Hydrock Lawnfield, Maidenhead Drainage Strategy Report

For Propco (Maidenhead) Ltd

Date:22 September 2023Doc ref:29512-HYD-XX-XX-RP-C-0001



DOCUMENT CONTROL SHEET

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CONTENTS

1.	INTRODUCTION	1
2.	SITE INFORMATION	2
2.1	Location	2
2.2	Existing site conditions	3
3.	PROPOSED DEVELOPMENT	3
4.	FLOOD RISK	4
5.	FOUL WATER DRAINAGE	5
5.1	Overview	5
6.	STORM WATER DRAINAGE	6
6.1	Objective	6
6.2	Suitable Run-off Destinations	6
6.3	Infiltration Rates	7
6.4	Suitability of Sustainable Drainage Systems (SuDS) Components	7
6.5	Proposed Interception Storage	10
6.6	Proposed Storm Water Strategy	10
6.7	Storm water Catchment areas	11
6.8	Exceedance Routes	11
6.9	Operation and maintenance	11
7.	APPENDIX A	12
(PROPC	DSED DRAINAGE STRATEGY)	12
8.	APPENDIX B	13
(SEWEI	R MAP)	13
9.	APPENDIX C	14
(EA FLC	DOD MAP)	14
10.	APPENDIX D	15
(MICRO	DDRAINAGE STORM MODELLING CALCULATONS)	15
11.	APPENDIX E	16
(SURFA	ACE WATER EXCEEDANCE ROUTES)	16
12.	APPENDIX F	17
(OPERA	ATIONS AND MAINTENANCE SCHEDULE)	17



1. INTRODUCTION

This Drainage Strategy Report has been prepared by Hydrock Consultants Limited (Hydrock) on behalf of our client Propco (Maidenhead) Ltd in support of a Planning Application for the development of a residential care home located at Lawnfield House, Maidenhead. This report has been prepared to address the requirements for storm and foul water discharge and provide guidance on how the proposed development site could effectively drain through on-site sustainable drainage techniques and off-site foul drainage infrastructure.

The drainage strategy is a guide on how compliant drainage scheme could be designed on site in accordance with the Flood and Water Management Act 2010, National Planning Policy Framework (NPPF), the Lead Local Flood Authority (LLFA) and Local Planning Authority (LPA) requirements.

The information received is summarised within this report. In the event that the information is relied upon and is subsequently found to be incorrect, Hydrock Consultants Ltd accepts no responsibility for any direct and/or consequential loss that may occur as a result.

The information has been reviewed against the following industry design standard to ensure the drainage is compliant;

- Building regulations Part H: Drainage & Waste Disposal;
- Sewers for Adoption/Design and Construction Guidance;
- The requirements of Wessex Water;
- CIRIA C753: The SuDS Manual; and
- Lead Local Flood Authority requirements;
- BS EN 752 Drain and Sewer Systems Outside Buildings.
- Local Authority Guidance.
- National Planning Policy Framework (NPPF).
- DEFRA Non-Statutory Technical Standards for Sustainable Drainage.



2. SITE INFORMATION

2.1 Location

The site is located in Maidenhead, with the A4 Bath Road to the North and Westmorland Road to the West. The site is bound by residential to the south and commercial properties to the east.

The site address and Ordnance Survey Grid Reference is provided in Table 1 with the site location included in Figure 1.

SITE REFERENCING INFORMATION				
Site address	Lawnfield House, Westmorland Road, Maidenhead, SL6 4HB			
Grid Reference	487846, 181046			

Table 1: Site referencing Information

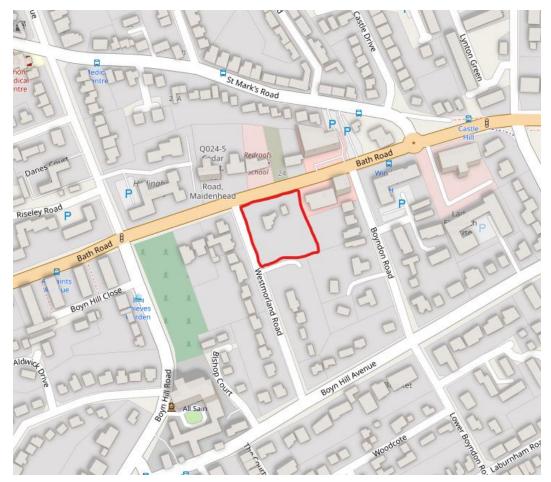


Figure 1: Site Location

Contains OS data © Crown copyright (2020)



2.2 Existing site conditions

The existing topography of the site generally slopes from east to west, with a fall at the north of the site of 50.600m AOD to 50.170m AOD over 84m to give a fall of 1:195. The levels fall away from the existing residential property.

A site investigation and ground assessment has been undertaken by bEk Enviro Ltd (ref. BEK-23079-2). The ground conditions consist of a reddish brown slightly clayey significantly gravelly sand/ greyish brown gravelly sand topsoil underlaid by gravelly sand. Further borehole logs within 250m of the site show firm rubbly chalk underlaying the clayey sandy gravel.

3. PROPOSED DEVELOPMENT

It is proposed to erect a 3-storey 71 bedroom residential care home with associated car parking, access, and landscaped areas.



4. FLOOD RISK

The Environment Agency flood risk mapping as shown within **Appendix C** of this report shows the site is located within flood risk zone 1 which is a low probability of flooding.

- > The site is **not** bigger than 1 hectare (ha)
- > The site is **not** in an area with critical drainage problems as notified by the Environment Agency
- The site is **not** identified as being at increased flood risk in future by the local authority's strategic flood risk assessment
- The site is not at risk from other sources of flooding (such as surface water or reservoirs) and its development would increase the vulnerability of its use (such as constructing an office on an undeveloped site or converting a shop to a dwelling)



Figure 2: Surface water flooding map

Based on the above information no further flood risk assessments are required.



5. FOUL WATER DRAINAGE

5.1 Overview

Foul water drainage from the building is to discharge, via a gravity system, to a proposed manhole connecting into the existing Thames Water 150Ø foul sewer located in Westmorland Road. Refer to **Appendix B** for Thames Water sewer mapping. A Section 104 agreement will be required for the adoption of the foul pipe within the Highway and Section 106 agreement for connection to the Public Sewer.

A foul pumping system will be required to discharge the foul drainage from the proposed basement. The proposed pump will be within the site boundary, and the rising main will connect into private foul network.

The occupant number for the proposed development is 70 residents and 30 members of staff during peak hours. The flow rate for a residential care home is 350 litres per day per occupant, based on British Water Flows and Loads. The care home's foul discharge will peak for 8 hours of the day, which gives a peak foul discharge of 7.29 l/s. The part-full conditions of a 150Ø with a 1:150 gradient gives a pipe capacity of 10.57 l/s which is greater than the peak foul discharge rate.

The foul drainage layout and arrangement is shown in Appendix A.



6. STORM WATER DRAINAGE

6.1 Objective

The objective of the concept drainage strategy is to provide guidance on how the proposed development site could effectively drain through on-site sustainable drainage techniques and to off-site drainage infrastructure, based on the drainage and ground condition information collected and reviewed to date. This document includes a fixed and calculated drainage strategy, in line with current legislation. The design of a successful compliant drainage system for this site is entirely dependent on sustainable drainage principles and requirements being fully incorporated into the site layout to meet the provisions of the Local Planning Authority and the Flood and Water Management Act 2010.

6.2 Suitable Run-off Destinations

An appraisal has been undertaken to confirm the most suitable and sustainable method for managing surface water runoff from the development in accordance with the following hierarchy as highlighted in Part H of Building Regulations and the National Planning Policy Framework (NPPF). This assesses the different surface water management techniques that can avoid, reduce, or delay the surface water discharge from site. The options of discharging storm water off site in order of priority is as follows:

- 1. Infiltration to the ground using a sustainable drainage system.
- 2. If this is not feasible, discharge to a watercourse or river; generally, at a controlled rate unless it does not affect flood risk e.g., if to the sea or an estuary.
- 3. Discharge at a controlled rate to a surface water sewer or drain.
- 4. Discharge at a controlled rate to a combined sewer system, with the approval from the Water Authority.
- 5. Only if the above have all been investigated and it has been proved that none of these options are suitable will discharge at a controlled rate to a foul sewer system, with the approval from the Water Authority.

The techniques consider the use of soakaways in accordance with the Building Regulations Approved Document H order of priority. As mentioned in Section 2.2, the existing ground conditions are suitable for the use of soakaways and the proposed storm network will discharge using cellular soakaway crates.

Method	Reasoning	
Interception / Re-use	Deemed inappropriate	Х
Infiltration	Ground is unsuitable for infiltration methods	\checkmark
Surface water body	Will discharge into Dean Brook Tributary to the south.	Х
To dedicated surface water sewer (public, highways or otherwise)	There are no storm water sewers in the vicinity	Х
To a combined sewer	Not required	Х
To a foul sewer	Not required	Х



6.3 Infiltration Rates

The infiltration rates were recorded as part of the site's ground investigation report (REF BEK-23079-2) and the results are shown in Table 2 below. The results were taken from two trial pits with a repeated test undertaken at TP1. The location of TP1 is near the proposed soakaway location. Further infiltration testing will need to be undertaken at the exact location of the soakaway to ensure the effectiveness of the proposed soakaway.

Trial pit location	Recorded infiltration rate (m/hour)
TP1 – test 1	0.4607
TP1 – test 2	0.3877
TP2 – test 1	0.1300

Table 2: Infiltration rate results

A conservative approach has been used for the infiltration rate required for the storm water calculations. An infiltration rate of 0.3877 m/hour has been used.

6.4 Suitability of Sustainable Drainage Systems (SuDS) Components

There is now a mandatory requirement to provide a sustainable drainage system throughout the development and not just at the "end" of the drainage system via length of pipe work. It is highly unlikely that the traditional "pipe and tank" system will be accepted by the LLFA and Local Planning Authority. The key points of the surface water drainage strategy will be to:

- » Utilise the external areas of the site that will be subject to rainfall to treat and improve the water quality and to store the surface water flows as close to source as possible.
- » Minimise the runoff from all impermeable areas through the widespread use of open SuDS drainage features.
- » To enhance the biodiversity and amenity value by incorporating suitable SuDS features into the development.
- » Avoid hard engineered pipes and tanks. The strategy described in this report is based on the principles of the CIRIA SuDS Manual C753

The implementation and selection of SuDS techniques is largely dependent on the site layout and context. Some SuDS techniques may be more appropriate than others.

The suitability of SuDS components has been assessed as follows:

Hierarchy	Description	Setting	Required area	Implemented	
Green roofs	A planted soil layer is constructed on the roof of a building to create a living surface. Water is stored in the soil layer and absorbed by vegetation.	Building	Building integrated.	No. Recommend for Architect to include where possible.	X
Rainwater harvesting	Rainwater is collected from the roof of a building or from other paved surfaces and stored in an over ground or underground tank for treatment and reuse locally. Water could be used for toilet flushing and irrigation.	Building	Water storage (Underground or above ground).	No. Recommend for Architect to include where possible.	X



Hierarchy	Description	Setting	Required area	Implemented	
Soakaway	A soakaway is designed to allow water to quickly soak into permeable layers of soil. Constructed like a dry well, an underground pit is dug filled with gravel or rubble. Water can be piped to a soakaway where it will be stored and allowed to gradually seep into the ground.	Open space	Dependent on runoff volumes, water table and soils.	Yes, Soakaway will be used to discharge the storm water.	\checkmark
Filter Strips	Filter drains are shallow stone filled trenches that provide attenuation, conveyance, and treatment of runoff	Open space	Dependent on runoff volumes	No due to restricted space.	Х
Permeable paving	Paving which allows water to soak through. Can be in the form of paving blocks with gaps between solid blocks or porous paving where water filters through the block itself. Water can be stored in the sub-base beneath or allowed to infiltrate into ground below.	Street / open space	Can typically drain double its area.	Yes. Permeable paving will be used for the majority parking spaces.	\checkmark
Bioretention area or Raingardens	A vegetated area with gravel and sand layers below designated to channel, filter, and cleanse water vertically. Water can infiltrate into the ground below or drain to a perforated pipe and be conveyed elsewhere. Bioretention systems can be integrated with tree-pits or gardens.	Street / open space	Typically, surface area is 5-10% of drained area with storage below.	No due to restricted space.	Х
Swale/Raingarden	Swales and raingardens are shallow depressions designed to convoy and filter water. These can be 'wet' where water gathers above the surface, or 'dry' where water gathers in a gravel layer beneath. Can be lined or unlined to allow infiltration.	Street / open space	Account for width to allow safe maintenance typically 2–3 metres wide.	No, pond will be used	Х
Hardscape storage	Hardscape water features can be used to store run-off above ground within a constructed container. Storage features can be integrated into public realm areas with a more urban character.	Street / open space	Could be above or below ground and sized to storage need.	No. Soakaway will be utilised	X



Hierarchy	Description	Setting	Required area	Implemented	
Pond / Basin	Ponds can be used to store and treat water. 'Wet' ponds have a constant body of water and run-off is additional, while 'dry' ponds are empty during periods without rainfall. Ponds can be designed to allow infiltration into the ground or to store water for a period before discharge.	Open space	Dependent on runoff volumes and soils.	No due to restricted space.	Х
Wetland	Wetlands are shallow vegetated water bodies with a varying water level. Specially selected plant species are used to filter water. Water flows horizontally and is gradually treated before being discharged. Wetlands can be integrated with a natural or hardscape environment.	Open space	Typically, 5– 15% drainage area to provide good treatment.	No due to restricted space.	Х
Underground storage	Water can be stored in tanks, gravel, or plastic crates beneath the ground to provide attenuation.	Open space	Dependent on runoff volumes and soils.	No. Additional underground storage not required	Х



6.5 Proposed Interception Storage

Interception can be defined as the capture and retention on site of the first 5mm of the majority of all rainfall events. Interception mechanisms have been assessed to show the site is compliant for zero run-off from the first 5mm for 80% of events during the summer and 50% in winter. (Ciria)

Systems	Reasoning	
Green roofs	All surfaces that have green / blue roofs	Х
Rainwater harvesting	All surfaces drained to RWH systems designed whether for surface water management or just water supply, provided the RWH system design is based on regular daily demand for non-potable water	X
Soakaways / infiltration	Areas of the site drained to systems that are designed to infiltrate run-off for events greater than a 1 month return period.	\checkmark
Permeable pavements	All permeable pavements, whether lined or not, can be assumed to comply, provided there is no extra area drained to the permeable pavement.	\checkmark
Filter strips / swales	Roads drained by filters strips / swales, where the longitudinal gradient of the vegetated area is less than 1:100, are suitable for interception delivery for impermeable areas up to 5 times the base of the vegetated surface area receiving the runoff.	Х
Infiltration trenches	Roads drained by infiltration trenches can be considered to provide interception	Х
Detention basins	Areas of the site drainage to detention basin with a flat base can be assumed to comply. The area of the basin that is assumed to contribute to interception of run-off should be below the outlet of the basin.	X
Bioretention / rain gardens	Areas of the site drainage to unlined bioretention components can be assume to comply where the impermeable area is less than 5 times the vegetated surface area receiving run-off/ They can be designed to deliver interception for larger areas, where suitable infiltration capacity is available.	Х
Ponds	Areas drained by ponds (with a permanent water pool that is effectively maintained by the outlet structure) are not assumed to deliver interception	Х

6.6 Proposed Storm Water Strategy

The proposed residential care home will be positively drained which includes the roof area and the impermeable asphalt road connecting the car park to Westmorland Road. The storm network runs along the perimeter of the building before collecting into the cellular soakaway crates located in the car park. A D-rainclean bioretention channel will run across the site entrance from Westmorland Road to capture the storm runoff, before connecting into the soakaway. Catchpits chambers will be used prior to the soakaway to limit any pollutants entering the crates.

The network has been modelled using Microdrainage for all storm events up to and including the 1in100yr+40% climate change storm water event with the results shown within Appendix D of this report. The modelling shows no flooding for events up to and including the 1in100yr+40%CC event with the infiltration rate of 0.3877 (m/hour)

The storm network is subject to approval from the Lead Local Flood Authority and the EA.

The storm drainage layout and arrangement are shown in Appendix A.



6.7 Storm water Catchment areas

The site storm water catchment area has been calculated for the roof (1310m2) and impermeable asphalt road (51m2) which will be positively drained, totalling to 0.136 ha. The permeable paving in the car park will percolate to the existing ground. The hard landscaping will be permeable and infiltrate to the ground.

6.8 Exceedance Routes

Surface levels will be designed to ensure finished levels fall away from the building. It should be noted that permeable paving will infiltrate into the ground and hard landscaping surrounding the building will be permeable. The surface water runoff from the impermeable asphalt onto Westmorland Road will be collected via a linear channel to stop discharge to the public highway.

Refer to Appendix E for surface water exceedance routes.

6.9 Operation and maintenance

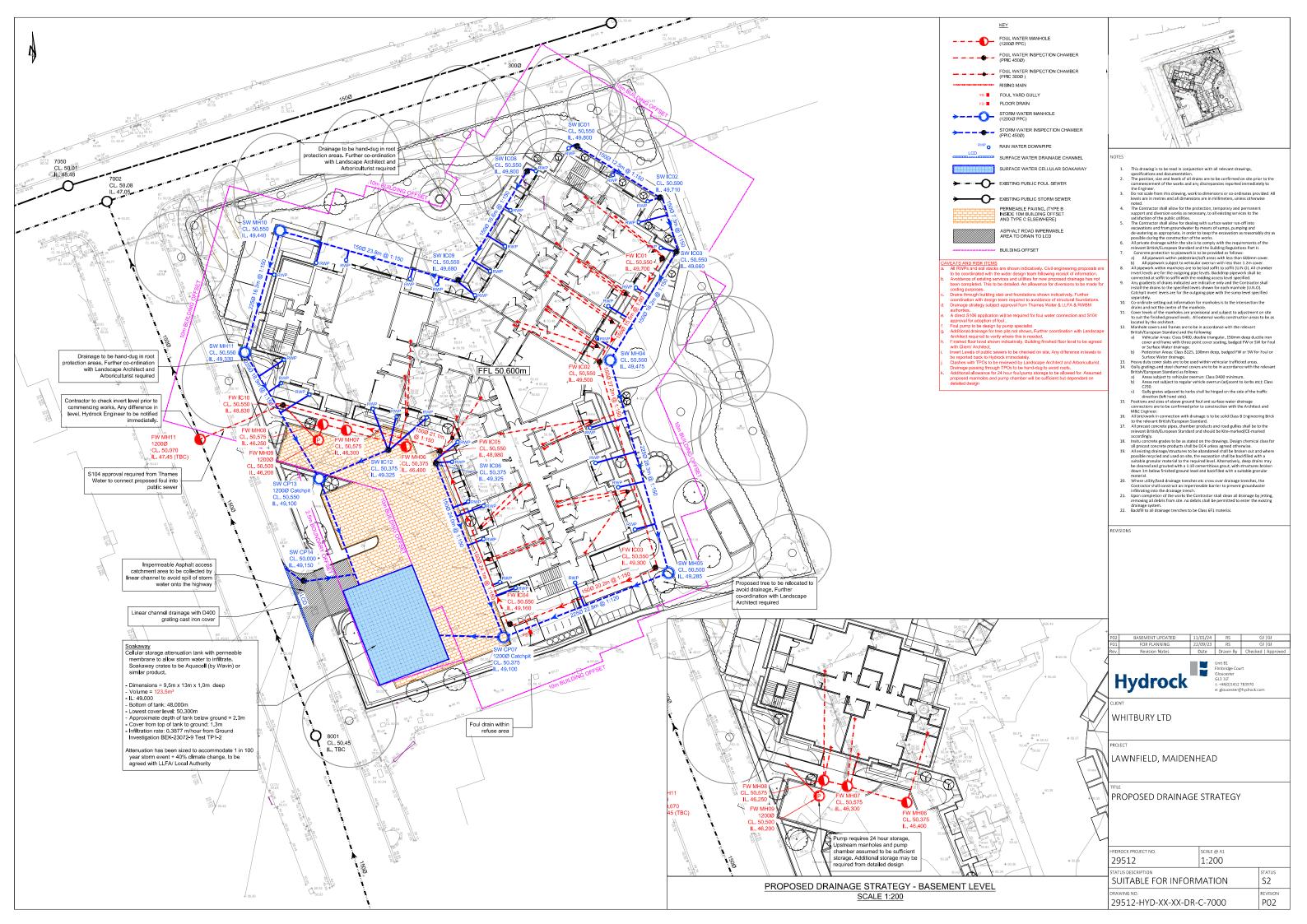
To ensure longevity and effective operation of SuDS they must be maintained in accordance with

- CIRIA 753 guidance and operation and maintenance
- CIRIA report C768 Guidance on the construction of SuDS
- Maintenance plan outlined in section 5.2

Refer to Appendix F operations and maintenance schedule

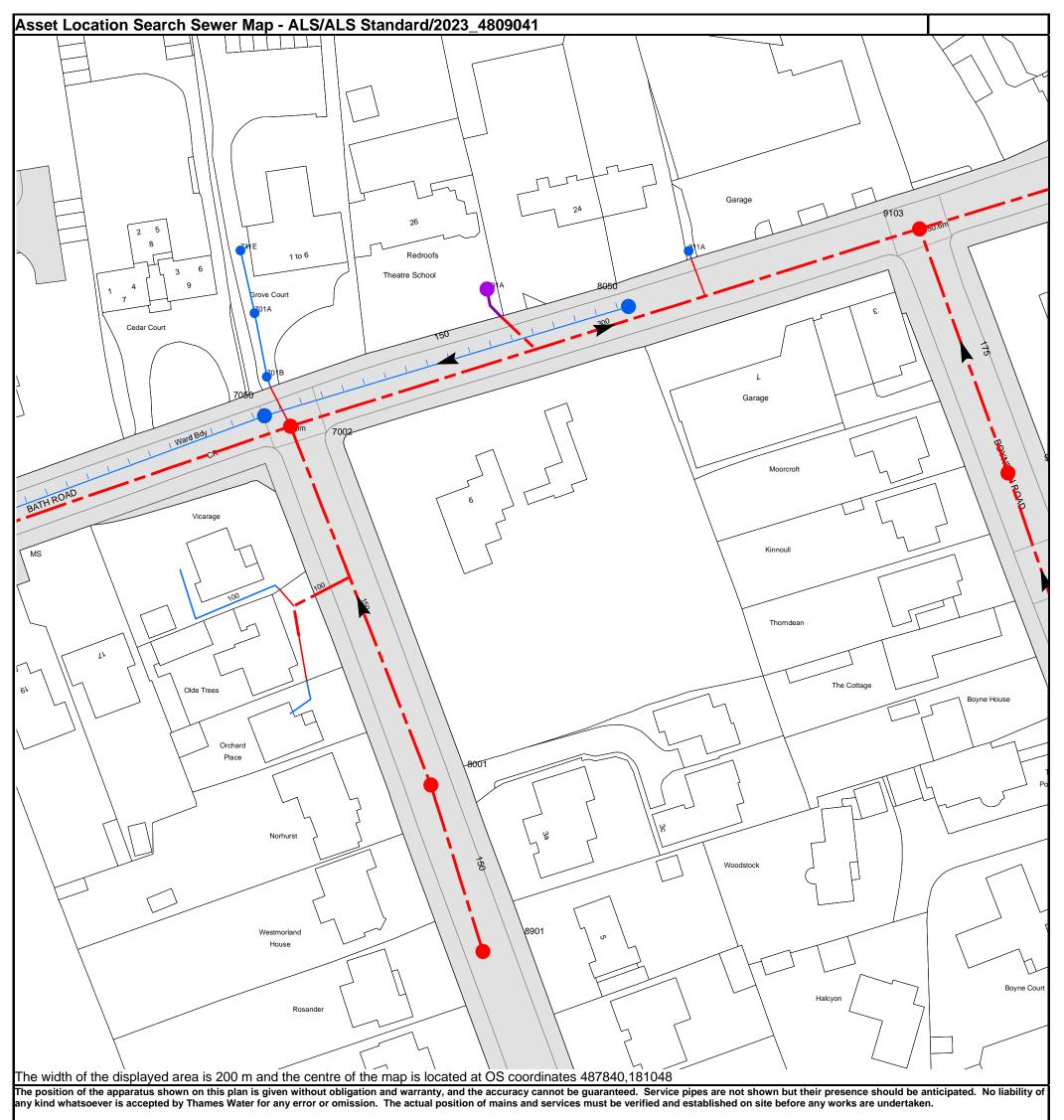


7. APPENDIX A (PROPOSED DRAINAGE STRATEGY)





8. APPENDIX B (SEWER MAP)



Based on the Ordnance Survey Map (2020) with the Sanction of the controller of H.M. Stationery Office, License no. 100019345 Crown Copyright Reserved.

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<u>Thames Water Utilities Ltd</u>, Property Searches, PO Box 3189, Slough SL1 4W, T 0800 009 4540 E <u>searches@thameswater.co.uk</u> I <u>www.thameswater-propertysearches.co.uk</u> NB. Levels quoted in metres Ordnance Newlyn Datum. The value -9999.00 indicates that no survey information is available

Manhole Reference	Manhole Cover Level	Manhole Invert Level
9103	50.83	46.72
9001	49.97	47.13
8901	50.09	48.33
8001	50.45	n/a
7002	50.08	47.05
7050	50.01	48.48
701B	n/a	n/a
701A	n/a	n/a
8050	50.45	48.94
801A	n/a	n/a
811A	n/a	n/a
711E	n/a	n/a

The position of the apparatus shown on this plan is given without obligation and warranty, and the accuracy cannot be guaranteed. Service pipes are not shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified and established on site before any works are undertaken.



9. APPENDIX C (EA FLOOD MAP)



Flood map for planning

Your reference <Unspecified>

Location (easting/northing) 487843/181046

Created **28 Jul 2023 10:47**

Your selected location is in flood zone 1, an area with a low probability of flooding.

You will need to do a flood risk assessment if your site is any of the following:

- bigger that 1 hectare (ha)
- In an area with critical drainage problems as notified by the Environment Agency
- identified as being at increased flood risk in future by the local authority's strategic flood risk assessment
- at risk from other sources of flooding (such as surface water or reservoirs) and its development would increase the vulnerability of its use (such as constructing an office on an undeveloped site or converting a shop to a dwelling)

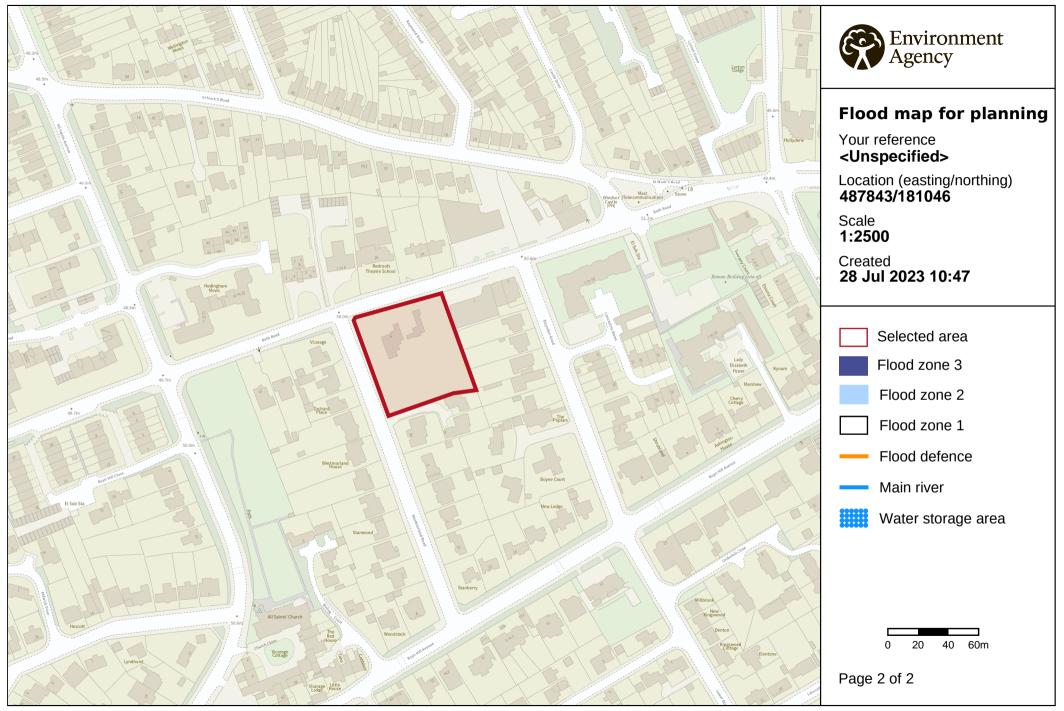
Notes

The flood map for planning shows river and sea flooding data only. It doesn't include other sources of flooding. It is for use in development planning and flood risk assessments.

This information relates to the selected location and is not specific to any property within it. The map is updated regularly and is correct at the time of printing.

Flood risk data is covered by the Open Government Licence **which** sets out the terms and conditions for using government data. https://www.nationalarchives.gov.uk/doc/open-government-licence/version/3/

Use of the address and mapping data is subject to Ordnance Survey public viewing terms under Crown copyright and database rights 2022 OS 100024198. https://flood-map-for-planning.service.gov.uk/os-terms

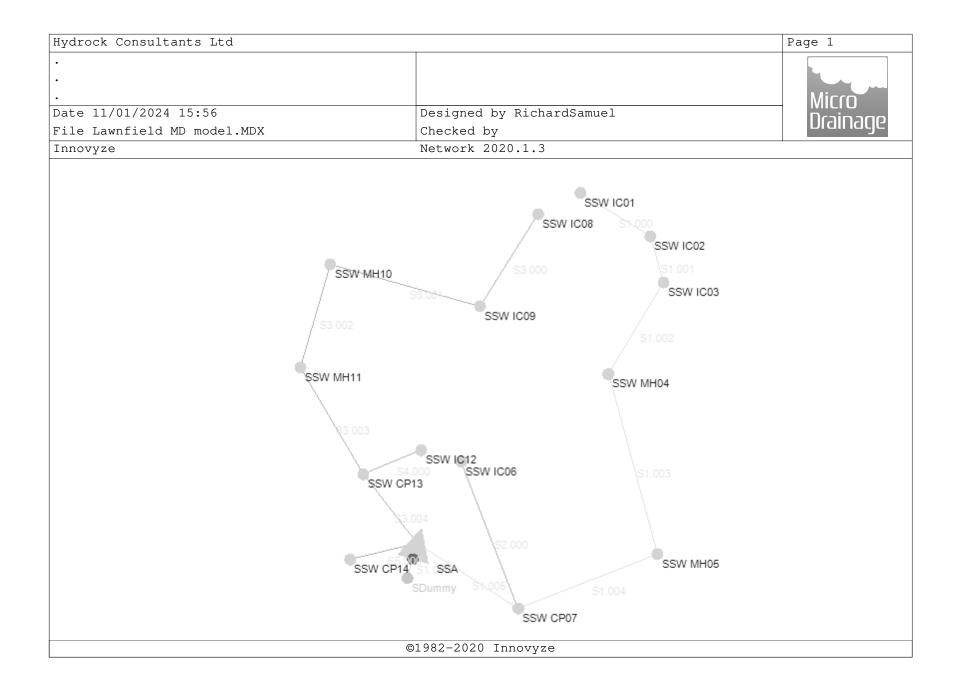


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10. APPENDIX D

(MICRODRAINAGE STORM MODELLING CALCULATONS)



Hydrock Consultants Ltd		Page 0
•	Lawnfield, Maidenhead	
	Storm water calculations	
	29512-HYD-XX-XX-CAL-C-7001	Micro
Date 11/01/2024	Designed by RS	
File Lawnfield MD model.MDX	Checked by GJ	Diamage
Innovyze	Network 2020.1.3	

STORM SEWER DESIGN by the Modified Rational Method

Design Criteria for LAWNFIELD MD MODEL.SWS

Pipe Sizes STANDARD Manhole Sizes STANDARD

FSR Rainfall Model - England and WalesReturn Period (years)100PIMP (%)100M5-60 (mm)19.600Add Flow / Climate Change (%)0Ratio R0.400Minimum Backdrop Height (m)0.200Maximum Rainfall (mm/hr)50Maximum Backdrop Height (m)0.000Maximum Time of Concentration (mins)30Min Design Depth for Optimisation (m)1.200Foul Sewage (l/s/ha)0.000Min Vel for Auto Design only (m/s)0.75Volumetric Runoff Coeff.0.750Min Slope for Optimisation (1:X)500

Designed with Level Soffits

Network Design Table for LAWNFIELD MD MODEL.SWS

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)		Base Flow (l/s)	k (mm)	HYD SECT	DIA (mm)	Section Type	Auto Design
S1.000 S1.001 S1.002 S1.003 S1.004	16.272 28.357	0.050 0.110 0.190	146.0 147.9 149.2	0.003 0.001 0.015 0.026 0.001	5.00 0.00 0.00 0.00 0.00	0.0	0 0.600 0 0.600 0 0.600 0 0.600 0 0.600	0 0 0 0	150 150 225	Pipe/Conduit Pipe/Conduit Pipe/Conduit Pipe/Conduit Pipe/Conduit	8 8 8
	23.984 18.342			0.021	5.00 0.00		0.600	0		Pipe/Conduit Pipe/Conduit	8
	16.565 23.772 16.307	0.165	144.1	0.013 0.021 0.004	5.00 0.00 0.00	0.0	0.600 0.600 0.600	0 0 0	150	Pipe/Conduit Pipe/Conduit Pipe/Conduit	ê 8

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)		Add Flow (l/s)	Vel (m/s)	Cap (1/s)	Flow (l/s)	
S1.000	50.00	5.25	49.800	0.003	0.0	0.0	0.0	0.85	15.0	0.4	
S1.001	50.00	5.39	49.710	0.004	0.0	0.0	0.0	0.83	14.7	0.5	
S1.002	50.00	5.72	49.660	0.019	0.0	0.0	0.0	0.82	14.6	2.6	
S1.003	50.00	6.16	49.475	0.045	0.0	0.0	0.0	1.07	42.5	6.1	
S1.004	50.00	6.49	49.285	0.046	0.0	0.0	0.0	1.18	46.8	6.2	
S2.000	50.00	5.50	49.325	0.021	0.0	0.0	0.0	0.79	14.0	2.8	
S1.005	50.00	6.81	49.100	0.067	0.0	0.0	0.0	0.96	38.3	9.1	
S3.000	50.00	5.32	49.800	0.013	0.0	0.0	0.0	0.85	15.1	1.8	
S3.001	50.00	5.80	49.680	0.034	0.0	0.0	0.0	0.84	14.8	4.6	
S3.002	50.00	6.05	49.440	0.038	0.0	0.0	0.0	1.07	42.6	5.1	
				©1982-2	020 Innov	yze					

Hydrock Consultants Ltd					
•	Lawnfield, Maidenhead				
	Storm water calculations				
	29512-HYD-XX-XX-CAL-C-7001	Mirro			
Date 11/01/2024	Designed by RS	Drainage			
File Lawnfield MD model.MDX	Checked by GJ	Diamage			
Innovyze	Network 2020.1.3				

Network Design Table for LAWNFIELD MD MODEL.SWS

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)		Base Flow (l/s)	k (mm)	HYD SECT	DIA (mm)	Section Type	Auto Design
S3.003	18.861	0.240	78.6	0.010	0.00	0.0	0.600	0	225	Pipe/Conduit	0
S4.000	9.589	0.150	63.9	0.009	5.00	0.0	0.600	0	150	Pipe/Conduit	•
S3.004	13.373	0.100	133.7	0.000	0.00	0.0	0.600	0	225	Pipe/Conduit	•
S5.000	10.569	0.075	140.9	0.005	5.00	0.0	0.600	0	150	Pipe/Conduit	8
S1.006	5.449	0.053	102.8	0.000	0.00	0.0	0.600	0	225	Pipe/Conduit	0

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)		Σ Base Flow (l/s)				Cap (1/s)	
S3.003	50.00	6.26	49.330	0.048	0.0	0.0	0.0	1.48	58.7	6.5
S4.000	50.00	5.13	49.325	0.009	0.0	0.0	0.0	1.26	22.3	1.2
S3.004	50.00	6.46	49.100	0.057	0.0	0.0	0.0	1.13	44.9	7.7
S5.000	50.00	5.21	49.150	0.005	0.0	0.0	0.0	0.84	14.9	0.7
S1.006	50.00	6.88	49.000	0.129	0.0	0.0	0.0	1.29	51.3	17.5

Free Flowing Outfall Details for LAWNFIELD MD MODEL.SWS

Outfall	Outfall	c.	Level	I.	Level		Min	D,L	W
Pipe Number	Name		(m)		(m)	I.	Level	(mm)	(mm)
							(m)		

S1.006 SDummy 50.375 48.947 48.847 1200 0

Simulation Criteria for LAWNFIELD MD MODEL.SWS

Volumetric Runoff Coeff	0.750	Additional Flow - % of Total Flow 0.000)
Areal Reduction Factor	1.000	MADD Factor * 10m³/ha Storage 0.000)
Hot Start (mins)	0	Inlet Coeffiecient 0.800)
Hot Start Level (mm)	0	Flow per Person per Day (1/per/day) 0.000)
Manhole Headloss Coeff (Global)	0.500	Run Time (mins) 60)
Foul Sewage per hectare (l/s)	0.000	Output Interval (mins) 1	L

Number of Input Hydrographs 0 Number of Storage Structures 1 Number of Online Controls 1 Number of Time/Area Diagrams 0 Number of Offline Controls 0 Number of Real Time Controls 0

Synthetic Rainfall Details

Hydrock Consultants Ltd		Page 2			
•	Lawnfield, Maidenhead				
	Storm water calculations				
	29512-HYD-XX-XX-CAL-C-7001	Mirro			
Date 11/01/2024	Designed by RS	Drainage			
File Lawnfield MD model.MDX	Checked by GJ	Diamage			
Innovyze	Network 2020.1.3				

Synthetic Rainfall Details

Rainfall Model		FSR		Profile Type	Summer
Return Period (years)		100		Cv (Summer)	0.750
Region	England	and Wales		Cv (Winter)	0.840
M5-60 (mm)		19.600	Storm	Duration (mins)	30
Ratio R		0.400			

Hydrock Consultants Ltd		Page 3			
•	Lawnfield, Maidenhead				
	Storm water calculations				
	29512-HYD-XX-XX-CAL-C-7001	Mirro			
Date 11/01/2024	Designed by RS	Dcainago			
File Lawnfield MD model.MDX	Checked by GJ	Diamage			
Innovyze	Network 2020.1.3				

Online Controls for LAWNFIELD MD MODEL.SWS

Weir Manhole: SSA, DS/PN: S1.006, Volume (m³): 2.9

Discharge Coef 0.544 Width (m) 1.200 Invert Level (m) 50.375

Hydrock Consultants Ltd		Page 4			
•	Lawnfield, Maidenhead				
	Storm water calculations				
	29512-HYD-XX-XX-CAL-C-7001	Mirro			
Date 11/01/2024	Designed by RS	Drainage			
File Lawnfield MD model.MDX	Checked by GJ	Diamage			
Innovyze	Network 2020.1.3				

Storage Structures for LAWNFIELD MD MODEL.SWS

Cellular Storage Manhole: SSA, DS/PN: S1.006

Invert Level (m) 47.900 Safety Factor 2.0 Infiltration Coefficient Base (m/hr) 0.00000 Porosity 0.95 Infiltration Coefficient Side (m/hr) 0.38770

Depth	(m)	Area	(m²)	Inf.	Area	(m²)	Depth	(m)	Area	(m²)	Inf.	Area	(m²)

0.000	125.0	0.0	1.001	0.0	0.0
1.000	125.0	0.0			

		tants Ltd					Pa	age 5
				Lawni	field, Maiden	nead		
				Storr	n water calcu	lations		
				29512	2-HYD-XX-XX-C	AL-C-7001	N	licco
)ate 1	1/01/202	4		Desid	gned by RS			licro
		MD model.	MDV					Irainac
-		MD model.	MDX		ked by GJ			_
Innovy	ze			Netwo	ork 2020.1.3			
1 vea	r Return	Period Su	mmary o	of Crit	ical Results	by Maximu	m Level	(Rank 1
					D MD MODEL.SW			
			-		on Criteria			
	Ar	eal Reductio Hot Star			Additional Flo	w - % of Te r * 10m³/ha		
	1	HOT Star Hot Start Le			MADD Facto		a Storage ffiecient	
Ma			. ,		Flow per Person			
		ge per hecta				- · ·		
					March - C. C.	<u> </u>		
			-		Number of Stora Number of Time,	-		
					Number of Real	-		
		D-4-6 13		hetic Ra	infall Details		,	
		Rainfall		naland a	FSR Rat nd Wales Cv (Sur	tio R 0.400		
			Region E) (mm)	путапа а	nd Wales CV (Sur 19.600 CV (Win			
		110 00	(11111)		19.000 00 (11)			
	Margi	in for Flood	Risk Wa	rning (m	m)		300.0	
					ep 2.5 Second In	ncrement (E	(xtended)	
				DTS Stat			ON	
				DVD Stat	110			
							OFF	
				tia Stat			OFF	
			Iner	tia Stat			OFF	
			Iner ofile(s)	tia Stat	us	Summer an	OFF d Winter	
	Potu	Duration(s	Iner ofile(s)) (mins)	tia Stat 15, 30,		360, 480, 9	OFF d Winter 60, 1440	
	Retur		Iner ofile(s)) (mins) (years)	tia Stat 15, 30,	us	360, 480, 9	OFF d Winter 60, 1440 30, 100	
	Retur	Duration(s)	Iner ofile(s)) (mins) (years)	tia Stat 15, 30,	us	360, 480, 9	OFF d Winter 60, 1440	
W. PN		Duration(s) n Period(s) Climate Cha	Iner ofile(s)) (mins) (years) ange (%) me has n Return	tia Stat 15, 30, ot been Climate	60, 120, 240, s calculated as th First (X)	360, 480, 9 1, ne structur	OFF 060, 1440 30, 100 0, 0, 40	Overflo
PN	ARNING: Ha US/MH Name	Duration(s) on Period(s) Climate Cha alf Drain Tin Storm	Iner ofile(s)) (mins) (years) ange (%) me has n Return Period	tia Stat 15, 30, ot been Climate Change	60, 120, 240, s calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	OFF 60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000	ARNING: Ha US/MH Name SSW IC01	Duration(s) n Period(s) Climate Cha alf Drain Tin Storm 15 Winter	Iner ofile(s)) (mins) (years) ange (%) me has n Return Period	tia Stat 15, 30, ot been Climate Change +0%	60, 120, 240, s calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	OFF 60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001	ARNING: Ha US/MH Name SSW IC01 SSW IC02	Duration(s) En Period(s) Climate Cha alf Drain Tin Storm 15 Winter 15 Winter	Iner ofile(s)) (mins) (years) ange (%) me has n Return Period 1 1	tia Stat 15, 30, ot been Climate Change +0% +0%	60, 120, 240, s calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	OFF 60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03	Duration(s) cn Period(s) Climate Cha alf Drain Tin Storm 15 Winter 15 Winter 15 Winter	Iner ofile(s)) (mins) (years) ange (%) me has n Return Period 1 1 1	tia Stat 15, 30, ot been Climate Change +0% +0% +0%	60, 120, 240, s calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	OFF 60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW MH04	Duration(s) cn Period(s) Climate Cha alf Drain Tin Storm 15 Winter 15 Winter 15 Winter 15 Winter	Iner ofile(s) (mins) (years) ange (%) me has n Return Period 1 1 1 1	tia Stat 15, 30, ot been Climate Change +0% +0% +0% +0%	60, 120, 240, s calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	OFF 60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03	Duration(s) cn Period(s) Climate Cha alf Drain Tin Storm 15 Winter 15 Winter 15 Winter	Iner ofile(s)) (mins) (years) ange (%) me has n Return Period 1 1 1 1 1	tia Stat 15, 30, ot been Climate Change +0% +0% +0%	60, 120, 240, s calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	OFF 60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW MH04 SSW MH05	Duration(s) cn Period(s) Climate Cha alf Drain Tin Storm 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter	Iner ofile(s)) (mins) (years) ange (%) me has n Return Period 1 1 1 1 1 1 1	tia Stat 15, 30, ot been Climate Change +0% +0% +0% +0% +0%	60, 120, 240, s calculated as th First (X)	360, 480, 9 1, ne structur First (Y) Flood	OFF 60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW MH04 SSW MH05 SSW IC06	Duration(s) cn Period(s) Climate Cha alf Drain Tin 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter	Iner ofile(s)) (mins) (years) ange (%) me has n Return Period 1 1 1 1 1 1 1 1	tia Stat 15, 30, ot been Climate Change +0% +0% +0% +0% +0% +0% +0%	60, 120, 240, s calculated as th First (X) Surcharge	360, 480, 9 1, ne structur First (Y) Flood	OFF 60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
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PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000 S3.001 S3.002 S3.003	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW IC03 SSW MH04 SSW IC06 SSW IC06 SSW IC06 SSW IC08 SSW IC09 SSW IC09 SSW MH10 SSW MH11	Duration(s) Climate Cha Climate Cha alf Drain Tin Storm 15 Winter 15 Winter	Iner ofile(s)) (mins) (years) ange (%) me has n Return Period 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	tia Stat 15, 30, ot been Climate Change +0% +0% +0% +0% +0% +0% +0% +0% +0% +0%	00, 120, 240, 3 calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	OFF 60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000 S3.001 S3.002 S3.003 S4.000	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW HC03 SSW HC03 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW IC08 SSW IC09 SSW HC10 SSW MH11 SSW IC12	Duration(s) Climate Cha Climate Cha alf Drain Tin Storm 15 Winter 15 Winter	Iner ofile(s)) (mins) (years) ange (%) me has n Return Period 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	tia Stat 15, 30, ot been Climate Change +0% +0% +0% +0% +0% +0% +0% +0% +0% +0%	60, 120, 240, 3 calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	OFF 60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000 S3.001 S3.002 S3.003 S4.000 S3.004	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW IC03 SSW MH04 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW IC08 SSW IC09 SSW IC09 SSW MH10 SSW MH11 SSW IC12 SSW IC12 SSW CP13	Duration(s) Climate Cha Climate Cha alf Drain Tin Storm 15 Winter 15 Winter	Iner ofile(s)) (mins) (years) ange (%) me has n Return Period 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	tia Stat 15, 30, ot been Climate Change +0% +0% +0% +0% +0% +0% +0% +0% +0% +0%	60, 120, 240, 3 calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	OFF 60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000 S3.001 S3.002 S3.003 S4.000 S3.004	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW IC03 SSW MH04 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW IC08 SSW IC09 SSW IC09 SSW MH10 SSW MH11 SSW IC12 SSW CP13 SSW CP14	Duration(s) Climate Cha Climate Cha alf Drain Tin Storm 15 Winter 15 Winter	Iner ofile(s)) (mins) (years) ange (%) me has n Return Period 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	tia Stat 15, 30, ot been Climate Change +0% +0% +0% +0% +0% +0% +0% +0% +0% +0%	60, 120, 240, 3 calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	OFF 60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo

Hydrock Consultants Ltd		Page 6
•	Lawnfield, Maidenhead	
	Storm water calculations	
	29512-HYD-XX-XX-CAL-C-7001	Micro
Date 11/01/2024	Designed by RS	Drainage
File Lawnfield MD model.MDX	Checked by GJ	Diamage
Innovyze	Network 2020.1.3	

<u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for LAWNFIELD MD MODEL.SWS</u>

PN	US/MH Name	Water Level (m)	Surcharged Depth (m)			Overflow (1/s)	Half Drain Time (mins)	Flow	Status
S1.000	SSW IC01	49.817	-0.133	0.000	0.03			0.4	OK
S1.001	SSW IC02	49.730	-0.130	0.000	0.04			0.5	OK
S1.002	SSW IC03	49.701	-0.109	0.000	0.17			2.2	OK
S1.003	SSW MH04	49.529	-0.171	0.000	0.13			5.2	OK
S1.004	SSW MH05	49.337	-0.173	0.000	0.12			5.3	OK
S2.000	SSW ICO6	49.372	-0.103	0.000	0.21			2.8	OK
S1.005	SSW CP07	49.173	-0.152	0.000	0.23			8.0	OK
S3.000	SSW IC08	49.835	-0.115	0.000	0.13			1.8	OK
S3.001	SSW IC09	49.736	-0.094	0.000	0.30			4.2	OK
S3.002	SSW MH10	49.492	-0.173	0.000	0.12			4.6	OK
S3.003	SSW MH11	49.379	-0.176	0.000	0.11			5.7	OK
S4.000	SSW IC12	49.349	-0.126	0.000	0.06			1.2	OK
S3.004	SSW CP13	49.164	-0.161	0.000	0.18			6.9	OK
S5.000	SSW CP14	49.172	-0.128	0.000	0.05			0.7	OK
S1.006	SSA	48.181	-1.044	0.000	0.00			0.0	OK

	US	/MH	Level
PN	Na	ame	Exceeded
S1.000	SSW	IC01	
S1.001	SSW	IC02	
S1.002	SSW	IC03	
S1.003	SSW	MH04	
S1.004	SSW	MH05	
S2.000	SSW	IC06	
S1.005	SSW	CP07	
S3.000	SSW	IC08	
S3.001	SSW	IC09	
S3.002	SSW	MH10	
S3.003	SSW	MH11	
S4.000	SSW	IC12	
S3.004	SSW	CP13	
S5.000	SSW	CP14	
S1.006		SSA	

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				Lawnf	ield, Maidenl	nead		
				Storm	Storm water calculations			
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ate 1	1/01/202	4			ned by RS			
		MD model.	MDY	-	and by GJ			rainaq
-		MD MOder.	MDA		-			
Innovy	ze			Netwo	ork 2020.1.3			
30 yea	<u>r Returr</u>	n Period Su			ical Results D MD MODEL.SW		ım Level	(Rank 1
	nhole Hea Foul Sewa	Hot Star Hot Start Le dloss Coeff ge per hecta umber of Inpu	n Factor t (mins) vel (mm) (Global) re (l/s) at Hydro	r 1.000 0 0.500 F 0.000 graphs 0	n Criteria Additional Flo MADD Facto Ylow per Person Number of Stora Number of Time,	r * 10m³/ha Inlet Coe: per Day (1, age Structu	a Storage Efiecient (per/day) res 1	0.000 0.800
	Ν				Number of Real	-		
				hetic Ra	infall Details			
		Rainfall				tio R 0.400		
			Region E) (mm)	-	nd Wales Cv (Sur 19.600 Cv (Win			
		M3-60	ο (11U11)		19.000 CV (W11	er) 0.040		
	Margi	in for Flood	Risk Wa	.rning (m	n)		300.0	
					ep 2.5 Second In	ncrement (E	xtended)	
				DTS Stati			ON	
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			ofile(s)		CO 100 040 7	Summer an		
	Retur	Duration(s) (mins)	15, 30,	60, 120, 240, 3	360, 480, 9	60, 1440	
	Retu) (mins) (years)	15, 30,	60, 120, 240, 3	360, 480, 9		
	Retu	Duration(s)) (mins) (years)	15, 30,	60, 120, 240, 3	360, 480, 9	60, 1440 30, 100	
W. PN		Duration(s) rn Period(s) Climate Cha) (mins) (years) ange (%) me has n Return	15, 30,	60, 120, 240, 3 calculated as th First (X) Surcharge	360, 480, 9 1, ne structur	60, 1440 30, 100 0, 0, 40	Overflo
PN	ARNING: Ha US/MH Name	Duration(s) nn Period(s) Climate Cha alf Drain Tin Storm) (mins) (years) ange (%) me has n Return Period	15, 30, not been of Climate Change	calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000	ARNING: Ha US/MH Name SSW IC01	Duration(s) n Period(s) Climate Cha alf Drain Tin Storm 15 Winter) (mins) (years) ange (%) me has n Return Period 30	15, 30, not been Climate Change +0%	calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001	ARNING: Ha US/MH Name SSW IC01 SSW IC02	Duration(s) n Period(s) Climate Cha alf Drain Tin Storm 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 30 30	15, 30, not been • Climate Change +0% +0%	calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002	ARNING: Ha US/MH Name SSW IC01	Duration(s) cn Period(s) Climate Cha alf Drain Tin Storm 15 Winter 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 30 30 30	15, 30, not been Climate Change +0%	calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03	Duration(s) cn Period(s) Climate Cha alf Drain Tin Storm 15 Winter 15 Winter 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 30 30 30 30	15, 30, not been of Climate Change +0% +0% +0%	calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW MH04	Duration(s) Climate Cha alf Drain Tin Storm 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 30 30 30 30 30	15, 30, not been Climate Change +0% +0% +0% +0%	calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW MH04 SSW MH05 SSW IC06 SSW IC06 SSW CP07	Duration(s) Climate Cha alf Drain Tin Storm 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter) (mins) (years) ange (%) me has n Period 30 30 30 30 30 30 30 30	15, 30, Climate Change +0% +0% +0% +0% +0% +0% +0% +0%	Calculated as th First (X) Surcharge 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW IC03 SSW MH04 SSW IC06 SSW IC06 SSW IC08	Duration(s) Climate Cha alf Drain Tin 5 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter) (mins) (years) ange (%) me has n Period 30 30 30 30 30 30 30 30 30 30	15, 30, Climate Change +0% +0% +0% +0% +0% +0% +0% +0%	Calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000 S3.001	ARNING: H US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW IC03 SSW MH04 SSW IC06 SSW IC06 SSW IC06 SSW IC08 SSW IC09	Duration(s) Climate Cha alf Drain Tin 5 Winter 15 Winter) (mins) (years) ange (%) me has n Period 30 30 30 30 30 30 30 30 30 30 30 30 30	15, 30, Climate Change +0% +0% +0% +0% +0% +0% +0% +0%	Calculated as th First (X) Surcharge 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000 S3.001 S3.002	ARNING: Ha US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW IC03 SSW MH04 SSW IC06 SSW IC06 SSW IC08	Duration(s) Climate Cha Climate Cha alf Drain Tin Storm 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 30 30 30 30 30 30 30 30 30 30 30 30 30	15, 30, Climate Change +0% +0% +0% +0% +0% +0% +0% +0%	Calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000 S3.001 S3.002 S3.003	ARNING: H US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW IC03 SSW MH04 SSW IC06 SSW IC06 SSW IC06 SSW IC08 SSW IC09 SSW MH10	Duration(s) Climate Cha Climate Cha alf Drain Tin Storm 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 30 30 30 30 30 30 30 30 30 30 30 30 30	15, 30, Climate Change +0% +0% +0% +0% +0% +0% +0% +0%	Calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000 S3.001 S3.002 S3.003 S4.000	ARNING: H US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW IC03 SSW MH04 SSW IC06 SSW IC06 SSW IC06 SSW IC08 SSW IC09 SSW IC09 SSW MH10	Duration(s) Climate Cha alf Drain Tin Storm 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 30 30 30 30 30 30 30 30 30 30 30 30 30	15, 30, Climate Change +0% +0% +0% +0% +0% +0% +0% +0%	Calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000 S3.001 S3.002 S3.003 S4.000 S3.004 S5.000	ARNING: H US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW IC03 SSW MH04 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW IC07 SSW IC08 SSW IC09 SSW MH10 SSW MH10 SSW MH11 SSW IC12 SSW CP13 SSW CP14	Duration(s) Climate Cha Climate Cha alf Drain Tin Storm 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 30 30 30 30 30 30 30 30 30 30 30 30 30	15, 30, Climate Change +0% +0% +0% +0% +0% +0% +0% +0%	Calculated as the First (X) Surcharge 100/15 Summer 100/15 Summer 100/15 Summer 100/1440 Winter	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000 S3.001 S3.002 S3.003 S4.000 S3.004	ARNING: H US/MH Name SSW IC01 SSW IC02 SSW IC03 SSW IC03 SSW MH04 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW IC07 SSW IC08 SSW IC09 SSW MH10 SSW MH10 SSW MH11 SSW IC12 SSW CP13 SSW CP14	Duration(s) Climate Cha alf Drain Tin Storm 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 30 30 30 30 30 30 30 30 30 30 30 30 30	15, 30, Climate Change +0% +0% +0% +0% +0% +0% +0% +0%	Calculated as the First (X) Surcharge 100/15 Summer 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo

Hydrock Consultants Ltd		Page 8
•	Lawnfield, Maidenhead	
	Storm water calculations	
	29512-HYD-XX-XX-CAL-C-7001	Micro
Date 11/01/2024	Designed by RS	Drainage
File Lawnfield MD model.MDX	Checked by GJ	Diamage
Innovyze	Network 2020.1.3	

 $\frac{30 \ \text{year Return Period Summary of Critical Results by Maximum Level (Rank 1)}{\text{for LAWNFIELD MD MODEL.SWS}}$

PN	US/MH Name	Water Level (m)	Surcharged Depth (m)			Overflow (1/s)	Half Drain Time (mins)	Flow	Status
S1.000	SSW IC01	49.827	-0.123	0.000	0.07			1.0	OK
S1.001	SSW IC02	49.748	-0.112	0.000	0.11			1.3	OK
S1.002	SSW IC03	49.735	-0.075	0.000	0.49			6.6	OK
S1.003	SSW MH04	49.574	-0.126	0.000	0.40			15.7	OK
S1.004	SSW MH05	49.381	-0.129	0.000	0.37			15.9	OK
S2.000	SSW IC06	49.403	-0.072	0.000	0.52			6.9	OK
S1.005	SSW CP07	49.233	-0.092	0.000	0.66			22.6	OK
S3.000	SSW IC08	49.857	-0.093	0.000	0.31			4.3	OK
S3.001	SSW IC09	49.786	-0.044	0.000	0.83			11.6	OK
S3.002	SSW MH10	49.532	-0.133	0.000	0.34			12.9	OK
S3.003	SSW MH11	49.417	-0.138	0.000	0.31			16.2	OK
S4.000	SSW IC12	49.364	-0.111	0.000	0.15			3.0	OK
S3.004	SSW CP13	49.213	-0.112	0.000	0.50			19.4	OK
S5.000	SSW CP14	49.185	-0.115	0.000	0.12			1.7	OK
S1.006	SSA	48.480	-0.745	0.000	0.00			0.0	OK

PN	US/MH Name		Level Exceeded
S1.000	SSW	IC01	
S1.001	SSW	IC02	
S1.002	SSW	IC03	
S1.003	SSW	MH04	
S1.004	SSW	MH05	
S2.000	SSW	IC06	
S1.005	SSW	CP07	
S3.000	SSW	IC08	
S3.001	SSW	IC09	
S3.002	SSW	MH10	
S3.003	SSW	MH11	
S4.000	SSW	IC12	
S3.004	SSW	CP13	
S5.000	SSW	CP14	
S1.006		SSA	

	k Consu	ltants Ltd					Pa	ıge 9
_				Lawni	field, Maident	nead		
				Storr	n water calcul	lations		
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ate 1	1/01/20	24		Desid	ned by RS			licro
		d MD model.	MDY		and by GJ			rainag
-		u MD MOder.	MDA		-			
nnovy	ze			Netwo	ork 2020.1.3			
<u>100 y</u>	ear Ret				itical Result		imum Leve	el (Ran)
			l) for	LAWNFIE	LD MD MODEL.S	SWS		
			:	Simulatio	on Criteria			
	A	real Reductio			Additional Flo	w - % of To	otal Flow	0.000
		Hot Star	rt (mins)	0	MADD Facto	r * 10m³/ha	a Storage	0.000
		Hot Start Le					fiecient	
					low per Person	per Day (l,	/per/day)	0.000
	Foul Sew	age per hecta	are (l/s)	0.000				
	N	lumber of Inc	ut. Hvdro	graphs 0	Number of Stora	age Structu	res 1	
	I.	-	-		Number of Time	-		
					Number of Real			
		Doinfall		hetic Ra	infall Details			
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			-	-	19.600 Cv (Wir			
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			-		ep 2.5 Second Ir	ncrement (E	xtended)	
				DTS Stat			ON	
				DVD Stat			OFF	
			Iner	tia Stat	lS		OFF	
		Pr	ofile(s)			Summer an	d Winter	
		Duration(s) (mins)		60, 120, 240, 3	360, 480, 9	60, 1440	
	Reti	Duration(s arn Period(s)) (mins) (years)		60, 120, 240, 3	360, 480, 9 1,	60, 1440 30, 100	
	Reti	Duration(s) (mins) (years)		60, 120, 240, 3	360, 480, 9 1,	60, 1440	
Ŵ		Duration(s arn Period(s) Climate Ch) (mins) (years) ange (%)	15, 30,	60, 120, 240, 3	360, 480, 9 1,	60, 1440 30, 100 0, 0, 40	all.
Ŵ.		Duration(s arn Period(s) Climate Ch) (mins) (years) ange (%)	15, 30,		360, 480, 9 1,	60, 1440 30, 100 0, 0, 40	ull.
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W. PN	ARNING: H	Duration(s arn Period(s) Climate Ch) (mins) (years) ange (%) me has n Return	15, 30, ot been	calculated as th	360, 480, 9 1, ne structur	60, 1440 30, 100 0, 0, 40 e is too f	Overflo
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PN S1.000 S1.001	ARNING: F US/MH Name SSW IC02 SSW IC02	Duration(s) nrn Period(s) Climate Ch Half Drain Ti Storm 1 15 Winter 2 15 Winter) (mins) (years) ange (%) me has n Return Period = 100 = 100	15, 30, ot been Climate Change +40% +40%	calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002	ARNING: F US/MH Name SSW ICO SSW ICO SSW ICO SSW ICO	Duration(s) Durn Period(s) Climate Ch Half Drain Ti Storm 15 Winter 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 100 100	15, 30, ot been Climate Change +40% +40% +40%	calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003	ARNING: F US/MH Name SSW ICO SSW ICO SSW ICO SSW ICO SSW MHO4	Duration(s) Durn Period(s) Climate Ch Half Drain Ti Storm 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period = 100 = 100 = 100	15, 30, ot been Climate Change +40% +40% +40% +40%	calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004	ARNING: F US/MH Name SSW ICO SSW ICO SSW ICO SSW MHO4 SSW MHO4	Duration(s) Climate Ch Half Drain Ti Storm 1 15 Winter 2 15 Winter 3 15 Winter 4 15 Winter 5 15 Winter) (mins) (years) ange (%) me has n Return Period 100 100 100 100	15, 30, ot been Climate Change +40% +40% +40% +40%	calculated as th First (X)	360, 480, 9 1, ne structur First (Y)	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000	ARNING: F US/MH Name SSW ICO SSW ICO SSW ICO SSW MHO SSW MHO SSW MHO SSW ICO	Duration(s Durn Period(s) Climate Ch Half Drain Ti Storm 15 Winter 15 Winter 15 Winter 15 Winter 5 15 Winter 5 15 Winter) (mins) (years) ange (%) me has n Return Period 100 100 100 100 100	15, 30, ot been Climate Change +40% +40% +40% +40% +40%	calculated as th First (X) Surcharge	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005	ARNING: F US/MH Name SSW ICO SSW ICO SSW ICO SSW MHO SSW MHO SSW MHO SSW ICO SSW CPO	Duration(s Durn Period(s) Climate Ch Half Drain Ti Storm 15 Winter 15 Winter 15 Winter 15 Winter 5 15 Winter 5 15 Winter 5 15 Winter 7 1440 Winter) (mins) (years) ange (%) me has n Return Period 100 100 100 100 100 100	15, 30, ot been Climate Change +40% +40% +40% +40% +40% +40%	Calculated as th First (X) Surcharge 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000	ARNING: F US/MH Name SSW ICO SSW ICO SSW ICO SSW MHO SSW MHO SSW MHO SSW ICO	Duration(s Duration(s) Climate Ch Half Drain Ti Storm 15 Winter 15 Winter 15 Winter 15 Winter 5 15 Winter 5 15 Winter 5 15 Winter 7 1440 Winter 8 15 Winter) (mins) (years) ange (%) me has n Return Period 100 100 100 100 100 100 100 100	15, 30, ot been Climate Change +40% +40% +40% +40% +40%	calculated as th First (X) Surcharge	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN \$1.000 \$1.001 \$1.002 \$1.003 \$1.004 \$2.000 \$1.005 \$3.000 \$3.001	ARNING: F US/MH Name SSW IC02 SSW IC02 SSW IC02 SSW MH04 SSW MH04 SSW MH05 SSW IC06 SSW IC06 SSW IC06	Duration (s Duration (s) Climate Ch Half Drain Ti Storm 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 100 100 100 100 100 100 100 100 100	15, 30, ot been Climate Change +40% +40% +40% +40% +40% +40% +40%	Calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN \$1.000 \$1.001 \$1.002 \$1.003 \$1.004 \$2.000 \$1.005 \$3.000 \$3.001 \$3.002	ARNING: F US/MH Name SSW IC02 SSW IC02 SSW IC02 SSW MH04 SSW MH04 SSW MH05 SSW IC06 SSW CP07 SSW IC08 SSW IC08	Duration (s Duration (s) Climate Ch Half Drain Ti Storm 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 100 100 100 100 100 100 100 100 100 10	15, 30, ot been Climate Change +40% +40% +40% +40% +40% +40% +40% +40%	Calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN \$1.000 \$1.001 \$1.002 \$1.003 \$1.004 \$2.000 \$1.005 \$3.000 \$3.001 \$3.002 \$3.003	ARNING: F US/MH Name SSW ICO SSW ICO SSW ICO SSW MHO SSW MHO SSW ICO SSW ICO SSW ICO SSW ICO SSW ICO SSW ICO SSW ICO	Duration (s Duration (s) Climate Ch Half Drain Ti Storm 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 100 100 100 100 100 100 100 100 100 10	15, 30, ot been Climate Change +40% +40% +40% +40% +40% +40% +40% +40%	Calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000 S3.001 S3.002 S3.003 S4.000 S3.004	ARNING: F US/MH Name SSW IC02 SSW IC02 SSW IC02 SSW MH04 SSW MH05 SSW IC06 SSW CP07 SSW IC06 SSW IC06 SSW IC07 SSW IC07 SSW IC07 SSW IC07 SSW MH10 SSW MH10 SSW MH10 SSW IC12 SSW CP13	Duration (s Duration (s) Climate Ch Half Drain Ti Storm 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 100 100 100 100 100 100 100 100 100 10	15, 30, ot been Climate Change +40% +40% +40% +40% +40% +40% +40% +40%	calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S3.000 S3.001 S3.002 S3.003 S4.000 S3.004 S5.000	ARNING: F US/MH Name SSW IC02 SSW IC02 SSW IC02 SSW MH04 SSW MH05 SSW IC06 SSW CP07 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW MH10 SSW MH10 SSW MH11 SSW IC12 SSW CP14	Duration (s Duration (s) Climate Ch Half Drain Ti Storm 15 Winter 15 Winter 140 Winter) (mins) (years) ange (%) me has n Return Period 100 100 100 100 100 100 100 100 100 10	15, 30, ot been Climate Change +40% +40% +40% +40% +40% +40% +40% +40%	<pre>calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer 100/15 Summer 100/140 Winter</pre>	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo
PN S1.000 S1.001 S1.002 S1.003 S1.004 S2.000 S1.005 S3.000 S3.001 S3.002 S3.003 S4.000 S3.004	ARNING: F US/MH Name SSW IC02 SSW IC02 SSW IC02 SSW MH04 SSW MH05 SSW IC06 SSW CP07 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW IC06 SSW MH10 SSW MH10 SSW MH11 SSW IC12 SSW CP14	Duration (s Duration (s) Climate Ch Half Drain Ti Storm 15 Winter 15 Winter) (mins) (years) ange (%) me has n Return Period 100 100 100 100 100 100 100 100 100 10	15, 30, ot been Climate Change +40% +40% +40% +40% +40% +40% +40% +40%	calculated as th First (X) Surcharge 100/15 Summer 100/15 Summer 100/15 Summer	360, 480, 9 1, ne structur First (Y) Flood	60, 1440 30, 100 0, 0, 40 e is too f First (Z)	Overflo

Hydrock Consultants Ltd		Page 10
•	Lawnfield, Maidenhead	
	Storm water calculations	
	29512-HYD-XX-XX-CAL-C-7001	Mirro
Date 11/01/2024	Designed by RS	Drainage
File Lawnfield MD model.MDX	Checked by GJ	Diamage
Innovyze	Network 2020.1.3	

 100 year Return Period Summary of Critical Results by Maximum Level (Rank

 1) for LAWNFIELD MD MODEL.SWS

PN	US/: Nan		Water Level (m)	Surcharged Depth (m)			Overflow (1/s)	Half Drain Time (mins)	Pipe Flow (l/s)	Status
S1.000	SSW 1	IC01	49.836	-0.114	0.000	0.13			1.8	OK
S1.001	SSW 1	IC02	49.778	-0.082	0.000	0.20			2.5	OK
S1.002	SSW 1	IC03	49.771	-0.039	0.000	0.89			12.1	OK
S1.003	SSW N	MH04	49.619	-0.081	0.000	0.72			28.3	OK
S1.004	SSW N	MH05	49.422	-0.088	0.000	0.67			28.5	OK
S2.000	SSW 1	IC06	49.473	-0.002	0.000	0.93			12.4	OK
S1.005	SSW (CP07	49.355	0.030	0.000	0.05			1.9	SURCHARGED
S3.000	SSW 1	IC08	50.083	0.133	0.000	0.56			7.9	SURCHARGED
S3.001	SSW 1	IC09	50.045	0.215	0.000	1.46			20.5	SURCHARGED
S3.002	SSW N	MH10	49.568	-0.097	0.000	0.61			23.0	OK
S3.003	SSW N	MH11	49.450	-0.105	0.000	0.54			28.8	OK
S4.000	SSW 1	IC12	49.379	-0.096	0.000	0.28			5.5	OK
S3.004	SSW (CP13	49.354	0.029	0.000	0.04			1.6	SURCHARGED
S5.000	SSW (CP14	49.357	0.057	0.000	0.03			0.4	SURCHARGED
S1.006		SSA	49.393	0.168	0.000	0.00			0.0	SURCHARGED

PN		/MH ame	Level Exceeded
S1.000	SSW	IC01	
S1.001	SSW	IC02	
S1.002	SSW	IC03	
S1.003	SSW	MH04	
S1.004	SSW	MH05	
S2.000	SSW	IC06	
S1.005	SSW	CP07	
S3.000	SSW	IC08	
S3.001	SSW	IC09	
S3.002	SSW	MH10	
S3.003	SSW	MH11	
S4.000	SSW	IC12	
S3.004	SSW	CP13	
S5.000	SSW	CP14	
S1.006		SSA	



11. APPENDIX E

(SURFACE WATER EXCEEDANCE ROUTES)



KEY:

SURFACE WATER EXCEEDANCE ROUTE



- All provides the set of all drains are to be confirmed on site prior to the commensation.
 This drawing is to be read in conjunction with all relevant drawings, specifications and documentation.
 The position, size and levels of all drains are to be confirmed on site prior to the commensation the site site of all drains are to be confirmed on site prior to the commensation of the site site of all drains are to all messations or co-ordinates provided. All levels are in metres and all dimensions are in millimeters, unless otherwise noted.
 The Contractor shall allow for the protection, temporary and permanent support and diversion works as necessary, to all existing services to the satiafaction of the public utilities.
 The Contractor shall allow for dear by when of sums provides as foreover, pumping and developing as apportates, in order to keep the ecosystion as reasonably dry as possible during the construction of the works.
 All pripherod subjective which are developing as the construction of the works.
 All pippeords within pedestrain/soft areas with less than 600mm cover.
 All pippeords within pedestrain/soft areas with less than 12m cover.
 All pippeords within pedestrain/soft areas with less than 12m cover.
 All pippeords within pedestrain/soft areas with less than 000mm cover.
 All pippeords allow if the hording pipe levels. Blackdrop pipevork shall be construction areas to be as located by the architect.
 Concrete and the formation for manholes is to the intersection the construction areas to be as located by the architect.
 Condinate setting out information for manholes is to the intersection the to suit the finished ground levels. All out and ubject to adjusticat during the role of the out of the architect and the following.
 Vehicular Areas: Class D400, double triangular, 150mm deep ductlie iron cover and frame with the relowant durin
- Where utility/land drainage tenches ter cross over drainage trenders. In the Contractor shall construct an impermeable barrier to prevent groundwater infiltrating into the drainage tench.
 Upon completion of the works the Contractor shall clean all drainage by jetting, removing all dehrist rom site: no dehrist able berriter to prevent groundwater infiltrating all dehrist rom site. No dehrist shall be permitted to enter the existing
- drainage system. 22. Backfill to all drainage trenches to be Class 6F1 material.

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P01	FOR PLANNING	22/09/23	RS		GJ GJ
Rev.	Revision Notes	Date	Drawn By	Checke	ed Approved
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	ING NO.				REVISION
29512-HYD-XX-XX-DR-C-7010 P01					



12. APPENDIX F

(OPERATIONS AND MAINTENANCE SCHEDULE)



Project name	Lawnfield, Maidenhead				
Design note title	Operation and Maintenance Schedule				
Document reference	29512-HYD-XX-XX-TN-C-0001				
Author	RS				
Revision	P01				
Date	22 September 2023	Approved			

1. MAINTENANCE SCHEDULE

1.1 Guidance

To ensure longevity and effective operation of SuDS they must be maintained in accordance with

- » CIRIA 753 guidance and operation and maintenance
- » CIRIA report C768 Guidance on the construction of SuDS
- » Maintenance plan outlined in section 5.2
- »

1.2 Maintenance Plan

Feature	Maintenance	Frequency
Private Drains	Inspection	CCTV survey every 5- 10 years.
	Regular Maintenance	Jet clean system fully every 5-10 years. (Recommend prior to CCTV drainage survey)
	Remedial / Occasional Maintenance	Carry out remedial works as identified in CCTV survey.
Outfall pipes,	Inspection	Visually - Quarterly
non-return pipe flaps, and anti- scour mat flow	Regular Maintenance	Clearance of silt and debris as necessary
channel	Remedial / Occasional Maintenance	Damage to pipes and headwall to be repaired as necessary



Gullies &	Inspection	Quarterly
Drainage Channels	Regular Maintenance	Remove silt and debris as necessary to prevent build up.
Catchpits	Inspection	Quarterly
	Regular maintenance	Remove silt and debris as necessary to prevent build up.
Soakaways,	Grass edges	
infiltration trenches and infiltration basins	Mow 1m min. wide grass surround to drain at 100mm and 150mm maximum to filter runoff and protect infiltration structure from silt.	
	Infiltration Basins	
	Protect grass surface from compaction and siltation and manage main area of basin for design function or appearance.	
	Infiltration Basins	
	Where there is a build up of silt in the basin at inlets, i.e. 50mm or more above the design level then remove when the ground is damp in autumn or early spring and turf to the original design levels.	
	Spread excavated material on site above SuDS design profile, e.g. top of banks, in accordance with E.A. Waste Exemption Guidance.	
	Infiltration Trench	
	Hand pull or spot treat individual weed growth only if necessary, ensuring weedkiller does not enter the drain and inhibit natural breakdown of pollutants.	
Overflows and flood routes	Overflows. Jet pipes leading from overflow structures annually and check by running water through the overflow. Check free flow at next SUDS feature – inlet to basin or chamber.	Annually
	Remove any accumulated grass cuttings or other debris on top of grass weirs or stone filled baskets overflows.	Monthly



	Flood Routes. Make visual inspection. Check route is not blocked by new fences, walls, soil or other rubbish. Remove as necessary.	Monthly
	Overflows. If overflow is not clear then dismantle structure and reassemble to design detail.	As required
Planting and existing vegetation	Amenity Grass - Mow all grass verges, paths and amenity grass at 35-50mm with 75mm max.	16 visits
vegetation	All cuttings to remain in situ	
	Rough grass – Mow at 75-100mm but not to exceed 150mm	4 - 8 visits
	All cuttings to wildlife piles	
	Wildflower areas strimmed to 50mm in Sept-Oct	1 visit
	or	2 visit
	Wildflower areas strimmed to 50mm July and Sept	1 visit
	or	
	Wildflower areas strimmed to 50mm on 3 year rotation 30% each year	
	All cuttings to wildlife piles	
	Ornamental tree & shrub planting.	4 visits
	Weed all shrub beds as detailed spec as necessary.	
	Cut back planting from lights, paths and visibility sight lines in late autumn and as necessary.	
	Cut hedges slightly tapered back from base with flat top at specified height.	
	Do not mulch planting adjacent to permeable/ porous paving surfaces.	
	Remove stakes and ties from trees when no longer needed for support and within 3 years of planting.	
	Protect from strimmer damage and remove competitive growth until well established.	
	Native trees & shrub planting.	1 visit
	Prune to shape in year 1.	
	Protect trees from strimmer damage and remove competitive growth until well established.	



	Remove stakes and ties from trees when no longer needed for support and within 3 years from planting.	
	Existing trees Check existing trees for safety.	1 visit
	Replace trees and shrubs which fail in the first five years after planting. Carry out tree surgery as necessary.	
Cellular storage	Ensure catchpits are installed upstream and downstream of cellular storage. These are to be emptied.	Quarterly
	Jetting should be carried out along main carrier drain through system.	As required