GAIL'S BAKERY, SEVEN DIALS, BRIGHTON

Plant Noise Assessment

Reference: 13302.RP01.PNA.0
Prepared: 24 January 2024
Revision Number: 0

Gail's Ltd
Unit 12-13
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Plant Noise Assessment

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Revision	Comment	Date	Prepared By	Approved By
0	First issue of report	24 January 2024	Matt Wildman	David Johnston

Terms of contract:

RBA Acoustics Ltd have prepared this report in accordance with our Scope of Work 13302.SW01.0 dated 20 December 2023. RBA Acoustics Ltd shall not be responsible for any use of the report or its contents for any purpose other than that for which it was provided. Should the Client require the distribution of the report to other parties for information, the full report should be copied. No professional liability or warranty shall be extended to other parties by RBA Acoustics Ltd without written agreement from RBA Acoustics Ltd.

The recommendations within this report relate to acoustics performance only and will need to be integrated within the overall design by the lead designer to incorporate all other design disciplines such as fire, structural integrity, setting-out, etc. Similarly, any sketches appended to this report illustrate acoustic principles only and will need to be developed into full working drawings by the lead designer to incorporate all other design disciplines.

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Contents

1. INTRODUCTION

It is proposed to locate new items of plant at the proposed Gail's Bakery site located in Seven Dials, Brighton. As part of the planning application, Brighton & Hove City Council requires consideration be given to atmospheric noise emissions from the proposed equipment to the nearest noise-sensitive receptors.

RBA Acoustics have been commissioned to undertake measurements of the prevailing noise conditions at the site and to determine the atmospheric noise emission limits in accordance with Brighton & Hove City Council requirements. This report presents the results of the noise measurements, associated criteria and provides the required assessment.

A summary of acoustic terminology is included in Appendix A.

2. STATEMENT OF EXPERIENCE

Matt Wildman (BSc Hons, AMIOA) is a Consultant at RBA Acoustics and has worked in acoustic consultancy for four years. In this time he has acquired much experience in carrying out noise impact assessments for building services and plant noise. Similarly, in this time Matt has developed a good working knowledge of key standards and guidance documentation relating to noise impact assessments such as BS 4142:2014 *'Methods for rating and assessing industrial and commercial sound'*.

David Johnston (IOA Dip, MIOA) is a Senior Consultant at RBA Acoustics with over eleven years of experience in acoustic consultancy. David has developed a particular experitise in carrying out noise impact assessments for building services specifically for the purposes of discharging planning conditions, and has established a relationship with some of RBA Acoustics' biggest clients through this work.

3. SITE DESCRIPTION

The site of the proposed Gail's Bakery is located at 108 Prestonville Road, overlooking the Seven Dials roundabout in Brighton. The unit occupies the ground floor of the building, while the first floor is occupied by an estate agents which has access to a flat roof terrace which is also located above the proposed Gail's Bakery unit.

The surrounding area comprises a mix of residential receptors as well as local commercial amenities such as shops and cafes. The area experiences a consistently high rate of traffic accessing the Seven Dials roundabout, which was also noted to be the primary noise source in the area during our time on site.

The site is shown in relation to its surroundings in the site plan in Figure 1 (Appendix D).

4. ENVIRONMENTAL NOISE SURVEY

4.1 Survey Methodology

Monitoring of the prevailing background noise was undertaken over the following period:

12:30 Wednesday 10 January to 12:15 Thursday 11th January 2024.

As the survey was unattended it is not possible to comment with certainty regarding meteorological conditions throughout the entire survey period. However, based on observations during the site visits and weather reports for the area, conditions were generally considered suitable for obtaining representative noise measurements, being predominantly dry with little wind.

Measurements were made of the L_{A90}, L_{Amax} and L_{Aeq} noise levels over sample periods of 15 minutes.

4.2 Measurement Location

To determine the existing noise climate around the site measurements were undertaken at the following location:

Measurement Position 1 – Flat Roof

Measurements were taken with the microphone positioned on a tripod on the flat roof of the unit, approximately 6m above ground level, overlooking Prestonville Road and the Seven Dials roundabout. The prevailing noise climate consisted mainly of traffic noise.

The measurement position is also illustrated on the site plan attached in Figure 1 and photo in Figures 3 (Appendix D).

4.3 Instrumentation

For information regarding the equipment used for the measurements please refer to Appendix B.

The sound level meter was calibrated both prior to and on completion of the survey with no significant calibration drift observed.

4.4 Results

The noise levels measured are shown as time-histories on the attached Graphs 1 – 6 in Appendix D.

The representative background L_{A90} and the period averaged L_{Aeq} noise levels measured are summarised below. Selection of an appropriately representative background sound level is discussed in BS 4142:2014 as follows:

> *"In practice, there is no "single" background sound level as this is a fluctuating parameter. However, the background sound level used for the assessment should be representative of the period being assessed.*
> [...] *A representative level should account for the range of background sound levels and should not automatically be assumed to be either the minimum or modal value."*

Graphs 3 and 6 present the range of background sound levels measured and, on this occasion, the minimum values have been chosen as representative of the background noise levels during operational hours being, as they are, statistical levels which occur at least 25% of the overall survey period. In our experience, this level is more appropriate than using the most commonly occurring (modal) L_{A90} noise level, which is not thought to be representative of quieter times of the day.

Table 1 – Measured Baseline Noise Levels

Measurement Period	Representative Background Noise Level (dB)	Period-Averaged Noise Level $L_{Aeq,T}$ (dB)
Daytime (07:00 – 23:00)	57 $L_{A90,1hour}$	66
Night-time (23:00 – 07:00)	38 $L_{A90,15min}$	59
Anticipated Operating Hours (06:00 – 19:00)	61 $L_{A90,1hour}$ (07:00 – 19:00) 51 $L_{A90,15min}$ (06:00 – 07:00)	67

5. PLANT NOISE CRITERIA

5.1 Local Authority Requirements

The Brighton and Hove City Council website gives the following advice in relation to installation of plant or machinery:

> *If you plan to install an external plant or machinery in your design, you may need an acoustic assessment. You need to have the plant assessed by an acoustics specialist in line with British Standard 4142 (BS4142:2014).*

(taken from https://www.brighton-hove.gov.uk/environment/noise-pollution-and-air-quality/find-advice-acoustic-requirements, last accessed 18 January 2024)

There have also been a number of guidance documents published by Brighton & City Council and the wider Sussex area which make reference to noise. These include the Brighton & Hove City Plan parts 1 and 2 (2016/2022), and the Planning Noise Advice Document: Sussex (2023). The publications all align on the use of BS 4142:2014 as an appropriate methodology for assessing the potenitial impact of plant noise. We have therefore used that assessment methodology for this development.

5.2 Summary of BS 4142 Guidance

BS 4142:2014 *Methods for rating and assessing industrial and commercial sound* describes methods for rating and assessing sound of an industrial and/or commercial nature, which includes:

- sound from industrial and manufacturing processes
- sound from fixed installations which comprise mechanical and electrical plant and equipment
- sound from the loading and unloading of goods and materials at industrial and/or commercial premises
- sound from mobile plant and vehicles that is an intrinsic part of the overall sound emanating from premises or processes, such as that from forklift trucks, or that from train or ship movements on or around an industrial and/or commercial site.

The methods described within BS 4142:2014 use outdoor sound levels to assess the likely effects of sound on people who might be inside or outside a dwelling or premises used for residential purposes upon which sound is incident.

The assessment method described in BS 4142:2014 is based on the continuous sound pressure level produced by a specific source ($L_{Aeq,Tr}$) at the assessment location. Appropriate corrections allowing for any tonality, impulsivity, other characteristics or intermittency of the specific sound source are then applied to derive the rating level ($L_{Ar,Tr}$). The rating level is then compared to the background sound level ($L_{A90,T}$) to produce the relative difference, or excess of rating level over background sound level. BS 4142:2014 quantifies the estimated impact from the excess as:

a) *Typically the greater this difference, the greater the magnitude of impact.*
b) *A difference of around +10dB or more is likely to be an indication of a significant adverse impact, depending on the context.*
c) *A difference of around +5dB is likely to be an indication of an adverse impact, depending on the context.*
d) *The lower the rating level is relative to the measured background sound level, the less likely it is that the specific sound source will have an adverse impact or a significant adverse impact. Where the rating level does not exceed the background sound level, this is an indication of the specific sound source having a low impact, depending on the context.*

When considering the above, we would consider that +5dB rating would indicate a LOAEL whereas a +10dB would be in line with SOAEL.

In line with the above requirements and the relatively high ambient noise levels we would propose items of mechanical services be designed so that the rating level of all mechanical plant is 5 dB below the representative background noise level at the nearest residential noise sensitive locations.

Table 2 – Adopted Plant Noise Limits

Assessment Period	Plant Noise Criteria to be achieved at 1m outside the window of the nearest Noise-Sensitive Receptor (NSR)
Plant Operating Hours (06:00 – 19:00)	56 $L_{Ar,Tr}$ (07:00 – 19:00) 46 $L_{Ar,Tr}$ (06:00 – 07:00)

6. PLANT NOISE ASSESSMENT

This assessment has been based on the information provided to RBA by Multiple Electrical Engineering Services Ltd, the project M&E Consultants and is described in the following sections.

6.1 Proposed Plant Items

The following plant is proposed for the scheme:

Table 3 – Plant Types

Ref.	Manufacturer/Model/Duty	Plant Type
CU1	Daikin AZAS125MV1	Condenser
CU2	Daikin RZAG60A	Condenser
EF1	Systemair PRIO315EC	Extract Fan
SF1	Systemair PRIO315EC	Supply Fanc

6.2 Plant Locations

It is proposed to locate CU1 and CU2 externally at ground floor level on the eastern boundary of site on Prestonville Road. The supply and extract ductwork will terminate on the eastern façade of the building, also at ground floor level and out onto Prestonville Road. The equipment positions are indicated on the plan in Figure 2 in Appendix D.

6.3 Plant Noise Levels

Information regarding the noise levels of the proposed plant has been provided by the manufacturers of the unit. The associated plant noise levels are detailed as follows:

Table 4 – Plant Noise Levels

Unit	Parameter	Sound Level (dB) at Octave Band Centre Frequency (Hz)							
		63	125	250	500	1k	2k	4k	8k
Daikin AZAS125MV1	L_p @ 1m (Heating Mode)	55	63	58	55	51	47	43	36
Daikin RZAG60A	L_p @ 1m (Heating Mode)	51	54	52	50	43	38	33	24
Systemair PRIO315EC	Outlet L_w	78	76	74	70	68	64	57	49
	Inlet L_w	72	84	73	71	69	64	58	50

Review of the octave band data has shown that CU1 and SF1 may have tonal characteristics at 125Hz. This has been taken into account in our calculation procedure and corrections applied to those items of plant.

6.4 Location of the Nearest Noise-Sensitive Receptors

Based on observations made on site and discussions with the design team we understand the nearest noise-sensitive receptors to the proposed plant to be as follows:

Receptor 1 – 40/41 Prestonville Road

The worst-affected nearby residential receptor is understood to be the first floor residence at 40/41 Prestonville road which directly overlooks all items of plant at a distance of approximately 9m from CU1, CU2 and EF1, and approximately 7m from SF1, 9m from EF1 and the condenser units.

Receptor 2 – 44 Prestonville Road

The nearest residential receptor is understood to be the first floor residence at 44 Prestonville road which is directly above the proposed Gail's Bakery unit. Although closer than Receptor 1, this receptor does not have direct line of site to the proposed items of plant and is also predicted to benefit from directivity losses and acoustic screening.

Receptor 3 – Pembertons (108A Dyke Road)

The nearest commercial receptor is understood to be Pembertons estate agents which is located at first floor level directly above the proposed Gail's Bakery site. The nearest window of this receptor to the proposed items of plant overlook CU1, CU2 and EF1 at a distance of 2-3m. Despite the short distance between the plant and this location, this receptor is predicted to benefit from directivity losses and screening losses from SF1.

The receptors are shown in the site plan in Figure 1 in Appendix D.

6.5 Calculation of Noise Levels at Nearest Noise-Sensitive Receptors

Our calculation method for predicting noise levels from the proposed external plant at the nearest noise-sensitive receptors, based on the information above, is summarised below.

- Source Term (L_p/L_w)
- Distance Attenuation
- In-Duct Losses (Duct Runs, Bends etc.)
- Grille End Reflections
- Directivity
- Reflections
- Screening

Calculation sheets are attached for further information in Appendix C.

The results of the calculations indicate the following noise levels at the nearest affected residential windows:

Table 5 – Predicted Plant Noise Levels

Parameter	CU1	CU2	EF1	SF1	Commentary
Receptor 1 – 41 Prestonville Road					
Representative background noise level $L_{A90,Tn}$	51/61	51/61	51/61	51/61	Representative night / day operating hours background noise level ($L_{A90,T}$)
Specific level $L_{eq,Tr}$	41	34	46	49	Predicted plant noise level at receptor (dBA)
On-time correction	0	0	0	0	No correction to be applied.
Acoustic feature correction	+4	0	0	+7	Correction for tonal elements applied to CU1 and SF1
Rating level $L_{Ar,Tr}$	45	34	45	56	Specific level plus acoustic feature correction (dBA)
Cumulative level at receptor (dB) $L_{Ar,Tr}$	57				
Excess over background	+6 night / -4 day				

Receptor 2 – 44 Prestonville Road					
Representative background noise level $L_{A90,Tn}$	51/61	51/61	51/61	51/61	Representative night / day operating hours background noise level ($L_{A90,T}$)
Specific level $L_{eq,Tr}$	37	30	40	56	Predicted plant noise level at receptor (dBA)
On-time correction	0	0	0	0	No correction to be applied.
Acoustic feature correction	+4	0	0	+7	Correction for tonal elements applied to CU1 and SF1
Rating level $L_{Ar,Tr}$	41	30	40	63	Specific level plus acoustic feature correction (dBA)
Cumulative level at receptor (dB) $L_{Ar,Tr}$	63				
Excess over background	+12 night / +2 day				
Receptor 3 – Commercial Office (108A Dyke Road)					
Representative background noise level LA90,Tn	51/61	51/61	51/61	51/61	Representative night / day operating hours background noise level ($L_{A90,T}$)
Specific level Leq,Tr	46	40	48	42	Predicted plant noise level at receptor (dBA)
On-time correction	0	0	0	0	No correction to be applied.
Acoustic feature correction	+4	0	0	+7	Correction for tonal elements applied to CU1 and SF1
Rating level LAr,Tr	50	40	48	49	Specific level plus acoustic feature correction (dBA)
Cumulative level at receptor (dB) $L_{Ar,Tr}$	54				
Excess over background	+3 night / -7 day				

The rating level from the proposed plant installations is between 3 – 12 dB above the representative background noise level in the night-time period. The night-time period during which plant is operational is between 06:00 – 07:00. During the rest of the operational hours of the plant (07:00 – 19:00) the rating level is between 7 dB below and 2 dB above the representative background noise level at the receptors. We recommend that mitigation is included in the design to achieve a rating level 5 dB below the background noise level.

6.6 Mitigation

It is recommended to install a circular silencer within the atmosphere side of the supply and extract dutwork.

An example product capable of achieving the following insertion losses would be acceptable:

Table 6 – Required Insertion Losses

Location	Example configuration	Insertion loss (dB) at Octave Band Centre Frequency (Hz)							
		63	125	250	500	1k	2k	4k	8k
EF1 – Atmosphere side	45% free area, 900mm	2	5	11	17	20	19	12	10
SF1 – Atmosphere side	35% free area, 1200mm	5	11	19	29	36	37	29	18

With the above mitigation measures included, the resultant predicted noise levels are as follows:

Table 7 – Predicted Plant Noise Level Summary With Mitigation

Operating Period	Noise Level (dB) at Receptor 1 – 41 Prestonville Road		Noise Level (dB) at Receptor 2 – 44 Prestonville Road		Noise Level (dB) at Receptor 3 – Pembertons (108A Dyke Road)	
	Night	Day	Night	Day	Night	Day
Cumulative level at receptor (dB) $L_{Ar,Tr}$	46	46	45	45	51	51
Excess over background	-5	-15	-6	-16	0	-10

The rating levels are at least 5 dB below the representative background noise levels during the day time and night-time periods with the exception of the commercial receptor between 06:00 -07:00. We do not consider this to represent a risk of adverse effects because the office would not typically be occupied during those hours, and a rating level of equal to background can be considered acceptable for a commercial office receptor.

7. UNCERTAINTY

Uncertainty is an unavoidable feature of measurements in the field, which can be subject to many factors; the weather typically being the most significant of which with respect to the measurement of sound. Uncertainty is also unavoidable in the prediction of sound levels, where naturally, before the scenario being considered becomes a reality, a number of assumptions need to be relied upon. There is also the uncertainty of people's reactions, which can be influenced by a number of factors, not just the magnitude or character of the sound in question.

In keeping with the scale of each project, therefore, it is the aim of RBA Acoustics to minimise uncertainty at each stage as far as reasonably practicable. With this is mind, RBA Acoustics follow the best practise methodologies based on the guidance within BS 4142:2014 and our experience in undertaking assessments of these nature.

Crucially, it has been determined that environmental noise measurements have been undertaken by suitably qualified staff, using in calibration equipment and avoiding adverse weather conditions.

The predictions have also been undertaken by suitably qualified staff, whilst using the best available information, an industry standard calculation method, and the most applicable calculation procedures.

Notwithstanding this, naturally some uncertainty remains. Given the sheer number of factors involved, however, it is not feasible to place a value on the level of uncertainty, without resulting in an unhelpful range of possible outcomes. It is the professional position of RBA Acoustics that uncertainty has been kept to a realistic minimum and that the outcome of this assessment is sufficiently representative.

8. VIBRATION CONTROL

In addition to the control of airborne noise transfer, it is also important to consider the transfer of noise as vibration to adjacent properties (as well as to any sensitive areas of the same building).

We would typically advise that condensing units and fans be isolated from the supporting structure by means of either steel spring isolators or rubber footings. For particularly sensitive locations, or when on lightweight structures the mounts should ideally be caged and be of the restrained type.

It is important the isolation is not "short-circuited" by associated pipework or conduits. To this end, any conduits should be looped and flexible connectors should be introduced between the condenser and any associated pipework. Pipework should be supported by brackets containing neoprene inserts.

9. CONCLUSION

RBA Acoustics have undertaken noise monitoring at Gail's Bakery, Seven Dials, Brighton. The measured noise levels are presented within this report. The resultant noise levels have been used to determine the required criteria for atmospheric noise emissions from the proposed plant installations.

The results of the assessment indicate atmospheric noise emissions from the proposed plant are within the criteria required by Brighton and Hove City Council provided the in-duct attenuation measures listed in Table 6 are installed. As such, the proposed plant installations can be considered acceptable in terms of noise.

Appendix A – Acoustic Terminology

A-weighting (e.g. dB(A))	A correction applied across the frequency bands to take into account the response of the human ear, and therefore considered to be more representative of the sound levels people hear.
DeciBel (dB)	Unit used for many different acoustic parameters. It is the logarithmic ratio of the level being assessed to a standard reference level.
L_{eq}	The level of a notional steady sound which, over a stated period of time, T, would have the same acoustic energy as the fluctuating noise measured over that period. Typically used to represent the average or ambient noise level.
$L_{Aeq,T}$	The A-weighted level of a notional steady sound which, over a stated period of time, T, would have the same acoustic energy as the fluctuating noise measured over that period. Typically used to represent the average or ambient noise level.
L_{An} (e.g. L_{A10}, L_{A90})	The sound level exceeded for n% of the time. E.g. L_{A10} is the A-weighted level exceeded for 10% of the time and as such can be used to represent a typical maximum level. Similarly, L_{A90} is the level exceeded for 90% of the measurement period, and is often used to describe the underlying background noise.
NR	Noise Rating – A single figure term to describe a measured noise level which considers the frequency content of the noise, generally used for internal noise level measurements (particularly mechanical services plant).

Appendix B – Instrumentation

The following equipment was used for the measurements.

Table B1– Equipment Calibration Details

Manufacturer	Model Type	Serial No.	Calibration	
			Certificate No.	Valid Until
Norsonic Type 1 Sound Level Meter	Nor140	1407476	U45756	26 October 2025
Norsonic Pre Amplifier	1209	22340		
Norsonic ½“ Microphone	1225	358242	45722	
Norsonic Sound Calibrator	1255	125525265	U45754	26 October 2025

Appendix C – Plant Calculations

Table C1 – Example Calculation, CU1 to Receptor 1

Calculation	Sound Level (dB) at Octave Band Centre Frequency (Hz)								dBA
	63	125	250	500	1k	2k	4k	8k	
Source Sound Pressure Level (L_p@1m)	55	63	58	55	51	47	43	36	**57**
Distance Loss (Point Source) (9m)	-19	-19	-19	-19	-19	-19	-19	-19	
Relections	+3	+3	+3	+3	+3	+3	+3	+3	
Resulting Level at Receptor (L_{eq})	39	47	42	39	35	31	27	20	**41**

Table C2 – Example Calculation, CU2 to Receptor 1

Calculation	Sound Level (dB) at Octave Band Centre Frequency (Hz)								dBA
	63	125	250	500	1k	2k	4k	8k	
Source Sound Pressure Level (L_p@1m)	51	54	52	50	43	38	33	24	**50**
Distance Loss (Point Source) (9m)	-19	-19	-19	-19	-19	-19	-19	-19	
Reflections	+3	+3	+3	+3	+3	+3	+3	+3	
Resulting Level at Receptor (L_{eq})	35	38	36	34	27	22	17	8	**34**

Table C3 – Example Calculation, EF1 to Receptor 1

Calculation	Sound Level (dB) at Octave Band Centre Frequency (Hz)								dBA
	63	125	250	500	1k	2k	4k	8k	
Source Sound Power Level (Induct L_w)	78	76	74	70	68	64	57	49	**73**
Duct Losses (including grille-end reflection)	-13	-9	-5	-3	-2	-3	-3	-3	
Silencer	-2	-5	-11	-17	-20	-19	-12	-10	
Directivity	0	+1	+2	+3	+4	+5	+6	+6	
Hemispherical Radiation	-8	-8	-8	-8	-8	-8	-8	-8	
Distance Loss (9m)	-19	-19	-19	-19	-19	-19	-19	-19	
Resulting Level at Receptor (L_{eq})	36	36	33	26	23	20	21	15	**30**

Table C4 – Example Calculation, SF1 to Receptor 1

Calculation	Sound Level (dB) at Octave Band Centre Frequency (Hz)								dBA
	63	125	250	500	1k	2k	4k	8k	
Source Sound Power Level (Induct L_w)	72	84	73	71	69	64	58	50	**74**
Duct Losses	-13	-9	-5	-3	-2	-3	-3	-3	
Example Silencer	-5	-11	-19	-29	-36	-37	-29	-18	
Directivity	0	+1	+2	+3	+4	+5	+6	+6	
Hemispherical Radiation	-8	-8	-8	-8	-8	-8	-8	-8	
Distance Loss (7m)	-17	-17	-17	-17	-17	-17	-17	-17	
Resulting Level at Receptor (L_{eq})	29	40	26	17	10	4	7	10	**25**

Table C2 – Summary Noise Levels

Unit	Received noise level (dB) at 1m from Receptor 1	Received noise level (dB) at 1m from Receptor 2	Received noise level (dB) at 1m from Receptor 3
CU1	46 (including corrections)	41 (including corrections)	50 (including corrections)
CU2	34	30	40
EF1	30	27	35
SF1	32 (including corrections)	42 (including corrections)	28 (including corrections)
Total Received Level	**46**	**45**	**51**

Appendix D – Graphs and Site Plans

Gails Bakery, Seven Dials, Brighton

L_{Aeq} Time History

MP1 - First Floor Roof Level, Wednesday 10th January to Thursday 11th January 2024

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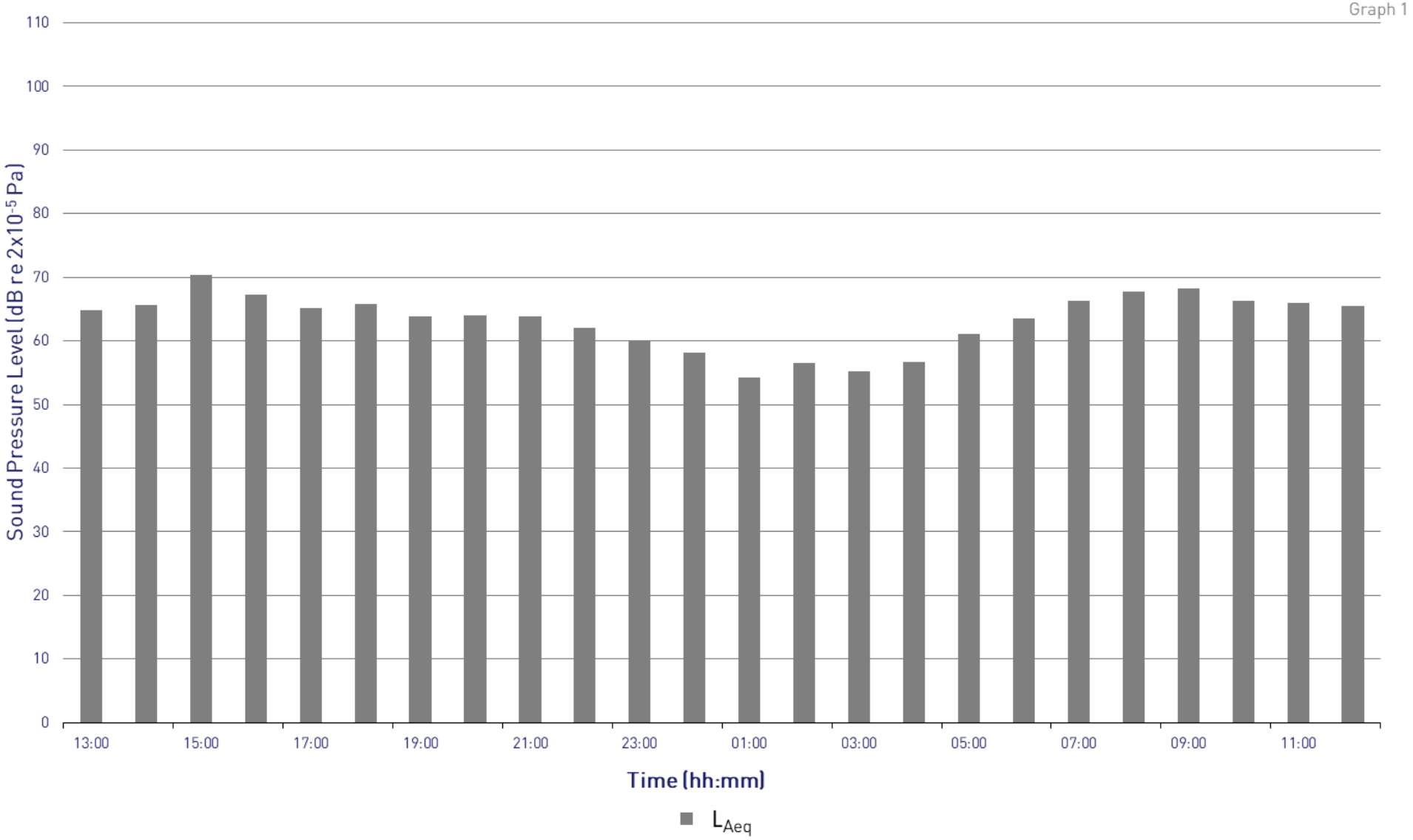
Graph 1



Gails Bakery, Seven Dials, Brighton

$L_{Amax,f}$ and L_{A90} Time History

MP1 - First Floor Roof Level, Wednesday 10th January to Thursday 11th January 2024

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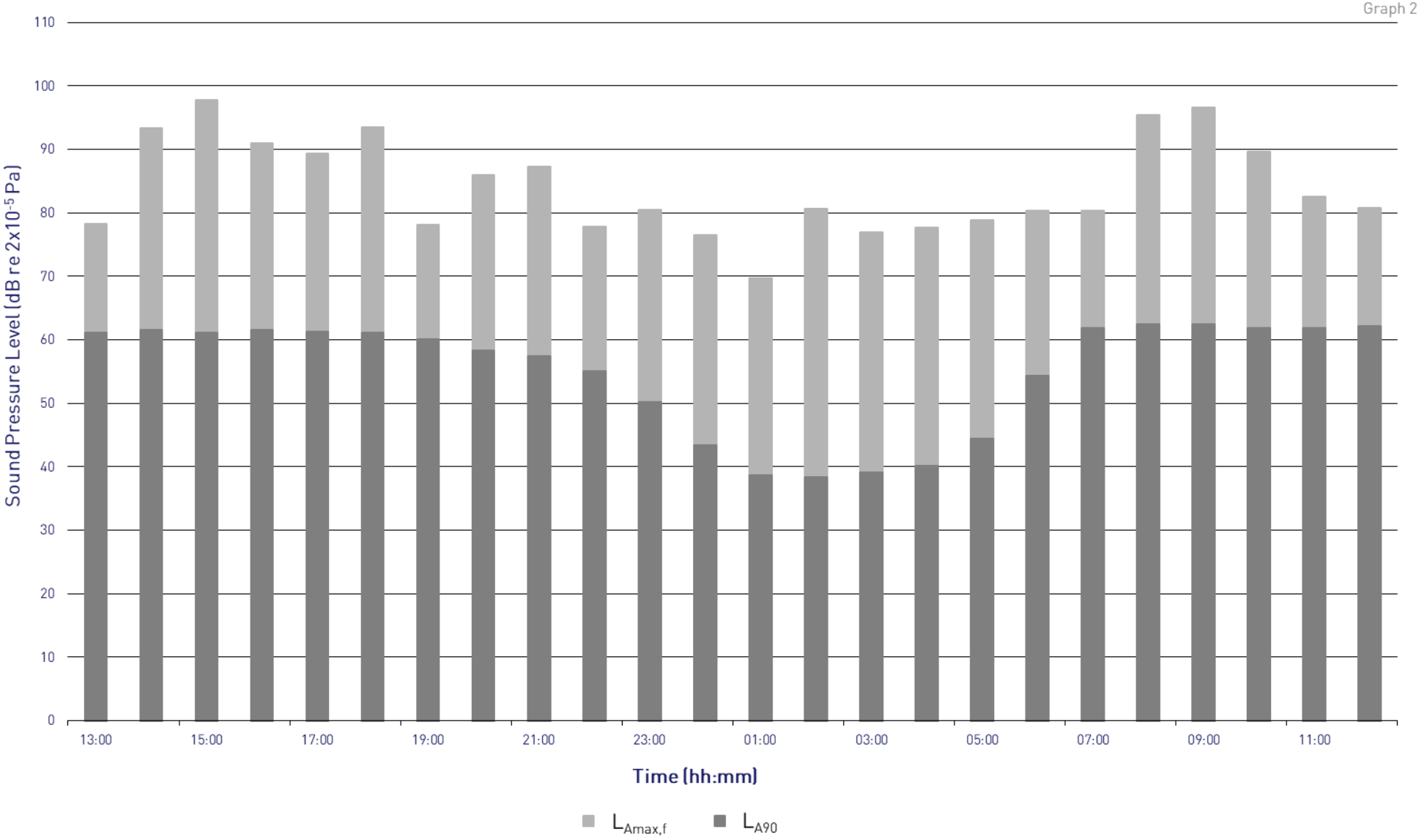
Graph 2



Gails Bakery, Seven Dials, Brighton

$L_{A90,1\,hour}$ Histogram

MP1 - First Floor Roof Level, Wednesday 10th January to Thursday 11th January 2024

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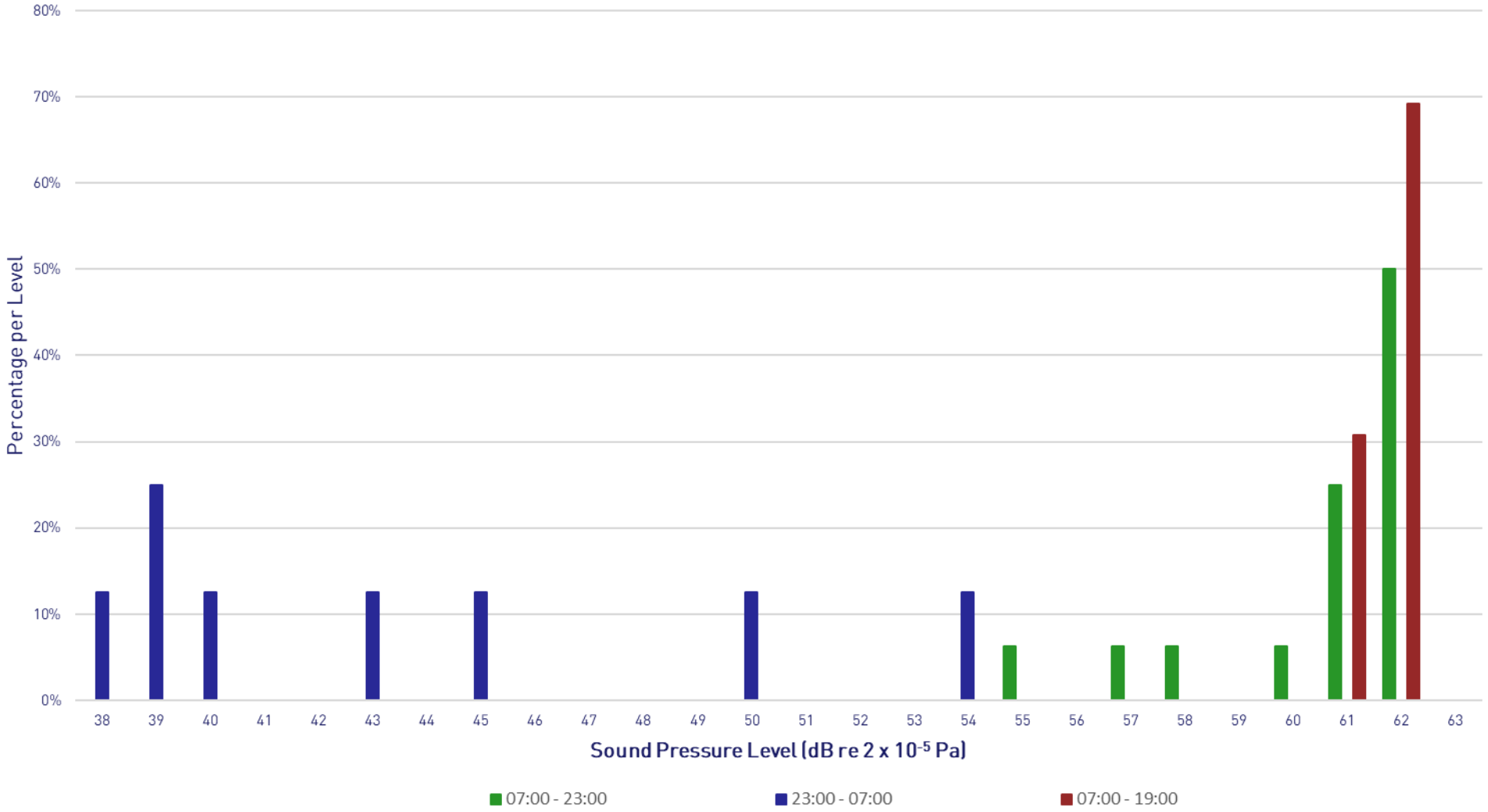
Graph 3



Gails Bakery, Seven Dials, Brighton

L_{Aeq} Time History

MP1 - First Floor Roof Level, Wednesday 10th January to Thursday 11th January 2024

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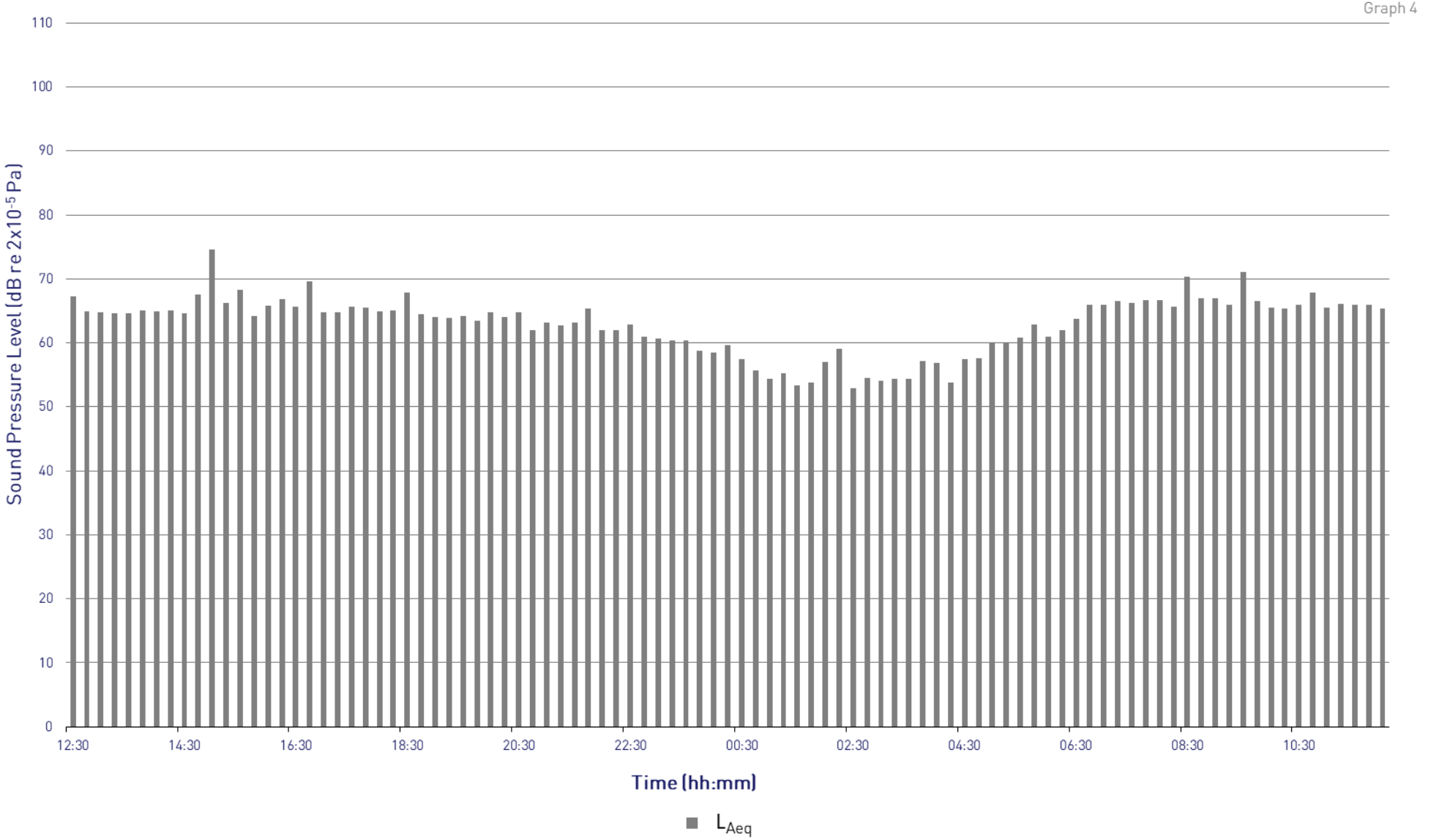
Graph 4



Gails Bakery, Seven Dials, Brighton

$L_{Amax,f}$ and L_{A90} Time History

MP1 - First Floor Roof Level, Wednesday 10th January to Thursday 11th January 2024

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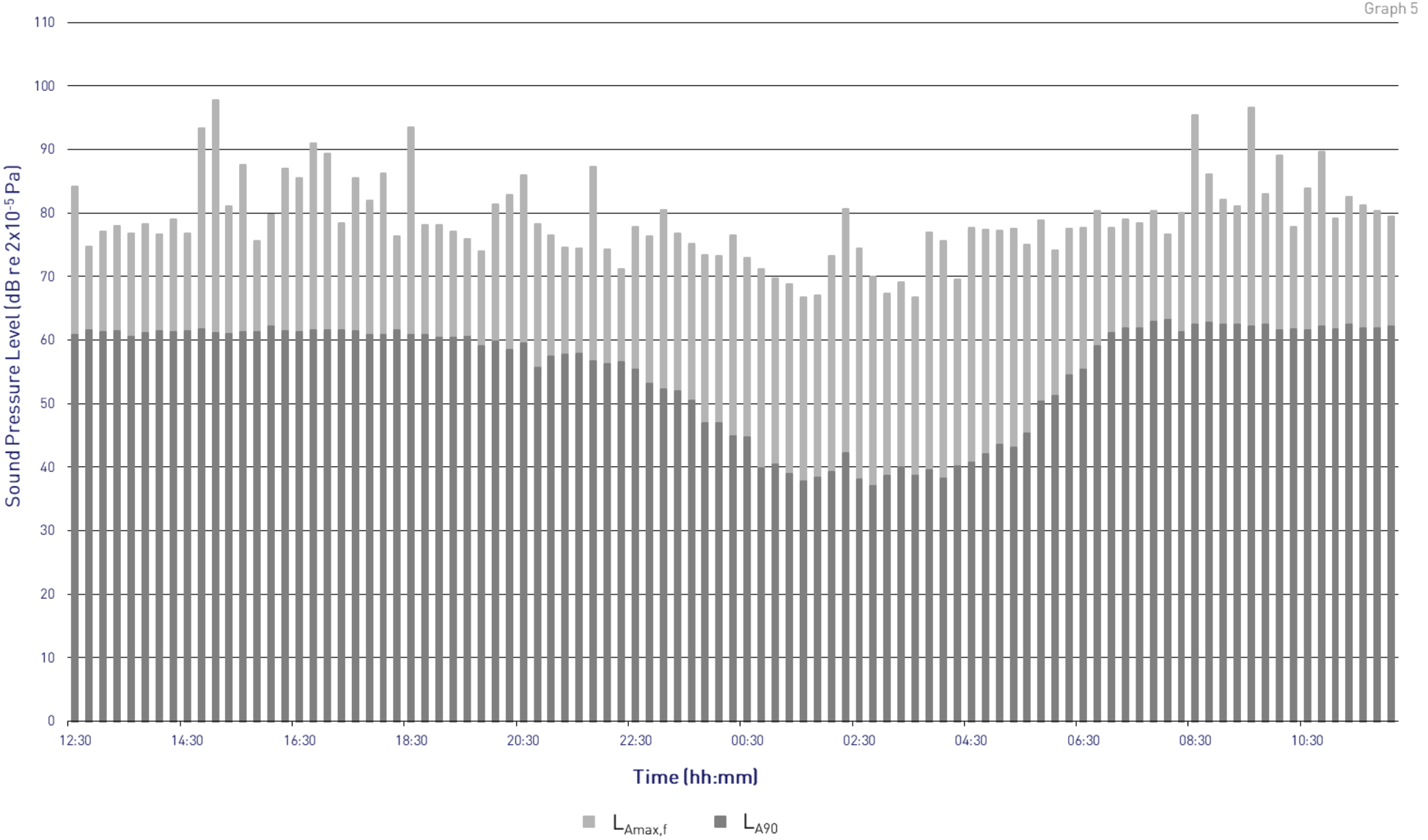
Graph 5



Gails Bakery, Seven Dials, Brighton

$L_{A90,15\ minutes}$ Histogram

MP1 - First Floor Roof Level, Wednesday 10th January to Thursday 11th January 2024

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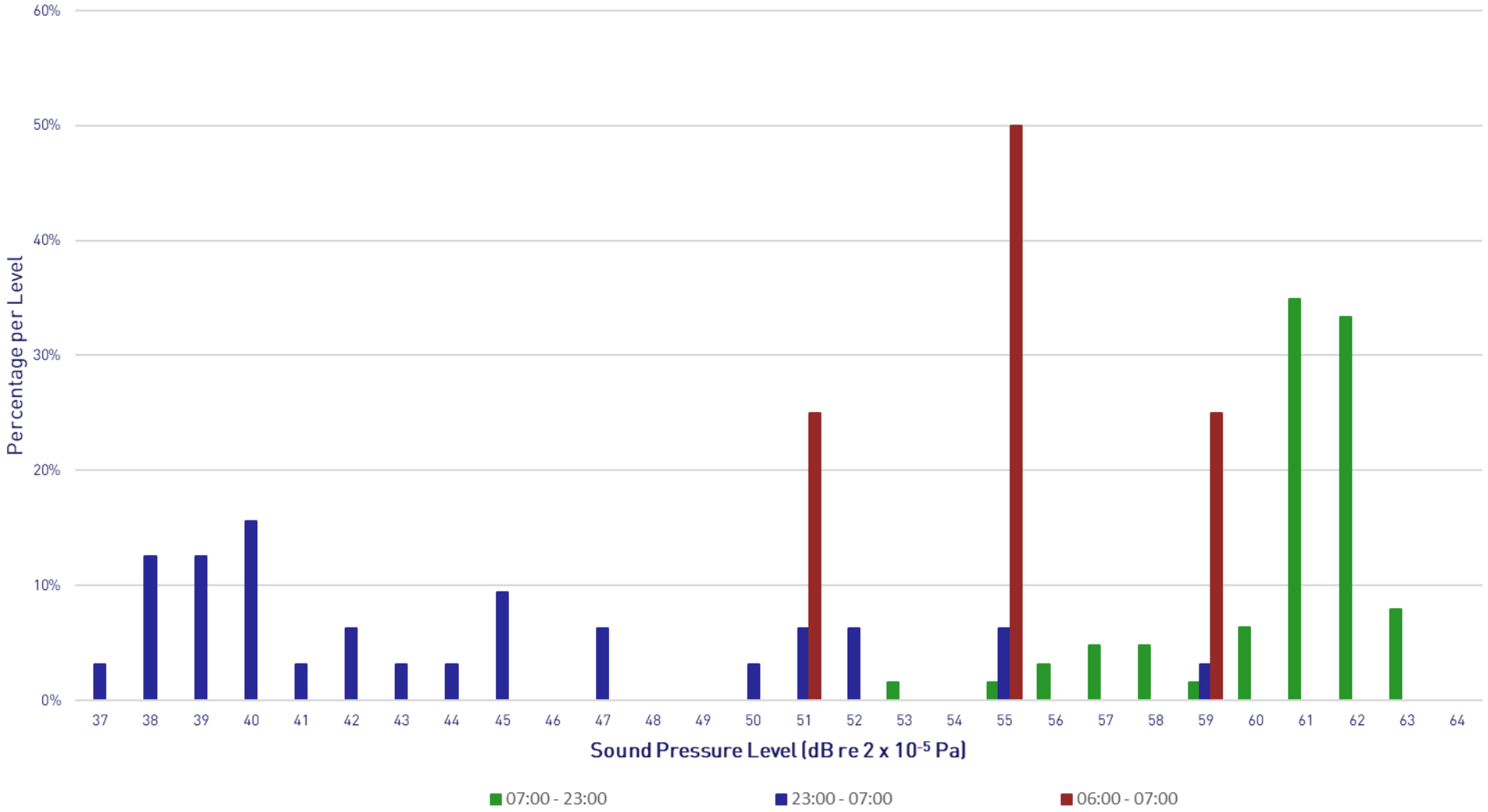
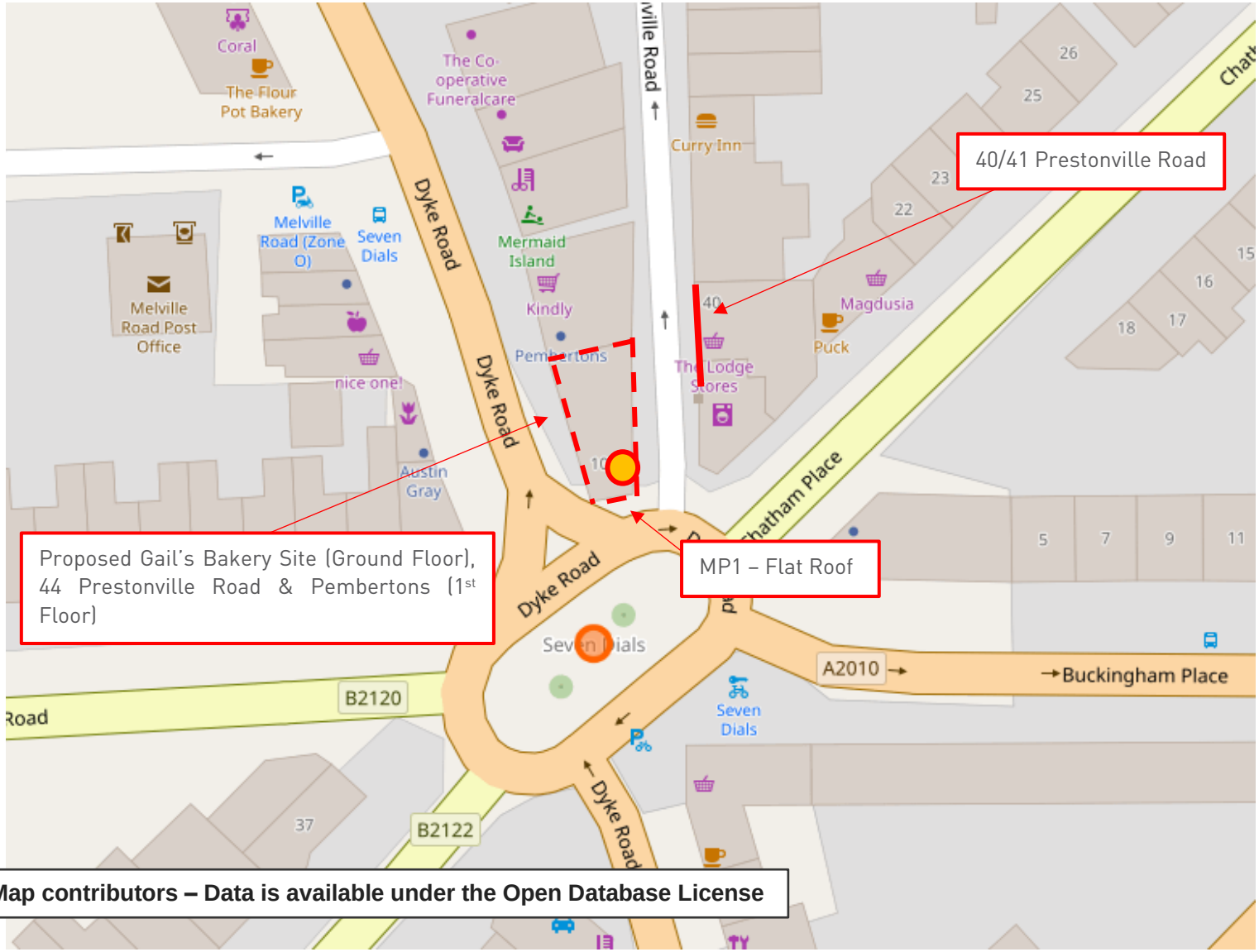
Graph 6





Gail's Bakery, Seven Dials, Brighton

Site Plan

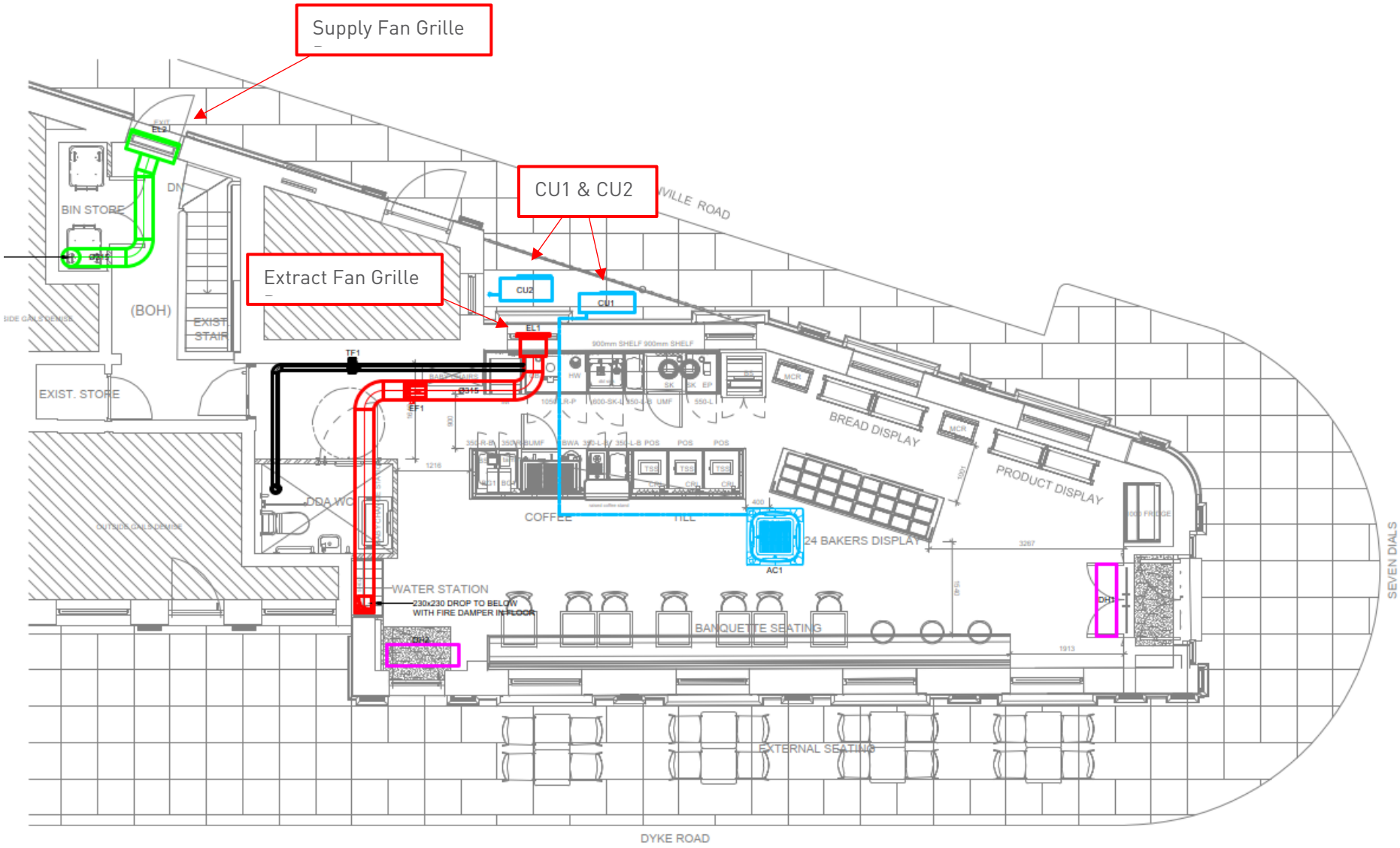
Project 13302

Figure 1

24 January 2024

Not to Scale

RBA ACOUSTICS



Gail's Bakery, Seven Dials, Brighton

Site Plan Showing Items of Plant

Project 13302

Figure 2

24 January 2024

Not to Scale

RBA ACOUSTICS

Gail's Bakery, Seven Dials, Brighton

Photographs

Project 13302

Figure 3

24 January 2024

Not to Scale

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