

DRAINAGE STRATEGY

LAND OFF HILL HOUSE INDUSTRIAL ESTATE, THORNTON-CLEVELEYS

October 2023

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DOCUMENT ISSUE RECORD

Revision	Date	Details
Full	October 2023	Issued for action

LAND OFF HILL HOUSE INDUSTRIAL ESTATE, THORNTON-CLEVELEYS

Report Approved by D.W.Hadwin B.Eng(Hons) C.Eng MICE For Keystone Design Associates

Signature.....

Date 19th October 2023.....

CONTENTS

- 1. INTRODUCTION
- 2. DESCRIPTION OF DEVELOPMENT
- 3. LOCATION OF SITE
- 4. EXISTING DRAINAGE
- 5. SURFACE WATER DRAINAGE STRATERGY
- 6. SUSTAINABLE DRAINAGE
- 7. PROPOSED DRAINAGE STRATEGY- SURFACE WATER
- 8. PROPOSED DRAINAGE STRATEGY -FOUL WATER
- 9. CONCLUSIONS
- 10. APPENDICES

1.0 INTRODUCTION

- 1.01 It is proposed to develop the existing site to accommodate an industrial unit on the site at land off Hill House Industrial Estate, Thornton-Cleveleys.
- 1.02 The works for the development would comprise the building of the industrial unit and installation of the new infrastructure, of which the drainage would be material. This report discusses the proposed strategy for the disposal of both foul and surface water.
- 1.03 This report is intended to provide supporting information for the consent of planning permission.

2.0 DESCRIPTION OF DEVELOPMENT

- 2.01 The development site is currently a brownfield site adjacent to Hill House Industrial Estate, Thornton-Cleveleys. The site is surrounded by land to the north and east, commercial/industrial buildings to the south and a residential development to the west.
- 2.02 The proposal is for the development of the site to accommodate an industrial unit.
- 2.03 The necessary infrastructure to cater for the industrial unit will need to be installed, this being drainage.
- 2.04 The drawing attached to appendix C as supplied by this office illustrates the proposed scheme.

3.0 LOCATION OF SITE

- 3.01 The site is located adjacent to Hill House Industrial Estate, Thornton-Cleveleys. The site is identified on the location plan at as appendix A.
- 3.02 The proposed site is surrounded by land to the north and east, commercial/industrial buildings to the south and a residential development to the west. The site is situated in Thornton-Cleveleys, in the borough of Wyre, approximately 4 miles north of Blackpool and 2 miles south of Fleetwood.
- 3.03 The site is located in a flood zone 2/3.
- 3.04 The ordnance survey grid reference is SD N444150, E334107.
- 3.05 The site is 0.42Ha area.

4.0 EXISTING DRAINAGE

- 4.01 No drainage was found on site. There is a dyke located to the east of the site. For the purpose of surface water drainage calculations the site will be treated as greenfield.
- 4.02 It is proposed to connect to a water treatment plant and dyke as shown on the drawing attached to appendix C.

5.0 SURFACE WATER DRAINAGE STRATEGY

- 5.01 The primary flood risk generated by a development is the surface water runoff. The proposed development will increase the amount of surface water discharge; to comply with the planning condition the surface water will be attenuated within the site boundary.
- 5.02 The surface water drainage for any development site should be designed so that the volumes and peak flow rates of surface water leaving the site are limited to the original greenfield rates.
- 5.03 In order to comply with not increasing volume of discharge as a consequence of the development it will be necessary to provide surface water storage and/or infiltration to limit and reduce both the peak rate of discharge from the site.
- 5.04 The Environment Agency require that, for the range of annual flow rate probabilities, up to and including the 1% annual probability (1 in 100 year event) the developed rate of run-off into a watercourse should be no greater than the undeveloped rate of run-off for the same event. Water Authorities take a similar approach to that of the Environment Agency, however they ask that flows be restricted to include up to the 3.33% annual probability (1 in 30 year event), whilst demonstrating that the 1 in 100 year event does not pose a threat to the locality (known as designing for exceedance).
- 5.05 Climate change (CC) will be taken into account by increasing the rainfall intensity by 40% in compliance with DEFRA technical standards.

6.0 SUSTAINABLE DRAINAGE

- 6.01 The Technical Guidance for the National Planning Policy Framework requires that a development exceeding 0.4Ha or more than 4 dwellings requires that the management of the surface water runoff utilises Sustainable Urban Drainage (SUDS) and considers the hierarchy of provision which are as follows
 - Infiltration to ground soakaways and permeable surfacing.
 - Discharge to local watercourse.
 - Discharge to public sewer.
 - Discharge to adjacent land drains and ponds.
- 6.02 The first option to be considered for surface water disposal for all proposed development must be infiltration into the ground. Even when there are alternative sewer connections or watercourses available infiltration must still be utilised unless it is proved unfeasible. The suitability for infiltration is determined by a percolation test. Where the underlying soil conditions are relatively impermeable, or the water table is high the site would not be suitable for ground infiltration and discharge to a water course or sewer may be considered.
- 6.03 The sub soil in this area is firm to stiff clay close to the surface. The water table is also close to the ground surface. These ground conditions are not suitable for ground infiltration.
- 6.04 As discharge to the ground is not appropriate, the next level of of SuDs is to be considered. The dyke to the east of the site is a watercourse as defined in the SuDs Manual 2015. It is proposed to discharge surface water to the watercourse.
- 6.05 In order to prevent an increase in flood risk to adjacent land and downstream of the site it will be necessary to restrict the surface water discharge from the development to the equivalent QBAR greenfield run-off rate from the site (mean annual greenfield peak flow). The SuDS Manual recommends the use of Report No.124 'Flood estimation for small catchments', Institute of Hydrology for catchments smaller than 50 hectares. The total site area of the development site 0.42 ha.
- 6.06 The Environment Agency standard advice is to calculate the existing greenfield run-off from the entire developable site. The calculated QBAR rate is 1.05 l/s, which is the maximum final discharge rate that should not be exceeded.
- 6.07 When calculating the final allowable discharge rate only the impermeable areas are considered. The other areas of the site which include landscaping and porous pavement will not contribute to the surface water run-off. The total area of impermeable surfacing is the whole site. Existing greenfield run-off rates are calculated at 0.92l/s and the 1 in 30 year event at 1.79l/s and the 1 in 100 year event at 2.19l/s.
- 6.08 Surface water flows from the site are to be restricted to the equivalent QBAR rate of 5.0l/s. This is greater than the calculated 1.05l/s as a practicable minimum limit on the discharge rate from a flow attenuation device is often a compromise between attenuating to a satisfactorily low flow rate while keeping the risk of blockage to an acceptable level. This limit is therefore set at 5 litres per second.

- 6.09 The Draft National Standards for Sustainable drainage systems covers the whole range of sustainable approaches to surface water drainage management including:
 - source control measures including rainwater recycling and drainage.
 - infiltration devices to allow water to soak into ground, that can include individual soakaways and communal facilities.
 - filter strips and swales, which are vegetated features that hold and drain water downhill mimicking natural drainage patterns.
 - filter drains and porous pavements to allow rainwater and run-off to infiltrate into permeable material below ground and provide storage if needed.
 - basins and ponds to hold excess water after rain and allow controlled discharge that avoids flooding, and
 - Underground storage to hold excess water after rain and allow controlled discharge that avoids flooding.
- 6.10 These SuDS solutions are considered below with reference to their suitability for the proposed development.

SuDS Group	Technique	Likely to be suitable?	Notes
Source Control	Rainwater Harvesting	Yes	Would not feasibly accommodate the full increase of volume of runoff created by the proposed development but would work alongside any attenuated system Rainwater butts can also be used to reduce run-off and water use.
Infiltration Devices	Permeable Paving	No	The ground sub striate is not suitable for infiltration
	Infiltration trenches and basins	No	Could be used to slow the movement of water down, but not as an effective means of dealing with run-off and The ground sub striate is not suitable for infiltration
Filtration	Soakaways	No	Ground is not suitable for surface water disposal
	Open Swales	No	Use for attenuation, evaporation, water quality and slowing water movement down and will fit with nature of site. Insufficient space to accommodate pond
			Hazardous to site users
	Filter Strips	No	Could be used to slow the movement of water down, but not as an effective means of directly dealing with run-off
Retention/ Detention	Basin / Ponds	No	Suitable for controlling discharge to watercourse via a piped outfall, evaporation and treatment of run-off.
			Insufficient space to accommodate pond
Underground Storage	Culverts / Tanks / Oversized Pipes	Yes	Suitable for controlling discharge to watercourse or sewer via a piped outfall No land take required to accommodate

7.0 PROPOSED DRAINAGE STRATEGY - SURFACE WATER

- 7.01 It is proposed that surface water drainage from the proposed development will be discharged into the water course located to the east of the site via the new proposed manholes.
- 7.02 It is important when designing drainage systems for new developments that a scheme be considered to deal with the first 5mm of rainfall to hit the site. Around 50% of rainfall events are less than 5mm and cause no measurable runoff from greenfield areas into receiving waters. In contrast, runoff from a development takes place for virtually every rainfall event. This difference means that watercourses receive frequent discharges with polluted washoff from urban surfaces (hydrocarbons, suspended solids, metals etc). Replication of the greenfield runoff from small events will result in many fewer polluted discharges so limiting the potentially damaging impact on the receiving environment. This concept is known as interception and the volume of rainfall required to replicate the event known as Interception Storage.
- 7.03 The concept of Interception storage to prevent any runoff from rainfall depths up to 5mm, should therefore be provided. Certain SuDS features such as Swales and Pervious Pavements provide runoff characteristics that reflect this behaviour depending on their design. These will be considered and designed in to the proposed layout at detailed design stage once final volumes are calculated. An estimation of the interception storage requirements for the proposal is included within the calculations below.
- 7.04 Above and beyond the Interception Storage requirements there are the more intense storms to consider. Attenuation will be required within the system to accommodate the volume of surface water created by restricting the outfall rates to the existing 5.0l/s equivalent.
- 7.05 There are a number of options available for attenuating the proposed flows from the development, however it is considered that the storage would be to utilise storm water crates. This solution allows for large quantities of storage at relatively shallow depths.
- 7.06 In calculating the surface water run off the following assumptions have been made:-
 - No infiltration Due to the ground conditions no infiltration is assumed,

however if any could be achieved the volume discharged would be reduced.

- No Rainwater Harvesting / Water Butts Suitably designed rainwater harvesting tanks can significantly reduce the volume of run-off and form an integral part of the attenuated system. United Utilities usually accept that such techniques are suitable for collecting water up to and including the 1 in 1 year event.
- **No storage within swales –** Swales have a combined advantage of providing a volume of storage, slowing the rate at which water enters the downstream system and providing a certain amount of infiltration into the ground.
- Within the analysis it has also been assumed that 100% of the rainwater falling on the proposed impermeable areas enters the system. It is therefore considered that the analysis undertaken is robust.
- 7.07 In order to comply with Environment Agency peak rates of run-off will be restricted to the existing greenfield run-off rate and storage will be provided up to and including the 1 in 100yr storm event plus an allowance of 40% increase for climatic change. This is above and beyond the requirements of a United Utilities adopted drainage system which requires storage up to and including the 1 in 30yr storm event. Flows would be restricted which will limit discharge to 5.0l/s.

- 7.08 Causeway Flow program has been used to calculate the storage volume required for the development attached as appendix D. The storage volume is calculated at 240m³. Proposed Run-off Rates include an increase of 40% climatic change allowance.
- 7.09 It is generally accepted that surface water systems are designed to accommodate the 1 in 30yr plus climatic change event and anything above and beyond that could be allowed to flood the system. This is known as designing for exceedance. It is not achievable to accommodate exceedance due to the topography therefore the system has been designed to full accommodate the full exceedance within the drainage network.
- 7.10 It is also important to note that this system takes no account of the peripheral storage that will be available within the remainder of the proposed drainage network and therefore, notwithstanding the techniques outlined in para 6.9, the storage attenuation requirements will be less.

MAINTENANCE OF PROPOSED SUDS SYSTEMS.

- 7.11 It is important during any development process to consider the long term maintenance of the proposed drainage system. The more traditional non-SuDS route would be to have the system offered up for adoption though United Utilities, where they would take on responsibility for the maintenance of the drainage network. However, this is not the case with SuDS.
- 7.12 With the emerging Flood and Water Management Act 2010 (although it is noted that Schedule 3 relating to SuDS has not yet come into force), the SuDS Approving Body (SAB), would be obliged to adopt sustainable drainage solutions which comply with National Standards. Consequently, the system would have to be reviewed and approved by the SAB to ensure it meets these relevant standards.
- 7.13 Until such a time as Schedule 3 of the Act comes into force, the SuDS system (although approved by both the LPA and the SAB) would remain private and be maintained and managed by a private management company. This maintenance would be secured through ownership of the property. The system has been designed to require minimum maintenance and, the inspection and upkeep of the drainage system can be maintained in perpetuity.

8.0 PROPOSED DRAINAGE STRATEGY – FOUL WATER

- 8.01 No foul sewers are recorded on site. It is proposed to connect to a water Sewage Treatment Plant which will then discharge into the watercourse located to the east of the site via new manholes that are to be installed.
- 8.02 The proposed development is to accommodate one industrial unit. The calculated foul discharge from the site in compliance with Approved Document part H of the Building Regulations Table A1 would be 5.4l/s.

9.0 CONCLUSIONS

- 9.01 The developer is committed to delivering a sustainable development and the drainage proposals will be designed in accordance with the techniques set out within the SuDS Manual. Future maintenance of the system will be secured in perpetuity, through the use of a planning condition.
- 9.02 Foul drainage will be discharged to the watercourse via a Sewage Treatment Plant.
- 9.03 Surface water drainage will be discharged to a watercourse.
- 9.04 The strategy outlined above shows a viable sustainable drainage solution is achievable within the constraints of the site. The delivery of a SuDS surface water system together with an appropriately designed foul network and connection can be secured through planning condition.

10.0 APPENCIES

- Appendix A Location plan
- Appendix B Environment Agency Flood Map
- Appendix C Proposed Scheme Drawing
- Appendix D Drainage Calculations

Appendix A Location plan



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Appendix B Environment Agency Flood Map



Fig 1 Extract from Environment Agency Flood Map

Appendix C Proposed Scheme Drawing



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TABLE 2 EMBEDMENT DIMENSIONS FOR RIGID PIPES									
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225	100	200	SIZED OR 14mm	100	825				
300	100	200	TO 5mm GRADED	100	925				
375	100	200	1.4mm SINGLE	100	1050				
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975	225	300	20mm SINGLE	300	2000				
1050	225	300	TO 5mm GRADED	300	2100				
1125	225	300	1	300	2200				
1200	250	350	1	300	2300				
1350	375	450	1	375	2500				
1500	375	450	1	375	2700				
1650	375	450	1	450	2800				
1800	375	500		450	3100				
1950	400	500	40mm SINGLE	525	3200				
2100	425	650	TO 5mm GRADED	525	3400				
2400	450	675		600	3700				



TABLE 3 THICKNESS OF COMPRESSIBLE FILL (L)							
NOMINAL INT PIPE DIA	DIMENSION Xmm	COMPRESSIBLE FILLER Lmm					
<400	160	18					
400-700	200	36					
725-1200	300	36					
> 200	300	54					

DRAWING No. AO23/236/P/105





Appendix D Drainage Calculations



Design Settings

Rainfall Methodology	FSR	Maximum Time of Concentration (mins)	30.00
Return Period (years)	1	Maximum Rainfall (mm/hr)	50.0
Additional Flow (%)	0	Minimum Velocity (m/s)	1.00
FSR Region	England and Wales	Connection Type	Level Soffits
M5-60 (mm)	17.000	Minimum Backdrop Height (m)	0.200
Ratio-R	0.400	Preferred Cover Depth (m)	0.900
CV	0.750	Include Intermediate Ground	\checkmark
Time of Entry (mins)	4.00	Enforce best practice design rules	\checkmark

<u>Nodes</u>

Name	Area (ha)	T of E (mins)	Cover Level (m)	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
sw01	0.054	4.00	6.100	1200	12.500	76.000	1.050
sw02	0.030	4.00	6.100	1200	28.600	76.000	1.091
sw03	0.036	4.00	6.100	1500	41.200	78.000	1.393
sw04	0.000		6.100	1500	55.200	78.000	1.428
sw05	0.072	4.00	6.100	1200	18.000	28.600	1.125
sw06	0.070	4.00	6.100	1200	41.600	16.000	1.050
sw07	0.070	4.00	6.100	1500	44.000	28.000	1.266
sw08	0.056	4.00	6.100	1500	42.000	52.400	1.328
outfall	0.000		6.100	1200	61.000	78.000	1.443

<u>Links</u>

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)
1	sw05	sw07	26.007	0.600	4.975	4.909	0.066	394.0	225	4.66	48.1
1.1	sw07	sw08	24.482	0.600	4.834	4.772	0.062	394.9	300	5.18	45.9
1.2	sw08	sw03	25.612	0.600	4.772	4.707	0.065	394.0	300	5.73	43.9
1.3	sw03	sw04	14.000	0.600	4.707	4.672	0.035	400.0	300	6.03	42.9
1.4	sw04	outfall	5.800	0.600	4.672	4.657	0.015	386.7	300	6.15	42.5
2.1	sw06	sw07	12.238	0.600	5.050	4.984	0.066	185.4	150	4.28	49.8
3.1	sw01	sw02	16.100	0.600	5.050	5.009	0.041	392.7	150	4.54	48.6
3.2	sw02	sw03	12.758	0.600	5.009	4.857	0.152	83.9	150	4.73	47.8

Name	Vel	Сар	Flow	US	DS	Σ Area	Σ Add	Pro	Pro
	(m/s)	(I/s)	(I/s)	Depth	Depth	(ha)	Inflow	Depth	Velocity
				(m)	(m)		(I/s)	(mm)	(m/s)
1	0.652	25.9	9.4	0.900	0.966	0.072	0.0	94	0.601
1.1	0.785	55.5	26.4	0.966	1.028	0.212	0.0	146	0.775
1.2	0.786	55.5	31.9	1.028	1.093	0.268	0.0	163	0.812
1.3	0.780	55.1	45.1	1.093	1.128	0.388	0.0	207	0.867
1.4	0.793	56.1	44.7	1.128	1.143	0.388	0.0	203	0.878
2.1	0.735	13.0	9.5	0.900	0.966	0.070	0.0	95	0.801
3.1	0.501	8.9	7.1	0.900	0.941	0.054	0.0	102	0.557
3.2	1.098	19.4	10.9	0.941	1.093	0.084	0.0	81	1.130

	1
	2
CAUSEVVAI 💕	E

Keystone Design Associates Ltd	File: storm01.pfd	Page 2
261 Church Street	Network: Storm Network	
Blackpool	David Hadwin	
FY1 3PB	01/11/2023	

Pipeline Schedule

Link	Length (m)	Slope (1:X)	Dia (mm)	Link Type	US CL (m)	US IL (m)	US Depth (m)	DS CL (m)	DS IL (m)	DS Depth (m)
1	26.007	394.0	225	Circular	6.100	4.975	0.900	6.100	4.909	0.966
1.1	24.482	394.9	300	Circular	6.100	4.834	0.966	6.100	4.772	1.028
1.2	25.612	394.0	300	Circular	6.100	4.772	1.028	6.100	4.707	1.093
1.3	14.000	400.0	300	Circular	6.100	4.707	1.093	6.100	4.672	1.128
1.4	5.800	386.7	300	Circular	6.100	4.672	1.128	6.100	4.657	1.143
2.1	12.238	185.4	150	Circular	6.100	5.050	0.900	6.100	4.984	0.966
3.1	16.100	392.7	150	Circular	6.100	5.050	0.900	6.100	5.009	0.941
3.2	12.758	83.9	150	Circular	6.100	5.009	0.941	6.100	4.857	1.093

Link	US	Dia	Node	МН	DS	Dia	Node	МН
	Node	(mm)	Туре	Туре	Node	(mm)	Туре	Туре
1	sw05	1200	Manhole	Adoptable	sw07	1500	Manhole	Adoptable
1.1	sw07	1500	Manhole	Adoptable	sw08	1500	Manhole	Adoptable
1.2	sw08	1500	Manhole	Adoptable	sw03	1500	Manhole	Adoptable
1.3	sw03	1500	Manhole	Adoptable	sw04	1500	Manhole	Adoptable
1.4	sw04	1500	Manhole	Adoptable	outfall	1200	Manhole	Adoptable
2.1	sw06	1200	Manhole	Adoptable	sw07	1500	Manhole	Adoptable
3.1	sw01	1200	Manhole	Adoptable	sw02	1200	Manhole	Adoptable
3.2	sw02	1200	Manhole	Adoptable	sw03	1500	Manhole	Adoptable

Manhole Schedule

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connections		Link	IL (m)	Dia (mm)
sw01	12.500	76.000	6.100	1.050	1200	→₀				
							0	3.1	5.050	150
sw02	28.600	76.000	6.100	1.091	1200	1	1	3.1	5.009	150
							0	3.2	5.009	150
sw03	41.200	78.000	6.100	1.393	1500		1	3.2	4.857	150
						1	2	1.2	4.707	300
						2	0	1.3	4.707	300
sw04	55.200	78.000	6.100	1.428	1500	1>0	1	1.3	4.672	300
							0	1.4	4.672	300
sw05	18.000	28.600	6.100	1.125	1200	()→o				
							0	1	4.975	225
sw06	41.600	16.000	6.100	1.050	1200	, in the second				
							0	2.1	5.050	150
sw07	44.000	28.000	6.100	1.266	1500	0 ↑	1	2.1	4.984	150
						2	2	1	4.909	225
						1	0	1.1	4.834	300

CAUSEWAY 🛟	Keystone Design 261 Church Stree Blackpool FY1 3PB	Associates Ltd et	File: stor Network David Ha 01/11/20	m01.pfd :: Storm Networ adwin 023	Page 3						
Manhole Schedule											
Node Easti (m)	ng Northing (m) (CL Depth m) (m)	Dia (mm)	Connections	Link	IL D (m) (m	ia m)				
sw08 42.00	00 52.400 6.	100 1.328	1500		1.1	4.772 3	300				
outfall 61.00	00 78.000 6.	100 1.443	1200 1		1.2 1.4	4.772 3 4.657 3	<u>800</u> 800				
		<u>Simulatio</u>	n Settings								
Rainfall M	Methodology FSF FSR Region Eng M5-60 (mm) 17. Ratio-R 0.4 Summer CV 0.7 Winter CV 0.8	R gland and Wale 000 50 40	s D Add C	Analysis Skip Stead rain Down Time itional Storage (heck Discharge V	Speed y State (mins) m³/ha) Rate(s) ⁄olume	Normal x 240 20.0 x x					
		Storm D	urations								
15 30 6	0 120 18	0 240	360 4	480 600	720	960	1440				
R	eturn Period Clin (years)	mate Change (CC %)	Additiona (A %	al Area Additio 5) (0	onal Flo ጊ %)	w					
	1 2 30 100	0 0 0 40		0 0 0 0		0 0 0 0					
	Node	sw03 Online H	Iydro-Brak	e [®] Control							
Replaces Downst Invert Design Design	Flap Valve x cream Link √ c Level (m) 4.707 Depth (m) 1.200 Flow (I/s) 5.0	F Min Outl Min Node	Obj Sump Ava Product Nu et Diameter Diameter	ective (HE) Mi ailable √ umber CTL-SH er (m) 0.150 (mm) 1200	nimise E-0103-	upstream st 5000-1200-	orage 5000				
	Noc	le sw08 Carpar	k Storage	<u>Structure</u>							
Base Inf Coefficien Side Inf Coefficien Safet	t (m/hr) 0.00000 t (m/hr) 0.00000 y Factor 2.0 Porosity 1.00	Time to h	Invert Lev alf empty Wid Leng	rel (m) 4.772 (mins) th (m) 32.000 th (m) 52.000	Inf	Slope (1:X) Depth (m) Depth (m)	1.0 0.100				
	Node	sw03 Depth/A	rea Storag	<u>e Structure</u>							
Base Inf Coefficie Side Inf Coefficie	nt (m/hr) 0.0000 nt (m/hr) 0.0000	00 Safety Fa 00 Por	actor 2.0 osity 1.0))0 Time to P	Invert nalf emp	Level (m) oty (mins)	4.707				
Depth (m) 0.000	Area Inf Area (m²) (m²) 200.0 0.0	Depth Ar (m) (m 1.200 200	ea Inf A 1 ²) (m 0.0	rea Depth ²) (m) 0.0 1.201	Area (m²) 0.0	Inf Area (m²) 0.0					