PROPOSED NEW DWELLING AT DEVONSIDE FARM SALINE

DRAINAGE OPTIONS REPORT

PREPARED FOR GRAEME STEWART





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### **Quality Management**

Issue/revision	Original Issue	Revision A	Revision B	Revision C
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Date	16/11/2023	28/11/2023		
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Checked by	Neil Stephen	Neil Stephen		
Project number	23805	23805		
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# Document Reference 23805 – Drainage Options Report Revision – A

## Contents

Contents	1
Design Criteria Summary	2
Foul Drainage	2
Surface Water Drainage	2
Surface Water Attenuation Conclusions	3
Maintenance Schedule	4
Summary	4
Appendix A – SEPA Simple Index Approach	5
Appendix B – Causeway Flow Calculations	6



## **Design Criteria Summary**

The project comprises of a new four-bedroom dwelling, with driveway and private garden space located at Devonside Farm, Saline.

The site currently does not have any drainage networks adopted by Scottish Water within the vicinity.

#### Foul Drainage

There is no foul water sewers within the vicinity and no suitable existing private treatment facilities were identified.

Following guidance from British Water Flows and Loads 4, a four-bedroom property has a minimum population equivalent of 6 P with the ultimate discharge point being to the Foulbutts Burn via an existing drainage ditch and outfall within the farm boundary. The effluent from a septic tank is not deemed of suitable quality for discharge to a watercourse, and therefore a treatment plant will be specified.

It should be noted that the land surrounding the property is also under the same ownership, therefore no additional permission is required from third parties for the outfall to the drainage ditch.

The proposed treatment plant is a BioDisc BA with an allowable 8 P and an effluent quality of 20 mg/l BOD5, 873 mg/l COD, 5 mg/l Suspended Solids and 23 mg/l of Ammonium Nitrogen.

A partial soakaway, 10m<sup>2</sup>, has been provided after treatment which will overflow into the drainage ditch. During dry months where flows in Foulbutts Burn may be lower, this should assist by reducing the remaining contamination entering the burn at times when dilution could be reduced.

### Surface Water Drainage

It is proposed that surface water run-off from the roof area and driveway will be managed and discharged via an existing drainage ditch to the Foulbutts Burn approximately 220m West from the development area.

The roof area of the new building is 218m<sup>2</sup> and external areas are 182m<sup>2</sup>. The greenfield run-off from this area would equate to 0.16 litres, based on 4 l/sec/ha. This rate is very low and would require the use of a very small orifice control to achieve and would be prone to frequent blockages.

Page | 2 28/11/2023



Sewers for Scotland 4 recommends the minimum orifice control for use on a private system is 30mm which has therefore been adopted to restrict the outflow to a more acceptable level.

An attenuation structure, constructed using standard Stormbloc Optimum cellular storage, 5.6x3.2m x 1.02 m deep is to be located within the garden area. This will provide sufficient attenuation from the surface water run-off from the roof and hardstanding areas.

Treatment of the surface water has been achieved within filter trenches for roof drainage, and porous paving for car parking spaces in accordance with the SEPA Simple Index Approach (SIA) on all required measures including; Suspended Solids, Metals and Hydrocarbons. A copy of the SEPA SIA Tool is included in Appendix A.

Based on the overall contributing hardstanding area, this would equate to an estimated discharge rate without attenuation of 4.45 l/sec (0.04 \* 2.78 \* 40 mm/hr).

Climate change has been determined using current guidance from Fife Council SuDS guide which recommends an allowance of 39% should be adopted.

This attenuation system has been simulated using Causeway Flow drainage design software to show the effects of 1:30, 1:100 and 1:200-year return periods including climate change. This output has been included in Appendix B.

This proposed cellular storage and associated drainage has been detailed on our drawing No. 23805-200.

### **Surface Water Attenuation Conclusions**

During a 1 in 30 year return period storm no water will escape from the system and there is no flooding. Water will be contained within the attenuation structure. The discharge rate through the control manhole is 1.5 l/sec.

During a 1 in 100 year return period storm no water will escape from the system and there is no flooding. Water will be contained within the attenuation structure. The discharge rate through the control manhole is 1.7 l/sec.

During a 1 in 200 year return period storm no water will escape from the system and there is no flooding. Water will be contained within the attenuation structure.. The discharge rate through the control manhole is 1.9 l/sec.

## **Maintenance Schedule**

Drainage Component	Maintenance Arrangements	Maintenance By
Piped storm	Clear by rodding or high-pressure jetting if	Property Owner
drainage	these become blocked.	
Filter Trenches	These will be jetted out from the silt trap or rodding accesses to clear any silting of the perforated pipes/stone filter medium on an annual basis.	Property Owner
Cellular Storage	Check silt traps on a bi-annual basis or at an increased frequency if required. Arrange inspections of cellular storage using specialist equipment, recommended once every two years.	Property Owner
Orifice Control and Inspection Chambers	Checked for blockages on an annual basis.	Property Owner

The maintenance provision for the development drainage is as follows;

# Summary

On this basis, adequate attenuation has been provided to cater for all storm events up to the 200-year return period.

#### Sean Turner

Direct Email sean.turner@mcgregor-mcmahon.com

# Appendix A – SEPA Simple Index Approach



#### SIMPLE INDEX APPROACH: TOOL



HRW shall not be liable for any direct or indirect damage claim, loss, cost, expense or liability howsoever arising out of the use or impossibility to use the tools, even when HRW has been informed of the possibility of the same. The user hereby indemnifies HRW from and against any damage claim, loss, expense or liability resulting from any action taken against HRW that is related in any way to the use of the tool or any reliance made in respect of the output of such use by any person whatsoever. HRW does not guarantee that the tool's functions meet the requirements of any person, nor that the tool is fore from errors.

1. The steps set out in the tool should be applied for each inflow or 'runoff area' (ie each impermeable surface area separately discharging to a SuDS component).

2. The supporting 'Design Conditions' stated by the tool must be fully considered and implemented in all cases.

3. Relevant design examples are included in the SuDS Manual Appendix C.

4. Each of the steps below are part of the process set out in the flowchart on Sheet 3.

5. Sheet 4 summarises the selections made below and indicates the acceptability of the proposed SuDS components.

DROP DOWN LIST RELEVANT INPUTS NEED TO BE SELECTED FROM THESE LISTS, FOR EACH STEP

USER ENTRY USER ENTRY CELLS ARE ONLY REQUIRED WHERE INDICATED BY THE TOOL

STEP 1: Determine the Pollution Hazard Index for the runoff area discharging to the proposed SuDS scheme This step requires the user to select the appropriate land use type for the area from which the runoff is occurring If the land use varies across the 'runoff area', either: - use the land use type with the highest Pollution Hazard Index - apply the approach for each of the land use types to determine whether the proposed SuDS design is sufficient for all. If it is not, consider collecting more hazardous runoff separately and providing additional treatment. If the generic land use types suggested are not applicable, select 'Other' and enter a description of the land use of the runoff area and agreed user defined indices in the row below the drop down lists. DESIGN CONDITIONS Pollution Hazard Indices Hazard Level Total Suspended Runoff Area Land Use Description Solids Hydrocarbons Metals Select land use type from the drop down list (or 'Other' if none applicable): -Individual driveway Low 0.5 0.4 0.4 If the generic land use types in the drop down list above are not applicable, select 'Other' and enter a description of the land use of the runoff area and agreed user defined indices in this row: Landuse Pollution Hazard Index 0.4 Low 0.5 0.4

STEP 2A: Determine the Pollution Mitigation Index for the proposed SuDS components

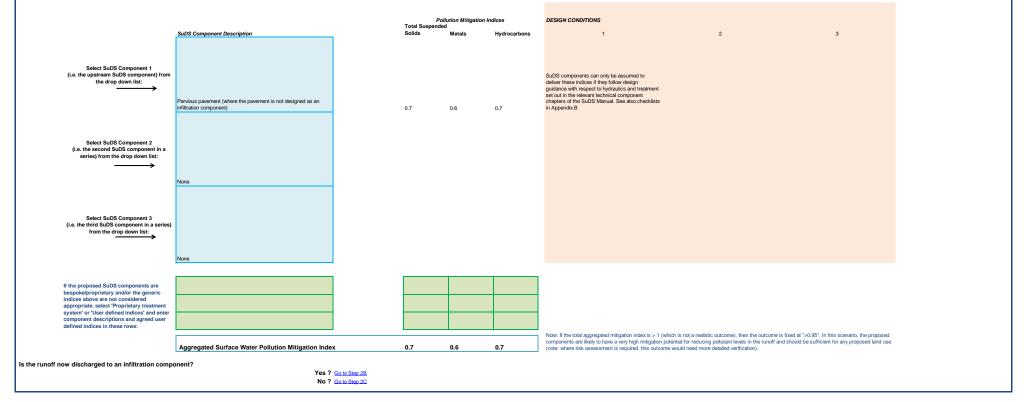
This step requires the user to select the proposed SuDS components that will be used to treat runoff - before it is discharged to a receiving surface waterbody or downstream infiltration component

If the runoff is discharged directly to an infiltration component, without upstream treatment, select 'None' for each of the 3 SuDS components and move to Step 2B

This step should be applied to evaluate the water quality protection provided by proposed SUDS components for discharges to receiving surface waters or downstream infiltration components (note: in England and Wales this will include components that allow any amount of infiltration, however small, even where infiltration is not specifically accounted for in the design).

If you have fewer than 3 components, select 'None' for the components that are not required

If the proposed component is bespoke and/or a proprietary treatment product and not generically described by the suggested components, then 'Proprietary treatment system' or 'User defined indices' should be selected and a description of the component and agreed user defined indices should be entered in the rows below the drop down lists



STEP 2B: Determine the Pollution Mitigation In	dex for the proposed Groundwater Protection						
This step requires the user to select the type of gro groundwater	undwater protection that is either part of the SuDS component or that lies b	etween the co	nponent and th	e			
This step should be applied where a SuDS component is specifical even where infiltration is not specifically accounted for in the design	y designed to infiltrate runoff (note: in England and Wales this will include components that allow ar	y amount of infiltra	tion, however small,				
'Groundwater protection' describes the proposed depth of soil or oth	er material through which runoff will flow between the runoff surface and the underlying groundwate	r.					
Where the discharge is to surface waters and risks to groundwater	need not be considered, select 'None'						
If the proposed groundwater protection is bespoke and/or a propriet should be entered in the row below the drop down list	ary product and not generically described by the suggested measures, then a description of the prot	ection and agreed	user defined indices		DESIGN CONDITIONS		
		P	ollution Mitigation	Indices			
		Total Suspend Solids					
Select type of groundwater protection from the drop down list:	None	Solids	Metals	Hydrocarbons	1 2 3 4		
If the proposed groundwater protection is bespoke/proprietary and/or the generic indices above are not considered appropriate, select "Proprietary product" or "User defined indices" and enter a description of the protection and agreed user defined indices in this row:	Groundwater Protection Pollution Mitigation Index	0	0	0			
STEP 2C: Determine the Combined Pollution N This is an automatic step which combines the prop	litigation Indices for the Runoff Area osed SuDS Pollution Mitigation Indices with any Groundwater Protection Po	-	ion Indices ned Pollution Mitig	ation Indiana			
		Total Suspend Solids		Hydrocarbons			
	Combined Pollution Mitigation Indices for the Runoff Area	0.7	0.6	0.7	Note: If the total aggregated miligation index is > 1 (which is not a realistic outcome), then the outcome is fixed at ">0.85°. In this scenario, the proposed components are which with a work optimal for advances in the runoff and should be sufficient for any proposed land use (note: where risk assessment is required, this outcome would need more detailed verification).		
STEP 2D: Determine Sufficiency of Pollution Mitigation Indices for Selected SuDS Components This is an automatic step which compares the Combined Pollution Mitigation Indices with the Land Use Hazard Indices, to determine whether the proposed components are sufficient to manage each pollutant category type							
When the combined mitigation index exceeds the land use pollution	hazard index, then the proposed components are considered sufficient in providing pollution risk mi	tigation.			DESIGN CONDITIONS		
that provides environmental protection in the event of an unexpected	waters or groundwater, an additional treatment component (ie over and above that required for stam pollution event or poor system performance. Protected surface waters are those designated for dri Northern Ireland, a more precautionary approach may be required and this should be checked with	nking water abstrac	tion. In England and	Wales, protected			
		Total Suspend	cy of Pollution Mit led				
		Solids	Metals Sufficient	Hydrocarbons	1 Reference to local planning documents should also be made to isenify any additional protection required for sites due to habitat conservation (see Chapter 7 The SUGS design process). The implications of developments on or within close provinity to an area with an environmental designation, such as a Site of Special Scientific Interest (SSS) should be considered via		

#### SIMPLE INDEX APPROACH: TOOL



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1. The steps set out in the tool should be applied for each inflow or 'runoff area' (ie each impermeable surface area separately discharging to a SuDS component).

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STEP 1: Determine the Pollution Hazard Index for the runoff area discharging to the proposed SuDS scheme This step requires the user to select the appropriate land use type for the area from which the runoff is occurring If the land use varies across the 'runoff area', either: - use the land use type with the highest Pollution Hazard Index - apply the approach for each of the land use types to determine whether the proposed SuDS design is sufficient for all. If it is not, consider collecting more hazardous runoff separately and providing additional treatment. If the generic land use types suggested are not applicable, select 'Other' and enter a description of the land use of the runoff area and agreed user defined indices in the row below the drop down lists. DESIGN CONDITIONS Pollution Hazard Indices Hazard Level Total Suspended Runoff Area Land Use Description Solids Hydrocarbons Metals Select land use type from the drop down list (or 'Other' if none applicable): -Residential roofing Very low 0.2 0.2 0.05 If the generic land use types in the drop down list above are not applicable, select 'Other' and enter a description of the land use of the runoff area and agreed user defined indices in this row: Landuse Pollution Hazard Index 0.05 Very low 0.2 0.2

STEP 2A: Determine the Pollution Mitigation Index for the proposed SuDS components

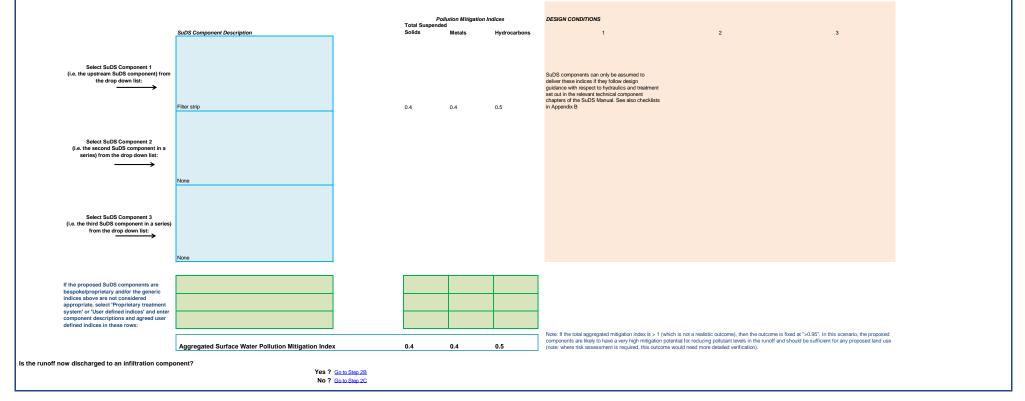
This step requires the user to select the proposed SuDS components that will be used to treat runoff - before it is discharged to a receiving surface waterbody or downstream infiltration component

If the runoff is discharged directly to an infiltration component, without upstream treatment, select 'None' for each of the 3 SuDS components and move to Step 2B

This step should be applied to evaluate the water quality protection provided by proposed SUDS components for discharges to receiving surface waters or downstream infiltration components (note: in England and Wales this will include components that allow any amount of infiltration, however small, even where infiltration is not specifically accounted for in the design).

If you have fewer than 3 components, select 'None' for the components that are not required

If the proposed component is bespoke and/or a proprietary treatment product and not generically described by the suggested components, then 'Proprietary treatment system' or 'User defined indices' should be selected and a description of the component and agreed user defined indices should be entered in the rows below the drop down lists



STEP 2B: Determine the Pollution Mitigation In	dex for the proposed Groundwater Protection						
This step requires the user to select the type of gro groundwater	undwater protection that is either part of the SuDS component or that lies b	etween the cor	nponent and th	9			
This step should be applied where a SuDS component is specifical even where infiltration is not specifically accounted for in the design	y designed to infiltrate runoff (note: in England and Wales this will include components that allow ar	y amount of infiltra	tion, however small,				
'Groundwater protection' describes the proposed depth of soil or oth	er material through which runoff will flow between the runoff surface and the underlying groundwate	r.					
Where the discharge is to surface waters and risks to groundwater	need not be considered, select 'None'						
If the proposed groundwater protection is bespoke and/or a propriet should be entered in the row below the drop down list	ary product and not generically described by the suggested measures, then a description of the prot	ection and agreed (	user defined indices		DESIGN CONDITIONS		
		P	ollution Mitigation	Indices			
		Total Suspend					
Select type of groundwater protection from the drop down list:	None	Solids	Metals	Hydrocarbons	1 2 3 4		
If the proposed groundwater protection is bespoke/proprietary and/or the generic indices above are not considered appropriate, select "Proprietary product" or "User defined indices" and enter a description of the protection and agreed user defined indices in this row:	Groundwater Protection Pollution Mitigation Index	0	0	0			
STEP 2C: Determine the Combined Pollution N This is an automatic step which combines the prop	litigation Indices for the Runoff Area osed SuDS Pollution Mitigation Indices with any Groundwater Protection Po	-					
		Total Suspend Solids	ned Pollution Mitig led Metals	Hydrocarbons			
	Combined Pollution Mitigation Indices for the Runoff Area	0.4	0.4	0.5	Note: If the total aggregated miligation index is > 1 (which is not a realistic outcome), then the outcome is fixed at ">0.267. In this scenario, the proposed components are which will have both and a ">0.467. In this scenario, the proposed land use (note: where risk assessment is required, this outcome would need more detailed verification).		
STEP 2D: Determine Sufficiency of Pollution Mitigation Indices for Selected SuDS Components This is an automatic step which compares the Combined Pollution Mitigation Indices with the Land Use Hazard Indices, to determine whether the proposed components are sufficient to manage each pollutant category type							
When the combined mitigation index exceeds the land use pollution	hazard index, then the proposed components are considered sufficient in providing pollution risk mi	tigation.			DESIGN CONDITIONS		
that provides environmental protection in the event of an unexpected	waters or groundwater, an additional treatment component (ie over and above that required for stan pollution event or poor system performance. Protected surface waters are those designated for dri Northern Ireland, a more precautionary approach may be required and this should be checked with	nking water abstrac	tion. In England and	Wales, protected			
		Total Suspend	cy of Pollution Mit led	igation Indices			
		Solids	Metals Sufficient	Hydrocarbons	1 Reference to local planning documents should also be made to isenify any additional protection required for sites due to habitat conservation (see Chapter 7 The SUGS design process). The implications of developments on or within close provinity to an area with an environmental designation, such as a Site of Special Scientific Interest (SSS) should be considered via		

# Appendix B – Causeway Flow Calculations



MCGREGOR MCMAHON CONSULTING ENGINEERS	1ahon us fe, KY11 8PB		Attenuation.pfd orm Network	Page 1	
		Design	Settings		
Maximum Time of	Rainfall Methodo Return Period (y Additional Flov Time of Entry (r Concentration (r num Rainfall (mr	rears) 2 w (%) 10 CV 0.750 mins) 5.00 mins) 30.00	Minimu Pre Includ	Ainimum Velocity Connection Im Backdrop Heig ferred Cover Dep le Intermediate G est practice design	h Type Level Soffits ht (m) $0.200$ th (m) $1.200$ round $\checkmark$
		<u>No</u>	<u>des</u>		
Name		of E Cover nins) Level (m)	Diameter ( (mm)	Easting Northin (m) (m)	ng Depth (m)
Attenuat	tion 0.040	5.00 100.000	600	0.000 0.00	00 1.000
		<u>Simulatio</u>	<u>n Settings</u>		
Rainfall Methodology Summer CV Winter CV	FEH-22 0.750 0.840 Di	Analysis S Skip Steady rain Down Time (	State x	Check	al Storage (m³/ha) 20.0 Discharge Rate(s) x Discharge Volume x
15 30 60	0 120 1	<b>Storm D</b> 80 240	urations 360 480	600 720	960 1440
Re		limate Change (CC %)	Additional Ar (A %)		Flow
	(years) 30 100 200	39 39 39 39		(Q %) 10 10 10	0 0 0
	Noc	le Attenuation O	nline Orifice C	<u>Control</u>	
Replaces Down	Flap Valve x stream Link √	Invert Leve Diameter		Discharge Co	oefficient 0.600
	Node At	ttenuation Dept	n/Area Storage	e Structure	
Base Inf Coefficien Side Inf Coefficien		,	ctor 2.0 osity 0.96	Inve Time to half en	rt Level (m) 99.000 npty (mins) 125
-	Area         Inf Area           (m²)         (m²)           17.9         0.0	Depth Are (m) (m 0.990 17	²) (m²)	Depth         Area           (m)         (m²)           0.991         0.0	) (m²)

	McGregor McMahon	File: 231107 Attenuation.pfd	Page 2
MCGREGOR 🖊 MCMAHON	2 Castle Court	Network: Storm Network	
CONSULTING_ENGINEERS		Sean Turner	
	Dunfermline, Fife, KY11 8PB	28/11/2023	

#### Results for 30 year +39% CC +10% A Critical Storm Duration. Lowest mass balance: 99.75%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
120 minute winter	Attenuation	94	99.621	0.621	6.3	11.3966	0.0000	ОК
•	Link Event Ipstream Depth)	No	JS ode	Link	Outflow (I/s)	Discharge Vol (m <sup>3</sup> )		
12	20 minute winter	Atten	uation	Orifice	1.5	18.1	L	

	McGregor McMahon	File: 231107 Attenuation.pfd	Page 3
McGregor 🖊 McMahon	2 Castle Court	Network: Storm Network	
CONSULTING_ENGINEERS	Carnegie Campus	Sean Turner	
	Dunfermline, Fife, KY11 8PB	28/11/2023	

#### Results for 100 year +39% CC +10% A Critical Storm Duration. Lowest mass balance: 99.75%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
60 minute winter	Attenuation	59	99.830	0.830	13.2	15.2381	0.0000	ОК
(U	Link Event pstream Depth)	N	JS ode	Link	Outflow (I/s)	Discharg Vol (m <sup>3</sup> )	-	
60	minute winter	Atten	uation	Orifice	1.7	19.	3	

	McGregor McMahon	File: 231107 Attenuation.pfd	Page 4
McGregor 🖊 McMahon	2 Castle Court	Network: Storm Network	
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	Dunfermline, Fife, KY11 8PB	28/11/2023	

#### Results for 200 year +39% CC +10% A Critical Storm Duration. Lowest mass balance: 99.75%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
60 minute winter	Attenuation	60	99.958	0.958	15.1	17.5795	0.0000	ОК
•	Link Event Upstream Depth) 0 minute winter	N	JS ode wation	<b>Link</b> Orifice	Outflow (I/s)	Discharg Vol (m <sup>3</sup> ) 21.	-	