

## Calculations for thermal insulation, moisture protection and heat protection

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### Content

Component	U-value W/m <sup>2</sup> K	Condensate kg	TA- Attenuation	Thickness cm	Weight kg/m <sup>2</sup>	Page
1 Wall	0,2	-	20,4	25,05	43,9	2
2 Roof	0,21	-	11,0	33,80	118,7	9

### Comparison with different maximum values\*

Component	GEG 2020 Bestand	BEG Einzelmaßn.	GEG 2020 Neubau	DIN 4108
Wall	✓	✓	✓	✓
Roof	✓			✓

## Wall

Exterior wall

### Thermal protection

$U = 0,198 \text{ W}/(\text{m}^2\text{K})$

GEG 2020 Bestand\*:  $U < 0,24 \text{ W}/(\text{m}^2\text{K})$



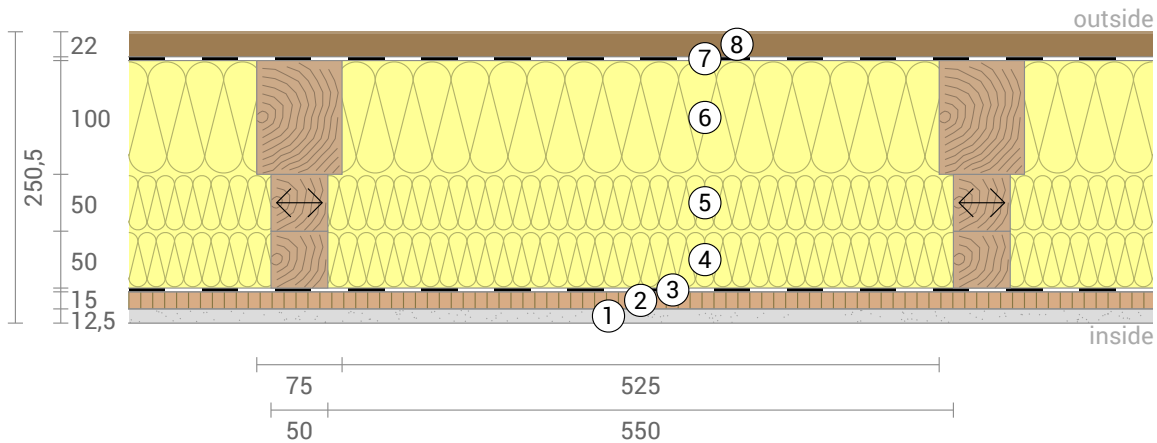
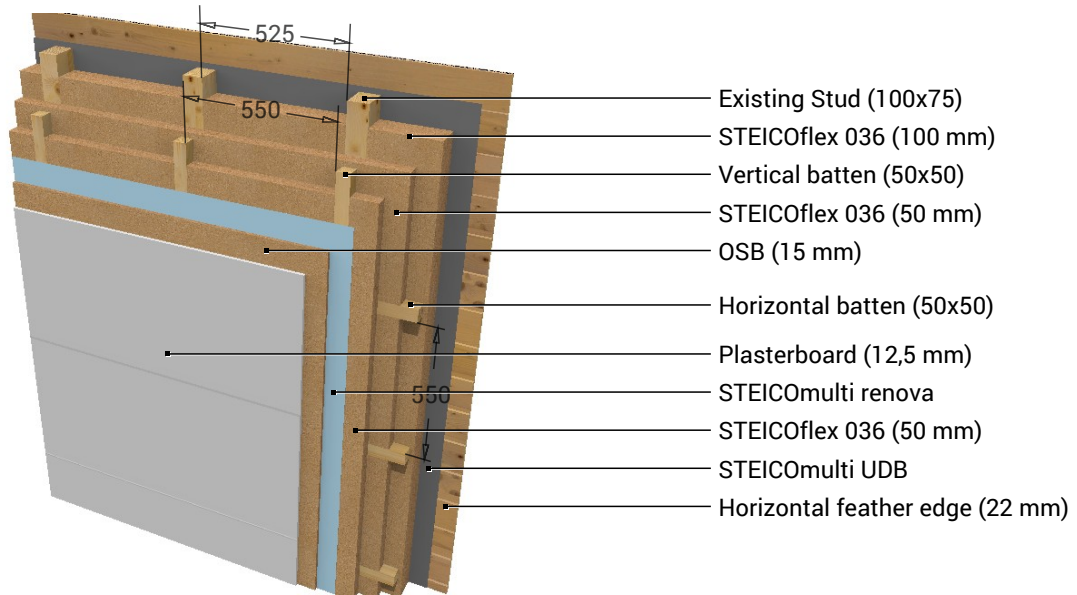
### Moisture proofing

Drying reserve:  $1405 \text{ g}/\text{m}^2\text{a}$   
No condensate



### Heat protection

Temperature amplitude damping: 20  
phase shift: 11,3 h  
Thermal capacity inside:  $41 \text{ kJ}/\text{m}^2\text{K}$



- ① Plasterboard (12,5 mm)
- ② OSB (15 mm)
- ③ STEICOmulti renova
- ④ STEICOflex 036 (50 mm)
- ⑤ STEICOflex 036 (50 mm)
- ⑥ STEICOflex 036 (100 mm)
- ⑦ STEICOmulti UDB
- ⑧ Horizontal feather edge (22 mm)

<-> Layers marked by arrows are perpendicular to the main axis.

Inside air :  $20,0^\circ\text{C} / 50\%$

Outside air:  $-5,0^\circ\text{C} / 80\%$

Surface temperature.:  $18,4^\circ\text{C} / -4,8^\circ\text{C}$

sd-value: 14,9 m

Drying reserve:  $1405 \text{ g}/\text{m}^2\text{a}$

Thickness: 25,1 cm

Weight:  $44 \text{ kg}/\text{m}^2$

Heat capacity:  $68 \text{ kJ}/\text{m}^2\text{K}$

- GEG 2020 Bestand
- BEG Einzelmaßn.
- GEG 2020 Neubau
- DIN 4108

Wall,  $U=0,198 \text{ W}/(\text{m}^2\text{K})$

## U-Value calculation according to DIN EN ISO 6946

#	Material	Dicke [cm]	$\lambda$ [W/mK]	R [m <sup>2</sup> K/W]
	Thermal contact resistance inside (Rsi)			0,130
1	Plasterboard (12,5mm)	1,25	0,210	0,060
2	OSB	1,50	0,130	0,115
3	STEICOmulti renova	0,05	0,170	0,003
4	STEICOflex 036	5,00	0,036	1,389
	Vertical batten (8,3%)	5,00	0,130	0,385
5	STEICOflex 036	5,00	0,036	1,389
	Horizontal batten (8,3%)	5,00	0,130	0,385
6	STEICOflex 036	10,00	0,036	2,778
	Existing Stud (12%)	10,00	0,130	0,769
7	STEICOmulti UDB	0,05	0,170	0,003
8	Horizontal feather edge	2,20	0,260	0,085
	Thermal contact resistance outside (Rse)			0,040

Thermal contact resistances have been taken from DIN 6946 Table 7.

Rsi: heat flow direction horizontally

Rse: heat flow direction horizontally, outside: Direct contact to outside air

Upper limit of thermal resistance  $R_{\text{tot,upper}} = 5,307 \text{ m}^2\text{K}/\text{W}$ .

Lower limit of thermal resistance  $R_{\text{tot,lower}} = 4,811 \text{ m}^2\text{K}/\text{W}$ .

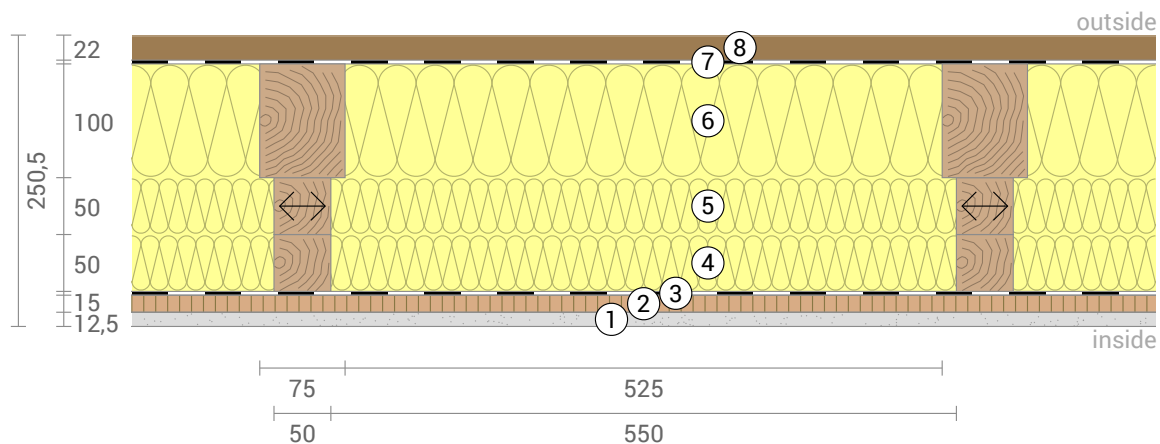
Check applicability:  $R_{\text{tot,upper}} / R_{\text{tot,lower}} = 1,103$  (maximum allowed: 1,5)

The procedure may be used.

Thermal resistance  $R_{\text{tot}} = (R_{\text{tot,upper}} + R_{\text{tot,lower}})/2 = 5,059 \text{ m}^2\text{K}/\text{W}$

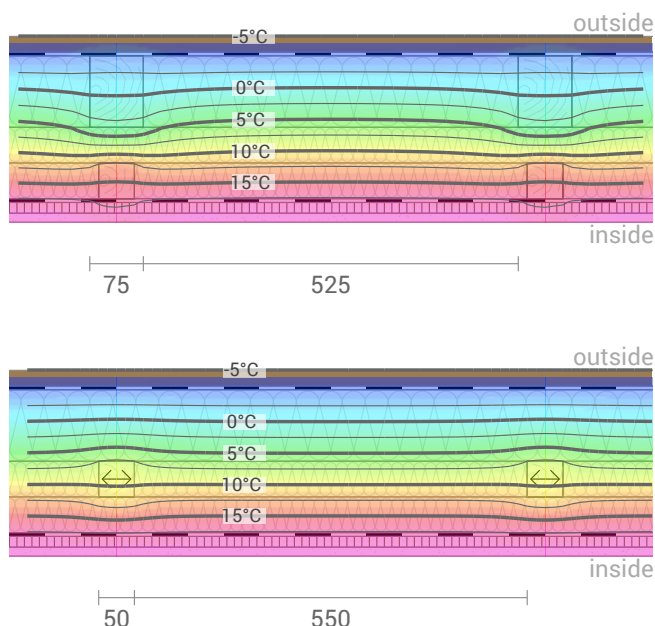
Estimated maximum relative uncertainty according to section 6.7.2.5: 4,9%

Heat transfer coefficient  $U = 1/R_{\text{tot}} = 0,20 \text{ W}/(\text{m}^2\text{K})$



Wall, U=0,198 W/(m²K)

## Temperature profile



Top left: Temperature profile in the blue section (see right illustration). Bottom left: Temperature profile in the green section.

## Layers (from inside to outside)

#	Material	$\lambda$ [W/mK]	R [m²K/W]	Temperatur [°C]		Weight [kg/m²]
				min	max	
	Thermal contact resistance*		0,250	18,4	20,0	
1	1,25 cm Plasterboard (12,5mm)	0,210	0,060	18,0	19,0	9,9
2	1,5 cm OSB	0,130	0,115	17,1	18,7	9,8
3	0,05 cm STEICOmulti renova	0,170	0,003	17,0	18,2	0,1
4	5 cm STEICOflex 036	0,036	1,389	12,0	18,2	2,8
	5 cm Vertical batten (8,3%)	0,130	0,385	13,5	17,3	1,9
5	5 cm STEICOflex 036	0,036	1,389	3,4	13,5	2,8
	5 cm Horizontal batten (8,3%)	0,130	0,385			1,9
6	10 cm STEICOflex 036	0,036	2,778	-4,5	6,8	5,3
	10 cm Existing Stud (12%)	0,130	0,769	-4,0	4,0	5,6
7	0,05 cm STEICOmulti UDB	0,170	0,003	-4,5	-3,9	0,2
8	2,2 cm Horizontal feather edge	0,260	0,085	-4,8	-3,9	3,9
	Thermal contact resistance*		0,040	-5,0	-4,7	
	25,05 cm Whole component		5,059			43,9

\*Thermal contact resistances according to DIN 4108-3 for moisture protection and temperature profile. The values for the U-value calculation can be found on the page 'U-value calculation'.

Surface temperature inside (min / average / max): 18,4°C 18,8°C 19,0°C  
 Surface temperature outside (min / average / max): -4,8°C -4,8°C -4,7°C

Wall,  $U=0,198 \text{ W}/(\text{m}^2\text{K})$

## Moisture proofing

For the calculation of the amount of condensation water, the component was exposed to the following constant climate for 90 days: inside: 20°C und 50% Humidity; outside: -5°C und 80% Humidity. This climate complies with DIN 4108-3.

This component is free of condensate under the given climate conditions.

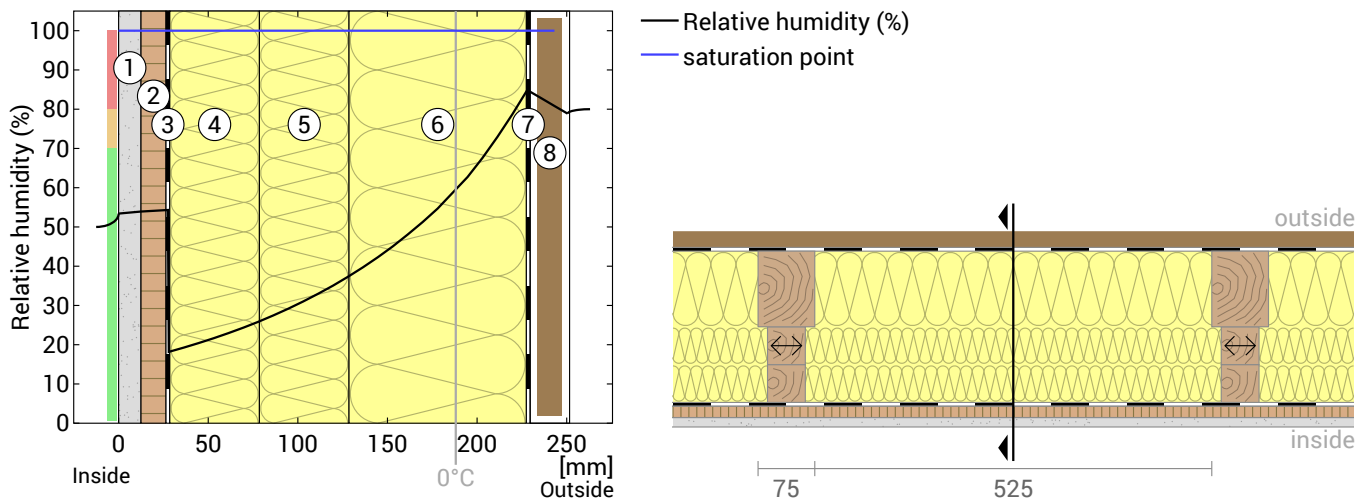
Drying reserve according to DIN 4108-3:2018: 1405 g/(m<sup>2</sup>a)  
 At least required by DIN 68800-2: 100 g/(m<sup>2</sup>a)

#	Material	sd-value [m]	Condensate [kg/m <sup>2</sup> ] [Gew.-%]	Weight [kg/m <sup>2</sup> ]
1	1,25 cm Plasterboard (12,5mm)	0,10	-	9,9
2	1,5 cm OSB	0,45	-	9,8
3	0,05 cm STEICOmulti renova	13,00	-	0,1
4	5 cm STEICOflex 036	0,10	-	2,8
	5 cm Vertical batten (8,3%)	1,00	-	1,9
5	5 cm STEICOflex 036	0,10	-	2,8
	5 cm Horizontal batten (8,3%)	-	-	1,9
6	10 cm STEICOflex 036	0,20	-	5,3
	10 cm Existing Stud (12%)	5,00	-	5,6
7	0,05 cm STEICOmulti UDB	0,02	-	0,2
8	2,2 cm Horizontal feather edge	0,55	-	3,9
	25,05 cm Whole component	14,95	0	43,9

## Humidity

The temperature of the inside surface is 18,4 °C leading to a relative humidity on the surface of 55%. Mould formation is not expected under these conditions.

The following figure shows the relative humidity inside the component.



- ① Plasterboard (12,5 mm)
- ④ STEICOflex 036 (50 mm)
- ⑦ STEICOmulti UDB
- ② OSB (15 mm)
- ⑤ STEICOflex 036 (50 mm)
- ⑧ Horizontal feather edge (22 mm)
- ③ STEICOmulti renova
- ⑥ STEICOflex 036 (100 mm)

Layers marked with <-> run parallel to the illustrated cutting plane and were not taken into account in the moisture protection calculation.

Notes: Calculation using the Ubakus 2D-FE method. Convection and the capillarity of the building materials were not considered. The drying time may take longer under unfavorable conditions (shading, damp / cool summers) than calculated here.

Wall,  $U=0,198 \text{ W}/(\text{m}^2\text{K})$

## Moisture protection in accordance with DIN 4108-3:2018 Appendix A

This moisture proofing is only valid for **non-air-conditioned** residential buildings.

Please note the hints at the end of these moisture proofing calculations.

#	Material	$\lambda$ [W/mK]	R [m <sup>2</sup> K/W]	sd [m]	$\rho$ [kg/m <sup>3</sup> ]	T [°C]	ps [Pa]	$\Sigma$ sd [m]
Thermal contact resistance			0,250			18,98	2193	0
1	1,25 cm Plasterboard (12,5mm)	0,210	0,060	0,1	790	18,73	2161	0,1
2	1,5 cm OSB	0,130	0,115	0,45	650	18,26	2098	0,55
3	0,05 cm STEICOmultiprenova	0,170	0,003	13	220	18,25	2096	13,6
4	5 cm STEICOflex 036	0,036	1,389	0,1	60	12,57	1456	13,7
5	5 cm STEICOflex 036	0,036	1,389	0,1	60	6,89	993	13,8
6	10 cm STEICOflex 036	0,036	2,778	0,2	60	-4,48	420	13,9
7	0,05 cm STEICOmultiprenova UDB	0,170	0,003	0,1	340	-4,49	419	14
8	2,2 cm Horizontal feather edge	0,260	0,085	0,55	175	-4,84	407	14,6
Thermal contact resistance			0,040					

Temperature (T), vapor saturation pressure (ps), and the sum of the sd-values ( $\Sigma$ sd) apply to the layer boundary.

### Relative air humidity on the surface

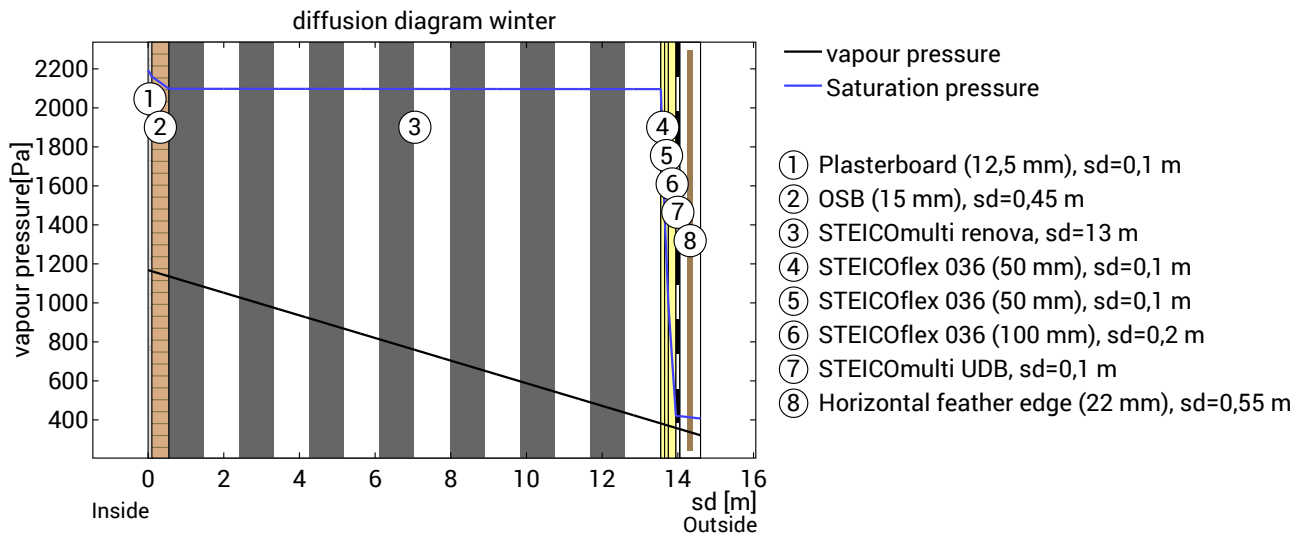
The relative humidity on the interior surface is 53%. Requirements for the prevention of building material corrosion depend on material and coating and have not been investigated.



### Dew period (winter)

#### Boundary conditions

Vapor pressure inside at 20°C and 50% humidity	$p_i = 1168 \text{ Pa}$
Vapor pressure outside at -5°C and 80% humidity	$p_e = 321 \text{ Pa}$
Duration of condensation period (90 days)	$t_c = 7776000 \text{ s}$
Water vapor diffusion coefficient in static air	$\delta_0 = 2.0E-10 \text{ kg}/(\text{m}^2\text{sPa})$
sd-value (Whole component.)	$s_{de} = 14,6 \text{ m}$



The section under investigation is free of condensate under the given climate conditions.



Calculate evaporation potential for the drying reserve in the dew period for the plane with the lowest evaporation potential:

$s_d=13,95 \text{ m}$ ;  $x=22,8 \text{ cm}$ ;  $p_s=420 \text{ Pa}$ :

Layer boundary between STEICOflex 036 and STEICOmultiprenova UDB

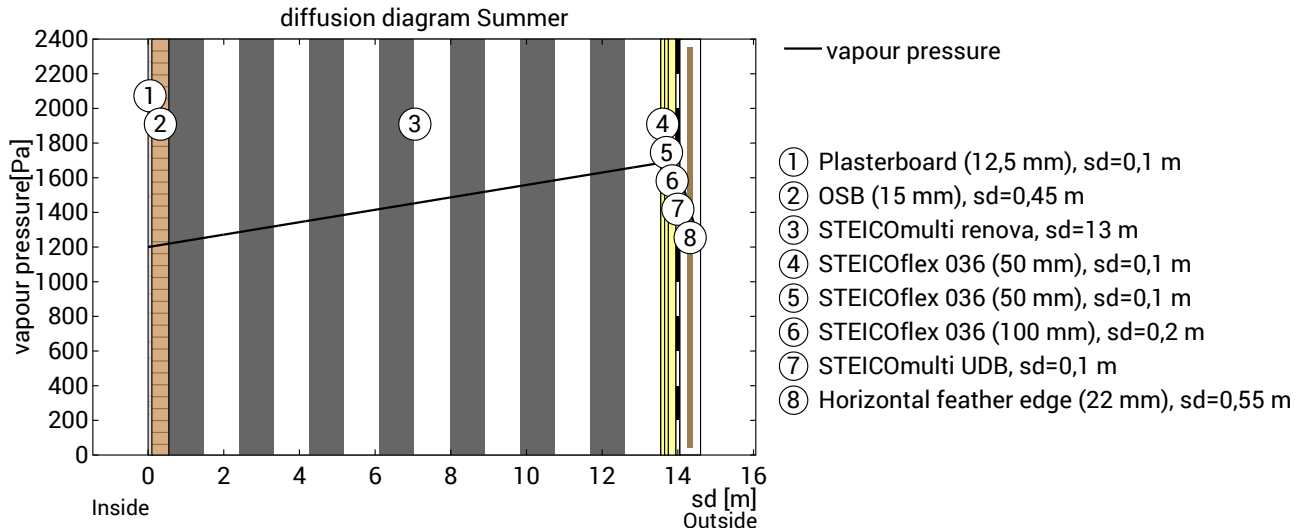
$$M_{ev, \text{Tauperiode}} = t_c \cdot \delta_0 \cdot ((p_s - p_i) / s_{d_{ev}} + (p_s - p_e) / (s_{d_e} - s_{d_{ev}})) = 0,153 \text{ kg/m}^2$$

Wall,  $U=0,198 \text{ W}/(\text{m}^2\text{K})$

Evaporation period (summer)

#### Boundary conditions

Interior vapor pressure	$p_i = 1200 \text{ Pa}$
Exterior vapor pressure	$p_e = 1200 \text{ Pa}$
Saturation vapour pressure in the condensation area	$p_s = 1700 \text{ Pa}$
Length of drying season (90 days)	$t_{ev} = 7776000 \text{ s}$
sd-values remain unchanged.	



Condensate-free component: The maximum possible evaporation mass for the drying reserve is calculated. Consider the level that has the lowest evaporation potential in the dew period, at  $sd=13,95 \text{ m}$ ;  $x=22,8 \text{ cm}$ :

Layer boundary between STEICOflex 036 and STEICOMulti UDB

Evaporation mass:  $M_{ev} = \delta_0 \cdot t_{ev} \cdot [(p_s - p_i)/sd + (p_s - p_e)/(s_{de} - sd)] = 1,25 \text{ kg}/\text{m}^2$

#### Drying reserve (DIN 68800-2)

Dew-water-free component: The evaporation potential of the dew period is also taken into account.

Drying reserve:  $M_r = (M_{ev} + M_{ev, Tauperiode}) \cdot 1000 = 1405 \text{ g}/\text{m}^2/\text{a}$

Minimum requested for walls and ceilings:  $100 \text{ g}/\text{m}^2/\text{a}$



#### Evaluation according to DIN 4108-3

The component is permissible regarding the moisture protection.

#### Hints

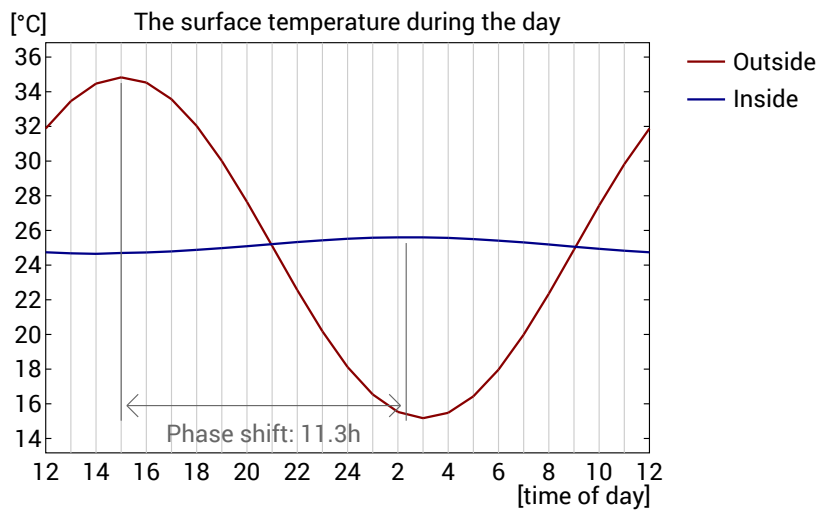
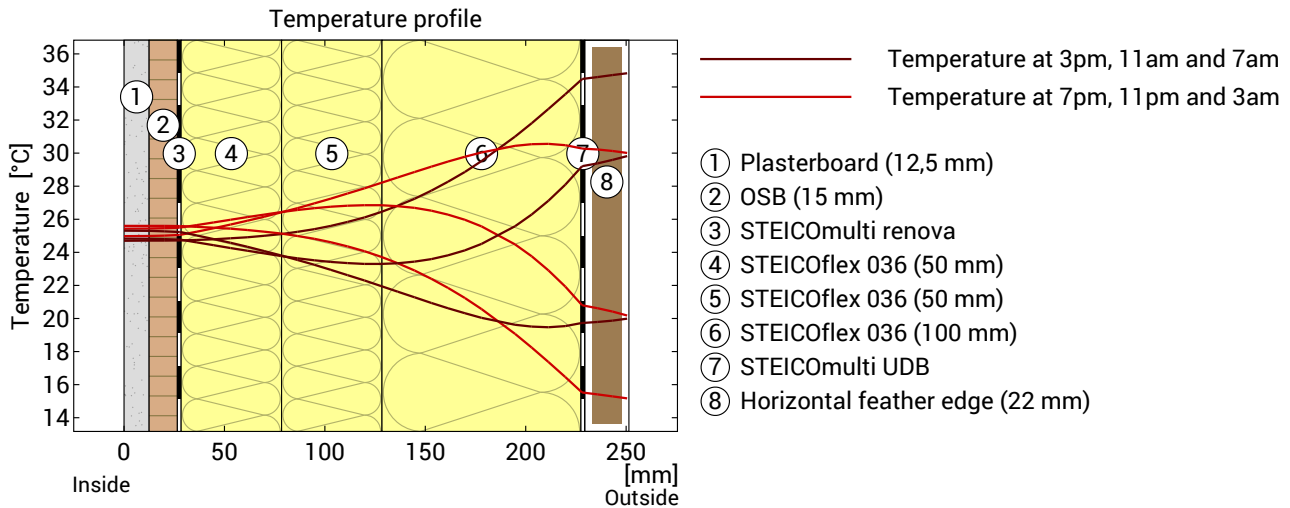
In the case of inhomogeneous constructions, such as skeleton-, stand- or frame constructions, as well as in wooden beam, rafter or half-timbered constructions or the like, the one-dimensional diffusion calculations are only to be demonstrated for the compartment area. Exceptional cases are special constructions in which, for example, The diffusion-inhibiting layer is also laid section-wise over the outer area. In these exceptional cases, the calculation performed here is invalid.

DIN 4108-3 describes in Section 5.3 components for which no moisture proofing is required as there is no risk of condensation water or the method is not suitable for the assessment. It is not possible to assess whether the component under test is underneath.

Wall,  $U=0,198 \text{ W}/(\text{m}^2\text{K})$

## Heat protection

The following results are properties of the tested component alone and do not make any statement about the heat protection of the entire room:



**Top:** Temperature profile within the component at different times. From top to bottom, brown lines: at 3 pm, 11 am and 7 am and red lines at 7 pm, 11 pm and 3 am.

**Bottom:** Temperature on the outer ( red ) and inner ( blue ) surface in the course of a day. The arrows indicate the location of the temperature maximum values. The maximum of the inner surface temperature should preferably occur during the second half of the night.

Phase shift*	11,3 h	Heat storage capacity (whole component):	68 kJ/m <sup>2</sup> K
Amplitude attenuation **	20,4	Thermal capacity of inner layers:	41 kJ/m <sup>2</sup> K
TAV ***	0,049		

\* The phase shift is the time in hours after which the temperature peak of the afternoon reaches the component interior.

\*\* The amplitude attenuation describes the attenuation of the temperature wave when passing through the component. A value of 10 means that the temperature on the outside varies 10x stronger than on the inside, e.g. outside 15-35 °C, inside 24-26 °C.

\*\*\* The temperature amplitude ratio TAV is the reciprocal of the attenuation:  $TAV = 1 / \text{amplitude attenuation}$

Note: The heat protection of a room is influenced by several factors, but essentially by the direct solar radiation through windows and the total amount of heat storage capacity (including floor, interior walls and furniture). A single component usually has only a very small influence on the heat protection of the room.

The calculations presented above have been created for a 1-dimensional cross-section of the component.



## Roof

Roof construction

### Thermal protection

$U = 0,209 \text{ W}/(\text{m}^2\text{K})$

GEG 2020 Bestand\*:  $U < 0,24 \text{ W}/(\text{m}^2\text{K})$



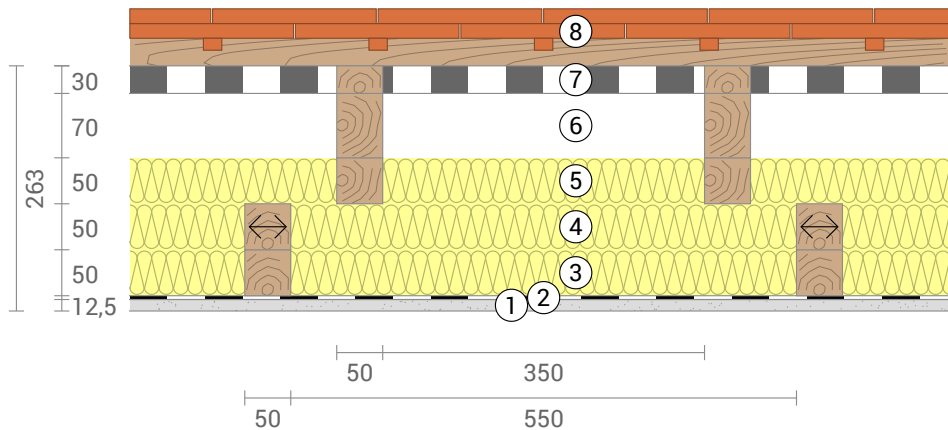
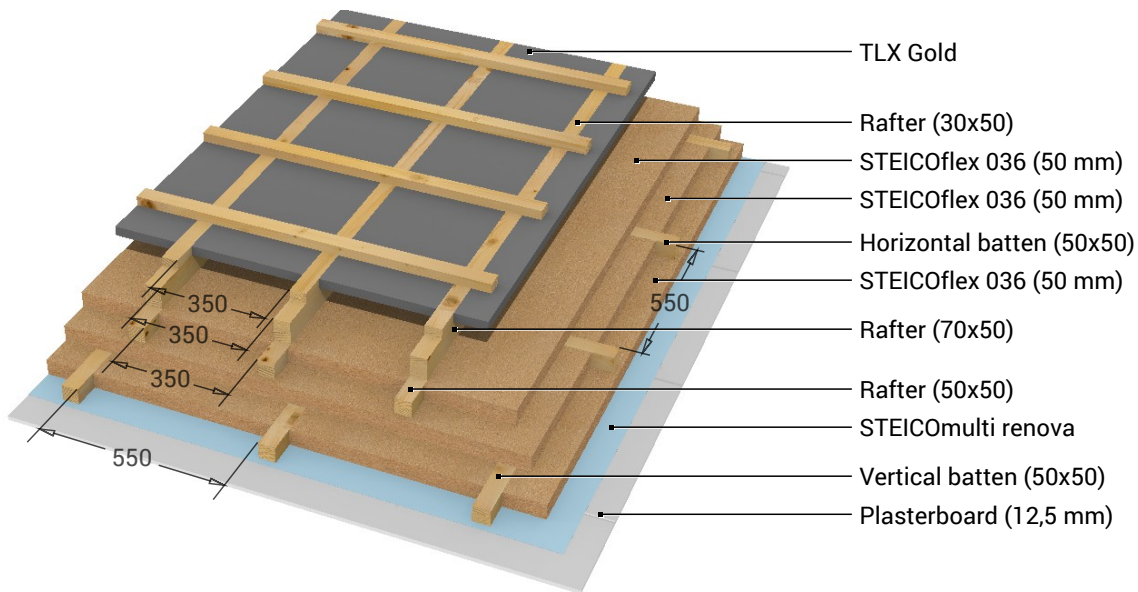
### Moisture proofing

Drying reserve:  $1877 \text{ g}/\text{m}^2\text{a}$   
No condensate



### Heat protection

Temperature amplitude damping: 11  
phase shift: 12,2 h  
Thermal capacity inside:  $29 \text{ kJ}/\text{m}^2\text{K}$



- |                          |                          |                              |
|--------------------------|--------------------------|------------------------------|
| ① Plasterboard (12,5 mm) | ④ STEICOflex 036 (50 mm) | ⑦ TLX Gold                   |
| ② STEICOmulti renova     | ⑤ STEICOflex 036 (50 mm) | ⑧ Slates and battens (75 mm) |
| ③ STEICOflex 036 (50 mm) | ⑥ Stationary air (70 mm) |                              |

<-> Layers marked by arrows are perpendicular to the main axis.

Roof, U=0,209 W/(m<sup>2</sup>K)

Inside air : 20,0°C / 50%

Outside air: -5,0°C / 80%

Surface temperature.: 18,5°C / -4,8°C

sd-value: 14,4 m

Drying reserve: 1877 g/m<sup>2</sup>a

Thickness: 33,8 cm

Weight: 119 kg/m<sup>2</sup>

Heat capacity: 121 kJ/m<sup>2</sup>K

GEG 2020 Bestand

BEG Einzelmaßn.

GEG 2020 Neubau

DIN 4108

Roof,  $U=0,209 \text{ W}/(\text{m}^2\text{K})$

## U-Value calculation according to DIN EN ISO 6946

#	Material	Dicke [cm]	$\lambda$ [W/mK]	R [m <sup>2</sup> K/W]
Thermal contact resistance inside (Rsi)				0,100
1	Plasterboard (12,5mm)	1,25	0,210	0,060
2	STEICOMulti renova	0,05	0,170	0,003
3	STEICOflex 036	5,00	0,036	1,389
	Vertical batten (8,3%)	5,00	0,130	0,385
4	STEICOflex 036	5,00	0,036	1,389
	Horizontal batten (8,3%)	5,00	0,130	0,385
5	STEICOflex 036	5,00	0,036	1,389
	Rafter (12%)	5,00	0,130	0,385
6	Stationary air (unventilated)	7,00	0,357	0,196
	Rafter (12%)	7,00	0,130	0,538
7	TLX Gold	3,00	0,036	0,845
	Rafter (12%)	3,00	0,130	0,231
8	Slates and battens	7,50	0,750	0,100
Thermal contact resistance outside (Rse)				0,040

Thermal contact resistances have been taken from DIN 6946 Table 7.

Rsi: heat flow direction upwards

Rse: heat flow direction upwards, outside: Direct contact to outside air

Thermal transfer resistances of resting air layers were calculated as follows:

Layer 6.1: Thickness 7 cm, Width 35 cm, DIN EN ISO 6946 Appendix D.4, heat flow direction 45° upwards, Temperature ca. -0°C, Emissionsgrad der Oberflächen: 0,9

Upper limit of thermal resistance  $R_{\text{tot;upper}} = 5,114 \text{ m}^2\text{K}/\text{W}$ .

Lower limit of thermal resistance  $R_{\text{tot;lower}} = 4,478 \text{ m}^2\text{K}/\text{W}$ .

Check applicability:  $R_{\text{tot;upper}} / R_{\text{tot;lower}} = 1,142$  (maximum allowed: 1,5)

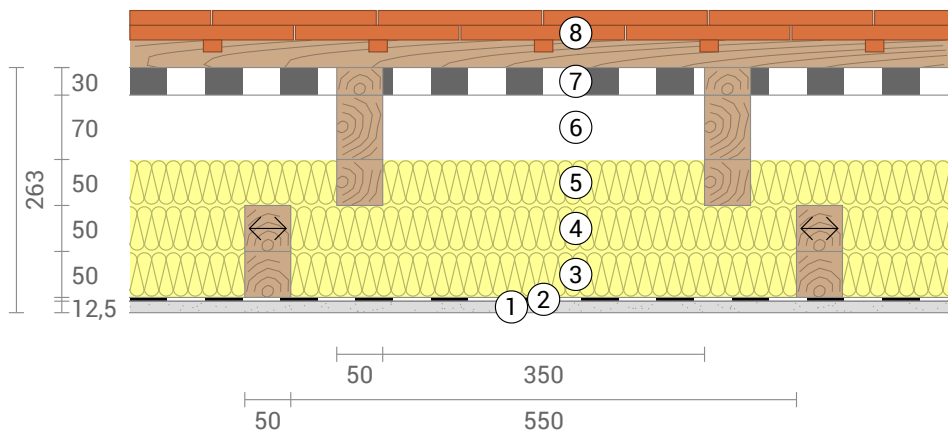
The procedure may be used.

Thermal resistance  $R_{\text{tot}} = (R_{\text{tot;upper}} + R_{\text{tot;lower}})/2 = 4,796 \text{ m}^2\text{K}/\text{W}$

Estimated maximum relative uncertainty according to section 6.7.2.5: 6,6%

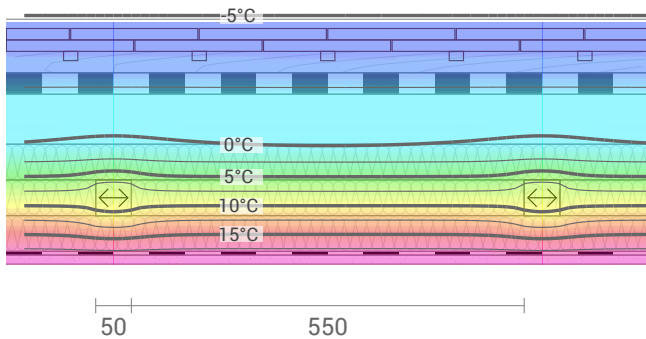
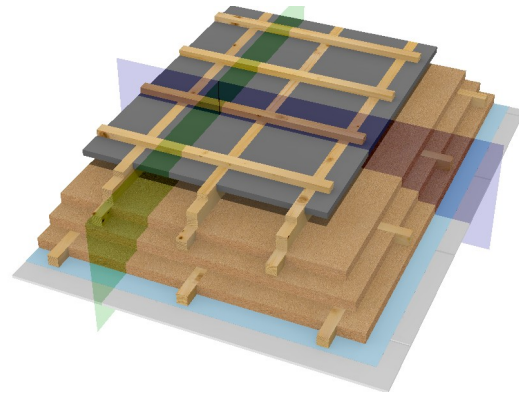
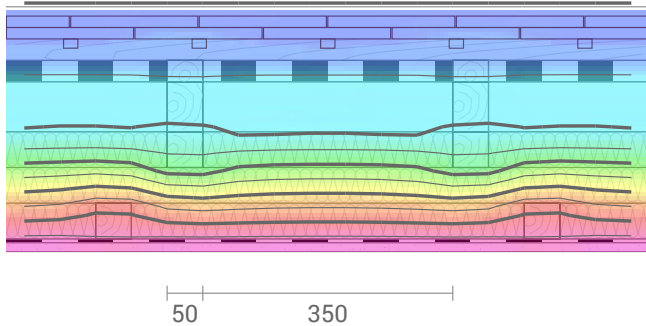
Heat transfer coefficient  $U = 1/R_{\text{tot}} = 0,21 \text{ W}/(\text{m}^2\text{K})$

This component includes several inhomogeneous layers of different overall width. For all the calculations it was assumed that the layer arrangement is repeated in width all 60 cm. This, however, is not true for at least layer 5 with a total width of 40 cm and can cause increased inaccuracy of the U-value.



Roof, U=0,209 W/(m²K)

## Temperature profile



Top left: Temperature profile in the blue section (see right illustration). Bottom left: Temperature profile in the green section.

## Layers (from inside to outside)

#	Material	$\lambda$ [W/mK]	R [m²K/W]	Temperatur [°C]		Weight [kg/m²]
				min	max	
	Thermal contact resistance*		0,250	18,5	20,0	
1	1,25 cm Plasterboard (12,5mm)	0,210	0,060	18,1	18,9	9,9
2	0,05 cm STEICOmulti renova	0,170	0,003	18,1	18,6	0,1
3	5 cm STEICOflex 036	0,036	1,389	11,5	18,6	2,8
4	5 cm Vertical batten (8,3%)	0,130	0,385	14,3	18,1	1,9
	5 cm STEICOflex 036	0,036	1,389	3,7	14,3	2,8
5	5 cm Horizontal batten (8,3%)	0,130	0,385			1,9
	5 cm STEICOflex 036	0,036	1,389	-0,1	6,9	2,6
6	5 cm Rafter (12%)	0,130	0,385	0,6	4,2	2,8
	7 cm Stationary air (unventilated)	0,357	0,196	-1,5	0,4	0,1
7	7 cm Rafter (12%)	0,130	0,538	-2,0	0,6	3,9
	3 cm TLX Gold	0,036	0,845	-4,4	-0,8	18,4
8	3 cm Rafter (12%)	0,130	0,231	-4,1	-1,4	1,7
	7,5 cm Slates and battens	0,750	0,100	-4,8	-4,1	70,0
	Thermal contact resistance*		0,040	-5,0	-4,8	
	33,8 cm Whole component		4,796			118,7

\*Thermal contact resistances according to DIN 4108-3 for moisture protection and temperature profile. The values for the U-value calculation can be found on the page 'U-value calculation'.

Surface temperature inside (min / average / max): 18,5°C 18,8°C 18,9°C  
 Surface temperature outside (min / average / max): -4,8°C -4,8°C -4,8°C

Roof, U=0,209 W/(m²K)

## Moisture proofing

For the calculation of the amount of condensation water, the component was exposed to the following constant climate for 90 days: inside: 20°C und 50% Humidity; outside: -5°C und 80% Humidity. This climate complies with DIN 4108-3.

This component is free of condensate under the given climate conditions.

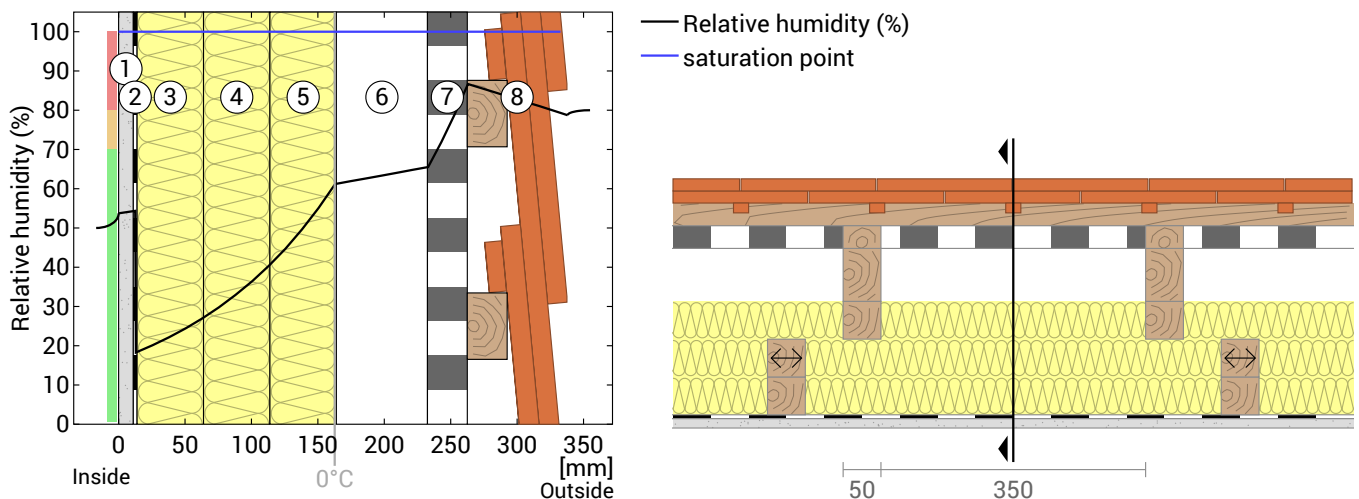
Drying reserve according to DIN 4108-3:2018: 1877 g/(m²a)  
At least required by DIN 68800-2: 250 g/(m²a)

#	Material	sd-value [m]	Condensate [kg/m²] [Gew.-%]	Weight [kg/m²]
1	1,25 cm Plasterboard (12,5mm)	0,10	-	9,9
2	0,05 cm STEICOmulti renova	13,00	-	0,1
3	5 cm STEICOflex 036	0,10	-	2,8
	5 cm Vertical batten (8,3%)	1,00	-	1,9
4	5 cm STEICOflex 036	0,10	-	2,8
	5 cm Horizontal batten (8,3%)	-	-	1,9
5	5 cm STEICOflex 036	0,10	-	2,6
	5 cm Rafter (12%)	1,00	-	2,8
6	7 cm Stationary air (unventilated)	0,01	-	0,1
	7 cm Rafter (12%)	3,50	-	3,9
7	3 cm TLX Gold	0,09	-	18,4
	3 cm Rafter (12%)	1,50	-	1,7
8	7,5 cm Slates and battens	0,75	-	70,0
	33,8 cm Whole component	14,39	0	118,7

## Humidity

The temperature of the inside surface is 18,5 °C leading to a relative humidity on the surface of 55%.Mould formation is not expected under these conditions.

The following figure shows the relative humidity inside the component.



- ① Plasterboard (12,5 mm)
- ④ STEICOflex 036 (50 mm)
- ⑦ TLX Gold
- ② STEICOmulti renova
- ⑤ STEICOflex 036 (50 mm)
- ⑧ Slates and battens (75 mm)
- ③ STEICOflex 036 (50 mm)
- ⑥ Stationary air (70 mm)

Layers marked with <-> run parallel to the illustrated cutting plane and were not taken into account in the moisture protection calculation.

Notes: Calculation using the Ubakus 2D-FE method. Convection and the capillarity of the building materials were not considered. The drying time may take longer under unfavorable conditions (shading, damp / cool summers) than calculated here.

Roof,  $U=0,209 \text{ W}/(\text{m}^2\text{K})$

## Moisture protection in accordance with DIN 4108-3:2018 Appendix A

This moisture proofing is only valid for **non-air-conditioned** residential buildings.

In the case of roof structures with **tile coverings and wooden gratings**, this standard may not be applied. Whether this construction falls under it, is to be examined by the planner.

Please note the hints at the end of these moisture proofing calculations.

#	Material	$\lambda$ [W/mK]	R [m <sup>2</sup> K/W]	sd [m]	$\rho$ [kg/m <sup>3</sup> ]	T [°C]	ps [Pa]	$\Sigma$ sd [m]
Thermal contact resistance			0,250			18,90	2182	0
1	1,25 cm Plasterboard (12,5mm)	0,210	0,060	0,1	790	18,63	2147	0,1
2	0,05 cm STEICOMulti renova	0,170	0,003	13	220	18,62	2145	13,1
3	5 cm STEICOflex 036	0,036	1,389	0,1	60	12,49	1448	13,2
4	5 cm STEICOflex 036	0,036	1,389	0,1	60	6,35	958	13,3
5	5 cm STEICOflex 036	0,036	1,389	0,1	60	0,22	621	13,4
6	7 cm Stationary air (unventilated)	0,357	0,196	0,01	1	-0,65	579	13,4
7	3 cm TLX Gold	0,036	0,845	0	700	-4,38	423	13,4
8	7,5 cm Slates and battens	0,750	0,100	0,75	933	-4,82	407	14,2
Thermal contact resistance			0,040					

Temperature (T), vapor saturation pressure (ps), and the sum of the sd-values ( $\Sigma$ sd) apply to the layer boundary.

### Relative air humidity on the surface

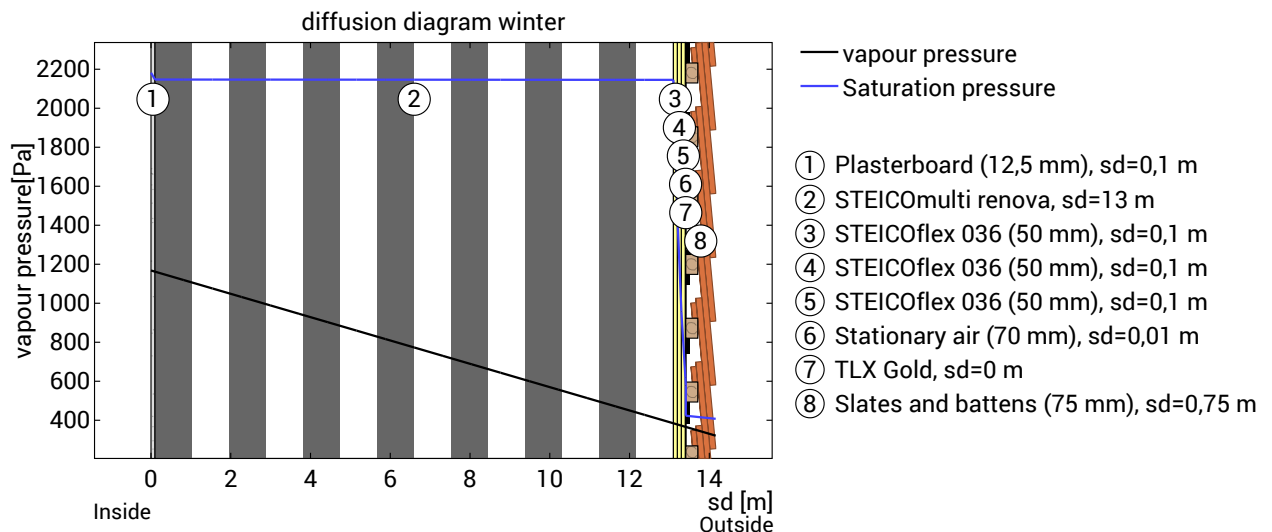
The relative humidity on the interior surface is 54%. Requirements for the prevention of building material corrosion depend on material and coating and have not been investigated.



### Dew period (winter)

#### Boundary conditions

Vapor pressure inside at 20°C and 50% humidity	$p_i = 1168 \text{ Pa}$
Vapor pressure outside at -5°C and 80% humidity	$p_e = 321 \text{ Pa}$
Duration of condensation period (90 days)	$t_c = 7776000 \text{ s}$
Water vapor diffusion coefficient in static air	$\delta_0 = 2.0\text{E-}10 \text{ kg}/(\text{m}^*\text{s}*\text{Pa})$
sd-value (Whole component.)	$s_{de} = 14,16 \text{ m}$



The section under investigation is free of condensate under the given climate conditions.



Roof,  $U=0,209 \text{ W}/(\text{m}^2\text{K})$

Calculate evaporation potential for the drying reserve in the dew period for the plane with the lowest evaporation potential:

$s_d=13,41 \text{ m}$ ;  $x=26,3 \text{ cm}$ ;  $p_s=423 \text{ pa}$ :

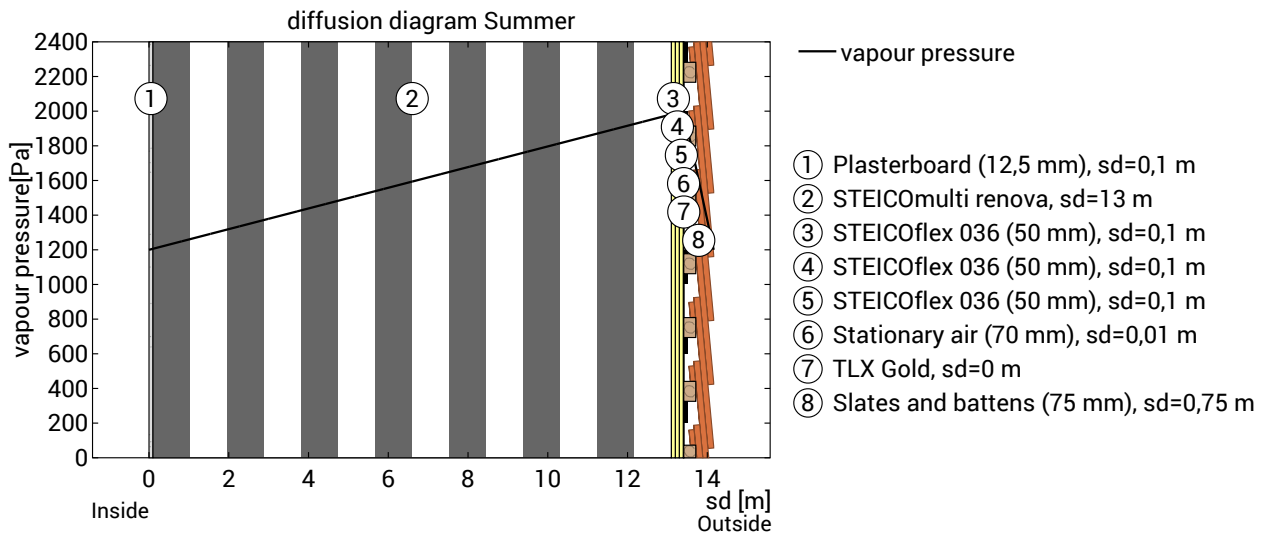
Layer boundary between TLX Gold and Slates and battens

$$M_{ev, \text{Tauperiode}} = t_c * \delta_0 * ((p_s - p_i) / s_{d_{ev}} + (p_s - p_e) / (s_{d_e} - s_{d_{ev}})) = \mathbf{0,126 \text{ kg/m}^2}$$

Evaporation period (summer)

#### Boundary conditions

Interior vapor pressure	$p_i = 1200 \text{ Pa}$
Exterior vapor pressure	$p_e = 1200 \text{ Pa}$
Saturation vapour pressure in the condensation area	$p_s = 2000 \text{ Pa}$ (Roof against outside air)
Length of drying season (90 days)	$t_{ev} = 7776000 \text{ s}$
sd-values remain unchanged.	



Condensate-free component: The maximum possible evaporation mass for the drying reserve is calculated. Consider the level that has the lowest evaporation potential in the dew period, at  $s_d=13,41 \text{ m}$ ;  $x=26,3 \text{ cm}$ :

Layer boundary between TLX Gold and Slates and battens

$$\text{Evaporation mass: } M_{ev} = \delta_0 * t_{ev} * [(p_s - p_i) / s_d + (p_s - p_e) / (s_{d_e} - s_d)] = \mathbf{1,75 \text{ kg/m}^2}$$

Drying reserve (DIN 68800-2)

Dew-water-free component: The evaporation potential of the dew period is also taken into account.

$$\text{Drying reserve: } M_r = (M_{ev} + M_{ev, \text{Tauperiode}}) * 1000 = \mathbf{1877 \text{ g/m}^2/\text{a}}$$

Minimum requested for roofs:  $250 \text{ g/m}^2/\text{a}$



Evaluation according to DIN 4108-3

The component is permissible regarding the moisture protection.

#### Hints

In the case of inhomogeneous constructions, such as skeleton-, stand- or frame constructions, as well as in wooden beam, rafter or half-timbered constructions or the like, the one-dimensional diffusion calculations are only to be demonstrated for the compartment area. Exceptional cases are special constructions in which, for example, The diffusion-inhibiting layer is also laid section-wise over the outer area. In these exceptional cases, the calculation performed here is invalid.

DIN 4108-3 describes in Section 5.3 components for which no moisture proofing is required as there is no risk of condensation water or the method is not suitable for the assessment. It is not possible to assess whether the component under test is underneath.

It is assumed that the roof is not predominantly shaded and does not have a very bright surface (as determined by the user).



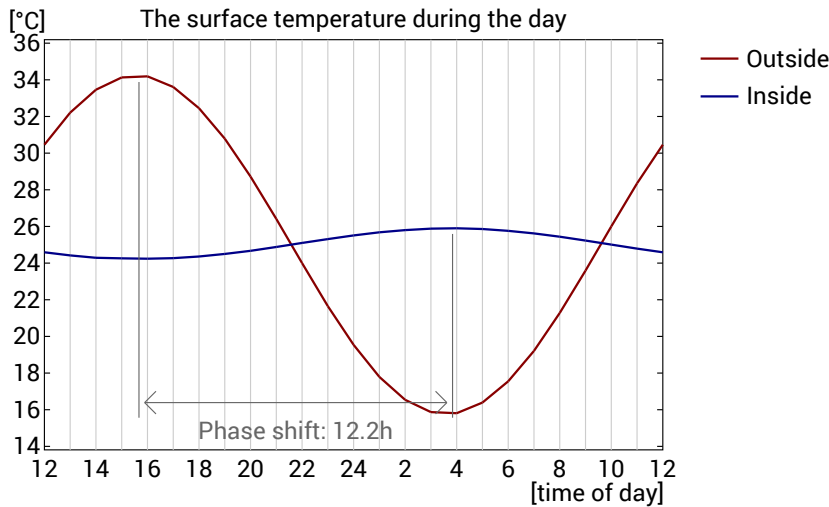
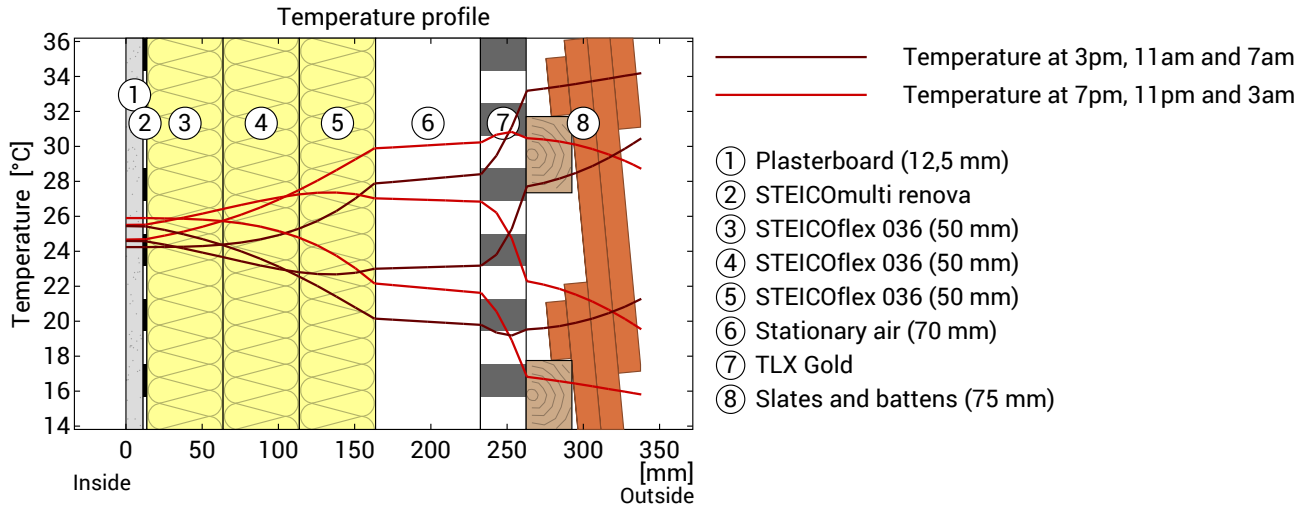
This has a positive effect on the drying capacity.



Roof,  $U=0,209 \text{ W}/(\text{m}^2\text{K})$

## Heat protection

The following results are properties of the tested component alone and do not make any statement about the heat protection of the entire room:



**Top:** Temperature profile within the component at different times. From top to bottom, brown lines: at 3 pm, 11 am and 7 am and red lines at 7 pm, 11 pm and 3 am.

**Bottom:** Temperature on the outer ( red ) and inner ( blue ) surface in the course of a day. The arrows indicate the location of the temperature maximum values. The maximum of the inner surface temperature should preferably occur during the second half of the night.

Phase shift*	12,2 h	Heat storage capacity (whole component):	121 kJ/m <sup>2</sup> K
Amplitude attenuation **	11,0	Thermal capacity of inner layers:	29 kJ/m <sup>2</sup> K
TAV ***	0,091		

\* The phase shift is the time in hours after which the temperature peak of the afternoon reaches the component interior.

\*\* The amplitude attenuation describes the attenuation of the temperature wave when passing through the component. A value of 10 means that the temperature on the outside varies 10x stronger than on the inside, e.g. outside 15-35 °C, inside 24-26 °C.

\*\*\* The temperature amplitude ratio TAV is the reciprocal of the attenuation:  $TAV = 1 / \text{amplitude attenuation}$

Note: The heat protection of a room is influenced by several factors, but essentially by the direct solar radiation through windows and the total amount of heat storage capacity (including floor, interior walls and furniture). A single component usually has only a very small influence on the heat protection of the room.

The calculations presented above have been created for a 1-dimensional cross-section of the component.