline the relevant guidance to be followed with respect to safety issues of the network.

4.2 SURFACE WATER DISCHARGE METHOD

The potential methods of surface water discharge, in order of preference, are:

Discharge to the ground via infiltration.

Discharge to a nearby watercourse.

Discharge to an existing surface water sewer.

Discharge to an existing combined water sewer.

A site investigation has not been carried out for the proposed development site; however, geological information can be obtained from the British Geological Survey (BGS) Geology of Britain Viewer (2014).

According to the BGS Geology of Britain Viewer (2014), the sites bedrock geology comprises of an Stainmore Formation, which consists of limestone, sandstone, and mudstone.

The BGS Geology of Britain Viewer (2014) also indicates that the sites superficial deposits consist of till, devensian (diamicton), which is predominantly bolder clay.

Based on the hierarchy of discharge of surface water, the preferred method of surface water disposal is by infiltration. However, using the desk top geological information above, the sites superficial deposits are not anticipated to be suitable to fully allow for infiltration.

The Ordnance Survey maps, and EA maps, show that the site is within the vicinity of a small watercourse located approximately 25 metres to the Southwest. However, there are no named bodies of water or

drainage ditches understood to be within the vicinity of the site. The watercourse transitions to a culverted watercourse which runs adjacent to the site boundary.

NWL have been contacted to identify any sewerage assets within the vicinity of the site (see Appendix C for the NWL Sewerage Plan).

NWL have verified that there is a 150mm combined water sewer approximately 5m south of the site, which is accessed via the access road to the site and connects to a pumping station to the east of the site. Chamber 6104 is shown to be 1.6m deep with 150mm inlet and outlet. However, it is anticipated that the most suitable location to discharge is at the SW manhole shown on the Topographic Survey (Appendix B) that is anticipated to be connection to the existing NWL culverted watercourse.

Following the hierarchy of discharge, it is therefore determined that the most suitable method of discharge for surface water will be into the NWL culverted watercourse whilst allowing for partial infiltration where possible at the development.

4.3 GREENFIELD RUN-OFF RATE CALCULATION

As discussed in the existing drainage discharge chapter it is assumed that the existing development would discharge into the NWL culverted watercourse at the chamber shown on the topographic survey. As part of the redevelopment works the network will be proposed to be split into separate surface and foul sewers with the surface discharging into the existing NWL surface water sewer. As a result, it would be proposed to restrict surface water flows to a rate agreed with the Lead Local Flood Authority (LLFA) to ensure that there will be no additional flooding to the surrounding area due to the development. It would be anticipated that surface water flows would be restricted as close as practicable to that of the predevelopment greenfield runoff rate.

The proposed development has an approximate area of 0.0596ha (596 m²). The greenfield run-off flow rate for the area has been calculated using the ICP SuDS Method (calculations carried out using MicroDrainage).

9	ICPSUDS								
Micro Drainage	ICP SUDS Input (FSI	R Method)				Results			
branidge	Return Period (Years)	30	Partly L	Irbanised Ca	R)	QBAR rural (I/s)			
	Area (ha)	0.060	Urban		0.000		0.3		
	SAAR (mm)	700	Region	Region 3	~		QBAR urban (l/s)		
	Soil	0.450	riegion	Incylonic	[0.3		
	Growth Curve	1	(None)		Calcul		0.5		
	Return Period Flood								
	Return Period Flood				ľ		1		
IH 124	Return Period Flood	QBAR (I/s)	Q (30yrs) (1/s)	Q (1 yrs) (l/s)	Q (30 yrs) (l/s)	Q (100 yrs) (l/s)			
ICP SUDS	Region	(l/s)	(l/s)	(l/s)	(l/s)	(Vs)			
	Region Region 1 Region 2 Region 3	(I/s) 0.3 0.3 0.3	(1/s) 0.5 0.5 0.5	(l/s) 0.2 0.2 0.2	(I/s) 0.5 0.5 0.5	(Vs) 0.7 0.5			
ICP SUDS	Region Region 1 Region 2 Region 3 Region 4	(I/s) 0.3 0.3 0.3 0.3	(1/s) 0.5 0.5 0.5 0.5	(Vs) 0.2 0.2 0.2 0.2	(I/s) 0.5 0.5 0.5 0.5	(I/s) 0.7 0.7 0.5 0.7			
ICP SUDS ADAS 345 FEH	Region Region 1 Region 2 Region 3 Region 4 Region 5	(Vs) 0.3 0.3 0.3 0.3 0.3 0.3	(1/s) 0.5 0.5 0.5 0.5 0.5 0.6	(Vs) 0.2 0.2 0.2 0.2 0.2 0.2	(l/s) 0.5 0.5 0.5 0.5 0.5 0.5	(l/s) 0.7 0.7 0.5 0.7 0.7 0.9			
ICP SUDS ADAS 345	Region Region 1 Region 2 Region 3 Region 4 Region 5 Region 6/Region 7	(Vs) 0.3 0.3 0.3 0.3 0.3 0.3 0.3	(1/s) 0.5 0.5 0.5 0.5 0.5 0.6 0.6	(Vs) 0.2 0.2 0.2 0.2 0.2 0.2 0.2	(l/s) 0.5 0.5 0.5 0.5 0.5 0.6	(l/s) 0.7 0.7 0.5 0.7 0.9 0.8			
ICP SUDS ADAS 345 FEH	Region Region 1 Region 2 Region 3 Region 4 Region 5	(Vs) 0.3 0.3 0.3 0.3 0.3 0.3	(1/s) 0.5 0.5 0.5 0.5 0.5 0.6	(Vs) 0.2 0.2 0.2 0.2 0.2 0.2	(l/s) 0.5 0.5 0.5 0.5 0.5 0.5	(l/s) 0.7 0.7 0.5 0.7 0.7 0.9			

Figure 4.3 – Greenfield Runoff Flow Rate Calculation

Given the relatively low flow rate calculated for greenfield runoff for all rainfall periods it is proposed to provide flow control restriction equivalent of using a minimum 75mm orifice sized flow control to avoid any blockages within the network, calculated to be 2.5 l/s. It is also understood that the existing development discharges unrestricted, whilst this rate is unknown it was a similar sized development, and the proposed restriction can reasonably be assumed to provide a significant betterment from the existing unrestricted discharge.

4.4 POST DEVELOPMENT ATTENUATION

It is proposed to provide a surface water drainage system serving all hard-standing areas for the site. Surface water flows are to be discharged to the existing NWL surface water culverted watercourse.

MicroDrainage has been used to model the proposed surface water drainage and carry out a simulation for various return periods for the site. Simulations were carried out to ensure that there is no exceedance of the surface water network for a 1 in 30-year return period event, in line with the NPPF guidelines. Further simulations have been carried out so that, for a 1 in 100-year return period event +45% for climate change and +10% urban creep), surface water flows are directed away from any buildings / structures and retained on-site, in accordance with the NPPF guidance.

The proposed drainage model does not show any flooding for a 1 in 30-year return period event or a 1 in 100-year return period event plus 45% allowance for climate change and plus 10% urban creep. Flows in exceedance of the surface water sewerage will be retained within the proposed permeable paving subbase and filter drain. It is proposed to drain surface water flows through permeable paving and a filter drain to provide a measure of SuDS source control and water quality improvement. Refer to Appendix D for the Proposed Drainage Arrangement, Appendix E for the MicroDrainage Results.

Exceedance flow management has been designed to ensure any flows exceeding the discharge rate will be attenuated on-site, within the below ground sewerage network and SuDS features. The required storage has been sized for a 1 in 100-year storm event, with +45% for climate change + 10% urban creep. The proposed ground levels would also dictate that if there was any exceedance of the network surface water flows would naturally fall away from the building and to the lower ground level at the proposed filter drain and soft landscaping.

4.5 SUDS SUITABILITY ASSESSMENT

The NPPF states that SuDS should be incorporated in all new developments unless evidence of unsuitability is provided. Therefore, the following SuDS components have been considered for the site:

SuDS Component	Description	Site Suitability	Comments
Rainwater Harvesting	Systems that collect runoff from the roof of a building or other paved surface for use.		Potential to water butts for soft landscaping irrigation but depends on occupants whether to adopt the use. Potential be retrofitted into property when occupied.
Green Roof	Planted soil layers on the roof of buildings that slow and store runoff.	×	The residential roofs are proposed to be pitched and unsuitable for green roofs.
Soakaway	Systems that collect and store runoff, allowing it to infiltrate into the ground.	×	Ground conditions deemed to be unsuitable for full infiltration and partial infiltration to be used.

Table 4.5 – SuDS Component Assessment

Pervious Pavement	Structural paving through which runoff can soak and subsequently be stored in the sub-base beneath, and/ or allowed to infiltrate into the ground below.		Potential for paving as part of car parking arrangements.
Filter Strip	Grass strips that promote sedimentation and filtration as runoff is conveyed over the surface.	×	Site layout unsuitable
Filter Trench	Shallow stone-filled trenches that provide attenuation, conveyance, and treatment of runoff.		Potential for Filter Trench
Infiltration Trench	Systems that collect and store runoff, allowing it to infiltrate to the ground.	×	Site layout unsuitable
Swale	Vegetated channels (sometimes planted) used to convey and treat runoff.	×	Site layout unsuitable
Bioretention	Shallow landscaped depressions that allow runoff to pond temporarily on the surface. Before filtering through vegetation and underlying soils.	×	Restricted space for ponding.
Infiltration Basin	Vegetated depressions that store and treat runoff, allowing it to infiltrate into the ground.	×	Restricted space on site.
Detention Basin	Vegetated depressions that store and treat runoff.	×	Restricted space on site.
Pond	Permanent pools of water used to facilitate treatment of runoff – runoff can also be stored in attenuation zone above pool.	×	Restricted space on site.
Stormwater Wetlands	Permanent pools of water used to facilitate treatment of runoff – runoff can also be stored in attenuation zone above pool.	×	Size of development unsuitable.

4.6 WATER QUALITY MANAGEMENT

The surface water drainage design is required to consider the potential for contaminants to be collected with surface water runoff and discharge to the wider water catchment. Following the guidance within the Ciria SuDS Manual C753, Chapter 26, the impermeable areas to be drained have been classified as having the following pollution hazard levels:

Table 4.6 – Land Classification Pollution Hazard Indices

Land Use	Pollution Hazard Level	Total Suspended Solids	Metals	Hydrocarbons
Desidential reaf			0.0	0.05
Residential roofs	Very Low	0.2	0.2	0.05
Individual property driveways, residential car parks, low traffic roads (e.g., cul de sacs, home zones and general access roads) and non- residential car parking with infrequent change (e.g., schools, offices) i.e., < 300 traffic movements/day	Low	0.5	0.4	0.4

Residential roofs have a 'very low' pollution hazard level; therefore, the risk to water quality is considered very low.

Table 4.6.1 – SuDS Mitigation Indices

SuDS Component	Total Suspended Solids	Metals	Hydrocarbons
Permeable Paving	0.7	0.6	0.7
Filter Drain	0.4	0.4	0.4

The pollution load associated with the total run-off volume from all storm events will be retained on-site, where it will have time to biodegrade or be acted on by natural treatment processes. Interception of the pollution load cannot be guaranteed for every rainfall event, due to the variations in evapotranspiration and rainfall. However, to ensure a high probability of interception, it is proposed to provide additional storage for the first 5mm of rainfall for the majority of rainfall events, which will mitigate the risk to water quality entering the network.

Permeable paving has been shown to decrease concentrations of surface water pollutants. Silt can be trapped within the top 30mm of the paving and further treatment is achieved via biodegradation of organic pollutants, such as petrol. The frequency of runoff from all types of pervious paving is significantly reduced compared to gully / pipe networks; therefore, runoff does not typically occur from permeable surfaces for rainfall events up to 5mm.

On this basis, it is considered that suitable SuDS features have been proposed for the development to mitigate potential contaminants to the wider water catchment.

4.7 SURFACE WATER MAINTENANCE ISSUES

Surface water drainage within the plot boundary is anticipated to be retained within private ownership. Therefore, this drainage will be the responsibility of the landowner. Refer to Appendix F for the Drainage Maintenance Schedule.

4.8 SURFACE WATER SAFETY ISSUES

Surface water pipework and manholes have been designed in accordance with the appropriate building regulations and Sewers for Adoption, to ensure suitable access for maintenance and operation as required.

Exceedance flow management caused by system blockages has been considered and the proposed network has been designed to mitigate the risks to people and property.

Works are to be carried out by an established and professional contractor and in accordance with standard good practice guidance. The potential for flooding, caused by surface water rainfall, during construction is to be mitigated by the contractor by providing an in-depth method statement in accordance with BS8582 2013 and CIRIA C768.

4.9 SURFACE WATER DRAINAGE SUMMARY

Based on the investigation carried out to date, the surface water drainage strategy can be summarised as:

Flows from rooftop will be collected by traditional rainwater pipes and discharged into the pipe network via gravity. The piped network will then discharge into the permeable paving sub-base through a permavoid diffuser unit.

Flows from property parking area will be drained through permeable paving and discharged into the pipe network via gravity.

Flows from the access track will be drained to a filter trench. The filter trench is shown as suitable for partial infiltration with any exceedance of flows discharging into the pipe network via an overflow pipe.

Surface water flows will be discharged to the existing NWL surface water culverted watercourse network via gravity at an existing chamber.

Peak flows in excess of the restricted discharge rate of 2.5 l/s during storms up to 1 in 100 years, plus 45% for climate change and 10% urban creep will be attenuated on-site to ensure there is no flooding of the proposed site or flooding off site.

SuDS water quality improvement will be provided by draining flows through permeable paving and a filter drain.

5 FOUL WATER DRAINAGE STRATEGY

5.1 METHODOLOGY

The following methodology was used to produce a foul water Drainage Strategy for the site:

Determine a suitable method for foul water discharge.

Calculate the post development foul water drainage flows, in accordance with BS EN 12056-2:2000.

Outline the maintenance procedures for the proposed drainage network & who will be responsible for the maintenance of the network, in accordance with the relevant codes of practice.

Outline the relevant guidance to be followed with respect to safety issues of the network.

5.2 FOUL DRAINAGE DISCHARGE METHOD

The potential methods of foul water discharge, in order of preference, are:

- Discharge to an existing foul water network.
- Discharge to an existing combined water network.
- Discharge to a septic tank, with an appropriate form of treatment or another wastewater treatment system.
- Discharge to a cesspool.

NWL have been contacted to identify any sewerage assets within the vicinity of the site (see Appendix C for the NWL Sewerage Plan).

NWL have verified that there is a 150mm diameter combined water sewer within the existing access road. The combined water sewer is expected to collect foul water drainage from the properties to the north and east of the site as well as the previous development.

It is proposed to discharge the foul water to combined water sewer with a new connection, within the site boundary. A Pre-development application enquiry will need to be submitted to NWL to confirm that foul flows can be discharged at an unrestricted rate to their network.

5.3 FOUL WATER MAINTENANCE ISSUES

Foul water drainage within the plot boundary is anticipated to be retained within private ownership. Therefore, this drainage will be the responsibility of the landowner. Refer to Appendix F for the Drainage Maintenance Schedule.

5.4 FOUL WATER SAFETY ISSUES

Foul water pipework and manholes have been designed in accordance with the appropriate building regulations and Sewers for Adoption, to ensure suitable access for maintenance and operation as required.

Works are to be carried out by an established and professional contractor and in accordance with standard good practice guidance. The potential for flooding, caused by surface water rainfall, during construction is to be mitigated by the contractor by providing an in-depth method statement in accordance with BS8582 2013 and CIRIA C768.

6 CONCLUSION

The Drainage Strategy has been produced for the development of 2 residential properties with associated hard and soft landscaping. This report has been produced to present the drainage proposals for the development and document the underlying analysis, as required by Northumberland County Council's planning process. The drainage strategy has been produced in accordance with the applicable regulatory framework and relevant best practice guidance, as set out within the report.

Based on the available geological data, it is anticipated that surface water discharge to the ground via infiltration will not be achievable and there is no feasible open watercourse in proximity to the development. However, it is proposed to discharge surface water to the NWL culverted watercourse at a restricted rate of 2.5 I/s with the appropriate level of water quality treatment. SuDS source control and water quality improvement will be provided through permeable paving and a filter drain. Attenuation for exceedance flows will be provided through the permeable paving and filter drain sub-base for rainfall events up to 1 in 100 years, plus 45% for climate change + 10% urban creep.

It is proposed to discharge foul water flows to the existing NWL combined network in the access road. A pre-planning enquiry must be made to NWL prior to construction to ensure that additional foul water flows can be accommodated within their network.

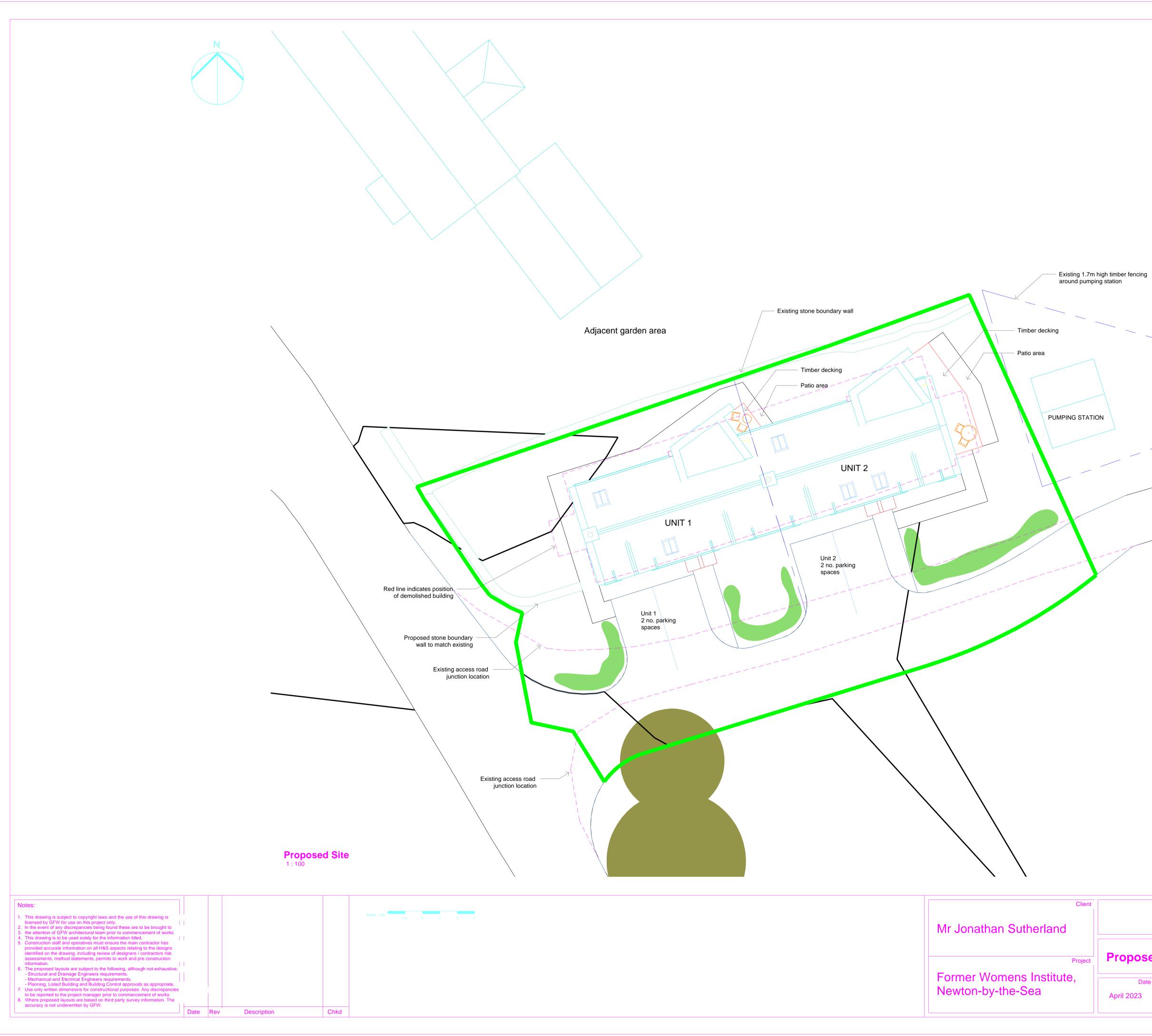
A S106 application must be agreed with NWL prior to construction, to ensure new connections can be made to their network.

7 LIST OF APPENDICES

- APPENDIX A: PROPOSED SITE PLAN
- APPENDIX B: TOPOGRAPHY SURVEY
- APPENDIX C: NORTHUMBRIAN WATER SEWERAGE PLAN
- APPENDIX D: PROPOSED DRAINAGE ARRANGEMENT
- APPENDIX E: PROPOSED MICRODRAINAGE RESULTS
- APPENDIX F: DRAINAGE MAINTENACE SCHEDULE

Report Ref: JCC23-111-C-01 Revision 00, August 2023

APPENDIX A PROPOSED SITE PLAN



		Status			
	Planning				
		Drawing Title	C/Users/geterstein/DivDrve - George F Vinte/Job-001843/2 Arch,MhDutgong/8	Brawngs/2023-05-04 DVG FRes/0000843-Proposed-P	02-OFW-title-block-757441png
opose	ed Site Pla	in			
Date	Drwn/Chkd	Scale	Project Number	Dwg No.	Revision
2023	PE CR	1 : 100	0001843	1120	

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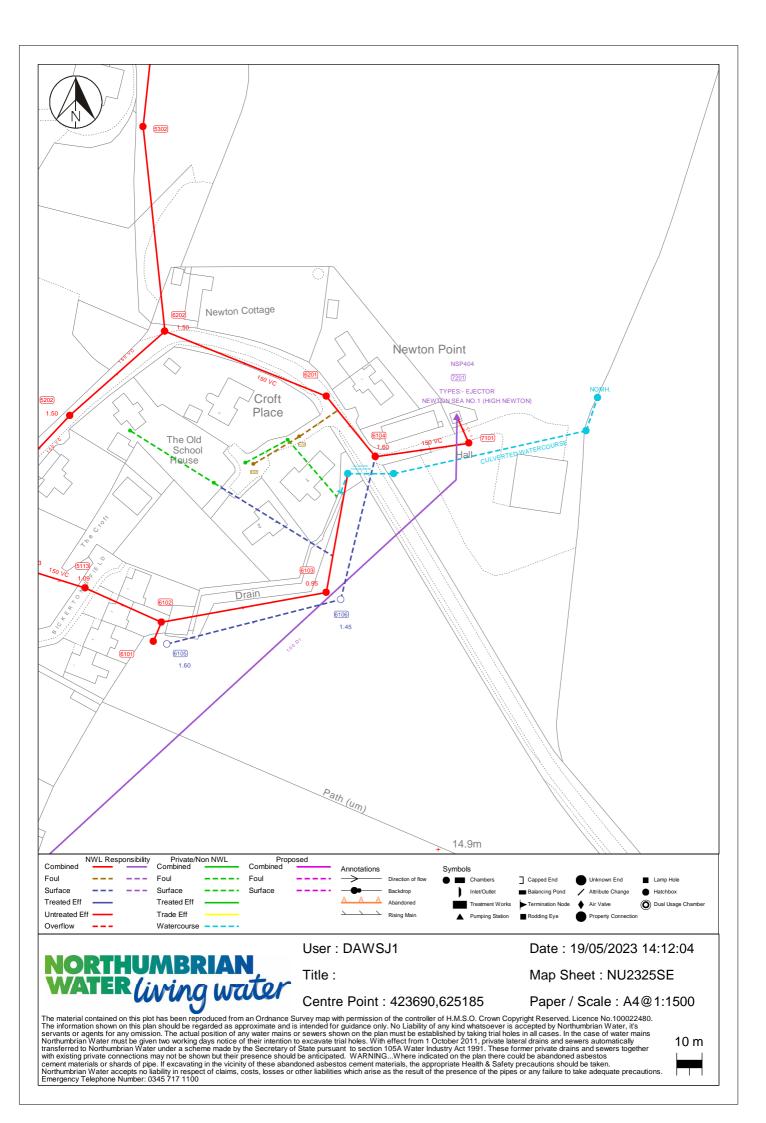
Report Ref: JCC23-111-C-01 Revision 00, August 2023

APPENDIX B TOPOGRAPHY SURVEY

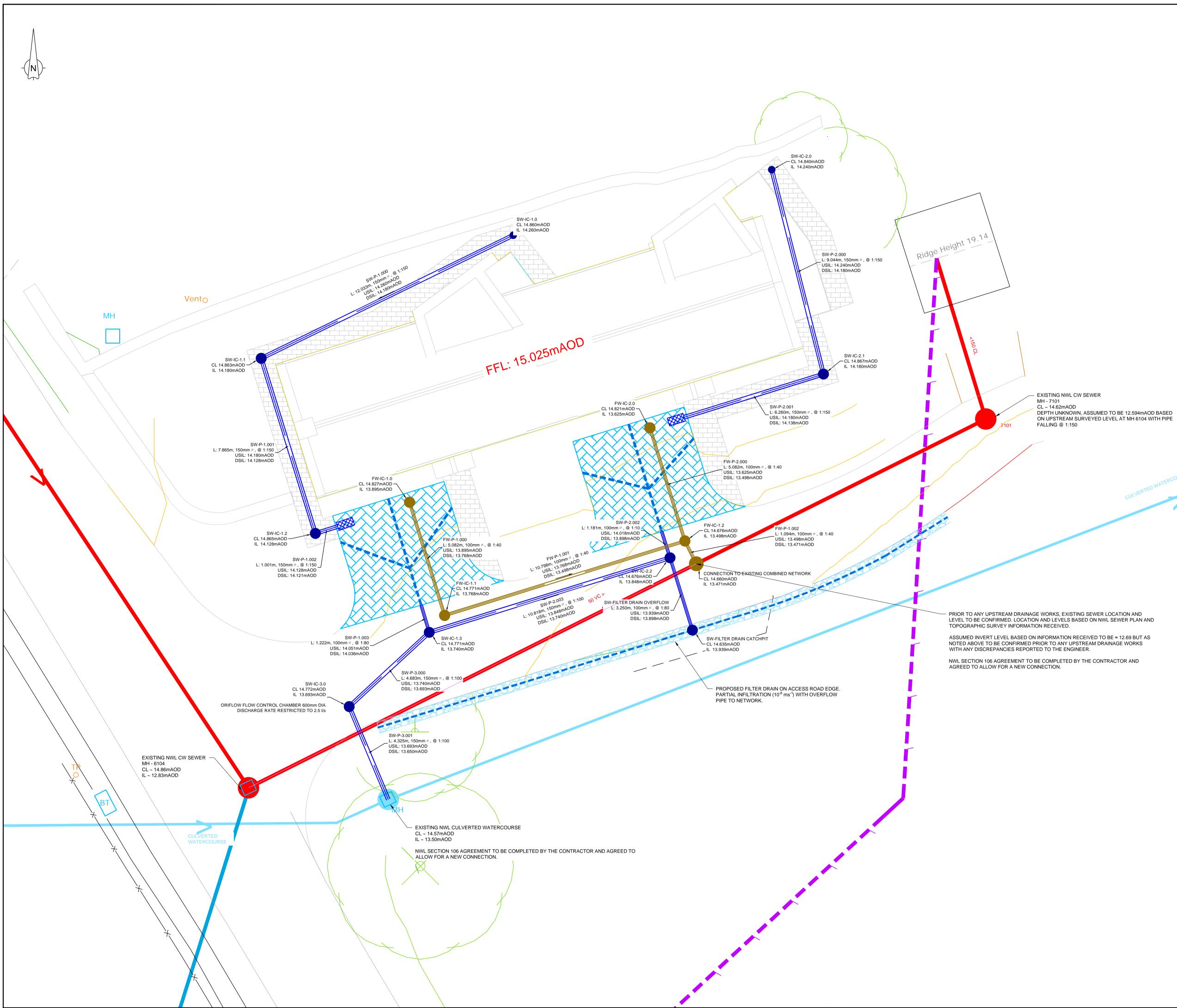


APPENDIX C

NORTHUMBRIAN WATER SEWERAGE PLAN



APPENDIX D PROPOSED DRAINAGE ARRANGEMENT



NOTES

- EXISTING SEWER INFORMATION FROM NWL PDF PLAN AND TOPOGRAPHICAL SURVEY RECEIVED DOES NOT COINCIDE WITH EACH OTHER. ASSUMPTION BASED ON NWL PLAN ON PDF AND USING KNOWN MANHOLE COVERS SHOWN ON THE TOPOGRAPHICAL SURVEY.
- 2. REFER TO ARCHITECTS DRAWINGS FOR CONFIRMATION OF LANDSCAPING ARRANGEMENTS.
- 3. ALL LEVELS ARE mAOD UNLESS STATED OTHERWISE.

DRAWING INFORMATION

- 4. EXISTING SITE INFORMATION BASED ON TOPOGRAPHICAL SURVEY CARRIED OUT BY PROJECT NORTH GEOMATICS, DRAWING No. A92-001, DATED 30/03/23.
- 5. PROPOSED SITE INFORMATION BASED ON GEORGE F WHITE ARCHITECTURAL DRAWINGS RECEIVED.

GENERAL NOTES:

- 5. THIS DRAWING IS BASED ON ORDNANCE SURVEY AND TOPOGRAPHICAL SURVEY INFORMATION RECEIVED. WE CAN ACCEPT NO LIABILITY FOR DESIGN BASED ON INFORMATION RECEIVED.
- . THIS DESIGN HAS BEEN CARRIED OUT TO APPROPRIATE STANDARDS BUT IT IS TO BE CHECKED IN ACCORDANCE WITH PROCUREMENT AND REQUIREMENTS PRIOR TO THE COMMENCEMENT OF WORKS.
- 3. ALL LEVELS, DIMENSIONS AND DETAILS TO BE CONFIRMED BY THE CONTRACTOR PRIOR TO THE COMMENCEMENT OF CONSTRUCTION OR FABRICATION.
- . NO EXISTING BELOW GROUND CONDITIONS HAVE BEEN PROVIDED. THEREFORE, ALL INFORMATION IS TO BE BE VERIFIED FURTHER TO ANY SITE WORKS.
- 0.NO EXISTING SERVICES INFORMATION HAVE BEEN PROVIDED. THEREFORE, ALL INFORMATION IS TO BE BE VERIFIED FURTHER TO ANY SITE WORKS.
- 1.EXISTING GROUND LEVELS AND GROUND PROFILES HAVE BEEN TAKEN FROM THE INFORMATION PROVIDED AND AS SUCH ARE TO BE VERIFIED BY THE CONTRACTOR PRIOR TO THE COMMENCEMENT OF WORKS. ANY DISCREPANCIES TO BE BROUGHT TO THE ATTENTION OF THE ENGINEER.

LEGEND:



P1	INI	TIAL ISSUE FOR PLANNING	3	RJ	AS	04/08/23
Rev		Description	<u>,</u>	Drawn	Check'd	Date
Drawing St	atus:					
		PLANNIN	<u>1G</u>			
E. ei ww Unit Bake Gosf	w.jc-consu 16, The Stott ers Yard, Chris	consulting.net Ilting.net ie Shed		_	neerir	-
© JC (CONSULTING LTI	D. Geo-Envi	ronmenta			-
Client:						
	1	MR JONATHAN SL	JTHERLAND)		
Project:	F	ORMER WOMEN'S	S INSTITUTE	Ξ,		
		NEWTON-BY-				
Drawing Ti		OSED DRAINAGE	ARRANGE	MENT		
Scale:	1:75	Drawn: RJ	Checked: AS		Date: 04/0	8/23
Job Numbe	er:	Drawing Number:			Rev:	Size:
JCC	23 - 111	C - G,	A - 001		P1	A1

APPENDIX E PROPOSED MICRODRAINAGE RESULTS

JC Consulting Ltd	Page 1
4 McMillan Close	
Gateshead	
Tyne & Wear NE9 5BF	Micco
Date 04/08/2023 15:58	Designed by rjones
File PROPOSED SW.MDX	Checked by Drainage
XP Solutions	Network 2017.1.1
Design Pipe Sizes STA FSR Rainfall Return Period (years) M5-60 (mm) Ratio R Maximum Rainfall (mm/hr) Maximum Time of Concentration (mins) Foul Sewage (1/s/ha) Volumetric Runoff Coeff.	0.298Minimum Backdrop Height (m)0.20050Maximum Backdrop Height (m)1.50030 Min Design Depth for Optimisation (m)1.200
Time Are	ea Diagram for Storm
	Area Time Area (ha) (mins) (ha) 0.023 4-8 0.006
Total Area	Contributing $(ha) = 0.028$
	pe Volume $(m^3) = 1.263$
Network D	esign Table for Storm
PN Length Fall Slope I.Area T.F (m) (m) (1:X) (ha) (mir	E. Base k HYD DIA Section Type Auto ns) Flow (l/s) (mm) SECT (mm) Design
1.000 12.033 0.080 150.0 0.003 5.	.00 0.0 0.600 o 150 Pipe/Conduit 🎁
1.001 7.865 0.052 150.0 0.002 0.	.00 0.0 0.600 o 150 Pipe/Conduit 💣
	.00 0.0 0.600 o 150 Pipe/Conduit
1.003 4.917 0.061 80.0 0.000 0.	.00 0.0 0.600 o 150 Pipe/Conduit 🔒
Netwo	ork Results Table
PN Rain T.C. US/IL Σ I.A	rea Σ Base Foul Add Flow Vel Cap Flow
(mm/hr) (mins) (m) (ha	
	003 0.0 0.0 0.0 0.82 14.5 0.3 004 0.0 0.0 0.0 0.82 14.5 0.6
	0.0 0.0 0.0 0.0 0.02 14.5 0.0 008 0.0 0.0 0.0 0.82 14.5 1.1
	008 0.0 0.0 0.0 1.12 19.9 1.1
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	ulting	шса									123	age 2
McMill	lan Clo	se									ſ	
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yne & V	Wear 1	JE9 5E	3F									- Cr
ate 04,					De	signed by	rione	s				
ile PR(ecked by						Drainag
P Solut		GW.HL	//1			twork 2017	7 1 1					J
F SOLU					ne	CWOIR ZOI	• - • -					
				Networ	k Desi	lgn Table	for S	torm				
				11001101				001				
PN	Length	Fall	Slope	I.Area	T.E.	Base	k	HYD	DIA	Secti	on Type	e Auto
	(m)	(m)	(1:X)	(ha)	(mins)	Flow (l/s)	(mm)	SECT	(mm)			Design
1.004	1 222	0.179	6.8	0.002	0.00	0 0	0.600	o	150	Pine/	Condui	t 🔐
1.001	1.000	5.17	0.0	0.002	0.00	0.0	5.000	0	100	PC/	Condut	- U
2.000	9.044	0.060	150.0	0.003	5.00	0.0	0.600	0	150	Pipe/	Condui	t 🔒
2.001	6.260	0.042	150.0	0.003	0.00	0.0	0.600	0	150	Pipe/	Condui	
2.002	4.998	0.120	41.7	0.000	0.00	0.0	0.600	0	150	Pipe/	Condui	
2.003	1.181	0.030	40.0	0.003	0.00	0.0	0.600	0	150	Pipe/	Condui	
3.000	3,101	0.031	100.0	0.009	5.00	0.0	0.600	0	150	Pipe/	Condui	t 🔒
51000	5.101	0.001	100.0	0.000	5.00	0.0		Ũ	200	1 1 1 0 /	condu	- -
2.004	10.818	0.108	100.0	0.000	0.00	0.0	0.600	0	150	Pipe/	Condui	t 🥚
1.005	4.683	0.047	100.0	0.000	0.00	0.0	0.600	0	150	Pipe/	Condui	t 🔐
1.006	4.325	0.043	100.0	0.000	0.00	0.0	0.600	0	150	Pipe/	Condui	
					. 1	D 1 -						
				Ne	<u>etwork</u>	Results 1	<u>able</u>					
P	N Rai	in 1	.c.	<u>Ν</u> α US/IL Σ				Add F	low	Vel	Cap	Flow
P		in I hr) (m					Foul	Add E			Cap (1/s)	
P) 1.0	(mm /		nins)	US/IL Σ	I.Area	Σ Base Flow (l/s)	Foul				-	
	(mm/)	hr) (m	nins)	US/IL Σ (m) 14.059	I.Area (ha)	Σ Base Flow (1/s) 0.0	Foul (l/s)		s)	(m/s)	(1/s)	(l/s)
1.0	(mm/) 004 50	hr) (m .00	nins) 5.50 1 5.18 1	US/IL E (m) 14.059 14.240	I.Area (ha) 0.011 0.003	Σ Base Flow (1/s) 0.0 0.0	Foul (1/s) 0.0 0.0		s) 0.0 0.0	(m/s) 3.88 0.82	(1/s) 68.6 14.5	(1/s) 1.4 0.4
1.0 2.0 2.0	(mm/ 004 50 000 50 001 50	(m)	5.50 5.18 5.31 5	US/IL Σ (m) 14.059 14.240 14.180	I.Area (ha) 0.011 0.003 0.006	Σ Base Flow (1/s) 0.0 0.0 0.0	Foul (1/s) 0.0 0.0 0.0		s) 0.0 0.0 0.0	(m/s) 3.88 0.82 0.82	(1/s) 68.6 14.5 14.5	(1/s) 1.4 0.4 0.8
1.0	(mm/ 004 50 000 50 001 50 002 50	hr) (m .00 .00 .00	nins) 5.50 1 5.18 1	US/IL Σ (m) 14.059 14.240 14.180 14.138	I.Area (ha) 0.011 0.003	Σ Base Flow (1/s) 0.0 0.0 0.0 0.0	Foul (1/s) 0.0 0.0		s) 0.0 0.0	(m/s) 3.88 0.82	(1/s) 68.6 14.5	(1/s) 1.4 0.4
1.0 2.0 2.0 2.0	(mm/ 004 50 000 50 001 50 002 50 003 50	(m)	5.50 5.18 5.31 5.37 5.38	US/IL Σ (m) 14.059 14.240 14.180 14.138	I.Area (ha) 0.011 0.003 0.006 0.006	Σ Base Flow (1/s) 0.0 0.0 0.0 0.0 0.0	Foul (1/s) 0.0 0.0 0.0 0.0		s) 0.0 0.0 0.0 0.0	(m/s) 3.88 0.82 0.82 1.56	(1/s) 68.6 14.5 14.5 27.6	(1/s) 1.4 0.4 0.8 0.8
1.0 2.0 2.0 2.0 2.0	(mm/ 004 50 000 50 001 50 002 50 003 50 003 50	(m)	5.50 5.18 5.31 5.37 5.38 5.05	US/IL Σ (m) 14.059 14.240 14.180 14.138 14.018	I.Area (ha) 0.011 0.003 0.006 0.006 0.008	Σ Base Flow (1/s) 0.0 0.0 0.0 0.0 0.0 0.0	Foul (1/s) 0.0 0.0 0.0 0.0 0.0		s) 0.0 0.0 0.0 0.0 0.0	(m/s) 3.88 0.82 0.82 1.56 1.60	(1/s) 68.6 14.5 14.5 27.6 28.2	(1/s) 1.4 0.4 0.8 0.8 1.1
1.0 2.0 2.0 2.0 2.0 3.0	(mm/ 004 50 000 50 001 50 002 50 003 50 000 50 000 50	<pre>hr) (m .00 .00 .00 .00 .00 .00 .00 .00</pre>	nins) 5.50 1 5.18 1 5.31 1 5.37 1 5.38 1 5.38 1 5.38 1 5.56 1	US/IL Σ (m) 14.059 14.240 14.180 14.138 14.018 13.879	I.Area (ha) 0.011 0.003 0.006 0.006 0.008 0.009	Σ Base Flow (1/s) 0.0 0.0 0.0 0.0 0.0 0.0	Foul (1/s) 0.0 0.0 0.0 0.0 0.0 0.0		s) 0.0 0.0 0.0 0.0 0.0 0.0	(m/s) 3.88 0.82 0.82 1.56 1.60 1.00	(1/s) 68.6 14.5 14.5 27.6 28.2 17.8	(1/s) 1.4 0.4 0.8 0.8 1.1 1.2

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JC Consulting Ltd					Page 3
4 McMillan Close					
Gateshead					4
Tyne & Wear NE9 5BF					
Date 04/08/2023 15:58	De	signed b	y rjones		MILLO
File PROPOSED SW.MDX		lecked by			Drainage
XP Solutions		etwork 20			
MI BOILCIOND	110	.eworn 20			
Ar	ea Su	mmary for	<u>Storm</u>		
Pipe PIMP PIM Number Type Name		Gross Area (ha)	Imp. Area (ha)	Pipe Total (ha)	
1.000 User -	100	0.003	0.003	0.003	
1.001 User -	100	0.002			
	- 100	0.004			
	· 100	0.000		0.000	
	- 100 - 100	0.002		0.002 0.003	
	· 100	0.003		0.003	
	- 100	0.000		0.000	
	100	0.003		0.003	
3.000 User -	100	0.009	0.009	0.009	
2.004	100	0.000	0.000	0.000	
	- 100	0.000		0.000	
1.006	- 100	0.000			
		Total			
		0.028	0.028	0.028	
Simula	tion	<u>Criteria</u>	for Stor	<u>rm</u>	
Volumetric Runoff Coef	f 0.75	50 Addit	ional Flow	- % of Total Flow	v 10.000
Areal Reduction Facto	or 1.00	00 M.	ADD Factor	* 10m³/ha Storage	e 2.000
Hot Start (mins		0		Inlet Coeffiecient	
Hot Start Level (mm		-	r Person pe		
Manhole Headloss Coeff (Global	,		Quetar	Run Time (mins)	
Foul Sewage per hectare (1/s	;) 0.00	0	Outpi	ut Interval (mins)) 1
Number of Input Hydrographs 0 Num Number of Online Controls 1 Numbe					-
<u>Synt</u>	<u>hetic</u>	Rainfal	L Details		
Rainfall Model		EGP	-	profile Trong Com	
Rainfall Model Return Period (years)		FSR 30		Profile Type Summe Cv (Summer) 0.75	
	ngland	and Wales		Cv (Winter) 0.84	
M5-60 (mm)	5				30
Ratio R		0.298			
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	Ltd						Page 4
4 McMillan Clo	se						
Gateshead							4
Tyne & Wear N	E9 5BF						
Date 04/08/202	3 15:58		Desig	ned by rj	ones		
File PROPOSED	SW.MDX			ed by			Drainage
XP Solutions				rk 2017.1	1		
		<u>On]</u>	line Contr	ols for S	torm		
<u>Hydro-I</u>	Brake® (Optimum N	Manhole: 6	, DS/PN:	1.006, Vo	lume (m³)	: 0.4
					-0075-2500-		
			Design Head sign Flow (]			1.000 2.5	
		De	Flush-F		С	alculated	
			Object	tive Minim	ise upstrea	m storage	
			Applicat			Surface	
			Sump Availa Diameter			Yes 75	
		т	nvert Level	. ,		13.693	
	Minimum (e Diameter	. ,		100	
	Suggest	ted Manhol	e Diameter	(mm)		1200	
Control Poi	ints	Head (m)	Flow (l/s)	Cont	rol Points	Head	(m) Flow (l/s)
Design Point (Ca F	lculated				Kick- over Head F		.627 2.0 - 2.2
			, ,	1	1/5/ 1		
The hydrologica Hydro-Brake® Op					-		-
Hydro-Brake Opt	-	-					
Depth (m) Fl	.ow (1/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
			2.7	3.000	4 1	7.000	C 0
0.100	2.1	1.200			4.1	1.000	6.2
0.200	2.4	1.400			4.5	7.500	6.4
0.200 0.300	2.4 2.5	1.400 1.600	3.1	4.000	4.5 4.7	7.500 8.000	6.4 6.6
0.200 0.300 0.400	2.4 2.5 2.5	1.400 1.600 1.800	3.1 3.3	4.000 4.500	4.5 4.7 5.0	7.500 8.000 8.500	6.4 6.6 6.8
0.200 0.300 0.400 0.500	2.4 2.5 2.5 2.4	1.400 1.600 1.800 2.000	3.1 3.3 3.4	4.000 4.500 5.000	4.5 4.7 5.0 5.3	7.500 8.000	6.4 6.6 6.8 7.0
0.200 0.300 0.400	2.4 2.5 2.5	1.400 1.600 1.800	3.1 3.3 3.4 3.6	4.000 4.500 5.000 5.500	4.5 4.7 5.0	7.500 8.000 8.500 9.000	6.4 6.6 6.8
0.200 0.300 0.400 0.500 0.600	2.4 2.5 2.5 2.4 2.1	1.400 1.600 2.000 2.200 2.400	3.1 3.3 3.4 3.6 3.7	4.000 4.500 5.000 5.500 6.000	4.5 4.7 5.0 5.3 5.5	7.500 8.000 8.500 9.000	6.4 6.6 6.8 7.0
0.200 0.300 0.400 0.500 0.600 0.800	2.4 2.5 2.5 2.4 2.1 2.3	1.400 1.600 2.000 2.200 2.400	3.1 3.3 3.4 3.6 3.7	4.000 4.500 5.000 5.500 6.000	4.5 4.7 5.0 5.3 5.5 5.7	7.500 8.000 8.500 9.000	6.4 6.6 6.8 7.0
0.200 0.300 0.400 0.500 0.600 0.800	2.4 2.5 2.5 2.4 2.1 2.3	1.400 1.600 2.000 2.200 2.400	3.1 3.3 3.4 3.6 3.7	4.000 4.500 5.000 5.500 6.000	4.5 4.7 5.0 5.3 5.5 5.7	7.500 8.000 8.500 9.000	6.4 6.6 6.8 7.0
0.200 0.300 0.400 0.500 0.600 0.800	2.4 2.5 2.5 2.4 2.1 2.3	1.400 1.600 2.000 2.200 2.400	3.1 3.3 3.4 3.6 3.7	4.000 4.500 5.000 5.500 6.000	4.5 4.7 5.0 5.3 5.5 5.7	7.500 8.000 8.500 9.000	6.4 6.6 6.8 7.0
0.200 0.300 0.400 0.500 0.600 0.800	2.4 2.5 2.5 2.4 2.1 2.3	1.400 1.600 2.000 2.200 2.400	3.1 3.3 3.4 3.6 3.7	4.000 4.500 5.000 5.500 6.000	4.5 4.7 5.0 5.3 5.5 5.7	7.500 8.000 8.500 9.000	6.4 6.6 6.8 7.0
0.200 0.300 0.400 0.500 0.600 0.800	2.4 2.5 2.5 2.4 2.1 2.3	1.400 1.600 2.000 2.200 2.400	3.1 3.3 3.4 3.6 3.7	4.000 4.500 5.000 5.500 6.000	4.5 4.7 5.0 5.3 5.5 5.7	7.500 8.000 8.500 9.000	6.4 6.6 6.8 7.0
0.200 0.300 0.400 0.500 0.600 0.800	2.4 2.5 2.5 2.4 2.1 2.3	1.400 1.600 2.000 2.200 2.400	3.1 3.3 3.4 3.6 3.7	4.000 4.500 5.000 5.500 6.000	4.5 4.7 5.0 5.3 5.5 5.7	7.500 8.000 8.500 9.000	6.4 6.6 6.8 7.0
0.200 0.300 0.400 0.500 0.600 0.800	2.4 2.5 2.5 2.4 2.1 2.3	1.400 1.600 2.000 2.200 2.400	3.1 3.3 3.4 3.6 3.7	4.000 4.500 5.000 5.500 6.000	4.5 4.7 5.0 5.3 5.5 5.7	7.500 8.000 8.500 9.000	6.4 6.6 6.8 7.0
0.200 0.300 0.400 0.500 0.600 0.800	2.4 2.5 2.5 2.4 2.1 2.3	1.400 1.600 2.000 2.200 2.400	3.1 3.3 3.4 3.6 3.7	4.000 4.500 5.000 5.500 6.000	4.5 4.7 5.0 5.3 5.5 5.7	7.500 8.000 8.500 9.000	6.4 6.6 6.8 7.0
0.200 0.300 0.400 0.500 0.600 0.800	2.4 2.5 2.5 2.4 2.1 2.3	1.400 1.600 2.000 2.200 2.400	3.1 3.3 3.4 3.6 3.7	4.000 4.500 5.000 5.500 6.000	4.5 4.7 5.0 5.3 5.5 5.7	7.500 8.000 8.500 9.000	6.4 6.6 6.8 7.0
0.200 0.300 0.400 0.500 0.600 0.800	2.4 2.5 2.5 2.4 2.1 2.3	1.400 1.600 2.000 2.200 2.400	3.1 3.3 3.4 3.6 3.7	4.000 4.500 5.000 5.500 6.000	4.5 4.7 5.0 5.3 5.5 5.7	7.500 8.000 8.500 9.000	6.4 6.6 6.8 7.0
0.200 0.300 0.400 0.500 0.600 0.800	2.4 2.5 2.5 2.4 2.1 2.3	1.400 1.600 2.000 2.200 2.400	3.1 3.3 3.4 3.6 3.7	4.000 4.500 5.000 5.500 6.000	4.5 4.7 5.0 5.3 5.5 5.7	7.500 8.000 8.500 9.000	6.4 6.6 6.8 7.0
0.200 0.300 0.400 0.500 0.600 0.800	2.4 2.5 2.5 2.4 2.1 2.3	1.400 1.600 2.000 2.200 2.400	3.1 3.3 3.4 3.6 3.7	4.000 4.500 5.000 5.500 6.000	4.5 4.7 5.0 5.3 5.5 5.7	7.500 8.000 8.500 9.000	6.4 6.6 6.8 7.0

JC Consulting Ltd		Page 5						
4 McMillan Close								
Gateshead		L.						
Tyne & Wear NE9 5BF		Micro						
Date 04/08/2023 15:58	Designed by rjones							
File PROPOSED SW.MDX	Checked by	Dialitacje						
XP Solutions	Network 2017.1.1							
Storage Structures for Storm								
Porous Car Park Manhole: PP1.2, DS/PN: 1.004								
Infiltration Coefficient Base	(m/hr) 0.00000 Width (m)	5.0						
Membrane Percolation (5.0						
Max Percolation		80.0						
	Factor2.0 Depression Storage (mm)orosity0.30Evaporation (mm/day)	5 3						
	rel (m) 14.059 Cap Volume Depth (m) 0	-						
<u>Porous Car Park</u>	Porous Car Park Manhole: PP2.2, DS/PN: 2.003							
Infiltration Coefficient Base Membrane Percolation (5.0 5.0						
Max Percolation		40.0						
	Factor 2.0 Depression Storage (mm)	5						
	prosity 0.30 Evaporation (mm/day)	3						
Invert Lev	rel (m) 14.018 Cap Volume Depth (m) 0	. 700						
<u>Filter Drain</u>	Manhole: FD, DS/PN: 3.000							
Infiltration Coefficient Base (m	n/hr) 0.00004 Pipe Diameter (m)	0.100						
	h/hr) 0.00004 Pipe Depth above Invert (m)							
Safety Fa	Actor2.0Number of Pipessity0.30Slope (1:X)							
	(m) 13.879 Cap Volume Depth (m)							
	(m) 0.5 Cap Infiltration Depth (m)							
Trench Length	(m) 26.0							
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McMillan C	lose							
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'yne & Wear	NE9 5BF							-m
ate 04/08/20		2		Designed by	riones		—— M	ICIO
ile PROPOSEI		5			I JOILED		D	rainaa
	J SW.MDX			Checked by	7 1 1			
P Solutions				Network 201	/.⊥.⊥			
year Retur	<u>n Period</u>	Summar	ry of Ci	<u>ritical Resu</u> <u>Storm</u>	lts by Ma	<u>ximum Le</u>	vel (Ran	<u>k 1) fo</u>
Foul S Number of Inpu	Hot Hot Sta Headloss (ewage per at Hydrogra	Start (art Level Coeff (G hectare aphs 0	Factor 1 (mins) (mm) lobal) 0 (l/s) 0 Number	0 .500 Flow per .000	nal Flow - D Factor * Inl Person per	10m³/ha St et Coeffic Day (1/per mber of Ti	corage 2. ccient 0. c/day) 0. me/Area D	000 800 000 iagrams
			Grantha	tia Daimfall D				
	Rai	.nfall Mo		<u>tic Rainfall D</u> FSR		R 0.298		
	1003			land and Wales				
		M5-60	(mm)	18.000	Cv (Winter	c) 0.840		
M	largin for			ing (mm) Fimestep 2.5 S	anand There	mont (Det	300.0	
		AI	-	S Status		ement (Exte	ON	
) Status			ON	
				a Status			ON	
		Durahi	Profile	. ,		and Winter		
	Dotum		n(s) (mı (s) (yea	ns) 15, 30, 60		, 240, 360 1, 30, 100		
	Recur		Change			0, 0, 45		
		CIIMACC	change	(0)		0, 0, 15		
								Wator
US/MH		Return	Climate	First (X)	First (Y)	First (Z)	Overflow	Water Level
PN Name	Storm		Change	Surcharge	Flood	Overflow	Act.	(m)
								. ,
		1	. 0 %					
	15 Winter		+0%					14.276
1.001 2	15 Winter	1	+0%					14.199
1.001 2 1.002 3	15 Winter 15 Winter	1	+0% +0%	100/30 Winter				14.199 14.156
1.001 2 1.002 3 1.003 PP1.1	15 Winter 15 Winter 15 Winter	1 1 1	+0% +0% +0%					14.199 14.156 14.144
1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2	15 Winter 15 Winter 15 Winter 15 Winter	1 1 1 1	+0% +0% +0% +0%	100/30 Winter 100/15 Winter				14.199 14.156 14.144 14.077
1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5	15 Winter 15 Winter 15 Winter 15 Winter 15 Winter	1 1 1 1	+0% +0% +0% +0%					14.199 14.156 14.144 14.077 14.257
1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5 2.001 6	15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter	1 1 1 1 1	+0% +0% +0% +0% +0% +0%					14.199 14.156 14.144 14.077 14.257 14.203
1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5 2.001 6 2.002 PP2.1	15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter	1 1 1 1 1 1	+0% +0% +0% +0% +0% +0% +0%	100/15 Winter				14.199 14.156 14.144 14.077 14.257 14.203 14.155
1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5 2.001 6 2.002 PP2.1 2.003 PP2.2	15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter		+0% +0% +0% +0% +0% +0% +0%					14.199 14.156 14.144 14.077 14.257 14.203
1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5 2.001 6 2.002 PP2.1 2.003 PP2.2 3.000 FD	15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter		+0% +0% +0% +0% +0% +0% +0% +0%	100/15 Winter 100/15 Summer 30/15 Summer				14.19914.15614.14414.07714.25714.20314.15514.042
1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5 2.001 6 2.002 PP2.1 2.003 PP2.2 3.000 FD 2.004 8	15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter		+0% +0% +0% +0% +0% +0% +0% +0% +0%	100/15 Winter 100/15 Summer 30/15 Summer 30/15 Summer				$14.199 \\ 14.156 \\ 14.144 \\ 14.077 \\ 14.257 \\ 14.203 \\ 14.155 \\ 14.042 \\ 13.911 \\$
1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5 2.001 6 2.002 PP2.1 2.003 PP2.2 3.000 FD 2.004 8 1.005 5	15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter		+0% +0% +0% +0% +0% +0% +0% +0% +0% +0%	100/15 Winter 100/15 Summer 30/15 Summer 30/15 Summer 30/15 Summer				$14.199\\14.156\\14.144\\14.077\\14.257\\14.203\\14.155\\14.042\\13.911\\13.881$
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1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5 2.001 6 2.002 PP2.1 2.003 PP2.2 3.000 FD 2.004 8 1.005 5	15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter		+0% +0% +0% +0% +0% +0% +0% +0% +0% +0%	100/15 Winter 100/15 Summer 30/15 Summer 30/15 Summer 30/15 Summer				$14.199 \\ 14.156 \\ 14.144 \\ 14.077 \\ 14.257 \\ 14.203 \\ 14.155 \\ 14.042 \\ 13.911 \\ 13.881 \\ 13.831 \\ 1$

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<u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for</u> <u>Storm</u>

PN	US/MH Name	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (1/s)	Pipe Flow (l/s)	Status	Level Exceeded
1.000	1	-0.134	0.000	0.02		0.3	OK	
1.001	2	-0.130	0.000	0.04		0.5	OK	
1.002	3	-0.121	0.000	0.08		0.9	OK	
1.003	PP1.1	-0.127	0.000	0.06		0.9	OK*	
1.004	PP1.2	-0.132	0.000	0.03		0.9	OK*	
2.000	5	-0.133	0.000	0.03		0.4	OK	
2.001	6	-0.127	0.000	0.06		0.7	OK	
2.002	PP2.1	-0.133	0.000	0.03		0.7	OK*	
2.003	PP2.2	-0.126	0.000	0.06		0.7	OK*	
3.000	FD	-0.118	0.000	0.10		1.1	OK	
2.004	8	-0.117	0.000	0.11		1.7	OK	
1.005	5	-0.059	0.000	0.17		2.3	OK	
1.006	6	-0.016	0.000	0.17		2.2	OK	

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PN Name Storm Period Change Surcharge Flood Overflow Act. (m) 1.000 1 15 Winter 30 +0% 14.284 1.001 2 15 Winter 30 +0% 14.213 1.002 3 15 Winter 30 +0% 140/30 1.003 PP1.1 15 Winter 30 +0% 14.162 1.004 PP1.2 30 Winter 30 +0% 140/15 2.000 5 15 Winter 30 +0% 14.265 2.001 6 15 Winter 30 +0% 14.215 2.002 PP2.1 15 Winter 30 +0% 14.215	C Consulti	ng L	ıtd							Pa	ge 8
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		Surcharged	Floodod			Pipe		
	US/MH	Depth		Flow /	Overflow			Level
PN	Name	(m)	(m ³)	Cap.	(1/s)	(1/s)	Status	Exceeded
		((=/=/	(=/=/		
1.000	1	-0.126	0.000	0.06		0.8	OK	
1.001	2	-0.117	0.000	0.11		1.4	OK	
1.002	3 PP1.1	-0.100 -0.109	0.000 0.000	0.24 0.16		2.6 2.5	OK OK*	
	PP1.1 PP1.2	-0.109	0.000	0.10		2.5	OK*	
2.000	5	-0.123	0.000	0.08		1.0	OK	
2.001	6	-0.111	0.000	0.15		1.8	OK	
2.002	PP2.1	-0.121	0.000	0.08		1.8	OK*	
2.003	PP2.2	-0.033	0.000	0.18		1.9	OK*	
3.000	FD	0.111	0.000	0.13		1.4	SURCHARGED	
2.004	8	0.209	0.000	0.20			SURCHARGED	
1.005	5	0.414	0.000	0.23			SURCHARGED	
1.006	б	0.529	0.000	0.19		2.5	SURCHARGED	
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PN Name	Storm	Climate Return Period	Change Climate Change	First (X) Surcharge		First (Z)		Level (m)
PN Name	Storm 60 Winter	Climate Return Period 100	Change Climate Change +45%	First (X) Surcharge		First (Z)		Level (m)
PN Name 1.000 1 1.001 2	Storm 60 Winter 60 Winter	Climate Return Period 100 100	Climate Change +45% +45%	First (X) Surcharge	Flood	First (Z)		Level (m) 14.298 14.297
PN Name 1.000 1 1.001 2 1.002 3	Storm 60 Winter 60 Winter 60 Winter	Climate Return Period 100 100 100	Climate Change +45% +45% +45%	First (X) Surcharge	Flood	First (Z)		Level (m) 14.298 14.297 14.303
PN Name 1.000 1 1.001 2 1.002 3 1.003 PP1.1	Storm 60 Winter 60 Winter 60 Winter 60 Winter	Climate Return Period 100 100 100	Climate Change +45% +45% +45% +45%	First (X) Surcharge 100/30 Winter	Flood	First (Z)		Level (m) 14.298 14.297 14.303 14.271
PN Name 1.000 1 1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2	Storm 60 Winter 60 Winter 60 Winter 60 Winter	Climate Return Period 100 100 100	Climate Change +45% +45% +45% +45%	First (X) Surcharge	Flood	First (Z)		Level (m) 14.298 14.297 14.303
PN Name 1.000 1 1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5	Storm 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter	Climate Return Period 100 100 100 100 100 100	Change Climate Change +45% +45% +45% +45% +45% +45%	First (X) Surcharge 100/30 Winter 100/15 Winter	Flood	First (Z)		Level (m) 14.298 14.297 14.303 14.271 14.304 14.309
PN Name 1.000 1 1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5	Storm 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter	Climate Return Period 100 100 100 100 100	Climate Change +45% +45% +45% +45% +45%	First (X) Surcharge 100/30 Winter 100/15 Winter	Flood	First (Z)		Level (m) 14.298 14.297 14.303 14.271 14.304
PN Name 1.000 1 1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5 2.001 6	Storm 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter	Climate Return Period 100 100 100 100 100 100 100 10	Change Climate Change +45% +45% +45% +45% +45% +45% +45%	First (X) Surcharge 100/30 Winter 100/15 Winter	Flood	First (Z)		Level (m) 14.298 14.297 14.303 14.271 14.304 14.309 14.307
PN Name 1.000 1 1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5 2.001 6 2.002 PP2.1 2.003 PP2.2	Storm 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter	Climate Return Period 100 100 100 100 100 100 100	Change Climate Change +45% +45% +45% +45% +45% +45% +45%	First (X) Surcharge 100/30 Winter 100/15 Winter	Flood	First (Z)		Level (m) 14.298 14.297 14.303 14.271 14.304 14.309 14.307 14.288
PN Name 1.000 1 1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5 2.001 6 2.002 PP2.1 2.003 PP2.2 3.000 FD	Storm 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter	Climate Return Period 100 100 100 100 100 100 100 100 100	Climate Change +45% +45% +45% +45% +45% +45% +45% +45%	First (X) Surcharge 100/30 Winter 100/15 Winter 100/15 Summer 30/15 Summer	Flood	First (Z)		Level (m) 14.298 14.297 14.303 14.271 14.304 14.309 14.307 14.288 14.303
PN Name 1.000 1 1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5 2.001 6 2.002 PP2.1 2.003 PP2.2 3.000 FD 2.004 8	Storm 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter 60 Winter	Climate Return Period 100 100 100 100 100 100 100 100 100 10	Climate Change +45% +45% +45% +45% +45% +45% +45% +45%	First (X) Surcharge	Flood	First (Z)		Level (m) 14.298 14.297 14.303 14.271 14.304 14.309 14.307 14.288 14.303 14.309
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PN Name 1.000 1 1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5 2.001 6 2.002 PP2.1 2.003 PP2.2 3.000 FD 2.004 8 1.005 5	Storm 60 Winter 60 Winter	Climate Return Period 100 100 100 100 100 100 100 100 100 10	Climate Change +45% +45% +45% +45% +45% +45% +45% +45%	First (X) Surcharge	Flood	First (Z)		Level (m) 14.298 14.297 14.303 14.271 14.304 14.309 14.307 14.288 14.303 14.309 14.381 14.587
PN Name 1.000 1 1.001 2 1.002 3 1.003 PP1.1 1.004 PP1.2 2.000 5 2.001 6 2.002 PP2.1 2.003 PP2.2 3.000 FD 2.004 8 1.005 5	Storm 60 Winter 60 Winter	Climate Return Period 100 100 100 100 100 100 100 100 100 10	Climate Change +45% +45% +45% +45% +45% +45% +45% +45%	First (X) Surcharge	Flood	First (Z)		Level (m) 14.298 14.297 14.303 14.271 14.304 14.309 14.307 14.288 14.303 14.309 14.381 14.587

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100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm

PN	US/MH Name	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (l/s)	Pipe Flow (1/s)	Status	Level Exceeded
1.000	1	-0.112	0.000	0.06		0.8	OK	
1.001	2	-0.033	0.000	0.12		1.5	OK	
1.002	3	0.025	0.000	0.25		2.7	SURCHARGED	
1.003	PP1.1	0.000	0.000	0.17		2.6	SURCHARGED*	
1.004	PP1.2	0.095	0.000	0.08		2.2	SURCHARGED*	
2.000	5	-0.081	0.000	0.08		1.1	OK	
2.001	б	-0.023	0.000	0.16		2.0	OK	
2.002	PP2.1	0.000	0.000	0.08		1.8	SURCHARGED*	
2.003	PP2.2	0.135	0.000	0.15		1.6	SURCHARGED*	
3.000	FD	0.280	0.000	0.17		1.9	SURCHARGED	
2.004	8	0.383	0.000	0.14		2.2	SURCHARGED	
1.005	5	0.697	0.000	0.23		3.1	FLOOD RISK	
1.006	б	0.915	0.000	0.19		2.5	FLOOD RISK	

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APPENDIX F DRAINAGE MAINTENANCE SCHEDULE

19



Project:	Former Women's Institute, Newton-By-The-Sea	Client:	Jonathan Sutherland
Subject:	SuDS Maintenance Plan & Inspection Check List	Date:	04/08/2023

INTRODUCTION

A 2 No. dwelling development in Newton-by-the-sea has been designed to incorporate a Sustainable Drainage System (SuDS) to collect, manage and dispose of rainfall on the development in an environmentally friendly manner. SuDS aim to:

Control the flow, volume and frequency of water leaving the development. Prevent pollution by intercepting silt and cleaning runoff from hard surfaces. Provide attractive surroundings for the community. Create opportunities for wildlife.

The SuDS strategy for the development has been designed to incorporate the following features:

Flows from rooftop will be collected by traditional rainwater pipes and discharged into the pipe network via gravity. The piped network will then discharge into the permeable paving sub-base through a permavoid diffuser unit.

Flows from property parking area will be drained through permeable paving and discharged into the pipe network via gravity.

Flows from the access track will be drained to a filter trench. The filter trench is shown as suitable for partial infiltration with any exceedance of flows discharging into the pipe network via an overflow pipe.

Surface water flows will be discharged to the existing NWL surface water culverted watercourse network via gravity at an existing chamber.

Peak flows in excess of the restricted discharge rate of 2.5 I/s during storms up to 1 in 100 years, plus 45% for climate change and 10% urban creep will be attenuated on-site to ensure there is no flooding of the proposed site or flooding off site.

The SuDS features have been designed to be easily maintained in accordance with the approved drainage strategy, including:

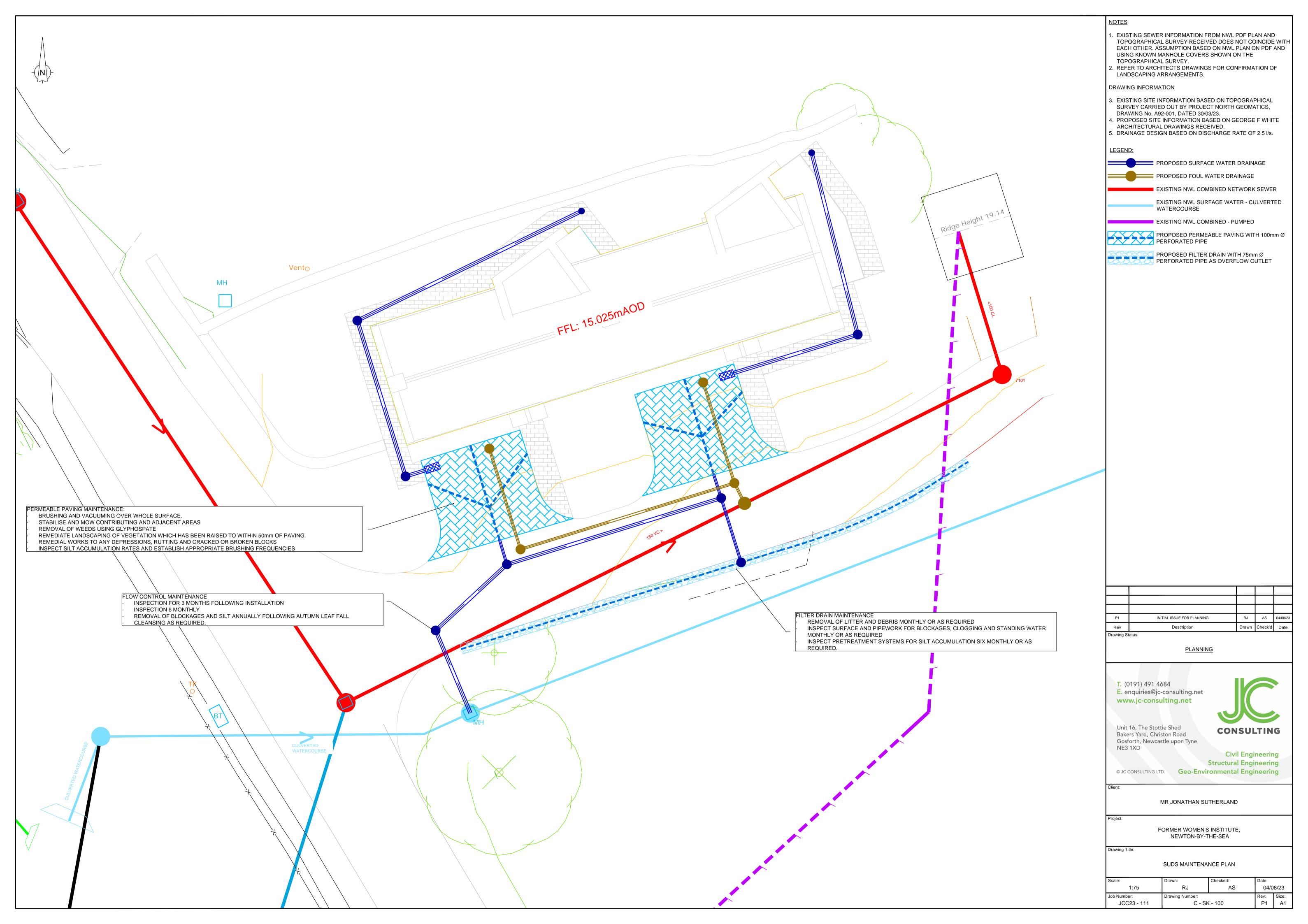
Regular day to day maintenance, such as removal of debris. Occasional maintenance, such as the removal of sediment. Remedial actions, such as reinstating areas of erosion.

Appendix A includes a SuDS Maintenance Plan identifying SuDS features. Appendix B includes a SuDS Inspection Checklist Appendix C includes the Maintenance Schedule.

It is the responsibility of Jonathan Sutherland, and will transfer to the landowner in the event of any future sale, and operator of the site to carry out the inspection and maintenance of all SuDS features.



APPENDIX A SUDS MAINTENANCE PLAN





APPENDIX B

SuDS INSPECTION CHECKLIST

General Information			
Site ID	Former Women's Institute, Newton-By-The-Sea, Alnwick		
Site Location	NU 23700 251196		
Items To Be Inspected	Traditional Sewerage Components Outfall Flow Control Permeable Paving Filter Drain		
Inspection Frequency	Annually		
SuDS Maintenance Plan	JCC23-111-100 SuDS Maintenance Plan		

SuDS Maintenance Inspection Checklist				
	Details	Y/N	Action Required	Date Completed
Sewerage Items				
Inspect and identify any areas that are not operating correctly including checking for blockages, if required, take remedial action.				
Remove debris from the catchment surface (where it may cause risk to performance).				
Remove sediment from access chambers.				
Inspect all inlets, outlets, flow control, headwall, overflows and vents to ensure they are operating as designed.				
Survey inside of pipework for sediment build up.				

SuDS Maintenance Inspection Checklist				
	Details	Y/N	Action Required	Date Completed
Permeable Paving				
Brushing and Vacuuming (standard cosmetic sweep over whole surface)				
Stabilise and mow contributing and adjacent areas				
Removal of weeds or management using glyphospate applied directly into the weeds by an applicator rather than spraying				



Remediate and landscaping which, through		
vegetation maintenance or soil slip, which has been		
raised to within 50mm of the level of the paving		
Remedial work to any depressions, rutting and		
cracked or broken blocks considered detrimental to		
the structural performance or a hazard to users, and		
replacing lost jointing material.		
Rehabilitation of surface and upper substructure by		
remedial sweeping		
Initial inspection		
Inspect for evidence of poor operation and/or weed		
growth – if required, take remedial action		
Inspect silt accumulation rates and establish		
appropriate brushing frequencies		
Monitor inspection chamber		

SuDS Maintenance Inspection Checklist				
	Details	Y/N	Action Required	Date Completed
Filter Drain				
Remove litter (including leaf litter) and debris.				
Cut the grass – to retain grass height within specified design range.				
Manage other vegetation and remove nuisance plants.				
Inspect inlets, outlets and overflows for blockages and clear as required.				
Inspect vegetation coverage				
Inspect inlets and facility surface for silt accumulation rates and establish appropriate removal frequencies.				
Reseed areas of poor vegetation growth, alter plant types to better suit conditions if required.				
Repair erosion or other damage by returfing or reseeding.				
Relevel uneven surfaces and reinstate design levels.				
Scarify and spike topsoil layer to improve infiltration performance, break up silt deposits and prevent compaction of the soil surface.				
Remove build up of sediment on upstream gravel trench, flow spreader or at the top of drain.				
Remove and dispose of oils or petrol residues using safe standard practices				



APPENDIX C

MAINTANCE SCHEDULE

DRAINAGE MAINTENANCE SCHEDULE

Maintenance of all drainage features not adopted by the local water authority will be the responsibility of the Jonathan Sutherland and will transfer to the landowner in the event of any future sale of the site. The works will need to be carried out by a competent contractor.

SEWERAGE MAINTENANCE SCHEDULE

This sewerage maintenance schedule covers collection gullies, pipework, chambers and flow control devices.

Maintenance Schedule	REQUIRED ACTION	Typical Frequency
Regular Maintenance	Removal of blockages to surface collection features and removal of silt from catch pits. Brushing and Vacuuming (standard cosmetic sweep over whole surface)	Once a year, after autumn leaf fall, or reduced frequent as required, based on site-specific observations of clogging or manufacturer's recommendations – paying particular attention to areas where water runs onto permeable surfacing from adjacent impermeable areas as this is the most likely to collect the most sediment
Occasional Maintenance	Stabilise and mow contributing and adjacent areas	As Required
	Removal of weeds or management using glyphospate applied directly into the weeds by an applicator rather than spraying	As Required – once per year on less frequently used pavements
Remedial Actions	Remediate and landscaping which, through vegetation maintenance or soil slip, which has been raised to within 50mm of the level of the paving	As Required
	Remedial work to any depressions, rutting and cracked or broken blocks considered detrimental to the structural performance or a hazard to users, and replacing lost jointing material.	As Required



	Rehabilitation of surface and upper substructure by remedial sweeping	Every 10 to 15 years or as required (if infiltration performance is reduced due to significant clogging)
Monitoring	Initial inspection	Monthly for 3 months after installation
	Inspect for evidence of poor operation and/or weed growth – if required, take remedial action	Three monthly, 48 hours after large storms in first 6 months
	Inspect silt accumulation rates and establish appropriate brushing frequencies	Annually
	Monitor inspection chamber	Annually

PERMEABLE PAVING MAINTENANCE SCHEDULE

MAINTENANCE SCHEDULE	REQUIRED ACTION	Typical Frequency
Regular Maintenance	Brushing and Vacuuming (standard cosmetic sweep over whole surface)	Once a year, after autumn leaf fall, or reduced frequent as required, based on site-specific observations of clogging or manufacturer's recommendations – paying particular attention to areas where water runs onto permeable surfacing from adjacent impermeable areas as this is the most likely to collect the most sediment
	Stabilise and mow contributing and adjacent areas	As Required
Occasional Maintenance	Removal of weeds or management using glyphospate applied directly into the weeds by an applicator rather than spraying	As Required – once per year on less frequently used pavements
Remedial Actions	Remediate and landscaping which, through vegetation maintenance or soil slip, which has been raised to within 50mm of the level of the paving	As Required



	Remedial work to any depressions, rutting and cracked or broken blocks considered detrimental to the structural performance or a hazard to users, and replacing lost jointing material.	As Required
	Rehabilitation of surface and upper substructure by remedial sweeping	Every 10 to 15 years or as required (if infiltration performance is reduced due to significant clogging)
	Initial inspection	Monthly for 3 months after installation
Monitoring	Inspect for evidence of poor operation and/or weed growth – if required, take remedial action	Three monthly, 48 hours after large storms in first 6 months
	Inspect silt accumulation rates and establish appropriate brushing frequencies	Annually
	Monitor inspection chamber	Annually

FILTER DRAIN SCHEDULE

MAINTENANCE SCHEDULE	REQUIRED ACTION	Typical Frequency
	Remove litter (including leaf litter) and debris from filter drain surface and access chambers.	Monthly (or as required)
Regular Maintenance	Inspect filter drain surface, inlet/ outlet pipework and control systems for blockages, clogging, standing water and structural damage.	Monthly
	Inspect pre-treatment systems, inlets and perforated pipework for silt accumulation and establish appropriate silt removal frequencies.	Six Monthly
	Remove sediment from pre- treatment devices.	Six Monthly
Occasional Maintenance	Remove or control tree roots where they are encroaching the sides of the filter drain, using recommended methods.	As required



At locations with high pollution loads, remove surface geotextile and replace, and wash or replace overlying filter medium.	Five yearly, or as required
Clear perforated pipework of blockages	As required

As required by CDM 2015 designs have been produced to ensure that all maintenance risks have been identified, eliminated, reduced and/ or controlled where appropriate.

Any manufacturer specific maintenance requirements are to be included as part of the site health and safety file.