

	A	B	C	D	E
1	<b>TITLE: Dead Load, Live Load &amp; Wind Load Calculation of FORCE on existing rear wall and front 4 no. columns AND Suitability of Steel</b>				
2	<b>(within decorative columns) to support TOTAL Roof Forces. RE: Proposed Porch at Melville Hall PO36 9DH</b>				
3					
4	A	Preliminary Calculations		value	
5	1	Angle of Roof Truss			
6		$\tan^{-1}(\text{Rise}/(L/2))$			
7		$\tan^{-1}(1/(6/2))m$			
8		$\tan^{-1} 0.333 =$		18.42	
9					
10	2	Length of Principal Rafter [PR]			
11		$\text{hyp} = 1 / \text{Sin. } 18.42 =$		3.17 m	
12					
13	3	Half Plan Area			
14		$L/2 \times \text{spacing of Roof Truss [RT]}$			
15		$(6/2) \times 0.9125 =$		2.74 m <sup>2</sup>	
16		multiply by 4 (RT 1-3 full plan (area supported by existing rear wall))		10.96 m <sup>2</sup>	
17		multiply by 4 (RT 3-6 full plan (area supported by 4 no. columns (front))		10.96 m <sup>2</sup>	
18					
19	4	Half Slope Area			
20		$L \text{ of PR } \times \text{ spacing of Roof Truss [RT]}$			
21		$3.17 \times 0.9125 =$		2.88 m <sup>2</sup>	
22		multiply by 4 (RT 1-3 full plan (area supported by existing rear wall))		11.52 m <sup>2</sup>	
23		multiply by 4 (RT 3-6 full plan (area supported by 4 no. columns (front))		11.52 m <sup>2</sup>	
24					
25					
26	B	Load			
27	1	Weight of Roofing Material			
28	a	Artificial slate (to match existing)		0.25 kN/m <sup>2</sup>	
29		Artificial slate x Half Slope Area: $0.25 \times 2.88 =$		0.72 kN/m <sup>2</sup>	
30		multiply by 4 (RT 1-3 full plan (weight supported by existing rear wall))		2.88 kN/m <sup>2</sup>	
31		multiply by 4 (RT 3-6 full plan (weight supported by 4 no. columns (front))		2.88 kN/m <sup>2</sup>	
32	b	external grade 1/2" composite board 0.1 kN/m <sup>2</sup> , Purlins/Battens + Felt 0.05 kN/m <sup>2</sup>		0.15 kN/m <sup>2</sup>	

	A	B	C	D	E
33		Board + battens + felt + purlins x Half Slope Area: $0.15 \times 2.88 =$		0.43 kN/m <sup>2</sup>	
34		multiply by 4 (RT 1-3 full plan (weight supported by existing rear wall))		1.7 kN/m <sup>2</sup>	
35		multiply by 4 (RT 3-6 full plan (weight supported by 4 no. columns (front)))		1.7 kN/m <sup>2</sup>	
36	c	Plastic interlock ceiling		0.01 kN/m <sup>2</sup>	
37		Ceiling x Half Plan area: $0.01 \times 2.74$		0.027 kN/m <sup>2</sup>	
38		multiply by 4 (RT 1-3 full plan (weight supported by existing rear wall))		0.11 kN/m <sup>2</sup>	
39		multiply by 4 (RT 3-6 full plan (weight supported by 4 no. columns (front)))		0.11 kN/m <sup>2</sup>	
40	d	Joists 0.1 kN/m <sup>2</sup>		0.1 kN/m <sup>2</sup>	
41					
42		TOTAL DEAD LOAD evenly spread on existing rear wall		4.82 kN/m <sup>2</sup>	
43		TOTAL DEAD LOAD evenly spread across 4 no. columns (front)		4.82 kN/m <sup>2</sup>	
44		<b>TOTAL DEAD LOAD on each column (front)</b>		<b>1.2 kN/m<sup>2</sup></b>	<b>[1]</b>
45					
46	2	Weight of five no. Roof Truss [RT]			
47		qty ( span/3 +5)			
48		$5(6/3 + 5) = 35 \text{ N/m}^2$		0.035 kN/m <sup>2</sup>	
49		TOTAL LIVE LOAD evenly spread on existing rear wall		0.02 kN/m <sup>2</sup>	
50		TOTAL LIVE LOAD evenly spread across 4 no. columns (front)		0.02 kN/m <sup>2</sup>	
51		<b>TOTAL LIVE LOAD on each column (front)</b>		<b>0.004 kN/m<sup>2</sup></b>	<b>[2]</b>
52					
53	3	Weight of Wind force			
54		Assume weight of wind bracing 12 N/m <sup>2</sup> on half plan area			
55		$12 \times 2.74 = 32.88 \text{ N/m}^2$		0.03 kN/m <sup>2</sup>	
56		TOTAL WIND LOAD evenly spread on existing rear wall		0.015 kN/m <sup>2</sup>	
57		TOTAL WIND LOAD evenly spread across 4 no. columns (front)		0.015 kN/m <sup>2</sup>	
58		<b>TOTAL WIND LOAD on each column (front)</b>		<b>0.004 kN/m<sup>2</sup></b>	<b>[3]</b>
59					
60		<b>TOTAL LOAD on each column (front): [1]+[2]+[3]</b>		<b>1.208 kN/m<sup>2</sup></b>	
61					
62					
63	C	<b>Suitability of Vertical Roof Support (Inside decorative fiberglass column), with 1m depth foundation</b>			
64					

	A	B	C	D	E
65			Galvanised Steel Tube O/S dia 60mm, wall thickness 10mm with stress factor up to 250,000 kN/m <sup>2</sup>		
66	1		Compression: stress on each column steel insert = Force applied/CSA, = 1.208/0.002 =	604 kN/m <sup>2</sup>	
67			604 kN/m <sup>2</sup> load is well within the proposed steel pole compression capacity of 250,000 kN/m <sup>2</sup>		
68	2		Buckling: critical = $\pi^2 E I / L^2 = 7,882 \text{ kN/m}^2$ , which is safely above the total load 1.208 kN/m <sup>2</sup> imposed on column	7,882 kN/m <sup>2</sup>	
69			where E = elasticity of steel = $200 \times 10^6 \text{ kN/m}^2$		
70			where I = moment of inertia = $60^4 / 12 ( 40^4 / 12 ) = 8.67 \times 10^{-5}$		
71			where L = length of steel tube+foundation, $L^2 = 21.69$		