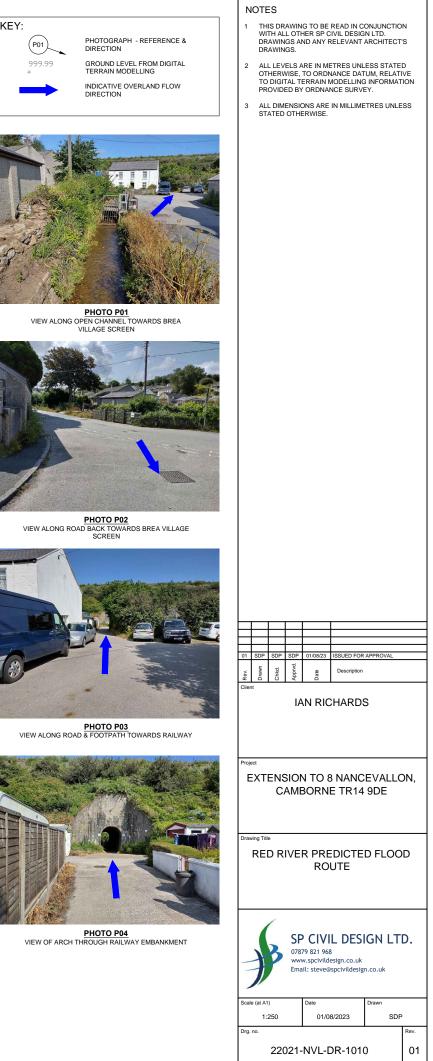
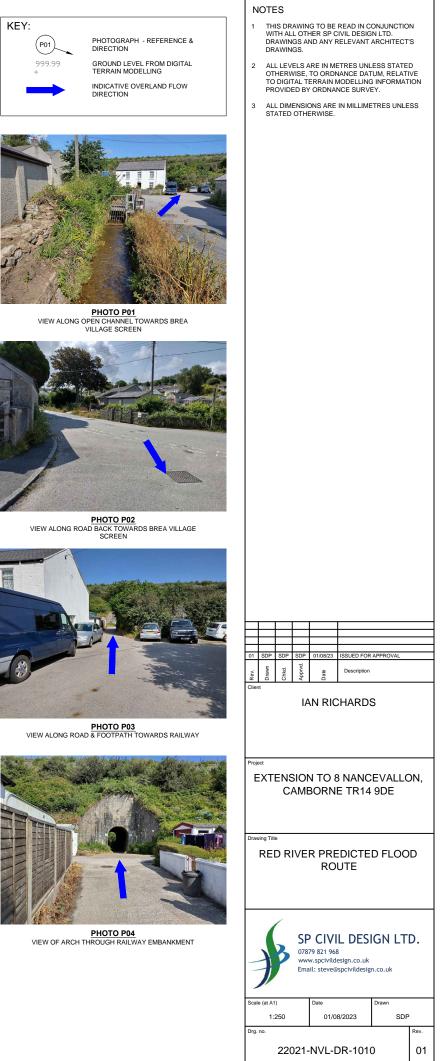
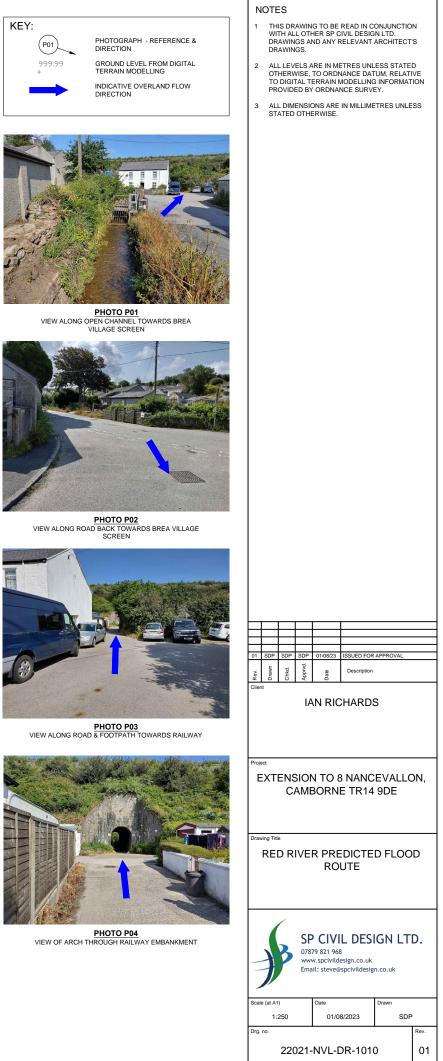
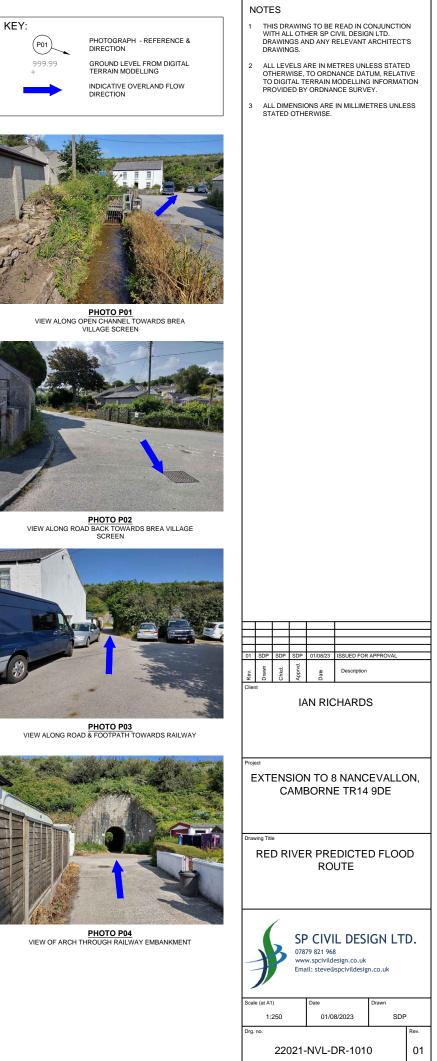
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::\Users\User\Documents	Steve\Work\2022	2\22021 Nanceva	Ion Camborne\04	Design\Drawing	s\22021-NV	/L-DR-1000to	- 1010-01.dwg.	Plot date and tim 97,76	98.14	4:04:56 98.94	99.33	99.17	99.95	100-25	100.47	101.07	101.65	102.02 -	-102.77	101 34	106.33	108.11	109.80	/104 GA	111/07	Z 111 PK	110.83	ÍN0.40	
[.00	+	+	+	+	+	+	+	+	+	+	102.02	+	+	+	+	+	+	+	/ /	110/05	+	
ALL RIGH	CE SURVEY ITS RESER\ NUMBER 10	/ED.	N COPYRIGI	HT 2022.			.59	97.08-	97.47	97.99	98.38	98.22	98.53	ath ((UM) 98.61	99.84	100.36	101.59	104.00	106.14	108.31	110,21	111.07	184,31	111.07	120.42	109.91	109.40	K
								+	+	+	+	+	+	+	+	+	^ +	+	+	+	+	+	///	+	+	+ Dry	+	+	
95.32	95.03 \	94.89	94.86	<u>)</u> 95;0	9 9	5.32	96.02	96.41	96.80 +	97.18	97.43	97.81	98.20	98.50	99.19	108.71	101.52	103.78	106.23	108.72	110.84	111.08	111.08	104.63	109.33	108.87	108.36	108.13	
							4	- OVERLAN RE-ENTER CHANNEL	R OPEN		'				//				I					\sim	X				
95.71 +	95.42 +	95.13 +	94.99 +	95.2	1 9	5.44	95.63 -	96.01 +	96.40 +	96.72 +	97.64 +	97.98 +	98.32	98.80 +	100.78 +	102.48 +	104.48 +	106.73 +	109.11 +	111.13 +	111.12 +	111.40	110.30 +	103.50 +	107.76	107.32 +	106.82	107.13 +	
	A			\backslash	$\left \right\rangle$													/	///							,			
96.10 +	95.8	95.52	\ \95.23 +	95/3	3 9	5.32	95.51	95.83 +	96.09 +	96.35 +	97.26	98.83 +	99.22 +	101.82 +	103.91 +	105.71 +	107.61 +	109.91	111.16	111.14	+ +	/ 109.76 +	107.48 +	103.02	105.85	105.78	105.54	106.13 +	
96,50		95.91	95.56	95.4	5 9	5.44	95.13	95.16	95.41	96.30	98.37	99.94	102.01	104.61	106.89	108.85-	0110.74	111.18	111.17	111,18	108.95	106.82	104.34	102.26	103.25	104.06	104.63	105.22	
+	+	Ţ	+	FB	\ +		1	+	+	+ /	+	+	+	+	+	+	?/¥ /	/ + / /	/ _ / /	M	+	+	//	+	+	+		+	
96.89	96,54	96.12	95,91	95.7	9	5.69	95.43	94.88	96132	99.38	100.97	102.71	104.93	107.18	109.50	111.22	111.21	111.19	110.42	107.67	105.40	103,64	101.41	102/18	102.69	103.21	103.80	104.42	
			I	\		$\overline{\ }$			$\langle \rangle$	·	'			I					/		'		·	/	/ /			'	
97.46 +	97.05 +	96.62	96.41	96.Ì% +	3 9 \ +	95.95	5 ,73	95.15	96,58 +	101.97 +	103.56 +	105.64 +	107.88 +	110.05 +	111.26 +	111,23	111.22	109.49 +	106.70 +	103.94 +	101.88 +	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	9+1400.81	101.32 +	101.84	102.38 +	102.98	103.61 +	
00.01	07.00	07 50						100.00			104.00	100 57	/					105 67	100.05	100.01				100.47		101 54	100.10	100 70	and the second s
98.31 +	97.92 +	97.50 +	97.06 +	96.8 +	4 9	1.24	98.44	100.68 +	102.78 +	104.57 +	Ttunn	108.57 et	110.82	111.33 +	/11.29 *	111,26	108.64 +	105.67 +	102.85 +	100.8r +	99.18	99.24	/99.95 +	100.47	100./99 +	101.56	102.19	102.79 +	
99.11	98.80	98.38	97,94	98.9	2 /	9.72	101.05	103.29	105.50	107.5	109.34	111.42	111.39	111.35	110.73	108.11	105.25	102.15	100.53	98.90	98.50	98,82	99.10	× 99.62	100.14	100.75	101.39	101.98	
+	+	+	+/	/	+		Ť	+	+	+	+	+	*//	+	+ 3.	ARCH THR	FLOWS THE	VAY	+	Ź	~	/* \	+	+	+	Ť	Ť	+	
99.90	99.68	99.26	99.2%	/100.7	4 10	02.19	103.65	105.99	108.27	110.15	111.49	111.45	111.42	109.51	106.6		ENT (GROUN E FOR EMBA		98.57	97.70	97.93	98.16	98.44	98.77	99.32	99.96	100.60	101.16	
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100.68	100.72	101.56	<u>_</u>	unne 104.9		07.21	109.44	111.64	111,61	x11.57	118.96	108.01	105.10	102.35	100.64	98.79	97,12	96.82	96.72	96.92	97.14	97.36	97.59	97.80	98.13	98.37	98.97	99.53	
+	+	+	103.10	+	+	07.LI		+	*	+	+	+	+	+	+	+	+	+	+	+	+	>+	+	+	+	- po		+	
101.46	101.80	101.50	105.74	107.5	27 11	10.19	111.70	111,67	111.64	110.29	107.28	104.19	36.96	97.65	28.00	96,30	96.25	98,36	96.40	96.68	96.8B	0 97.08. K	ח 97.27	97.49	97.70	98.00	88.32	98.83	4
+	+	+	+	\checkmark	\rightarrow	\langle		///	/+ //	+	+	+	+		+	+	+	+	+	+	\searrow	'ynny <u>∘</u>	5 /	+	+	4			
103.87	104.55 +	106.27 +	108.71 +	110.9				111.70	109.58 +	106.98 +	3 104.07 +	101.23 +	95.30 +	95.73	95.95 +	96.08		96.22 +	>96.22/ +	96.35 +	96.51	96.73 +	96.95 +	97.17 +	97.39 4	97.60 +	97.95	98.38	
				// /		\nearrow	X	\nearrow	_					X	<		$\langle \ \rangle$	1	/	\langle				/				>//	and the
106.62 +	107.30 +	109.09	111.58 +	111.8 +	3 14	11.79	117.51	108.73	+	103.67	7 101.33 +	98.58 +	96.03	95.90 +	95.94	96.09	\96.09\ +	0-+ +	96.07 +	96.16	96.30\ +	96.43	96.63	96.86 +	97.07 +	97.29 \ +	97.61	98.84 +	
109,37	110.04	111.78	Burl, St	111-8		11.00	108.22	105.24	99.26	99.11	98.69	4733	96.31	95.92	95.96	\$5.95	. 55.95	95.94	95 93	95.97	96.11	96.25	96.38	96.54	96.76	97.08	97.41	97.73	
+	+	+	+		+	11.00	T	+	+	+	+	+	+	+	+	+	$ \perp $	+	+	+	+	+	+	+	+	+	-	+	-
111.10	111.73	111.78	111.78	110.3	1 10	08.25	105.55	102.38	99.67	99.13	98.35	97.12	96.62	96.22	95.91	95.91	95.80	95.80	95.79	95.79	95.92	96.06	96.19	96.35	96.60	96.88	97.20	97.53	
+				+	+			/	+		+		+	+	+	+ ``		+	Follo)ch	+	/	/+/	+	+	+	T)	+	1
111.68 +	111.71 +	111.57	109.68 +	107.6 +	54 10	05.46	-	100.84	99.65 +	98.86	/ 98.01 +	97.39	96.88 +	96.49 +	96.04 +	95.94 +	95.85 +	95.75	95.65 Mh	95.64 04	95.73 +	/ 95.89/ +	_ 96.07 ↓+	96.27 +	96.55	96.82 +	97.10	97. 3 8	
								rea	/	$\langle \rangle$			\rangle	\checkmark			\checkmark /	\sim		\langle						\wedge			
111.65	110.84	109.26	107.79	106.5 +	52 10 +	04.59	102.4¢4	r100/98	99.82 +	98.96 +	98.27	97.66 +	97.15	96,74 +	96.29 +	96.08 +	95.98 +	95.88\ +	95.78	95.697	95.61 +	95,79	+ \	96.22 + RLAND FLO	+ \ '	96.77 +	¥7.05	97/38 +	
111.23	109,83	108.26	107.61	106.4	-3 10	04.75	103.07 /	101.13	99.99	99.28	98.56-	97.92	97.42	96.99	- 96.54	96,21	96.12	96.02	95.92	-	95.67	95.68	DOW	NHILL ALO		96.65	96.88	9711	14 10
+	+	+	+	+	+			+	+	+	+	+	+	9 ⁺ 7.0r	+ / \	+ \	+	>	+	+	+	±	Huntir			+	>†)+	Sec. 1
110.40	108.84	108.18	107:52	106.3	86 10 +	04.66/	102.98	101.30	100.24	99/59	98.88		97.68	97.24	96.79	96.35	96.25	96.15	deen 95.98	95.81	\$5.73	95.74			96.19 +	96.42	96.65	<i>9</i> 6.89 +	
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109.40 +	108.75 +	108.09 +	107.43 +	106.2 +	29 10	04.57	102.89 -	101.37	100.33	+ + +	99.13 +	98:48 +	97,93	- 97.49 +	97\04 +	96,60	96.38	<u>}96</u> 21	96.04	95.87 +) 95.80 +	95.83\ +	95.86	95,88 +	95.96 +	96.19 +	96.42	96.66 +	1
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109.31 +	108.66 +	+	107.34 +	+	2 II +	04.48	102.80	101.60	+	1 99.80	+	99.03	+	98.53	97.89\ +	+	96.53\ +	96.36	96.19 † The	96.02	+	95.91 +	+	+	95. 9 9 +	96.01 +	96.19	96.43 +	1
109.18	108.55	107.91	107.25	106.1	5 10	04.41	102.87	101.83	100.79	100.21	100.54	100.53	199.21	99.49	98.51	97.64	97,11	96.58	t \$60t be		96,23	95.99	96.02	96.03	96.07	96.10	96.12	96. 20 5	
+	+	+	+	+	/			+	+]+	*	/4	+	+	+	+	+	+	+	+	+	+	+	/ L	_+⊖V	ver	+ H	2
109.16	108.50	107.83	107.16	186.0	13 10	04.12	103.76	102.91	102.06	102.01	102.00	101.77	100.83	99.85 +	98.87	98.23 +	97.70	97.17	96.77		96.59	96.35	96.10	96.13		ER OVERTO	JPS AT	96.19	
T	1	r	<u> </u>	·/ ⁺				`//		· · /	-						`	\sim	+2	+	1.		A Solution	ь:Um	' \	·		/	
109.18		107.96	106.67	184.8	35 10	03.46	103.59	104.27	108.43 +	103.41 +	102.99 +	102.52 +	101.36 +	100.21 +	99.84 +	98.82 +	+	97.77 +	97.25 +	+>	96.95 +	% .71	96.46	96.21	96.24 +	96/82	96.16	/ 96.09 +	
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108.48	106.57	104.60	104.48	105.4	+0 11	06.45	107.11	106.67	106.06	105.35	5 104.74	103.70	102.78	101.86	100.94	100.02	99.50	98.98	98.45	97.93	97.67	97,43	97.21/	96,99	96.76		96.31	96.17	
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ORIGINAL DRAWING SIZE 841 x 594