

| | | |
|---------------------------|---|---|
| 1. Project & Site Details | Project / Site Name (including sub-catchment / stage / phase where appropriate) | 295 Green Lanes |
| | Address & post code | 295 Green Lanes, London, N13 4XS. |
| | OS Grid ref. (Easting, Northing) | E 530981 |
| | | N 192636 |
| | LPA reference (if applicable) | 23/03349/FUL |
| | Brief description of proposed work | Refer to the DAS. However, in summary the proposed redevelopment on the site comprises the re-use, conversion and extension of the existing upper floors of the public house building to provide sleeping accommodation and the re-use of and construction within the existing rear yard area to provide a new build block containing accessible bedrooms together with associated landscaping. |
| | Total site Area | 900 m ² |
| | Total existing impervious area | 900 m ² |
| | Total proposed impervious area | 500 m ² |
| | Is the site in a surface water flood risk catchment (ref. local Surface Water Management Plan)? | No |
| | Existing drainage connection type and location | Re-use of the existing sewer connection. |
| | Designer Name | Tom Quigg |
| Designer Position | Director - Civil Engineer | |
| Designer Company | Flume Consulting Engineers | |

| | | | | | |
|----------------------|--|---------------------------------------|-------------------------------|---|-------------------------------|
| 3. Drainage Strategy | 3a. Discharge Rates & Required Storage | | | | |
| | | Greenfield (GF) runoff rate (l/s) | Existing discharge rate (l/s) | Required storage for GF rate (m ³) | Proposed discharge rate (l/s) |
| | Qbar | 0.40 | 9.83 | - | |
| | 1 in 1 | 0.34 | 8.26 | - | 4.26 |
| | 1 in 30 | 0.93 | 20.76 | - | 8.05 |
| | 1 in 100 | 1.27 | 26.52 | - | 12.27 |
| | 1 in 100 + CC | N/A | N/A | - | 16.38 |
| | Climate change allowance used | | 40% | | |
| | 3b. Principal Method of Flow Control | Green/Blue Roofs and Permeable Paving | | | |
| | 3c. Proposed SuDS Measures | | | | |
| | | Catchment area (m ²) | Plan area (m ²) | Storage vol. (m ³) allowance for void ratios included in calculations | |
| | Rainwater harvesting | 0 | 0 | 0 | |
| | Infiltration systems | 0 | 0 | 0 | |
| | Green roofs | 16 | 16 | 0.72 | |
| | Blue roofs | 222 | 222 | 33.3 | |
| | Filter strips | 0 | 0 | 0 | |
| | Filter drains | 0 | 0 | 0 | |
| | Bioretention / tree pits | 0 | 0 | 0 | |
| Pervious pavements | 400 | 400 | 42 | | |
| Swales | 0 | 0 | 0 | | |
| Basins/ponds | 0 | 0 | 0 | | |
| Attenuation tanks | 0 | | 0 | | |
| Total | 638 | 638 | 76.02 | | |

| | | | |
|---|---|---|----------------|
| 2. Proposed Discharge Arrangements | 2a. Infiltration Feasibility | | |
| | Superficial geology classification | Boys Hill Gravel Member | |
| | Bedrock geology classification | London Clay | |
| | Site infiltration rate | 0.000026 | m/s |
| | Depth to groundwater level | Not observed in GI m below ground level | |
| | Is infiltration feasible? | Yes | |
| | 2b. Drainage Hierarchy | | |
| | | Feasible (Y/N) | Proposed (Y/N) |
| | 1 store rainwater for later use | Y | Y |
| | 2 use infiltration techniques, such as porous surfaces in non-clay areas | Y | Y |
| | 3 attenuate rainwater in ponds or open water features for gradual release | N | N |
| | 4 attenuate rainwater by storing in tanks or sealed water features for gradual release | Y | N |
| 5 discharge rainwater direct to a watercourse | N | N | |
| 6 discharge rainwater to a surface water sewer/drain | N | N | |
| 7 discharge rainwater to the combined sewer. | Y | Y | |
| 2c. Proposed Discharge Details | | | |
| Proposed discharge location | Existing sewer connection | | |
| Has the owner/regulator of the discharge location been consulted? | Existing connection remains unchanged and overall flow rates will be reduced. However, a Section 106 application will be made following planning permission and prior to construction commencing. | | |

| | | |
|---------------------------------|---|---------------------------------|
| 4. Supporting Information | 4a. Discharge & Drainage Strategy | Page/section of drainage report |
| | Infiltration feasibility (2a) - geotechnical factual and interpretive reports, including infiltration results | Appendix B |
| | Drainage hierarchy (2b) | Page 8 |
| | Proposed discharge details (2c) - utility plans, correspondence / approval from owner/regulator of discharge location | Appendix A |
| | Discharge rates & storage (3a) - detailed hydrologic and hydraulic calculations | Appendix A |
| | Proposed SuDS measures & specifications (3b) | Appendix A |
| | 4b. Other Supporting Details | Page/section of drainage report |
| | Detailed Development Layout | Appendix A |
| | Detailed drainage design drawings, including exceedance flow routes | Appendix A |
| | Detailed landscaping plans | Appendix A |
| | Maintenance strategy | Page 17 |
| | Demonstration of how the proposed SuDS measures improve: | |
| a) water quality of the runoff? | Page 14 | |
| b) biodiversity? | Page 15 | |
| c) amenity? | Page 15 | |



295 Green Lanes

Flood Risk and SuDS Assessment

Job Number: 1256

| Date | Version | Notes/Amendments |
|----------------|---------|------------------------|
| September 2022 | 1 | Issued for Information |
| November 2023 | 2 | Updated scheme |
| | | |
| | | |

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| Acronyms | |
|--------------|--|
| CIRIA | Construction Industry Research and Information Association |
| EA | Environment Agency |
| NPPF | National Planning Policy Framework |
| PPG | Planning Practice Guidance |
| NSTS | Non-Statutory Technical Standards |

Introduction

Flume Consulting Engineers have been appointed to undertake a Flood Risk and Sustainable Drainage Systems (SuDS) Assessment for the proposed development at 295 Green Lanes, London, N13 4XS.

This report has been carried out in accordance with the National Planning Policy Framework (NPPF) and the Planning Practice Guidance 'Flood Risk and Coastal Change' (PPG). This report also incorporates advice and guidance from the Environment Agency (EA), the Strategic Flood Risk Assessment (SFRA) produced by the London Borough of Enfield, Enfield's SuDS Design and Evaluation Guide, DEFRA's Non-statutory technical standards (NSTS) for sustainable drainage systems and CIRIA documents.

The EA's indicative floodplain map (Figure 3) shows that the site is located in Flood Zone 1, however a SuDS Assessment has been carried out to assess the available options for SuDS use for the proposed development.

Site Description and Location

The application site comprises a part two, part three-storey building, which fronts onto Green Lanes. The ground floor is occupied by the Green public house. There is a covered passage on the northern side of the building which provides pedestrian and vehicle access to a substantial rear area, which is currently in use for informal parking by customers (approximately 5 spaces) and for open storage, with a constrained boundary between the adjacent properties which is set against the boundary line.

The New River and Pymmes Brook (upstream of the Salmon Brook confluence), flows within 0.50 kilometres from the development, although this does not impact the proposed development.

The site postcode is N13 4XS and the OS grid reference is TQ 30981 92636.

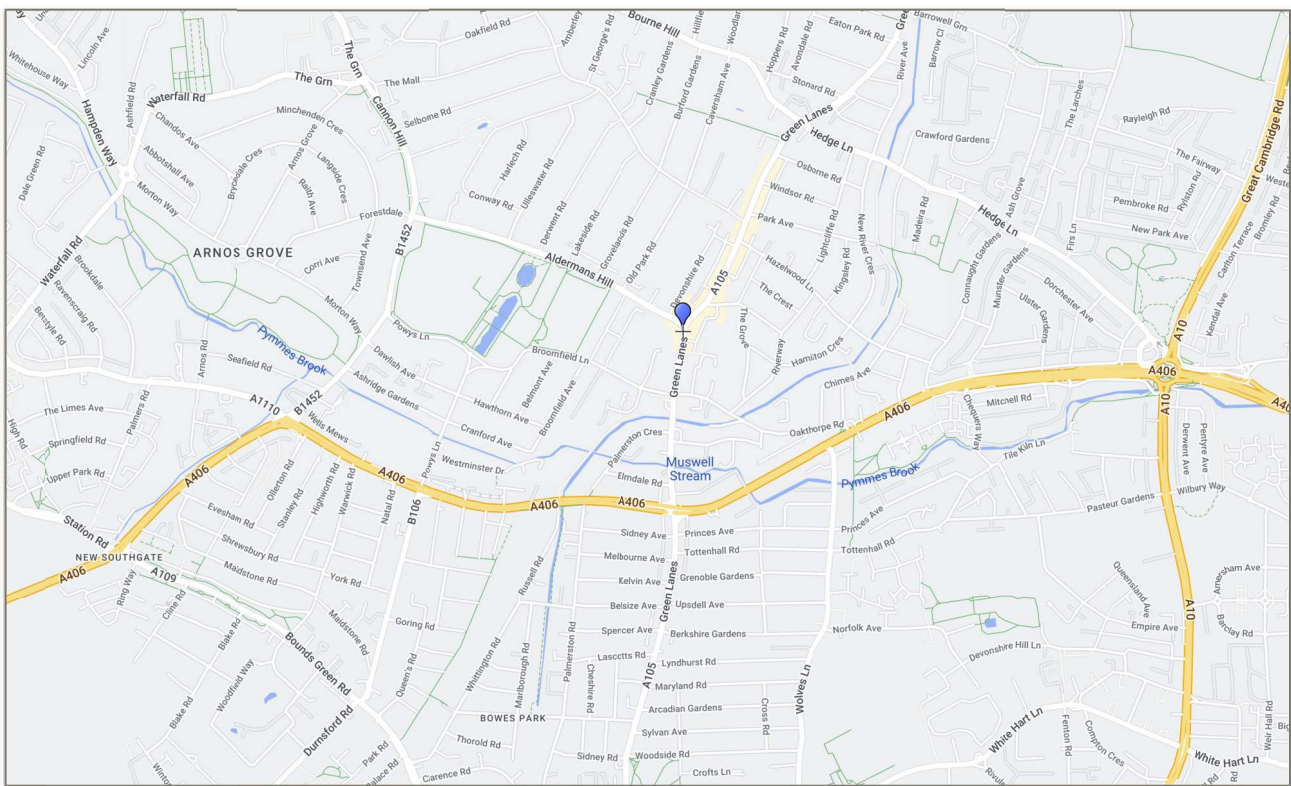


FIGURE 1. SITE LOCATION

Development Proposal

The ground floor of the development will retain current A4 use and operate as a public house with associated back of house spaces for the public house, as well as a reception for the guest house.

The proposed redevelopment on the site comprises the re-use, conversion and extension of the existing upper floors of the public house building to provide sleeping accommodation and the re-use of and construction within the existing rear yard area to provide a new build block containing accessible bedrooms together with associated landscaping - Figure 2.

The guest house accommodation will support the commercial A4 use and enable the property to continue to use floorspace for a public house. Although the floorspace will be reduced the marketing of the property has established that the existing footprint is too large to be sustained in the current commercial market.

The aim of the scheme is to ensure the continued retention of a public house as a social function in the community on the site by supporting it through the guest accommodation proposed.

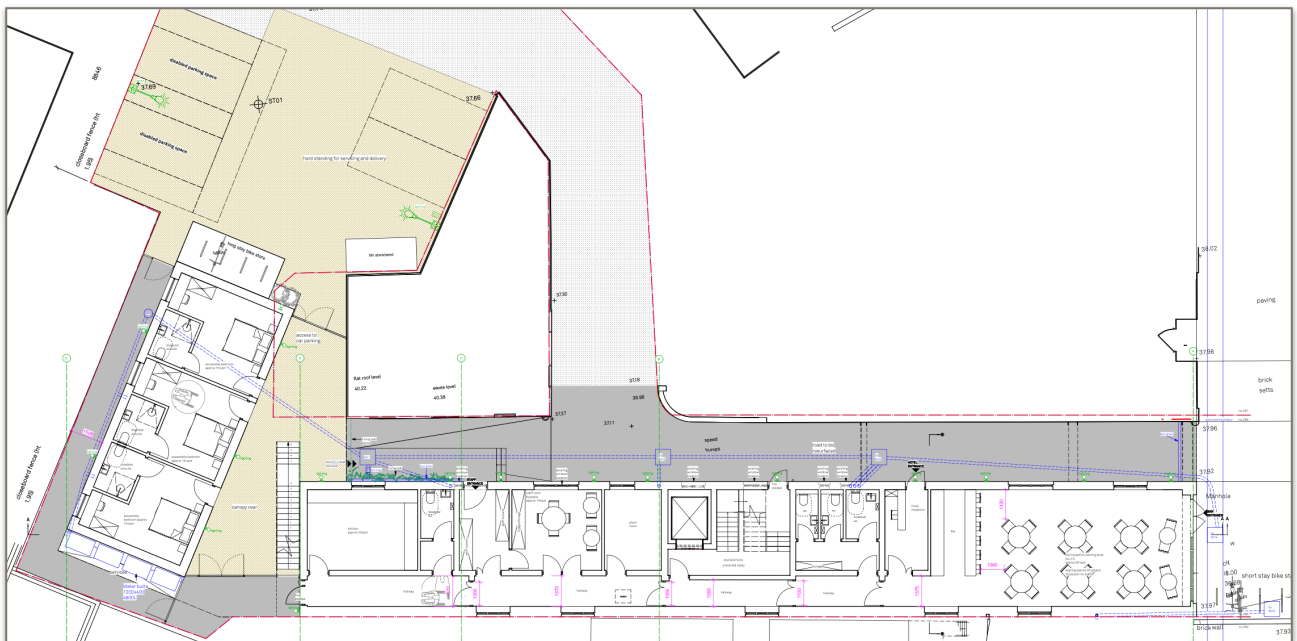


FIGURE 2. PROPOSED DEVELOPMENT

Flood Risk

The EA's indicative floodplain map shows that the site is located in Flood Zone 1 and is not at risk of flooding (Figure 3). Developments in this flood zone do not have any restrictions, provided they do not increase the risk of flooding elsewhere.

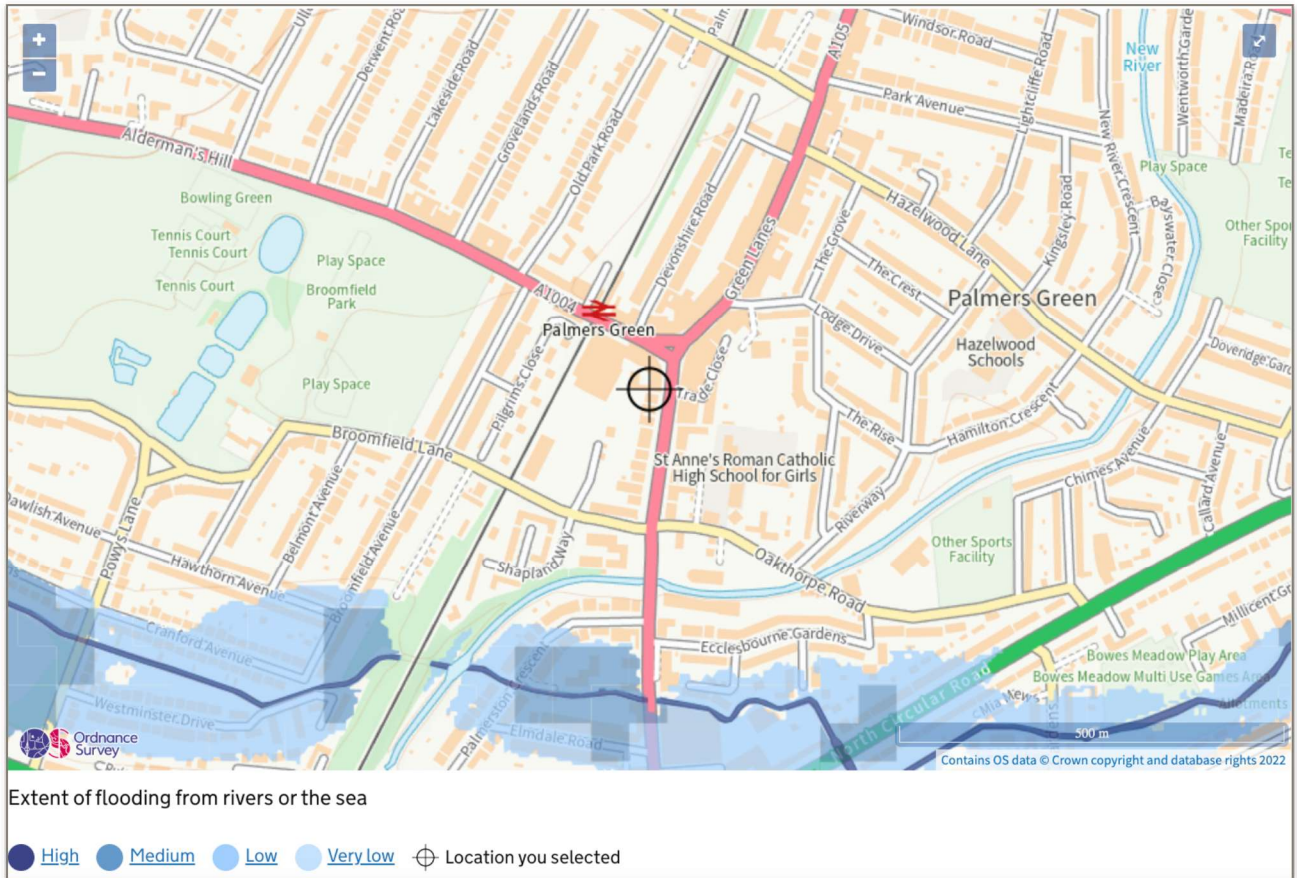


FIGURE 3. ENVIRONMENT AGENCY FLOOD RISK FROM RIVERS OR SEA MAP (GOV.UK, 2022)

Surface Water Run-off Assessment

Existing Run-off

The total site area which includes the existing building and associated external landscaping, is approximately 900m²/0.09ha, and all of which is impermeable hardstanding areas.

The existing peak run-off rate for the design storm event (1 in 1, 1 in 30 and 1 in 100 year) was calculated using the Modified Rational Method | Wallingford Procedure as shown below:

as shown below:

$$Q = 2.78 \times i \times A$$

Where 'A' is the catchment area in ha and 'i' is the rainfall intensity in mm/hr as estimated using the relevant maps presented in the Flood Studies Report.

$$Q_{1ex} = 2.78 \times 33 \times 0.09 = \underline{8.26 \text{ l/s}}$$

$$Q_{30ex} = 2.78 \times 83 \times 0.09 = \underline{20.76 \text{ l/s}}$$

$$Q_{100ex} = 2.78 \times 106 \times 0.09 = \underline{26.52 \text{ l/s}}$$

Proposed Run-off (Unmitigated without SuDS Measures)

According to Planning Practice Guidance (PPG), “generally the aim should be discharge surface runoff as high up the following hierarchy of drainage options as reasonably practicable: 1. Into the ground (infiltration) 2. To a surface water body; 3. To a surface water sewer, highway drain or another drainage system; 4. To a combined sewer”, whilst ensuring that surface water run-off is managed as close to its source as possible.

The proposed development does not introduce any additional hardstanding areas compared with the existing case, and will therefore not generate any additional surface water run-off. An allowance for a future increase in rainfall intensity is provided below:

$$Q_{100+40cc} = 2.78 \times 148 \times 0.09 = \underline{37.13 \text{ l/s}}$$

The following chapters aims to outline the possibility of incorporating SuDS features in the design. Figure 4 outlines the possibility of incorporating SuDS into the scheme to reduce the surface water run-off and volumes further.

SuDS Assessment

It is recommended that SuDS be introduced to mimic natural drainage pathways as close to source as possible, reducing the impact of urbanisation on watercourse flows, and ensures the protection and enhancement of water quality, while encouraging the recharge of groundwater.

To effectively manage surface water run-off, it is crucial to implement SuDS as close to its source as possible, as per the guidance provided. By adopting this approach, the proposed SuDS will work towards achieving the desired rates for reducing surface water run-off whenever feasible and practical. This initiative is in line with Sustainable Infrastructure Policy 13 (SI13) of the London Plan, which specifically emphasises the importance of sustainable drainage practices.

The NSTS states stormwater flows off site should achieve the greenfield runoff rate as best practicably possible, or are at least a 50% betterment of the existing flow rates for all periods.

CIRIA SuDS Manual (C753) states that a development should utilise SuDS unless there are practical reasons for not doing so, and should aim to achieve greenfield run-off rates and ensure that surface water run-off is managed as close to its source as possible in line with the following drainage hierarchy:

- I. Use infiltration techniques, such as porous surfaces in non-clay areas,
- II. attenuate rainwater in ponds or open water features for gradual release,
- III. attenuate rainwater by storing in tanks or sealed water features for gradual release,
- IV. discharge rainwater direct to a watercourse,
- V. discharge rainwater to a surface water sewer / drain,
- VI. discharge rainwater to the combined sewer.

The possibility of implementing SuDS at the site was assessed using a hierarchy of preferred surface water management methods, and in line with comments received from the LLFA. The following paragraphs discuss the various methods in order of that hierarchy and evaluate the site's suitability for each method.

The SuDS site suitability table (Figure 4) has been used to determine the suitability for each SuDS element for this development.

| SuDS Component | Site Suitability | Comments |
|------------------------------------|------------------|--|
| Green Blue Roofs & Rainwater Reuse | ✓ | Green Blue Roofs will be incorporated on the flat roofs at various levels on the upper levels of the building. The first floor terrace will also incorporate a series of Trees, shrubs and planting beds. These SuDS features will reduce both the surface water run-off for smaller storm events and reduce water demand. |
| Soakaways | ✗ | Not feasible in this instance due to the requirement for a minimum 5m easement from adjacent structures and 2.5m easement from boundaries which restricts their use. |
| Filter Strips | ✗ | Not feasible to use throughout the scheme in this instance due to the requirement for a minimum 5m easement from adjacent structures and 2.5m easement from boundaries which restricts their use. |
| Infiltration Trenches | ✗ | Not feasible to use throughout the scheme in this instance due to the requirement for a minimum 5m easement from adjacent structures and 2.5m easement from boundaries which restricts their use. |
| Swales | ✗ | Not suitable due to site layout and size of the development. |
| Bioretention | ✗ | Not suitable due to site layout and size of the development. |
| Porous Pavements | ✓ | Permeable Paving will be introduced to the proposed hard landscaped areas. |
| Geocellular Systems | ✗ | Permeable Paving is preferred to the introduction of a below ground drainage attenuation tank. |
| Infiltration basins | ✗ | Not suitable due to site layout and size of the development. |
| Detention basins | ✗ | Not suitable due to site layout and size of the development. |
| Ponds | ✗ | Not suitable due to site layout and size of the development. |
| Stormwater wetlands | ✗ | Not suitable due to site layout and size of the development. |

FIGURE 4. SUDS SITE SUITABILITY

Green Roofs

When feasible, priority should be placed on establishing blue-green infrastructure over hardscape or subterranean options because it offers broader advantages for biodiversity, recreational spaces, and local climate conditions.

The SuDS Manual C753 states “Green roofs can provide benefits in terms of reducing peak flow rates to the site drainage system – principally for small and medium-sized events.”

Green Roofs are proposed on the second and third floor flat roofs with smaller localised ‘intensive’ Green Planters used as part of the the first floor terrace, contributing to a reduction of proposed peak flow rates, reducing the overall run-off by **16m²** for small-medium storm events. An overflow will be provided, which will drain back into the existing surface water drainage system. Figure 5 provides a schematic of the Green Roof.

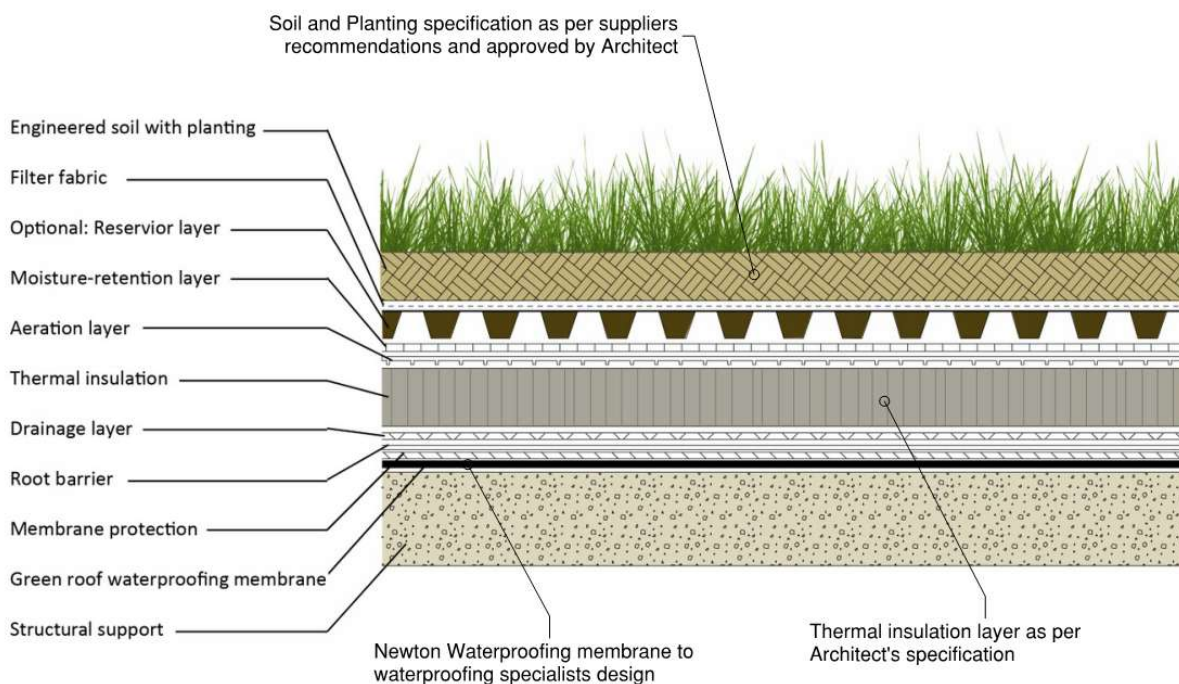


FIGURE 5. GREEN ROOF DETAIL

Blue Roofs

Blue roofs replicate natural hydrological processes in urban settings. A "blue roof" is a system intended to temporarily hold and manage stormwater, facilitating a controlled release into the drainage system, thereby mimicking the functions of natural water bodies. Designing a blue roof involves shaping the roof surface to capture and store stormwater by creating depressions, channels, or reservoirs for temporary containment.

The advantages of blue roofs include effective stormwater management through the retention and gradual release of water, which lessens the burden on traditional drainage systems during periods of heavy rain. Blue roofs also contribute to flood prevention by managing the rate of stormwater outflow, thereby reducing both the volume and rate of flow entering public sewer systems. Moreover, by storing stormwater on rooftops, these systems promote the natural breakdown of pollutants, improving water quality before it is discharged into the drainage network.

Blue roofs must be equipped with appropriate overflow mechanisms to avoid excessive water buildup, which could otherwise harm the building's structure. These mechanisms are designed to reroute surplus water into the conventional drainage system when necessary.

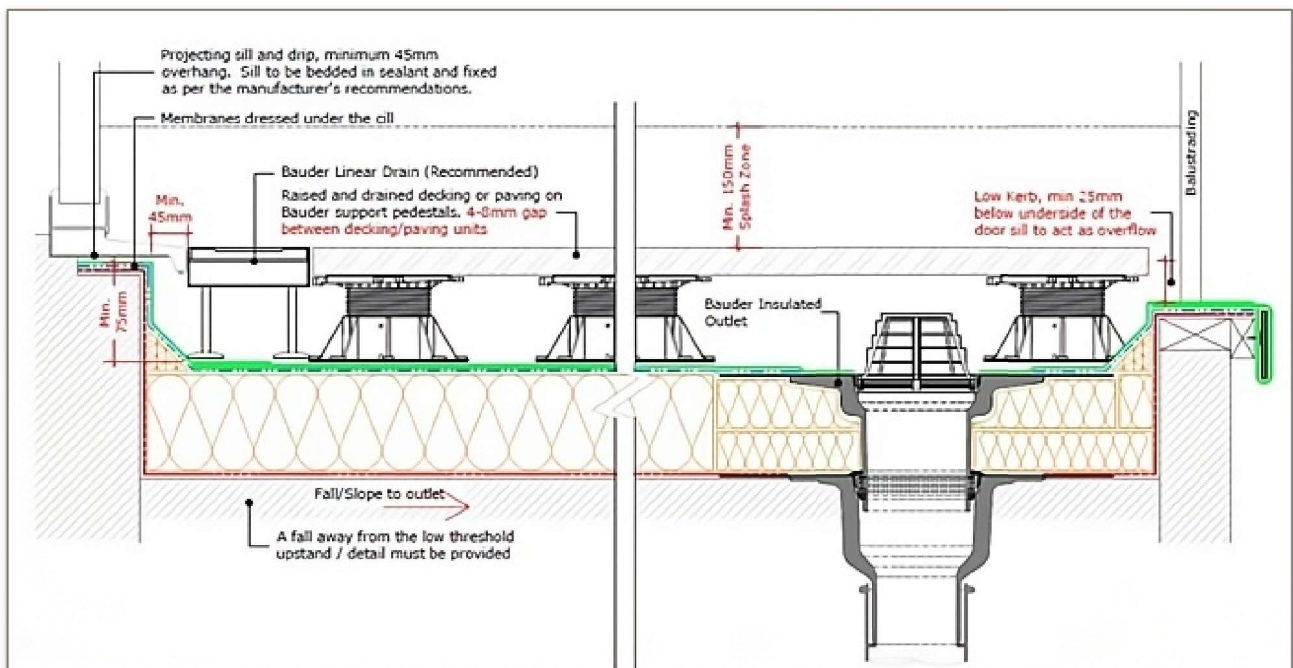


FIGURE 6. BLUE ROOF DETAIL

Threshold levels may incorporate a 150mm upstand height beneath an overhanging door sill (minimum 45mm) provided that the roof slopes away from the doorway and that suitable outlets and overflow pipes are installed. Alternatively, a balcony curb could be set to a minimum of 25mm below the door threshold.

It is proposed that the Blue Roof, when paired with a properly sized flow control device like an orifice plate, will cap the peak outflow from the roof at a manageable rate of 1 litres per second. Tools such as HR Wallingford's Run-off tool, and guidance from EA/DEFRA, suggest that for flow rates under 5.0 l/s, discharge consent is commonly granted at 5.0 l/s, taking into account potential blockages from vegetation and debris. Nevertheless, BS8582:2013 indicates that a further reduction to below 5 l/s may be negotiated with the future owner, and control measures of 25mm are feasible with appropriate safeguards.

The initial design of the Blue Roof and its corresponding outflow was conceived to handle a 1 in 100-year return period storm plus a 40% climate change, limiting surface water discharge to 1 l/s using a 18mm orifice plate. This very small flow control was thought to be acceptable, so long as an appropriate overflow is incorporated to ensure a fail-safe solution is provided, allowing the blue roof to act as a traditional roof in the event of a blockage.

Infiltration

The preferred means of surface water drainage for any new development is into a suitable soakaway or infiltration system. The EA/DEFRA's maps confirm that infiltration may be feasible in this instance due to the presence of the Boyn Hill Gravels. Infiltration through permeable paving is considered to be a practical solution to reduce surface water run-off rates and volumes. It is proposed to utilise permeable paving for the hardstanding area, infiltrating to ground and reducing the run-off by **400m²**. An overflow may also be incorporated to mitigate against overland flooding.

Infiltration through permeable paving is considered to be a practical solution to reduce surface water run-off rates and volumes. It is proposed to utilise permeable paving for the external hardstanding areas, infiltrating to ground and reducing the run-off by approximately **400m²**.

Centralised '3d' soakaways are not feasible due to the proximity to adjacent structures, and the necessary 1m easement from the groundwater table. The requirement for a minimum 5m easement from adjacent structures and 2.5m from any adjacent boundary restricts their use.

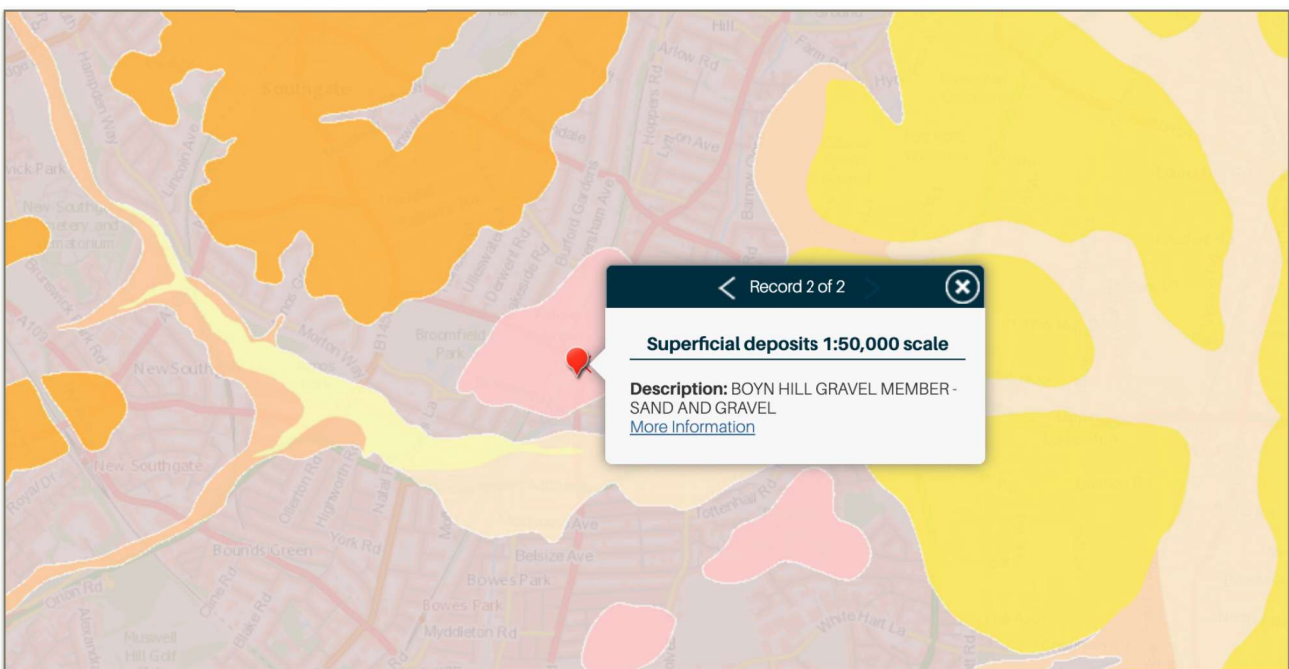


FIGURE 7. BGS GEOLOGICAL MAPS

Permeable Pavements

Ground Investigation (2.6×10^{-6} m/s) confirms that Infiltration is suitable to permit surface water run-off from the hardstanding areas to ground. Infiltration through permeable paving is considered to be a practical solution to reduce surface water run-off rates and volumes. An overflow will also be incorporated as a failsafe due to the inherent variability of the infiltration properties of the underlying ground, which will be connected to the surface water drainage. Infiltration through Permeable Pavements (2D plane only) can also be utilised closer to structures. Permeable Pavements serving themselves behave in a similar way to soft landscaping and can be placed directly against the edge of structures.

Capacity of the Permeable Pavement

The surface water run-off from the permeable paving will self-attenuate and infiltrate into the ground. A conservative infiltration rate of 1×10^{-7} m/s was used to define the paving thicknesses.

Infiltration rate = 1×10^{-7} m/s

| | | 1 in 10 | 1 in 30 | 1 in 100 | 1 in 100 + 20% | 1 in 100 + 30% |
|-------|-----|---------|---------|----------|----------------|----------------|
| M5-60 | r | 10 | 3.33 | 1 | 0.5 | 0.25 |
| 20 | 0.4 | 90 | 120 | 160 | 210 | 225 |
| | 0.3 | 100 | 140 | 190 | 240 | 270 |
| | 0.2 | 135 | 180 | 250 | 310 | 370 |
| 17 | 0.4 | 70 | 100 | 140 | 180 | 190 |
| | 0.3 | 80 | 110 | 160 | 210 | 225 |
| | 0.2 | 105 | 150 | 210 | 270 | 305 |
| 14 | 0.4 | | | | | |
| | 0.3 | 60 | 90 | 130 | 170 | 180 |
| | 0.2 | 75 | 110 | 160 | 220 | 245 |

FIGURE 8. MINIMUM PAVING THICKNESSES REQUIRED - HYDRAULIC CAPACITY (INTERPAVE, 2018)

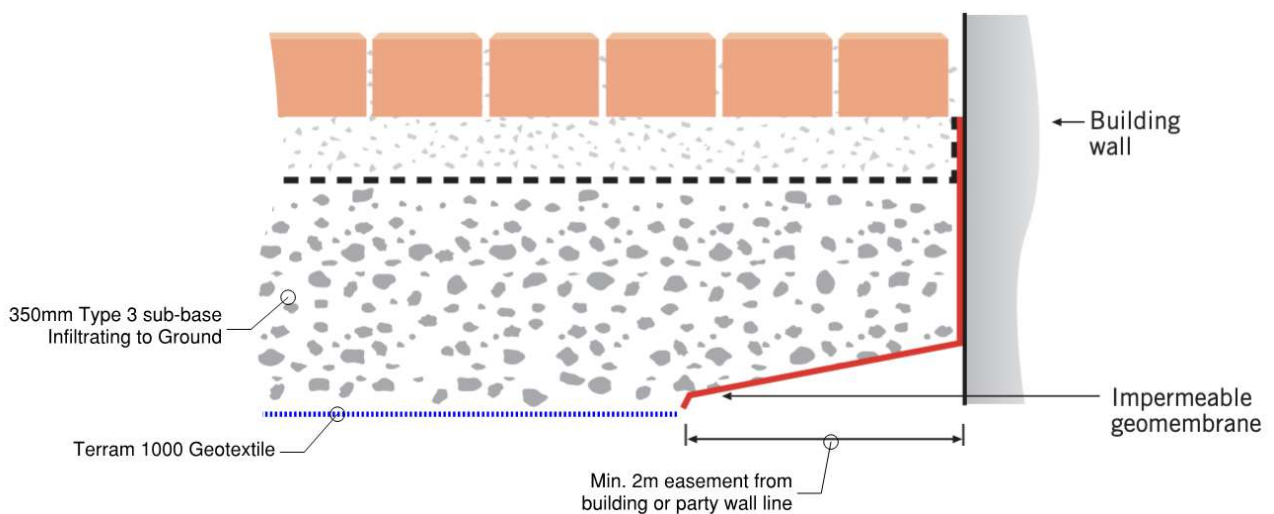


FIGURE 9. PERMEABLE PAVEMENT USED FOR THE HARDSTANDING AREAS

Attenuation (Below Ground)

Attenuation via modular attenuation tanks, ponds or swales is not considered a feasible option due to the site's space constraints (among others, as previously noted). Furthermore, the existing building would require the complete reconstruction of the existing drainage network to facilitate attenuation in the hard paved areas. This would then require surface water to chase below the existing buildings before discharging into the public sewers at restricted rates. To restrict to reduced surface water run-off rates this would also require complicated conveyancing to ascertain ownership of the prospective shared attenuation tank and associated drainage systems in third-party land.

Finally, deep excavation works associated with draining the existing RWPs to a below ground tank next to the existing building and the adjacent existing buildings would risk undermining the adjacent structure of the building. By draining the RWPs from the existing building into a below ground tank, pumps would be needed to reconnect into the existing outfall. It was concluded that this would not be appropriate for the size or scale of the development proposals.

Water Quality Improvements through SuDS Design

The Surface Water Run-off Assessment indicates no additional hardstanding areas in the proposed development, which means the potential for increased surface water run-off is minimised. Nonetheless, the design includes measures for managing run-off, notably in response to a potential future increase in rainfall intensity.

The inclusion of Sustainable Urban Drainage Systems (SuDS) is essential for mimicking natural drainage and reducing urbanisation impacts on watercourses. By prioritising these measures, the design addresses the greenfield runoff rates and meets Sustainable Infrastructure Policy requirements.

1. Green Roofs: Planned for upper levels to reduce peak flow rates, enhancing water absorption and aiding biodiversity.
2. Blue Roofs: Designed to temporarily store water and slowly release it, thereby easing pressure on drainage systems and improving water quality.
3. Infiltration through Permeable Paving: This approach will be used for the hardstanding areas, reducing run-off by allowing water to percolate into the ground, while also providing a contingency for overflow.
4. Permeable Pavements: Confirmed as a viable solution for managing run-off closer to the building structures.

The design excludes soakaways due to site constraints, instead focusing on source control SuDS solutions. The careful application of these measures, such as green and blue roofs and permeable pavements, enhances the site's water management and supports local biodiversity, offering a sustainable approach to development.

Amenity and Biodiversity Enhancements

Given the space constraints of the site, it is crucial to select enhancements that make the most of the available space while providing meaningful amenities and biodiversity improvements. Through a thorough evaluation of potential enhancements, the following six additions have been identified as particularly well-suited for this setting:

Selected Enhancements

1. **Vertical Gardens and Green Walls:** Vertical space on walls, fences, or trellises can be harnessed for the creation of vertical gardens or the installation of green walls. This approach will enhance aesthetics, introduce greenery, and maximise space efficiency, resulting in the establishment of a visually captivating and environmentally-conscious setting. The integration of vertical gardens or planters on walls or fences presents a feasible option for future additions. Notably suitable for compact areas, vertical gardens will offer a visually pleasing verdant atmosphere that complements the limited site.
2. **Native Plant Landscaping:** A strategic approach involving the use of native plants for landscaping is recommended. Native plants have demonstrated their ability to thrive in confined spaces and, concurrently, contribute to the preservation of local biodiversity.
3. **Green|Blue Roofs:** The integration of green and blue roofs is identified as a key component for the site. Green roofs, with their soil and vegetation layers, offer habitats for diverse plant and animal species, enhancing urban biodiversity. They also contribute to improving air quality, insulating buildings, and reducing the urban heat island effect. Blue roofs are engineered to manage rainwater by temporarily holding it and then releasing it slowly, thereby reducing the impact on the drainage system during heavy rainfall. Together, these green and blue roof systems can maximise the limited space by creating a multifunctional landscape overhead. This dual approach not only enriches the urban ecosystem but also provides a resilient strategy for stormwater management and climate adaptation.
4. **Micro Habitats and Wildlife Features:** Enhancing the site's ecological value can be achieved by incorporating features like birdhouses, bat boxes, or insect hotels on walls or in corners. These microhabitats provide support for local wildlife without significantly encroaching on available space.
5. **Permeable Paving and Pathways:** Use permeable materials for pathways and driveways to allow rainwater to infiltrate and reduce runoff. This combines functionality with sustainable stormwater management, contributing to groundwater recharge.
6. **Sustainable Drainage Systems:** To enhance water management and habitat creation, the design of sustainable drainage systems is proposed. These systems will effectively filter and clean runoff water, contributing to improved water quality and the establishment of small aquatic habitats.

The careful selection of these six amenity and biodiversity enhancements aligns with the context of the proposed site. By adopting these strategies, the development proposals provide a more sustainable and ecologically rich environment while optimising the limited space available.

SuDS Run-off Summary

| Return Period | Greenfield - interpolated (l/s) | Existing (l/s) | Proposed - without additional Mitigation Measures (l/s) | Proposed with SuDS Measures (l/s) |
|-----------------------|---------------------------------|----------------|---|-----------------------------------|
| 1 in 1 Year | 0.34 | 8.26 | 8.26 | 4.26* |
| 1 in 30 Year | 0.93 | 20.76 | 20.76 | 8.05** |
| 1 in 100 Year | 1.27 | 26.52 | 26.52 | 12.27** |
| 1 in 100 Year + 40%cc | - | - | 37.13 | 16.38** |

*The proposed surface water run-off from the development considers 16m² of the Green Roofs will be retained within the drainage medium.

** Calculations include surface water run-off that cannot be attenuated, plus the combined 2 l/s restricted rates from Blue Roofs.

In conclusion, the easements from boundaries and from structures limits the options in regards to centralised '3d' infiltration systems. However, the incorporation of source control features including Green|Blue Roofs and Permeable Paving, will reduce the development's surface water run-off rates for the 1 in 100 year return period plus an allowance for climate change. These SuDS elements provide an overall reduction in surface water run-off rates for all storm events compared to the unmitigated scenario by up to **56%**. The proposed SuDS features also offer significant improvements in 'Water Quality' in accordance with the SuDS Manual C753.

Surface Water Maintenance Strategy

The drainage design will be designed to be fully maintainable in accordance with building regulations and the recommendations of CIRIA C753 – SuDS Manual, outlined below. The applicant or their appointed management team will be responsible for the management and maintenance of the respective SuDS systems in perpetuity.

Green Roof | Rain Gardens

| Maintenance Schedule | Required Action | Typical Frequency |
|------------------------|--|--------------------------|
| Regular Maintenance | Weed spray with environmentally friendly chemicals | Half yearly |
| | Clear leaves and litter | Half yearly |
| | Plants to be pruned | Half yearly |
| Occasional maintenance | Remove silt build-up from inlets and surface and replace mulch as necessary | Annually, or as required |
| | Remove silt build-up from outlets and surface and replace mulch as necessary | Annually, or as required |
| Remedial Actions | Repair of overflow erosion damage or damage to outfall | As required |

Permeable Paving

| Maintenance Schedule | Required Action | Typical Frequency |
|------------------------|---|---|
| Monitoring/Inspections | Initial Inspection. | Monthly for three months after installation |
| | Inspect for evidence of poor operation and/or weed growth - if required take remedial action. | Annually (and after severe storms) |
| Regular Maintenance | Rubbish and litter removal | As required |
| | Brushing and vacuuming - standard cosmetic sweep across surface | Once a year after Autumn leaf fall |
| Remedial Actions | Remedial work to any depressions or rutting considered detrimental to the structural performance. | As required |
| | Rehabilitation of surface with remedial sweeping | Every 10-15 years or as required. |

Blue Roof

| Maintenance Schedule | Required Action | Typical Frequency |
|--------------------------|--|--|
| Monitoring / Inspections | Inspect all inlets, outlets, vents, overflows and control structures to ensure they are working as they should | Annually or after severe storms |
| Regular Maintenance | Inspect and identify any elements that are not operating correctly. | Monthly for three months, then Half yearly or as required. |
| | Remove sediments / debris from catch pits / gullies and control structures | Annually, after severe storms or as required |
| Remedial Actions | Repair inlets, outlets, vents, overflows and control structures. | As required |

Effective SuDS design must assess all foreseeable risks during construction and maintenance. These must be mitigated during the detailed design stages where effective design will aim to avoid, reduce and mitigate risks. This process will also require input from the principal contractor who will ensure the construction of SuDS components are carried out in a safe and sustainable manner. The CDM Regulations place specific Health and Safety duties on those commissioning, planning and undertaking construction works. If you are uncertain what this means you should seek the advice of your architect, builder or other competent professional. Flume does not provide health and safety advisory services, but we are required to advise you of your general responsibilities under CDM.

Conclusions

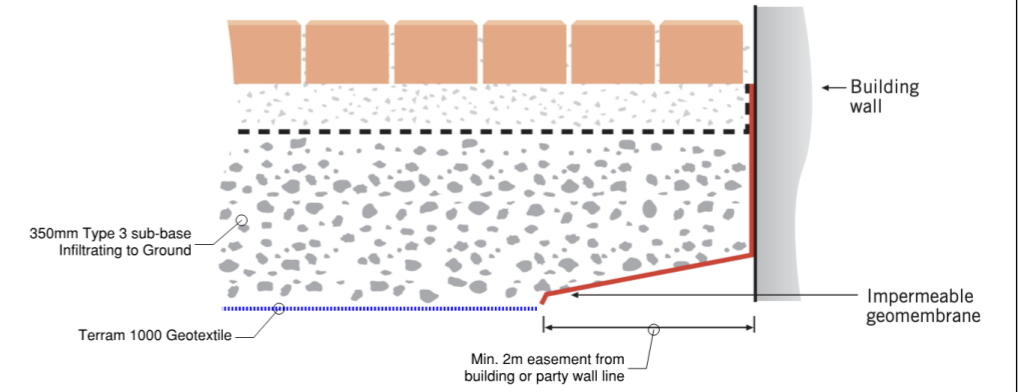
- The site resides in Flood Zone 1 where there is less than 1 in 1000 annual probability of river or sea flooding (<0.1%). Developments in this flood zone have no restrictions other than ensuring surface water drainage proposals do not increase the flood risk on site and the surrounding areas.
- The existing development discharges surface water at unrestricted rates to the public sewer. The proposed development will reduce the overall hardstanding areas compared to the existing scenario. The proposals will therefore not increase the flood risk from surface water, as there will be no increase in the surface water run-off rate or volumes.
- Infiltration will be prioritised on site where feasible, with the use of permeable paving serving the external hardstanding areas infiltrating to ground. A combination of Green|Blue Roofs, Vertical Green Walls and permeable paving for hardstanding areas, will be used to reduce surface water run-off rates from the proposed development. These SuDS proposals will reduce the surface water run-off by up to 56% compared to existing - exceeding the NSTS 50% betterment of the existing flow rates for all periods.
- Site constraints prevent reducing surface water run-off rates further. The existing building's below ground drainage system would have to be reconfigured in order to limit surface water run-off rates for the entire site boundary further and would not be appropriate for the size or scale of the development proposals. However, peak surface water run-off rates have been reduced where possible and practical in line with the London Plan, NSTS and Enfield's SuDS guidance.
- Permeable Pavements and Green Roofs are placed highly in the SuDS Hierarchy, and will ensure that water quality, water quantity, amenity and biodiversity are all promoted in the SuDS design.
- A SuDS Maintenance Plan will also be in place to ensure efficient operation and prevent failure of the system.




Note:

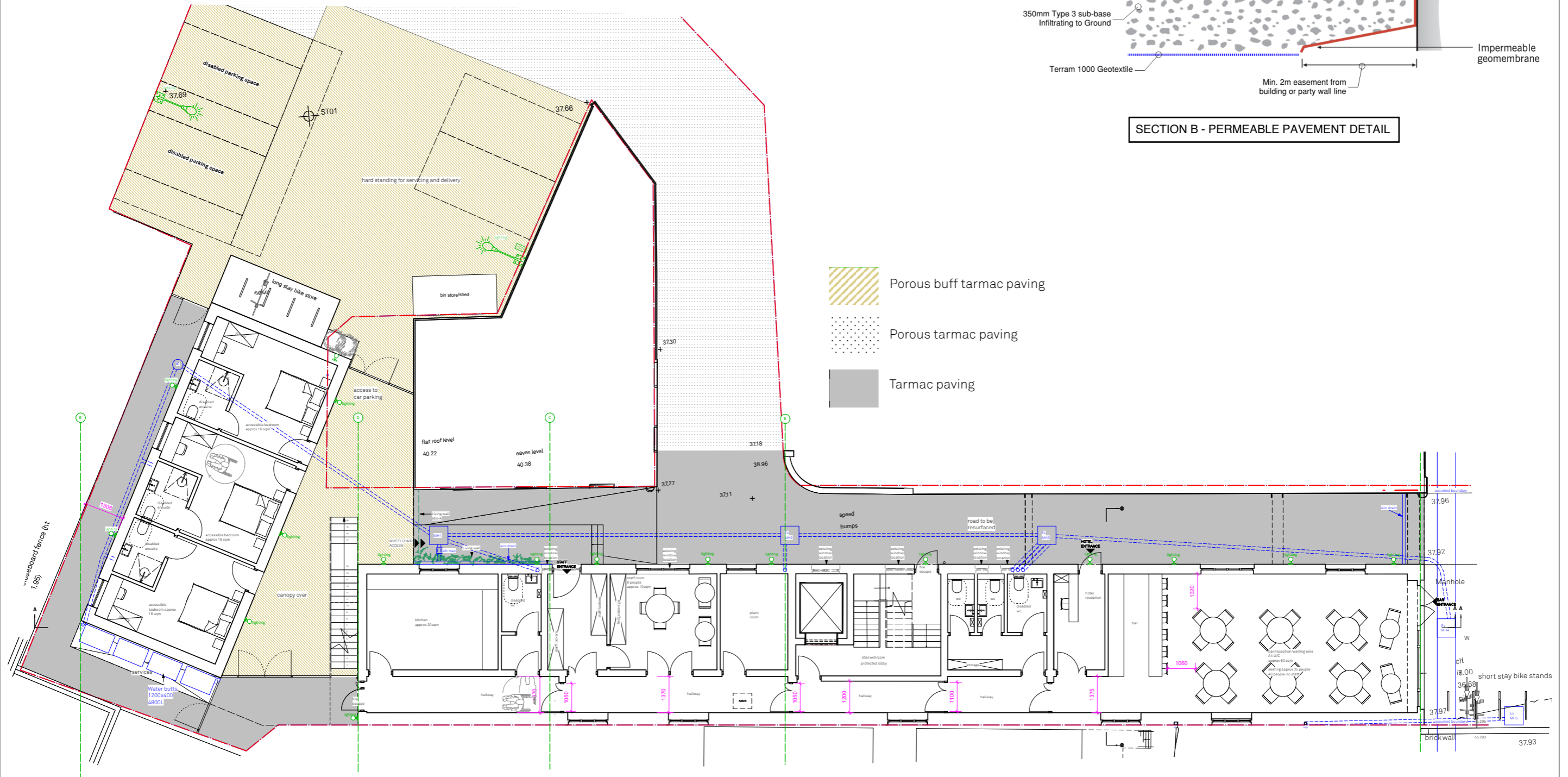
This report has been prepared for the purposes of submitting for planning to the local planning authority for review in relation to the associated Flood Risk and SuDS for the proposed development, and uses the most up-to-date information available to us at the time. It should not be relied upon by anyone else or used for any other purpose. This report is confidential to our Client; it should only be shown to others with their permission. We retain copyright of this report which should not be reproduced without our permission.

| | Prepared By | Checked By | Approved for issue |
|------------------|-----------------------------|-------------------|-----------------------------|
| Name | Tom Quigg BSc MSc CEng MICE | Magaly Sedeño BA | Tom Quigg BSc MSc CEng MICE |
| Signature | TQ | MST | TQ |
| Date | 8 November 2023 | 8 November 2023 | 8 November 2023 |

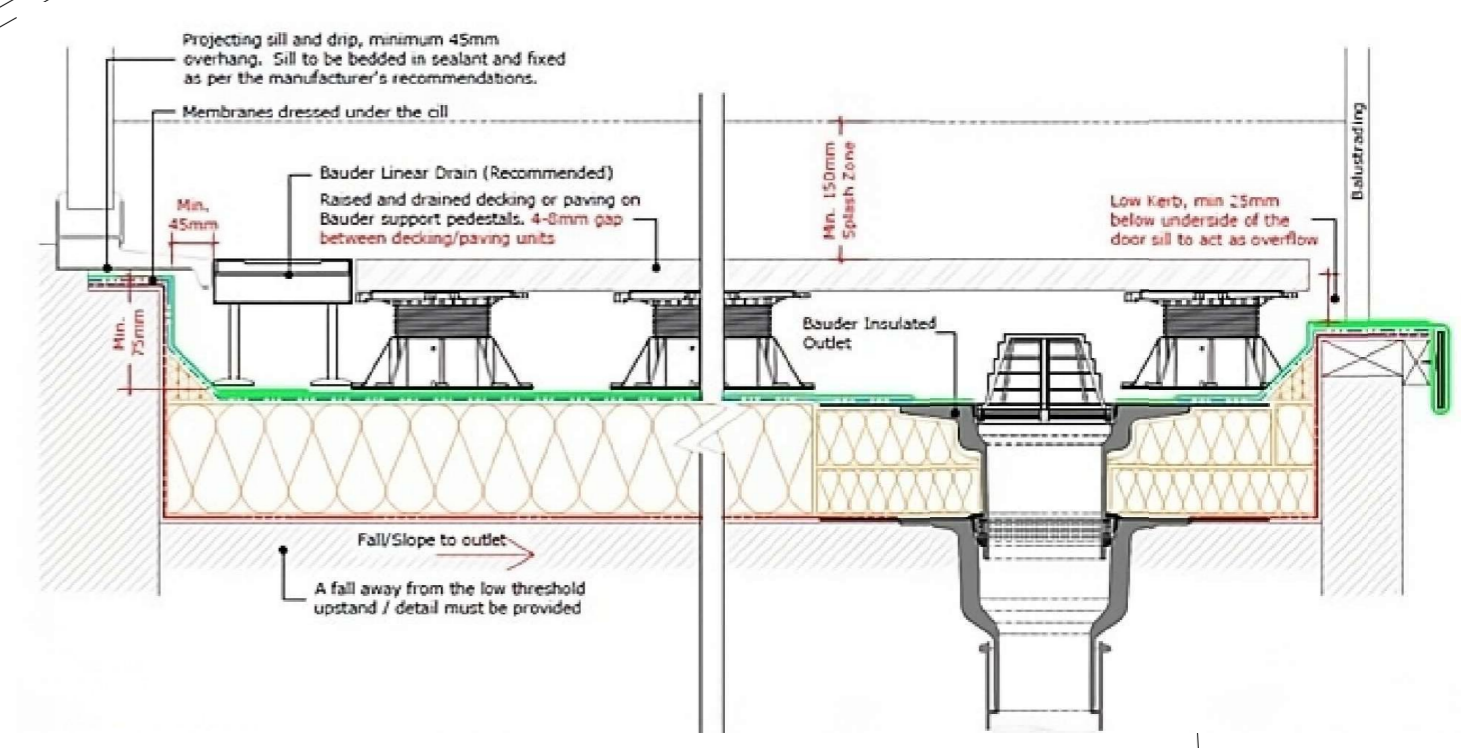
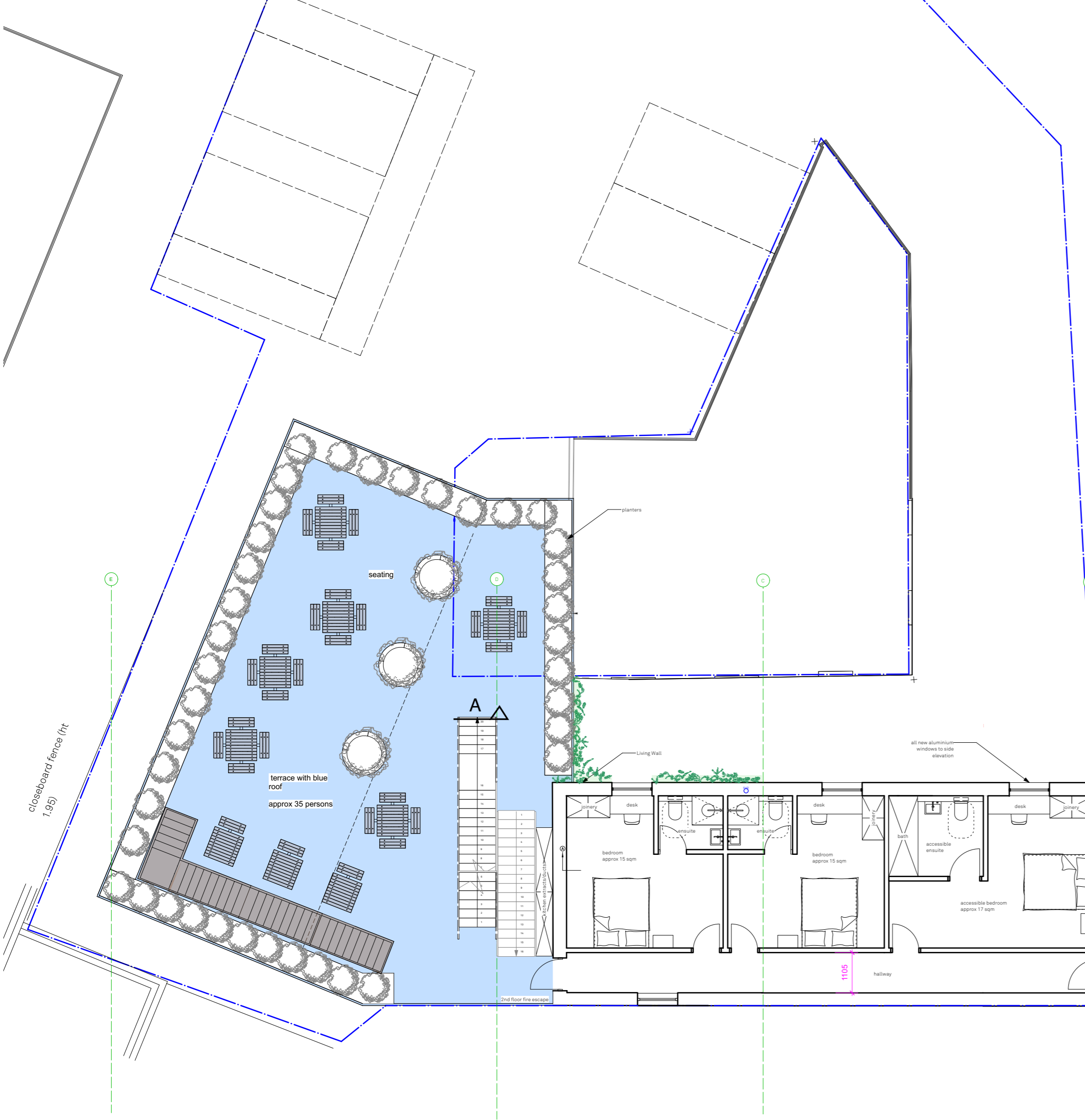
Appendix A - SuDS Strategy and Hydraulic Calculations



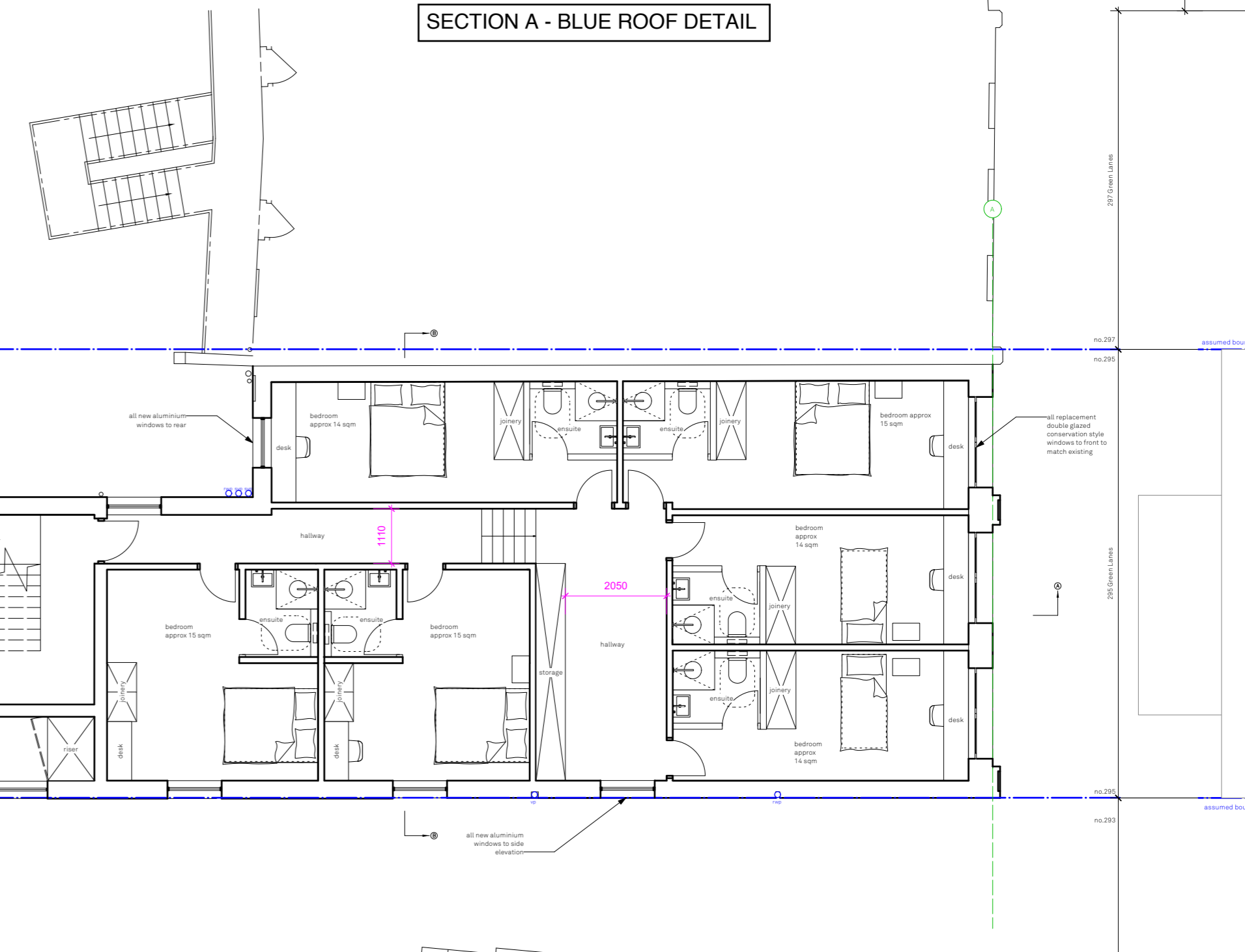
-  Porous buff tarmac paving
-  Porous tarmac paving
-  Tarmac paving



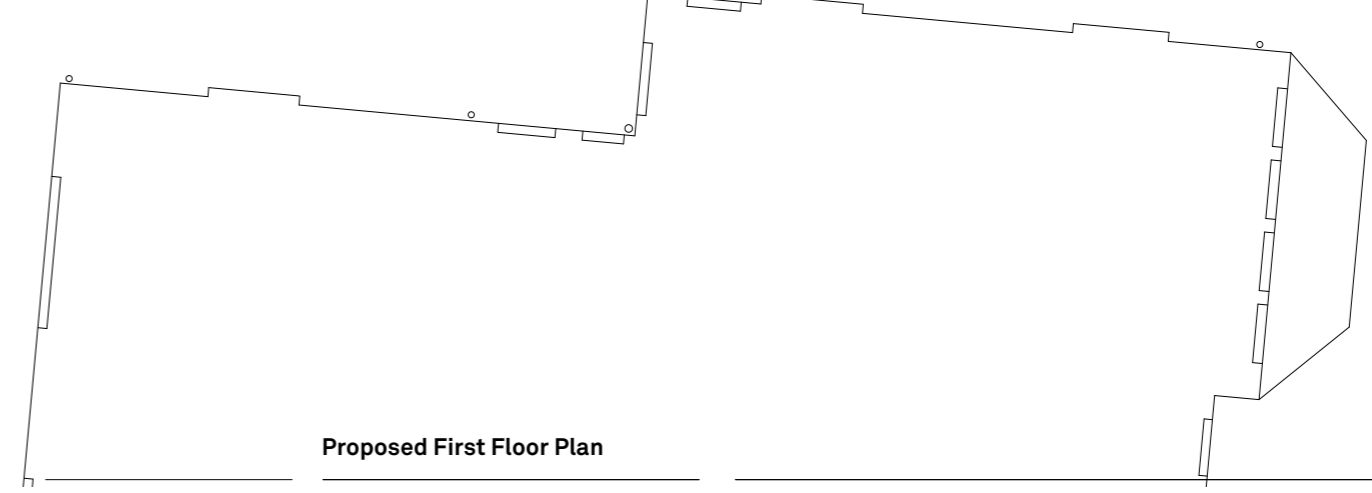
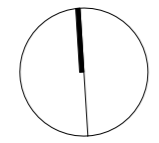
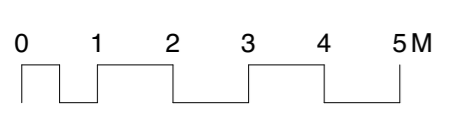




SECTION A - BLUE ROOF DETAIL



**PLANNING DRAWINGS ONLY
NOT FOR CONSTRUCTION.
CONTRACTOR RESPONSIBLE FOR
ALL SITE DIMENSIONS AND COORDINATION**



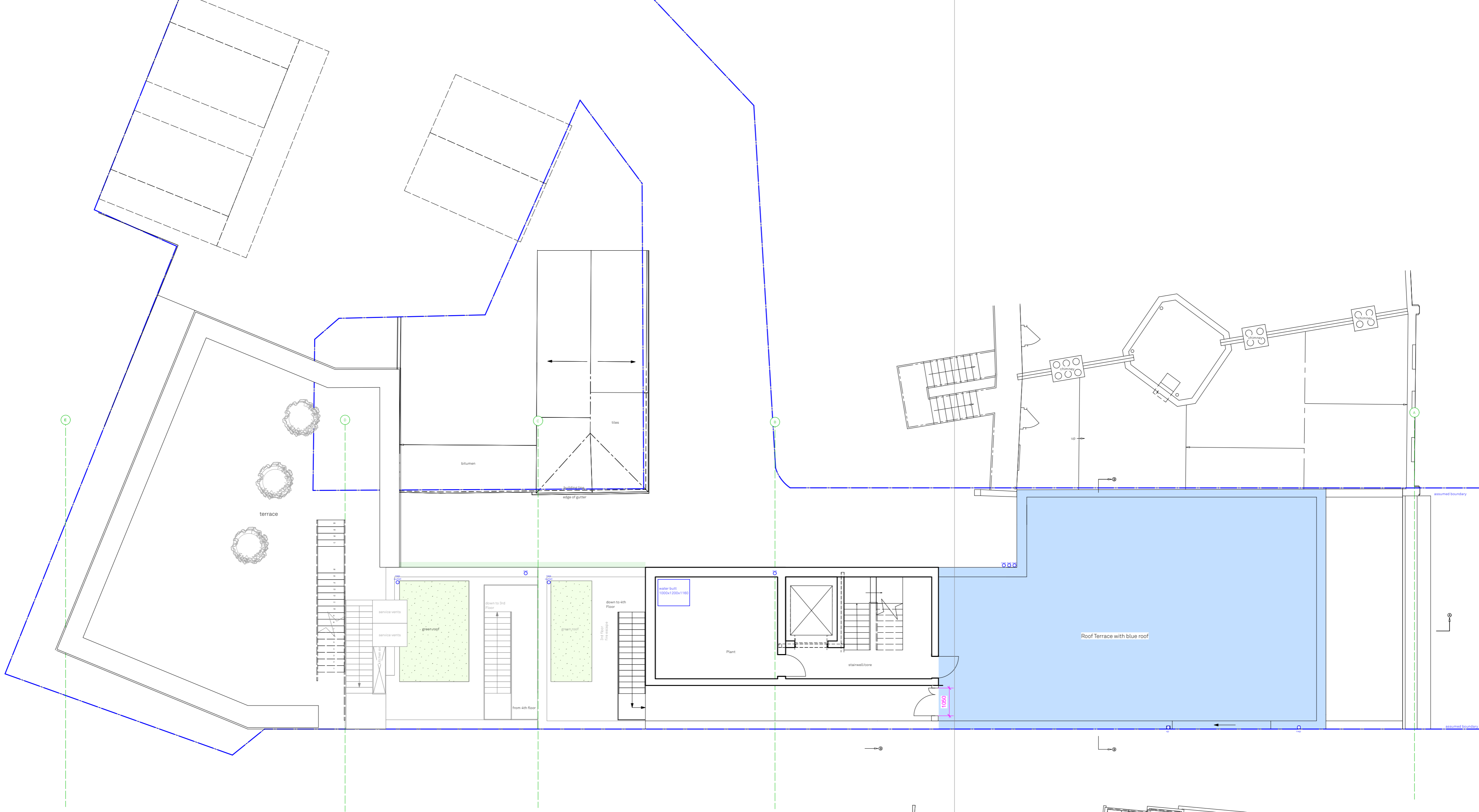
Proposed First Floor Plan

| Key | Green Lanes |
|--|------------------------|
| Green roof | 295 Green Lanes, N13 |
| Living wall | Drawn By SJ |
| Blue roof | Scale 1:100@A2 |
| | Status Information |
| | Project Stage PLANNING |

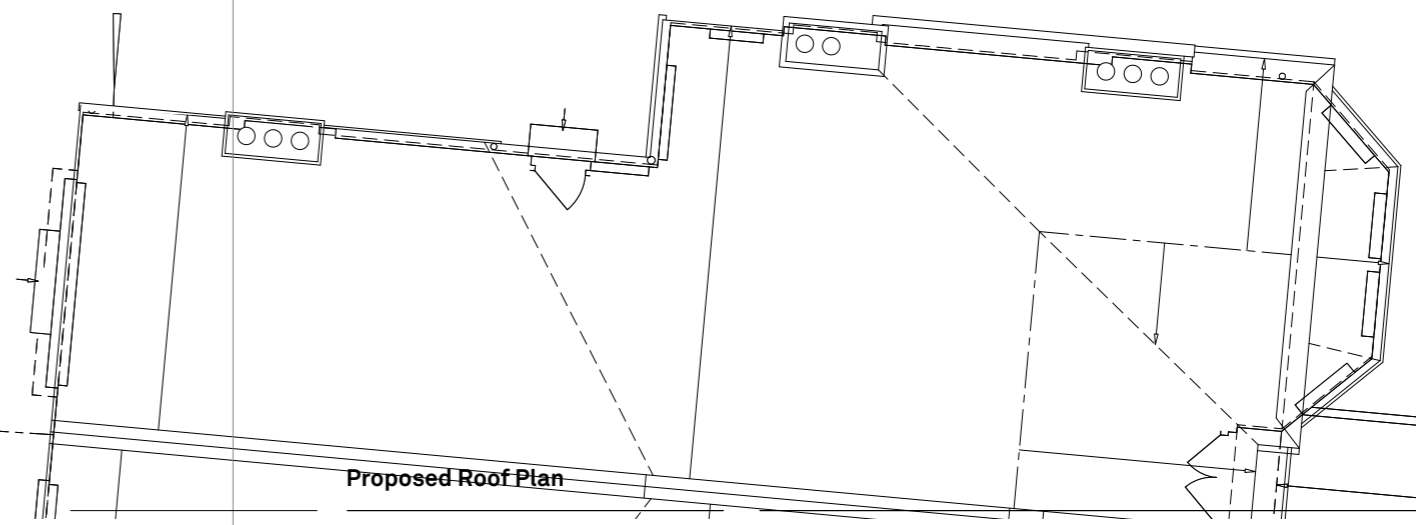
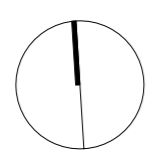
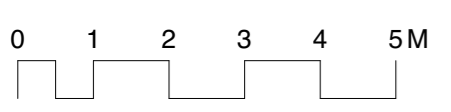
| Issue | Notes | Date |
|-------|----------------------|------------|
| B | Issued for comments | 02/09/2022 |
| C | Planning Application | 14/09/2022 |
| D | issued for comments | 01/06/2023 |

889.202C

paul archer
design



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 CONTRACTOR RESPONSIBLE FOR
 ALL SITE DIMENSIONS AND COORDINATION**



Key

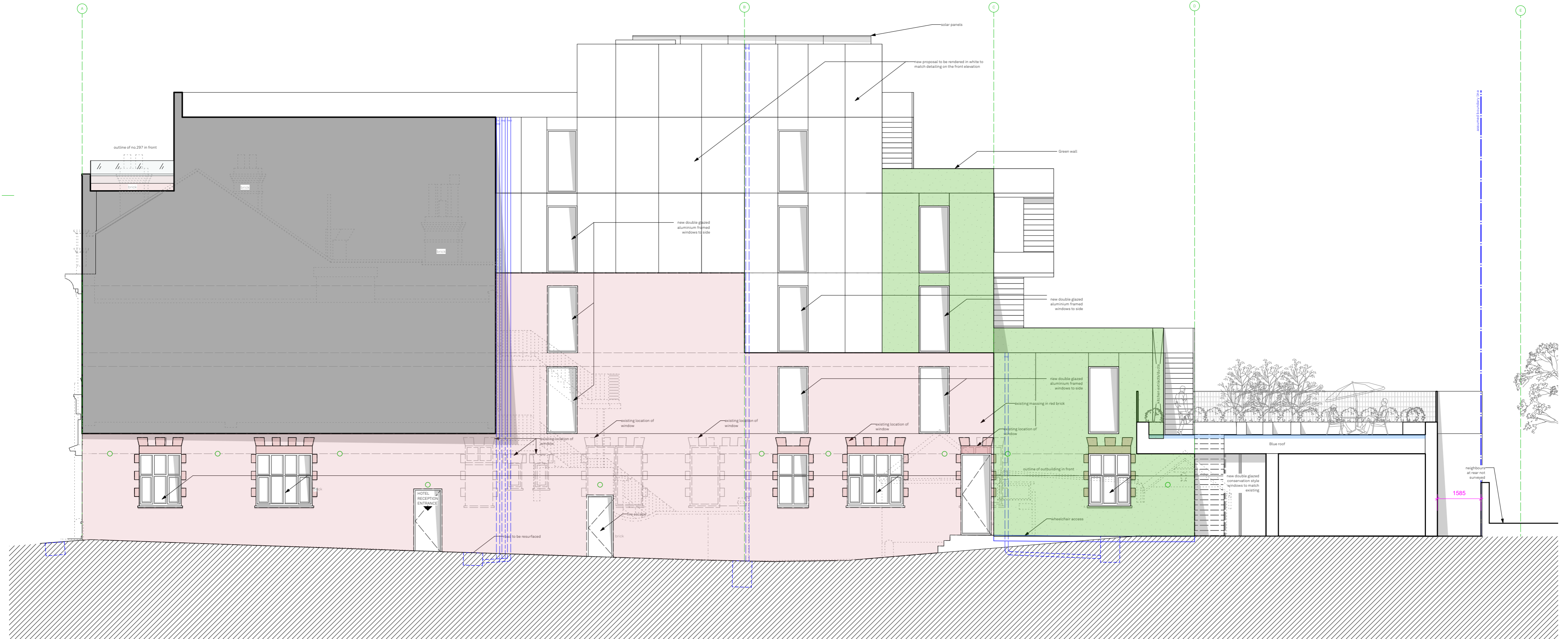
| | |
|--|-------------|
| | Green roof |
| | Living wall |
| | Blue roof |

Green Lanes
 295 Green Lanes, N13
 Drawn By SJ
 Scale 1:100@A2
 Status Information
 Project Stage PLANNING

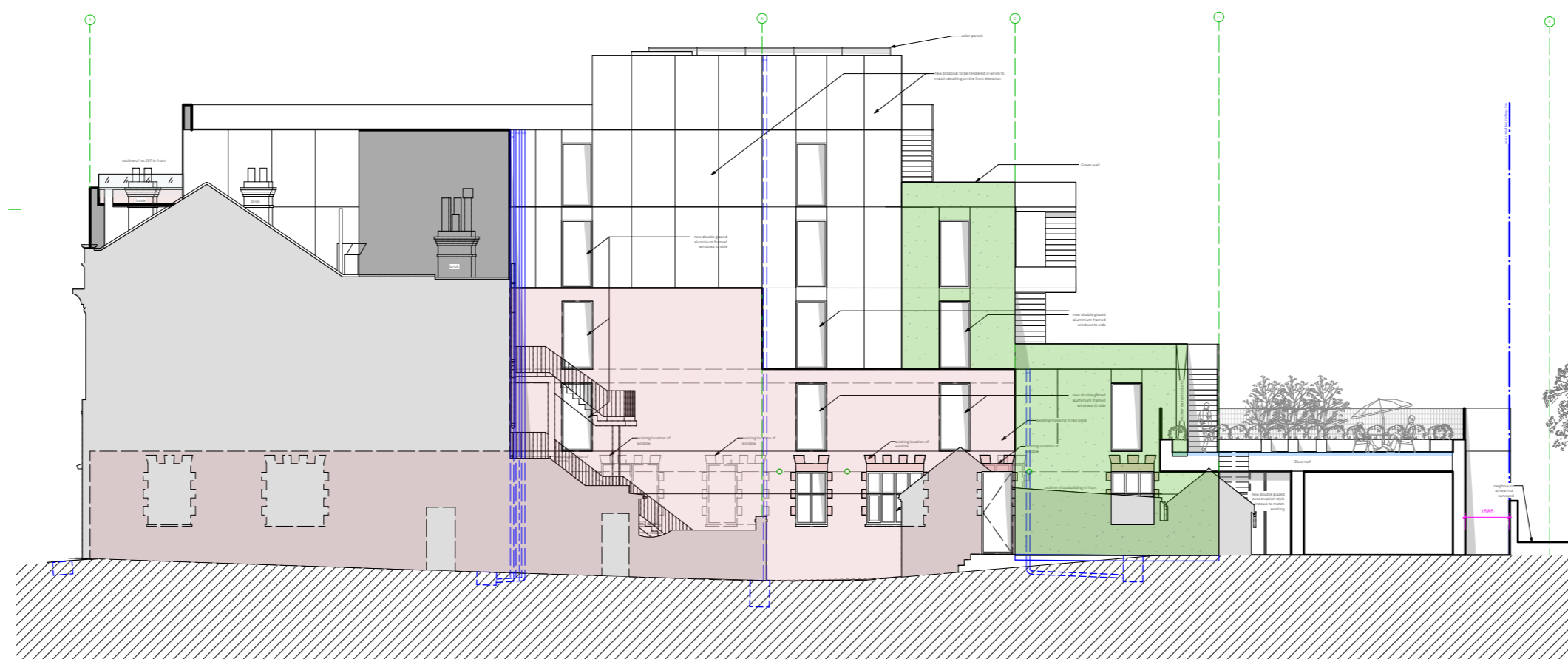
| Issue | Notes | Date |
|-------|----------------------|------------|
| B | Planning Application | 14/09/2022 |
| C | issued for comments | 01/06/2023 |
| D | Drainage added | 05/10/2023 |

889.210D

paul archer
design

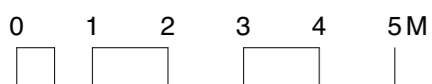


Proposed North Elevation
Scale 1:100



Proposed Elevation showing 297 Green Lanes in grey
Scale 1:200

**PLANNING DRAWINGS ONLY
NOT FOR CONSTRUCTION.
CONTRACTOR RESPONSIBLE FOR
ALL SITE DIMENSIONS AND COORDINATION**



Proposed North Elevation

| Key | Green Lanes |
|--|------------------------|
| Green roof | 295 Green Lanes, N13 |
| Living wall | Drawn By SJ |
| Blue roof | Scale 1:100@A2 |
| | Status Information |
| | Project Stage PLANNING |

Paul Archer Design Ltd

| Issue | Notes | Date |
|-------|----------------------|------------|
| B | Planning Application | 14/09/2022 |
| C | issued for comments | 01/06/2023 |
| D | Drainage added | 05/10/2023 |

Unit D204 Lana House 116 Commercial Street London E1 6NF Tel. 020 3668 2668

889.206D

paul archer
design

www.paularcherdesign.co.uk

Calculated by:

Site name:

Site location:

Site Details

Latitude:

Longitude:

Reference:

Date:

This is an estimation of the greenfield runoff rates that are used to meet normal best practice criteria in line with Environment Agency guidance "Rainfall runoff management for developments", SC030219 (2013), the SuDS Manual C753 (Ciria, 2015) and the non-statutory standards for SuDS (Defra, 2015). This information on greenfield runoff rates may be the basis for setting consents for the drainage of surface water runoff from sites.

Runoff estimation approach

Site characteristics

Total site area (ha):

Methodology

Q_{BAR} estimation method:

SPR estimation method:

Soil characteristics

| | Default | Edited |
|--------------|-----------------------------------|-----------------------------------|
| SOIL type: | <input type="text" value="4"/> | <input type="text" value="4"/> |
| HOST class: | <input type="text" value="N/A"/> | <input type="text" value="N/A"/> |
| SPR/SPRHOST: | <input type="text" value="0.47"/> | <input type="text" value="0.47"/> |

Hydrological characteristics

| | Default | Edited |
|--------------------------------|-----------------------------------|-----------------------------------|
| SAAR (mm): | <input type="text" value="654"/> | <input type="text" value="654"/> |
| Hydrological region: | <input type="text" value="6"/> | <input type="text" value="6"/> |
| Growth curve factor 1 year: | <input type="text" value="0.85"/> | <input type="text" value="0.85"/> |
| Growth curve factor 30 years: | <input type="text" value="2.3"/> | <input type="text" value="2.3"/> |
| Growth curve factor 100 years: | <input type="text" value="3.19"/> | <input type="text" value="3.19"/> |
| Growth curve factor 200 years: | <input type="text" value="3.74"/> | <input type="text" value="3.74"/> |

Notes

(1) Is $Q_{BAR} < 2.0$ l/s/ha?

When Q_{BAR} is < 2.0 l/s/ha then limiting discharge rates are set at 2.0 l/s/ha.

(2) Are flow rates < 5.0 l/s?

Where flow rates are less than 5.0 l/s consent for discharge is usually set at 5.0 l/s if blockage from vegetation and other materials is possible. Lower consent flow rates may be set where the blockage risk is addressed by using appropriate drainage elements.

(3) Is $SPR/SPRHOST \leq 0.3$?

Where groundwater levels are low enough the use of soakaways to avoid discharge offsite would normally be preferred for disposal of surface water runoff.

| Greenfield runoff rates | Default | Edited |
|-------------------------|-----------------------------------|-----------------------------------|
| Q_{BAR} (l/s): | <input type="text" value="0.45"/> | <input type="text" value="0.45"/> |
| 1 in 1 year (l/s): | <input type="text" value="0.38"/> | <input type="text" value="0.38"/> |
| 1 in 30 years (l/s): | <input type="text" value="1.03"/> | <input type="text" value="1.03"/> |
| 1 in 100 year (l/s): | <input type="text" value="1.42"/> | <input type="text" value="1.42"/> |
| 1 in 200 years (l/s): | <input type="text" value="1.67"/> | <input type="text" value="1.67"/> |

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at www.uksuds.com/terms-and-conditions.htm. The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.

Design Settings

| | | | |
|-----------------------|-------------------|--------------------------------------|---------------|
| Rainfall Methodology | FSR | Maximum Time of Concentration (mins) | 30.00 |
| Return Period (years) | 1 | Maximum Rainfall (mm/hr) | 150.0 |
| Additional Flow (%) | 0 | Minimum Velocity (m/s) | 1.00 |
| FSR Region | England and Wales | Connection Type | Level Soffits |
| M5-60 (mm) | 20.000 | Minimum Backdrop Height (m) | 0.200 |
| Ratio-R | 0.400 | Preferred Cover Depth (m) | 1.200 |
| CV | 1.000 | Include Intermediate Ground | ✓ |
| Time of Entry (mins) | 5.00 | Enforce best practice design rules | x |

Nodes

| Name | Area (ha) | T of E (mins) | Cover Level (m) | Diameter (mm) | Depth (m) |
|------------------|-----------|---------------|-----------------|---------------|-----------|
| Permeable Paving | 0.040 | 5.00 | 0.500 | 450 | 0.500 |
| Outfall | 0.000 | | 0.500 | 450 | 0.500 |

Links

| Name | US Node | DS Node | Length (m) | ks (mm) / n | US IL (m) | DS IL (m) | Fall (m) | Slope (1:X) | Dia (mm) | T of C (mins) | Rain (mm/hr) |
|-------|------------------|---------|------------|-------------|-----------|-----------|----------|-------------|----------|---------------|--------------|
| 1.000 | Permeable Paving | Outfall | 3.000 | 0.600 | 0.000 | 0.000 | 0.000 | 0.0 | 100 | 5.05 | 54.5 |

| Name | Vel (m/s) | Cap (l/s) | Flow (l/s) | US Depth (m) | DS Depth (m) | Σ Area (ha) | Σ Add Inflow (l/s) | Pro Depth (mm) | Pro Velocity (m/s) |
|-------|-----------|-----------|------------|--------------|--------------|-------------|--------------------|----------------|--------------------|
| 1.000 | 1.000 | 7.9 | 7.9 | 0.400 | 0.400 | 0.040 | 0.0 | 0 | ∞ |

Pipeline Schedule

| Link | Length (m) | Slope (1:X) | Dia (mm) | Link Type | US CL (m) | US IL (m) | US Depth (m) | DS CL (m) | DS IL (m) | DS Depth (m) |
|-------|------------|-------------|----------|-----------|-----------|-----------|--------------|-----------|-----------|--------------|
| 1.000 | 3.000 | 0.0 | 100 | Circular | 0.500 | 0.000 | 0.400 | 0.500 | 0.000 | 0.400 |

| Link | US Node | Dia (mm) | Node Type | MH Type | DS Node | Dia (mm) | Node Type | MH Type |
|-------|------------------|----------|-----------|-----------|---------|----------|-----------|-----------|
| 1.000 | Permeable Paving | 450 | Manhole | Adoptable | Outfall | 450 | Manhole | Adoptable |

Manhole Schedule

| Node | CL (m) | Depth (m) | Dia (mm) | Connections | Link | IL (m) | Dia (mm) |
|------------------|--------|-----------|----------|-------------|-------|--------|----------|
| Permeable Paving | 0.500 | 0.500 | 450 | | | | |
| | | | | 0 | 1.000 | 0.000 | 100 |
| Outfall | 0.500 | 0.500 | 450 | | | | |
| | | | | 1 | 1.000 | 0.000 | 100 |

Simulation Settings

| | | | | | |
|----------------------|-------------------|-------------------|--------|----------------------------|------|
| Rainfall Methodology | FSR | Summer CV | 1.000 | Drain Down Time (mins) | 1440 |
| FSR Region | England and Wales | Winter CV | 1.000 | Additional Storage (m³/ha) | 0.0 |
| M5-60 (mm) | 20.000 | Analysis Speed | Normal | Check Discharge Rate(s) | x |
| Ratio-R | 0.400 | Skip Steady State | x | Check Discharge Volume | x |

Storm Durations

15 | 30 | 60 | 120 | 180 | 240 | 360 | 480 | 600 | 720 | 960 | 1440

| Return Period (years) | Climate Change (CC %) | Additional Area (A %) | Additional Flow (Q %) | Return Period (years) | Climate Change (CC %) | Additional Area (A %) | Additional Flow (Q %) |
|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| 5 | 0 | 0 | 0 | 100 | 40 | 0 | 0 |
| 30 | 0 | 0 | 0 | | | | |

Node Permeable Paving Online Depth/Flow Control

| | | | | | |
|--------------------------|---|------------------|-------|-------------------|-----|
| Flap Valve | x | Invert Level (m) | 0.000 | Design Flow (l/s) | 0.2 |
| Replaces Downstream Link | ✓ | Design Depth (m) | 1.000 | | |

| Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) |
|-----------|------------|-----------|------------|
| 0.001 | 0.000 | 0.500 | 0.000 |

Node Permeable Paving Carpark Storage Structure

| | | | | | | | |
|-----------------------------|---------|---------------------------|-------|-------------|--------|---------------|-------|
| Base Inf Coefficient (m/hr) | 0.03600 | Porosity | 0.30 | Width (m) | 20.000 | Depth (m) | 0.350 |
| Side Inf Coefficient (m/hr) | 0.03600 | Invert Level (m) | 0.000 | Length (m) | 20.000 | Inf Depth (m) | |
| Safety Factor | 2.0 | Time to half empty (mins) | 0 | Slope (1:X) | 300.0 | | |

Results for 5 year Critical Storm Duration. Lowest mass balance: 100.00%

| Node Event | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m ³) | Flood (m ³) | Status |
|------------------|------------------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|--------|
| 60 minute summer | Permeable Paving | 42 | 0.071 | 0.071 | 7.8 | 4.4666 | 0.0000 | OK |
| 15 minute summer | Outfall | 1 | 0.000 | 0.000 | 0.0 | 0.0000 | 0.0000 | OK |

| Link Event (Upstream Depth) | US Node | Link | DS Node | Outflow (l/s) | Discharge Vol (m ³) |
|-----------------------------|------------------|--------------|---------|---------------|---------------------------------|
| 60 minute summer | Permeable Paving | Depth/Flow | Outfall | 0.0 | 0.0 |
| 60 minute summer | Permeable Paving | Infiltration | | 2.0 | |

Results for 30 year Critical Storm Duration. Lowest mass balance: 100.00%

| Node Event | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m ³) | Flood (m ³) | Status |
|------------------|------------------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|--------|
| 60 minute summer | Permeable Paving | 46 | 0.096 | 0.096 | 11.6 | 7.5731 | 0.0000 | OK |
| 15 minute summer | Outfall | 1 | 0.000 | 0.000 | 0.0 | 0.0000 | 0.0000 | OK |

| Link Event (Upstream Depth) | US Node | Link | DS Node | Outflow (l/s) | Discharge Vol (m ³) |
|-----------------------------|------------------|--------------|---------|---------------|---------------------------------|
| 60 minute summer | Permeable Paving | Depth/Flow | Outfall | 0.0 | 0.0 |
| 60 minute summer | Permeable Paving | Infiltration | | 2.0 | |

Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 100.00%

| Node Event | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m ³) | Flood (m ³) | Status |
|------------------|------------------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 60 minute winter | Permeable Paving | 59 | 0.173 | 0.173 | 15.5 | 16.7896 | 0.0000 | SURCHARGED |
| 15 minute summer | Outfall | 1 | 0.000 | 0.000 | 0.0 | 0.0000 | 0.0000 | OK |

| Link Event (Upstream Depth) | US Node | Link | DS Node | Outflow (l/s) | Discharge Vol (m ³) |
|-----------------------------|------------------|--------------|---------|---------------|---------------------------------|
| 60 minute winter | Permeable Paving | Depth/Flow | Outfall | 0.0 | 0.0 |
| 60 minute winter | Permeable Paving | Infiltration | | 2.1 | |

Appendix B - Ground Investigation Report - BRE 365 Infiltration Tests



JAXX ENGINEERING CONSULTANCY

Jaxx Engineering Consultancy

12 Colville Close

Stanford-le-Hope, Corringham, Essex

Telephone/Fax: 020 3576 2390 Mobile: 07508 853739

Email: info@jaxxeng.com Website: www.jaxxeng.com



Factual Report

Client : Naem Ishak

Site Name : 295 Green Lanes, London, N13 4XS

Client Reference : JEC3445

Laboratory Reference : -

Date of Completion : 28-Jul



JAXX ENGINEERING CONSULTANCY

Content Summary

Lab Reference : JEC3445

Client Reference : 295 Green Lanes, London, N13 4XS

For the attention of : Naem Ishak

- This report comprises of the following :
- 1 Site Plan
 - 1 Material Logs
 - 1 Infiltration Testing
 - 1 Limitations

Notes :

General

Please refer to report summary notes for details pertaining to methods undertaken and their subsequent accreditations

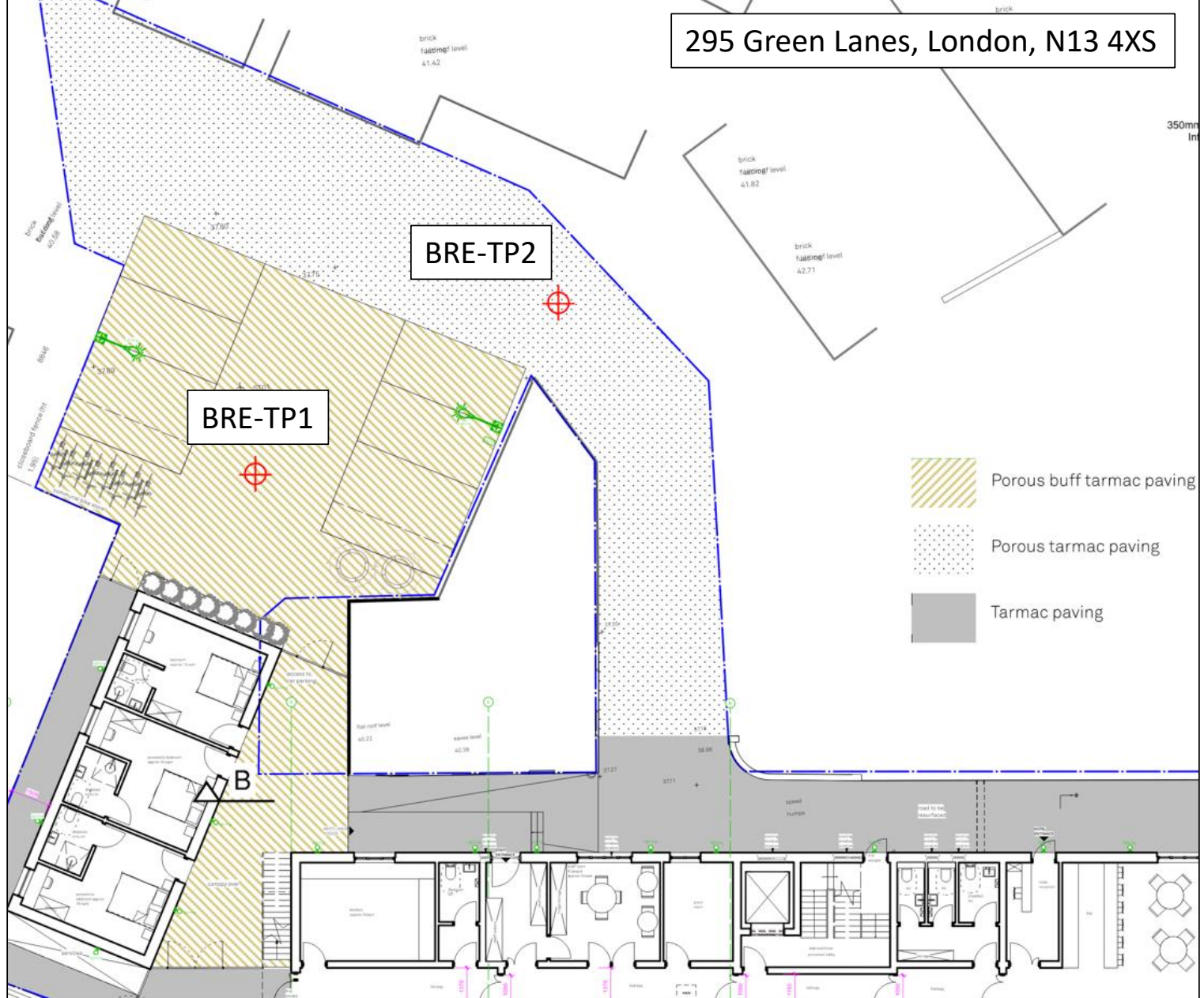
Samples were supplied by Customer

All tests performed in-house unless otherwise stated

Deviant Samples

| | |
|--|-----|
| Samples were received in suitable containers | Yes |
| A date and time of sampling was provided | Yes |
| Arrived damage/denaturing free | Yes |

295 Green Lanes, London, N13 4XS



BRE-TP2

BRE-TP1

B

-  Porous buff tarmac paving
-  Porous tarmac paving
-  Tarmac paving

Jaxx Engineering Consultancy

12 Colville Close
Stanford le Hope, Essex, SS17 7RS

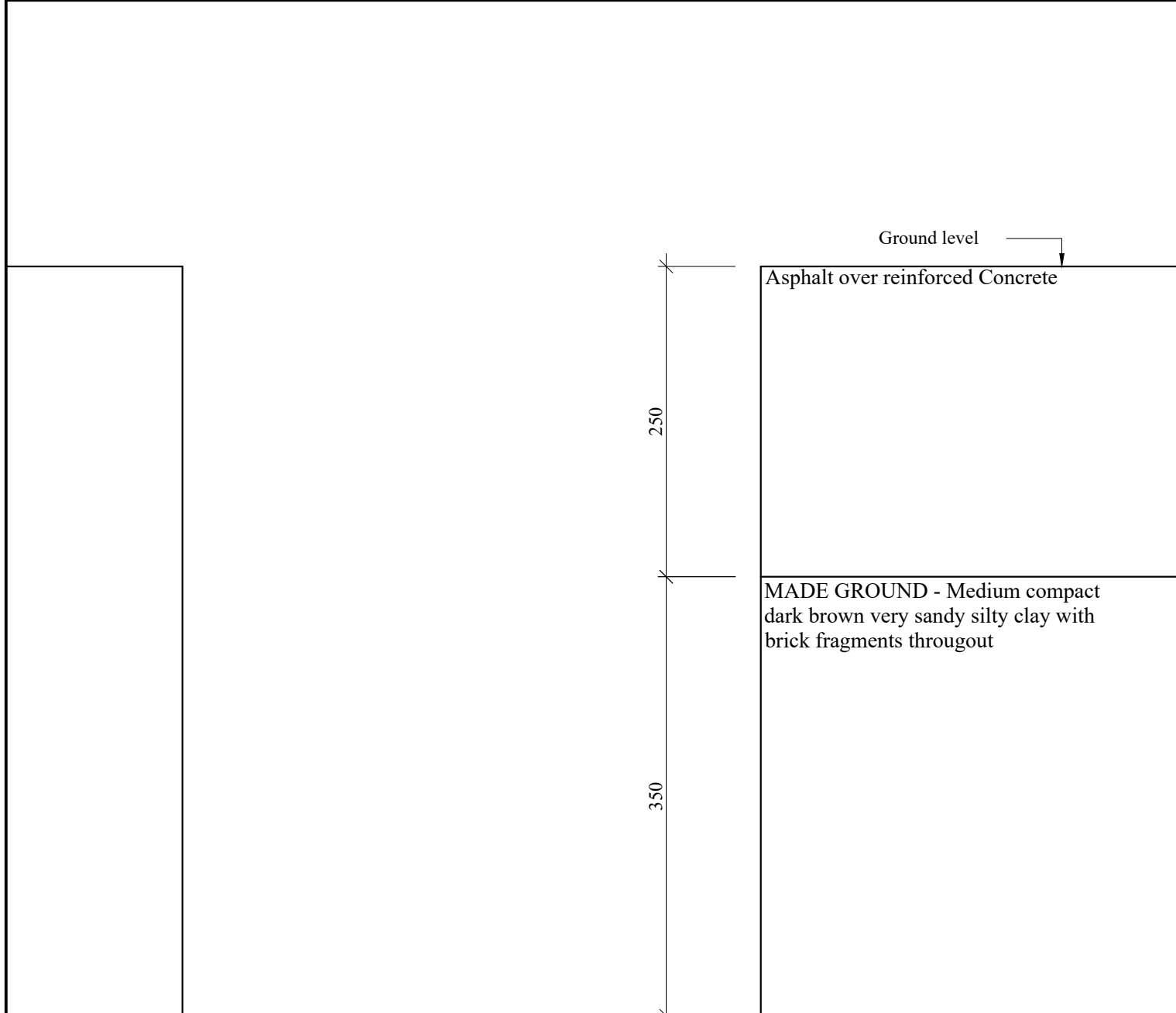
Telephone: 0203 576 2390 Mob: 07508 853739

Email: engineering@jaxxeng.com Website: www.jaxxeng.com



**JAXX
ENGINEERING
CONSULTANCY**

| | | | |
|---|----------------------|--------------------------|--------------------------|
| Client: Naem Ishak | Scale: N.T.S. | Sheet No: 1 of 1 | Date: 27/07/23 |
| Location: 295 Green Lanes, London, N13 4XS | Job No: 3445 | Trial Pit No: TP1 | Weather: Overcast |
| Excavation Method: Mechanical & Hand | | Drawn by: MB | Checked by: GW |



TRIAL PIT ENDS AT 600mm

Remarks: Trial Pit completed to 0.6m

- Key:
- D** Small disturbed sample
 - B** Bulk disturbed sample
 - U** Undisturbed sample (U100)
 - N** Standard Penetration Test Blow Count
 - J** Jar sample
 - V** Pilcon Vane (kPa)
 - M** Mackintosh Probe
 - W** Water Sample

Jaxx Engineering Consultancy

12 Colville Close
Stanford le Hope, Essex, SS17 7RS

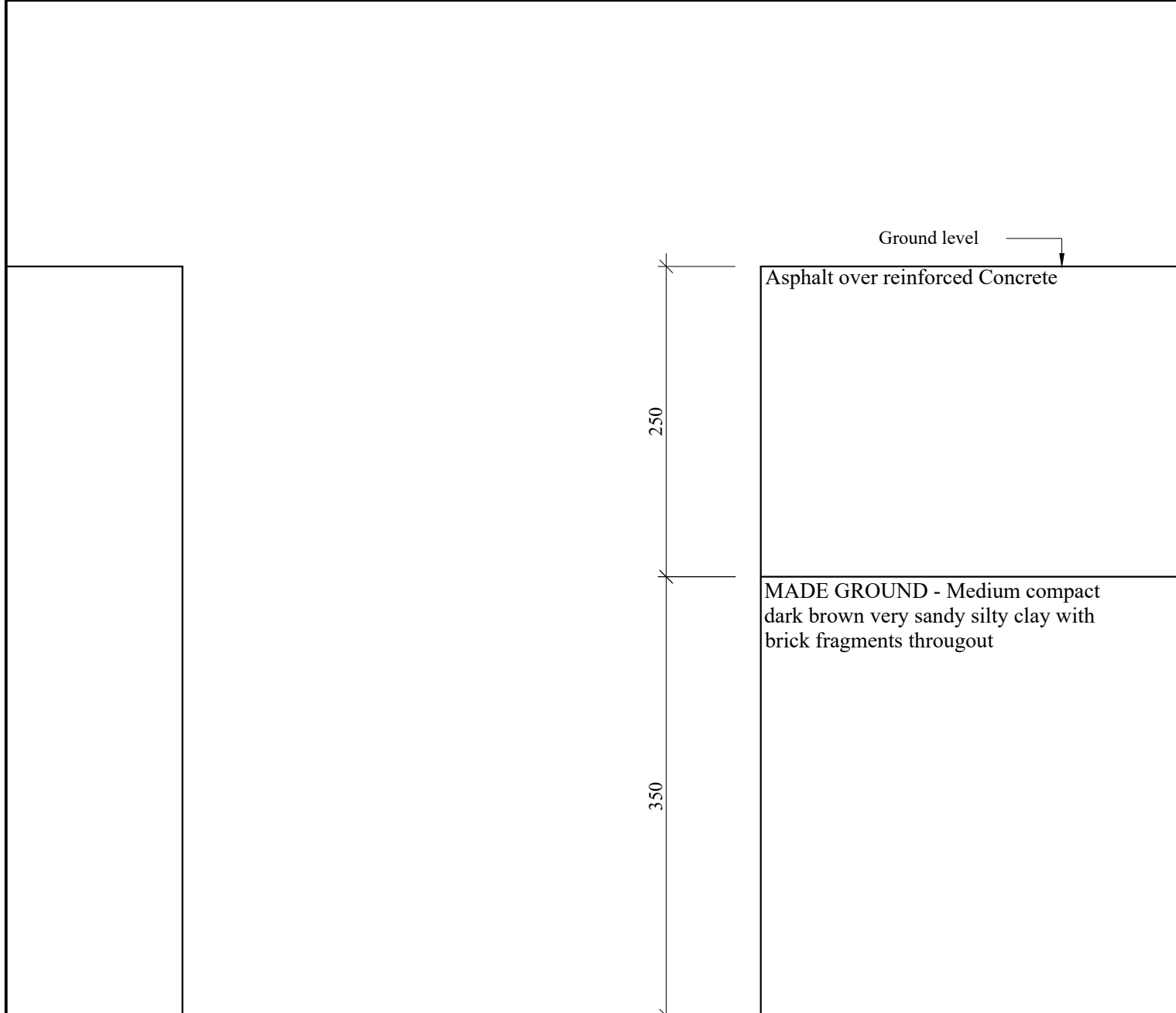
Telephone: 0203 576 2390 Mob: 07508 853739

Email: engineering@jaxxeng.com Website: www.jaxxeng.com



**JAXX
ENGINEERING
CONSULTANCY**

| | | | |
|---|----------------------|--------------------------|--------------------------|
| Client: Naem Ishak | Scale: N.T.S. | Sheet No: 1 of 1 | Date: 27/07/23 |
| Location: 295 Green Lanes, London, N13 4XS | Job No: 3445 | Trial Pit No: TP2 | Weather: Overcast |
| Excavation Method: Mechanical & Hand | | Drawn by: MB | Checked by: GW |



TRIAL PIT ENDS AT 600mm

Remarks: Trial Pit completed to 0.6m

Key:

- | | |
|---|----------------------------|
| D Small disturbed sample | J Jar sample |
| B Bulk disturbed sample | V Pilcon Vane (kPa) |
| U Undisturbed sample (U100) | M Mackintosh Probe |
| N Standard Penetration Test Blow Count | W Water Sample |

Project Name : 295 Green Lanes, London, N13 4XS

Job No : TGT3445

Performed By : NI

Date : 27/07/23

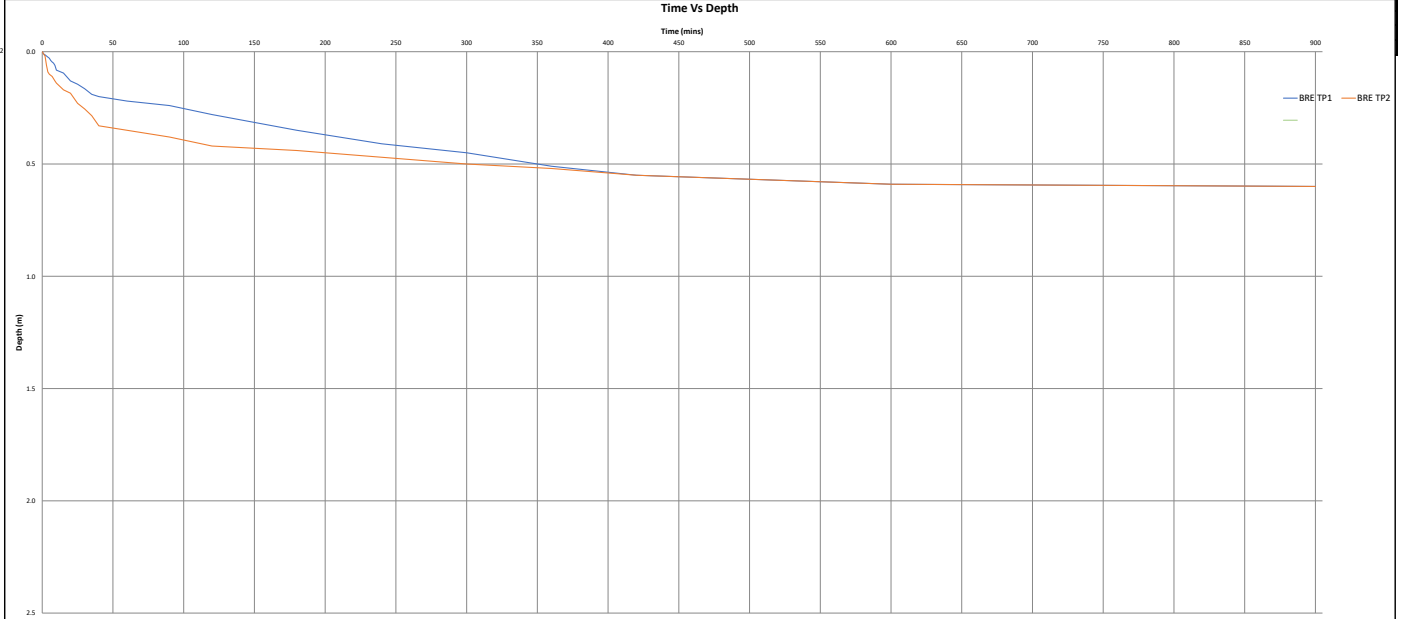
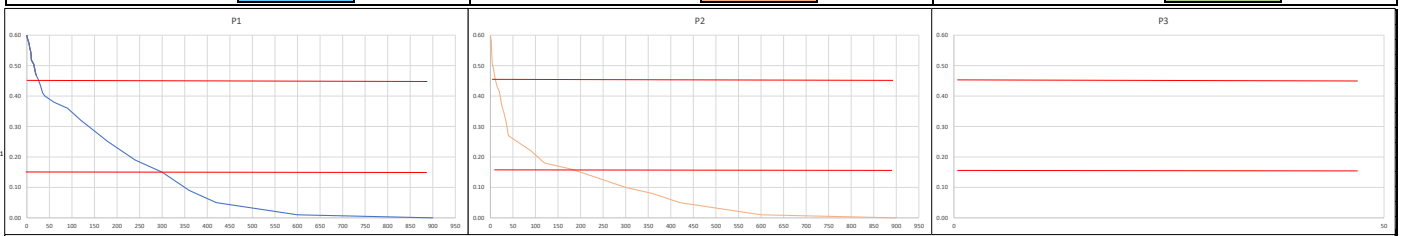
Checked By : GW

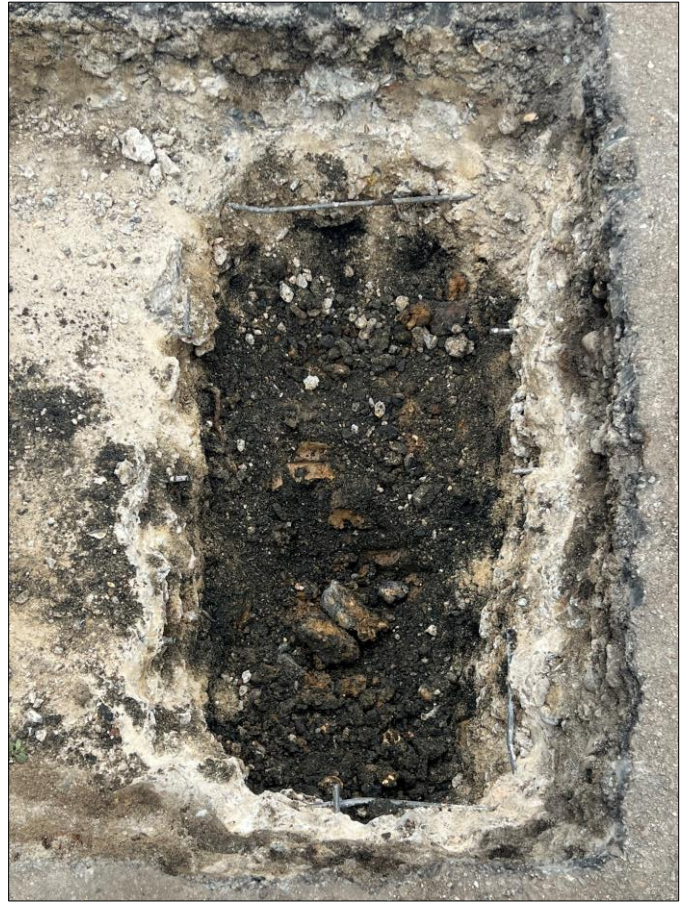
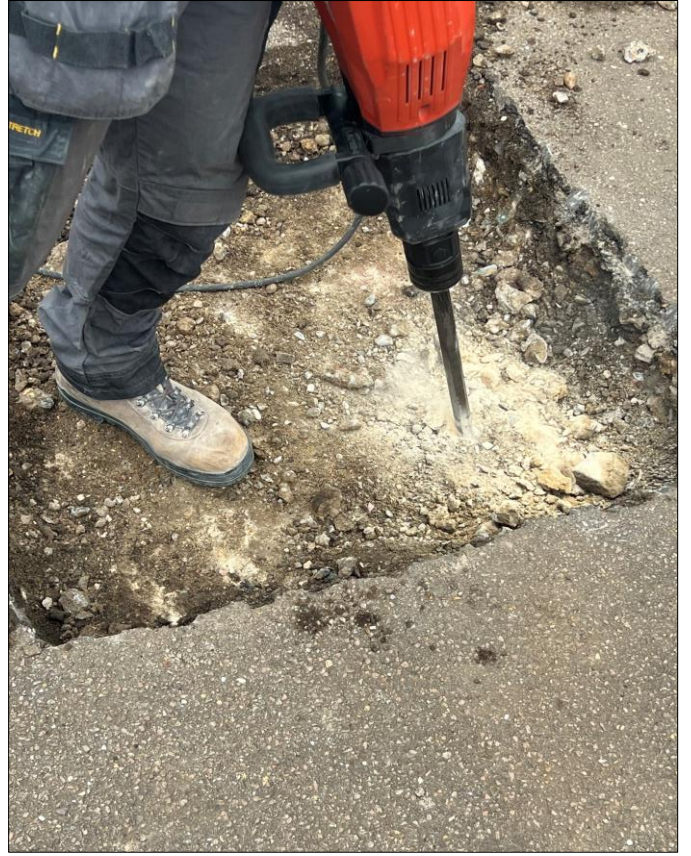
| BRE TP1 | | | | BRE TP2 | | | |
|---|-------------|--------------|------------------|---|-------------|--------------|------------------|
| Test Dimensions 1.0m (w) x 1.0m (l) x 0.6m (d) | | $H_0 = 0.60$ | | Test Dimensions 1.0m (w) x 1.0m (l) x 0.6m (d) | | $H_0 = 0.60$ | |
| Depth to Water (m) | Time (mins) | H | H/H ₀ | Depth to Water (m) | Time (mins) | H | H/H ₀ |
| 0.000 | 0 | 0.60 | 1.00 | 0.000 | 0 | 0.60 | 1.00 |
| 0.010 | 1 | 0.59 | 0.98 | 0.010 | 1 | 0.59 | 0.98 |
| 0.014 | 2 | 0.59 | 0.23 | 0.020 | 2 | 0.58 | 0.97 |
| 0.019 | 3 | 0.58 | 0.23 | 0.060 | 3 | 0.54 | 0.90 |
| 0.024 | 4 | 0.58 | 0.23 | 0.090 | 4 | 0.51 | 0.85 |
| 0.029 | 5 | 0.57 | 0.23 | 0.100 | 5 | 0.50 | 0.83 |
| 0.039 | 6 | 0.56 | 0.22 | 0.105 | 6 | 0.50 | 0.83 |
| 0.046 | 7 | 0.55 | 0.22 | 0.110 | 7 | 0.49 | 0.82 |
| 0.051 | 8 | 0.55 | 0.22 | 0.120 | 8 | 0.48 | 0.80 |
| 0.061 | 9 | 0.54 | 0.22 | 0.130 | 9 | 0.47 | 0.78 |
| 0.082 | 10 | 0.52 | 0.21 | 0.140 | 10 | 0.46 | 0.77 |
| 0.095 | 15 | 0.51 | 0.20 | 0.170 | 15 | 0.43 | 0.72 |
| 0.130 | 20 | 0.47 | 0.19 | 0.185 | 20 | 0.42 | 0.69 |
| 0.145 | 25 | 0.46 | 0.18 | 0.230 | 25 | 0.37 | 0.62 |
| 0.165 | 30 | 0.44 | 0.17 | 0.255 | 30 | 0.35 | 0.58 |
| 0.190 | 35 | 0.41 | 0.16 | 0.285 | 35 | 0.32 | 0.53 |
| 0.200 | 40 | 0.40 | 0.16 | 0.330 | 40 | 0.27 | 0.45 |
| 0.220 | 60 | 0.38 | 0.15 | 0.350 | 60 | 0.25 | 0.42 |
| 0.240 | 90 | 0.36 | 0.14 | 0.380 | 90 | 0.22 | 0.37 |
| 0.280 | 120 | 0.32 | 0.13 | 0.420 | 120 | 0.18 | 0.30 |
| 0.350 | 180 | 0.25 | 0.10 | 0.440 | 180 | 0.16 | 0.27 |
| 0.410 | 240 | 0.19 | 0.08 | 0.470 | 240 | 0.13 | 0.22 |
| 0.450 | 300 | 0.15 | 0.06 | 0.500 | 300 | 0.10 | 0.17 |
| 0.510 | 360 | 0.09 | 0.04 | 0.520 | 360 | 0.08 | 0.13 |
| 0.550 | 420 | 0.05 | 0.02 | 0.550 | 420 | 0.05 | 0.08 |
| 0.590 | 600 | 0.01 | 0.00 | 0.590 | 600 | 0.01 | 0.02 |
| 0.600 | 900 | 0.00 | 0.00 | 0.600 | 900 | 0.00 | 0.00 |

| | |
|--|----------|
| Volume of Excavation (m ³) = | 0.60 |
| Storage volume between 75-25% 'tp' [m ³] = | 0.30 |
| Time for water to fall from 75-25% 'tp' [min] = | 275 |
| 50% Internal Surface Area (as50) = | 2.20 |
| Soil infiltration rate 'Y' [m/s] = | 2.06E-06 |

| | |
|--|----------|
| Volume of Excavation (m ³) = | 0.60 |
| Storage volume between 75-25% 'tp' [m ³] = | 0.30 |
| Time for water to fall from 75-25% 'tp' [min] = | 195 |
| 50% Internal Surface Area (as50) = | 2.20 |
| Soil infiltration rate 'Y' [m/s] = | 2.23E-06 |

| | |
|--|--|
| Volume of Excavation (m ³) = | |
| Storage volume between 75-25% 'tp' [m ³] = | |
| Time for water to fall from 75-25% 'tp' [min] = | |
| 50% Internal Surface Area (as50) = | |
| Soil infiltration rate 'Y' [m/s] = | |







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Where our involvement consists exclusively of testing samples, the results and comments (if provided) relate only to the samples tested.

Any samples that are deemed to be subject to deviation will be recorded as such within the test summary.