## Welling United FC

Kingfisherlighting.com

## Kingfisher Lighting

## Executive Summary

A detailed site visit to record the current vertical levels achieved by the existing installation was carried out. This is the best way to look at the current environmental impact of the site lighting to local residence and habitat.
We have provided all readings and relevant photographs taken on site as evidence of this visit.

Then a detailed desk top design was undertaken on AGI32 software. This has taken into account the new pitch location for the designed levels. In this design we have built in the proposed development and placed vertical grids along the façade facing the pitch in order to show the resulting vertical lux levels and candelas on the properties. There has also been vertical grids placed along the existing housing on Roseacre Road and the side perimeter on the South edge where the site meets Danson Park which is a Site of Importance for Nature Conservation to show a reduced impact on these residence and the tree line with new LED fittings.

As can be seen in the design report vertical levels provided by a new LED installation at the same height as taken on site currently on the North, South and West boundaries have been reduced.

For example the highest level on the Southern tree boundary was 243Lux at 2 m . The highest vertical level at the same height for LED is 65Lux

However as can also be seen by the report the levels are high on the higher verticals on the North and south boundaries. This is due to the proximity of the Masts and fittings to the boundaries. Without lifting equipment it is impossible to take current on site levels at these heights. As the levels have reduced at lower level I would recommend that the current install would also be achieving higher vertical levels at these heights than the new LED installation is showing. Cowls have been added to the fittings but due to the limited size of these its impossible to reduce the vertical levels any further. High levels are purely a result of the location.
Optics which are sensitive to the spill of light have also been utilised where appropriate.

By reducing these levels we are directly protecting the surrounding biodiversity and environment which complies with the required local SP9 and DP20 guidelines.

The Cricket field to the East of the site currently has no lighting and so shouldn't be effected by the new LED installation on Welling FC ground as it is unlikely to be used during the same hours where the new lighting would be on.
LED fittings are more efficient at controlling light spill than the current light source on site which should reduce any nuisance lighting currently spilling over. We have also directed the new LED fittings specifically to minimise any spill. As can be seen on the lighting design there is minimal horizonal spill onto the cricket field. Stands and the new front building have been built into the site which effectively block the light spill. Cowls have also been used on the fittings to the South East which further help to reduce spill where there will be no building.


## Kingfisher Lighting

## Welling United FC

This report has been created to outline the new installation of LED lighting and its effect on obtrusive light on the surrounding new flat development, Current residential houses along Roseacre road and the tree line which borders Danson Park Grade I Site of Importance for Nature Conservation (SINC).


The new LED install has been designed based on New 18m masts with 1300w Amnis Following the FA regulations and guidance the scheme has been designed to achieve 200 Lux 0.6 $\mathrm{Min} / \mathrm{Av}$ and $0.25 \mathrm{~min} / \mathrm{max}$. with a 88 point grid and a 2.5 m instep

| Football |  |  |  | Table A.21 BS EN 12193:2007 |
| :--- | ---: | :--- | :--- | :--- | :--- |
|  | I 500 | 0.7 | 60 |  |
|  | II 200 | 0.6 | 60 |  |
|  | III 75 | 0.5 | 20 | FA recommend minimum 120 Lux for <br> Class III Football <br> Refer to wrww. TheFA.com |

## Method of design

To achieve this specification, we have selected the Amnis LED fitting, the lighting design provides instant, controllable white light, with no warmup time- improving visual acuity of people, objects and colours. The asymmetric reflector-based floodlight has a narrow beam with a $65^{\circ}$ peak therefore complies with ULWR and overspill onto any properties or boundaries.

The New FA regulations require a fitting which is 5000k and
 for the current none televised level of this club a CRI70

Beams Used:

- 1300w and 665w Amnis Flood with NST, NFT, WST \& WST B Optic
*Please see the attached design for full details*


## Colour Temperature

For the lighting designs with the Amnis LED luminaire a colour temperature of 5000K was chosen. This is required by the new FA regulations and maintains the efficiency of the LEDs without bringing an uninviting ambience to the locations making for a more comfortable and natural working environment for those on site. Other colour temperatures can be provided on request.


## Software

We have produced the lighting design using AGI 32 software to calculate the horizontal lighting levels measured FFL and spill light. A Maintenance Factor of 0.9 has been used for the designs, which means that the site is not over-lit in the early years, preserving the luminaire. We would recommend cleaning period of 12 months.


The \# 1 Independent Author of Illumination Engineering Software
Join the thousands of manutacturers, agencies, engineers, municipalities, DoTs, architects and lighting designers using our products! The fastest and most powerful path to successful lighting design.

## Kingfisher Lighting

## LED scheme

Using AGI lighting design software and the Kingfisher Amnis LED fitting the resulting levels on the pitch are achieved



In order to calculate the effect of artificial flood lighting installations on existing and new local residences one of the main documents used is 'ILP Guidance notes for the reduction of obtrusive light 2021'. This document helps prevent and safeguard against the effect of artificial light on surrounding areas. If not correctly controlled this would cause detrimental effects to local residents and wildlife.

The industry recommendations for determining the environmental area, as detailed in the guidance notes, refers to all planning authorities detail the environmental zones in advance, as alterations would cause our design to change dramatically. Categories are shown in Table 2 below;

Table 2: Environmental zones

| Zone | Surrounding | Lighting environment | Examples |
| :--- | :--- | :--- | :--- |
| E0 | Protected | Dark <br> (SQM 20.5+) | Astronomical Observable dark skies, UNESCO <br> starlight reserves, IDA dark sky places |
| E1 | Natural | Dark <br> (SQM 20 to 20.5) | Relatively uninhabited rural areas, National Parks, <br> Areas of Outstanding Natural Beauty, IDA buffer <br> zones etc. |
| E2 | Rural | Low district brightness <br> (SQM ~15 to 20) | Sparsely inhabited rural areas, village or relatively <br> dark outer suburban locations |
| E3 | Suburban | Medium district <br> brightness | Well inhabited rural and urban settlements, small <br> town centres of suburban locations |
| E4 | Urban | High district brightness | Town / City centres with high levels of night-time <br> activity |

The following table breaks down each environmental zone (EO - E4) and the limitation to which we must abide by. Once we know the environmental zone, we use the table to generate a report within AGI to make sure we are inside the parameters. Table 3 and 4 show the allowable values for each Environmental zone that a design must be compliant with.

Table 3 (CIE 150 table 2): Maximum values of vertical illuminance on premises

| Light technical parameter | Application conditions | Environmental zone |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | E0 | E1 | E2 | E3 | E4 |
| Illuminance in the vertical plane ( $\mathrm{E}_{\mathrm{v}}$ ) | Pre-curfew | n/a | 21 x | 51 x | 10 lx | 251 x |
|  | Post-curfew | n/a | <0.1 1x* | 1 lx | 21 x | 5 lx |

Kingfisher Lighting

Table 4 (CIE 150 table 3): Limits for the luminous intensity of bright luminaires ${ }^{4}$

| Light technical parameter | Application conditions | Luminaire group (projected area $\mathrm{A}_{\mathrm{p}}$ in $\mathrm{m}^{\mathbf{2}}$ ) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} 0<A_{p} \\ \leq 0.002 \end{gathered}$ | $\begin{gathered} 0.002<A_{p} \\ \leq 0.01 \end{gathered}$ | $\begin{gathered} 0.01<A_{p} \\ \leq 0.03 \end{gathered}$ | $\begin{gathered} 0.03<A_{p} \\ <0.13 \end{gathered}$ | $\begin{gathered} 0.13<A_{p} \\ \leq 0.50 \end{gathered}$ | $A_{p}>0.5$ |
| Maximum luminous intensity emitted by luminaire ( $I$ in cd) ${ }^{5}$ | EO <br> Pre-curfew <br> Post-curfew | 0 | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ |
|  | E1 Pre-curfew Post-curfew | $\begin{gathered} 0.29 d \\ 0 \end{gathered}$ | $\begin{gathered} 0.63 d \\ 0 \end{gathered}$ | $\begin{gathered} 1.3 d \\ 0 \end{gathered}$ | $\begin{gathered} 2.5 d \\ 0 \end{gathered}$ | $\underset{0}{5.1 d}$ | 2,500 0 |
|  | E2 <br> Pre-curfew <br> Post-curfew | $\begin{aligned} & 0.57 d \\ & 0.29 d \end{aligned}$ | $\begin{aligned} & 1.3 d \\ & 0.63 d \end{aligned}$ | $\begin{aligned} & 2.5 d \\ & 1.3 d \end{aligned}$ | $\begin{aligned} & 5.0 d \\ & 2.5 d \end{aligned}$ | $\begin{aligned} & 10 d \\ & 5.1 d \end{aligned}$ | $\begin{gathered} 7,500 \\ 500 \end{gathered}$ |
|  | E3 Pre-curfew Post-curfew | $\begin{aligned} & 0.86 d \\ & 0.29 d \end{aligned}$ | $\begin{aligned} & 1.9 d \\ & 0.63 d \end{aligned}$ | $\begin{aligned} & 3.8 \mathrm{~d} \\ & 1.3 \mathrm{~d} \end{aligned}$ | $\begin{aligned} & 7.5 d \\ & 2.5 \mathrm{~d} \end{aligned}$ | $\begin{aligned} & 15 d \\ & 5.1 d \end{aligned}$ | $\begin{gathered} 10.000 \\ 1,000 \end{gathered}$ |
|  | E4 <br> Pre-curfew Post-curfew | $\begin{aligned} & 1.4 d \\ & 0.29 d \end{aligned}$ | $\begin{gathered} 3.1 d \\ 0.63 d \end{gathered}$ | $\begin{aligned} & 6.3 d \\ & 1.3 d \end{aligned}$ | $\begin{aligned} & 13 d \\ & 2.5 d \end{aligned}$ | $\begin{aligned} & 26 d \\ & 5.1 d \end{aligned}$ | $\begin{gathered} 25,000 \\ 2,500 \end{gathered}$ |

*Full documents can be supplied if required*

Proposed New development and Pitch Location


Obtrusive light is classified as the below by the ILP

Obtrusive light, whether it keeps you awake through a bedroom window, impedes your view of the night sky or adversely affects the performance of an adjacent lighting installation, is a form of pollution. It may also be a nuisance in law and can be substantially mitigated without detriment to the requirements of the task.

After completing the initial design, grids have been placed on each house, the new flat development and along the South woodland perimeter within AGI lighting software in order to represent windows overlooking the site. Vertical levels are to ascertain the effect of new LED lighting against those recorded from the existing installation

North Vertical View

|  | \％ | \％ | \％ | \％ | \％ | b | \％ | \％ |  |  | $\dot{0}$ |  | ${ }^{\circ}$ |  |  |  | ${ }^{\circ}$ | ${ }^{\circ}$ |  |  | ， | \％ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| g－： | $\bigcirc$ | $\%$ | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $0_{0}^{0}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\bigcirc$ | 0 | $\bigcirc \frac{0}{0}$ |
| － 0 | \％ | $\stackrel{0}{0}$ | － | ${ }^{\circ}$ | ${ }_{0}$ | b | 0 | ${ }^{\circ}$ | 0 | \％ | $\dot{0}$ | \％ | $\dot{0}$ | \％ | \％ | \％ | ${ }^{\circ}$ | 0 | ${ }_{0}$ | － | 0 | 0 | 0 | $\bigcirc \frac{0}{0}$ |
| E－ | $\stackrel{0}{0}$ | $\stackrel{0}{0}$ | 0 | ${ }^{0}$ | 0 | p | 0 | 0 | $\stackrel{0}{0}$ | $\dot{0}$ | $\stackrel{0}{0}$ | $\dot{0}$ | $\dot{0}$ | $\stackrel{0}{0}$ | 0 | $\dot{0}$ | 0 | 0 | 0 | 0 | 0 | $\dot{0}$ | $\dot{0}$ | $0 \cdot 1$ |
| E 0 | 0 | $\stackrel{0}{0}$ | 0 | 0 | 0 | p | 0 | 0 | 0 | ${ }^{\circ}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\stackrel{0}{0}$ | 0 | 0 0， |
| E： | 0 | 0 | 0 | 0 | 0 | b | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\stackrel{0}{0}$ | 0 | 0 | 0 | 0 | 0 | 0 | 1. |
| E． | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | \％ | 0 | \％ | 0 | 0 | 0 | $\stackrel{0}{0}$ | 2 |
| $00^{-5}$ | 0 | $\stackrel{0}{0}$ | 0 | 0 | 0 | b | 0 | 0 | 0 | $\stackrel{0}{0}$ | \％ | 0 | 0 | 0 | \％ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 69 |
| － 38 | 0 | 0 | 0 | 0 | 0 | \％ | 0 | 0 | 0 | $\dot{0}$ | 0 | \％ | \％ | 0 | \％ | \％ | \％ | 0 | 0 | 0 | 0 | 0 | $\dot{0}$ | 480 |
| $805-20$ | ． 108 | 21 | 6 | 2 | 1 | ］ | 1 | 0 | 0 | 0 | 0 | \％ | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 |  | 23 | ［9］． |
| C0E－1047 | 1652 | 254 | 39 | 10 | 4 | 2 | 1 | 1 | 1 | 0 | 0 | 0 | 0 |  |  |  | 1 | 1 | 2 | 5 | 20 | 173 | 1479 |  |
| 200\％${ }^{662}$ | $\stackrel{1509}{ }$ | 496 | ． 147 | 32 | 10 | 4 | 2 | 1 | 1 | 9 | 9 | 9 | 9 | 9 | 9 | 9 | 1 | 2 | 5 | 15 | 82 | 580 | ． 1407 | 造 |
| 68E－447 | 639 | $\stackrel{484}{4}$ | 206 | 82 | 26 | 3 | 4 | $\stackrel{2}{2}$ | 2 | 1 | 1 | 1 | 1 | 9 | 9 | 9 | 2 | 4 | 11 | 46 | 217 | 409 | 550 | 6920 |
| 264－292 | 387 | 473 | ． 180 | ． 104 | 50 | 21 | 9 | 4 | $\stackrel{2}{2}$ | 2 | 9 | 1 | 1 | 9 | 1 | 2 | 4 | 9 | 29 | 98 | ． 180 | 318 | 303 | 0 明 |
| 55\％－188 | 268 | 364 | ． 184 | 87 | 60 |  | 16 |  |  |  |  |  |  | 2 |  |  |  |  | 52 | 98 | ． 128 | 254 | 217 | 发造 |
| $65^{-1}{ }^{\text {c }}$ | ． 192 | 201 | ． 165 | 86 | 53 | 38 | 23 | 13 | 7 | 4 | 3 | 2 | 2 | 2 | 3 | 6 | 14 | 31 | 57 | 74 | 104 | ． 199 | ． 160 | 0 \％ |
| 昛 86 | 137 | 96 | ． 140 | 84 | 49 | 35 | 25 | ${ }^{16}$ | 10 | 6 | 4 | 3 | 3 | 4 | 6 | 11 | 20 | 35 | 47 | 57 | 88 | 133 | ． 118 | 9396 |
| 樶 62 | 98 | 69 | 117 | 75 | 48 | 31 | 24 | 18 | 12 | 8 | 6 | 5 | 5 | 6 | 9 | 15 | 23 | 32 | 37 | 48 | 75 | 77 | 89 | 73 國 |
| 2t－ 46 | 72 | 53 | 89 | ${ }^{6} 6$ | 45 | 30 | 22 | 18 | 14 | 10 | 8 | 7 | 7 | 8 | 12 | 817 | 22 | 26 | 31 | 42 | 63 | 48 | 68 | 54． |
| Et 35 | 54 | 43 | 53 | 58 | 41 | 9 | 21 | 16 | ${ }^{14}$ | ． 11 | 9 | 8 | 9 | 11 | $\stackrel{14}{ }$ | 97 | 20 | 23 | ． 27 | 37 | 53 | 35 | 53 | 46 |
| 樶－27 | 42 | 36 | 34 | 51 | 37 | 88 | 20 | 16 | .$^{13}$ | 12 | ． 11 | 10 | 11 | 12 | 14 | 16 | ${ }^{18}$ | 20 | 24 | 33 | 43 | 30 | 42 |  |
| 95－22 | 33 | 30 | 25 | 42 | 33 | ${ }^{6}$ | 20 | 16 | $\stackrel{13}{ }$ | 12 | 12 | 12 | 12 | 13 | 14 | $\stackrel{15}{ }$ | $\stackrel{16}{ }$ | 18 | 23 | 30 | 34 | ${ }^{26}$ | 35 | 26 |
| 92－ 18 | 26 | ${ }^{26}$ | 20 | 32 | 30 | 34 | ．19 | ．${ }^{16}$ | .$^{13}$ | 12 | 12 | 12 | 13 | 13 | $\stackrel{14}{ }$ | 14 | $\stackrel{15}{15}$ | 1.17 | 21 | 27 | 25 | $\stackrel{23}{ }$ | $\stackrel{29}{ }$ | $2{ }^{2}$ |
| 02－ 14 | 21 | 22 | 17 | 22 | 28 | p2 | 18 | 16 | 14 | 13 | 12 | 13 | $\stackrel{13}{ }$ | $\stackrel{13}{ }$ | 14 | 14 | $\stackrel{15}{15}$ | 17 | 20 | 25 | 19 | 21 | 25 | 2.0 |
| 0F－ 12 | 18 | 19 | $\stackrel{15}{14}$ | 17 | 25 | 21 | 18 | 16 | ． 14 | 13 | 13 | 13 | 13 | 13 | 13 | 14 | 15 | ${ }^{16}$ | 19 | ${ }_{2} 2$ | 16 | 19 | 22 | 1920］ |
|  | 45 | 47 | 14 | 14 | 24 | 20 | 17 | ${ }_{6} 6$ | ${ }_{15}$ | 14 | 43 | 43 | 43 | 13 | ${ }_{13}$ | 14 | 45 | 46 | i9 | 21 | ${ }_{16}$ | 18 | 20 | 48 |

House 5

West Vertical View


## East Vertical View



## South Vertical View

| \% | i | \% | ${ }_{8}^{\square I}$ | 1848 | 218 | i9 | 4 | 2 | ; | ; | ; | ${ }^{1}$ | ; | ; | ; | 2 | 2 | 3 | 4 | 8 | 9 | ${ }^{18}$ | 39 | ${ }^{35}$ | 224 | ${ }^{38}$ | 2 | ; | i | $\bigcirc \frac{0}{0}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 12 | ; | 281 | 270 | 489 | 220 | 32 | 12 | \% | 3 | 2 | 2 | 2 | 2 | 3 | 4 | 8 | 10 | ${ }^{17}$ | 30 | so | 112 | 238 | 350 | 371 | iss | 31 | ; | ; | $1 \rightarrow$ |
| 5 | 14 | 45 | ${ }^{148}$ | 147 | 298 | ${ }^{135}$ | 3 | 48 | 19 | 5 | 5 | 4 | 5 | 8 | 8 | is | ${ }_{16}$ | 25 | 41 | 89 | 114 | i78 | 220 | 228 | 330 | 78 | 34 | , | $i$ | $1 \rightarrow$ |
| 8 | 12 | ${ }^{33}$ | 81 | 32 | 148 | 38 | 38 | 42 | 30 | 19 | 12 | 9 | 9 | i1 | 14 | i9 | 27 | 40 | 80 | 38 | 113 | ${ }^{138}$ | 171 | 230 | 249 | 78 | 87 | 48 | i | $\vec{i}$ |
| 5 | i1 | 28 | 31 | 39 | 48 | 74 | 48 | 33 | 28 | 22 | 18 | ${ }^{16}$ | ${ }^{15}$ | 17 | 20 | 27 | 35 | 47 | \%1 | 75 | 89 | i11 | 149 | T98 | 116 | 38 | 35 | 38 | $i$ |  |
| 5 | 10 | 20 | 34 | 40 | 33 | \$2 | 39 | 29 | 23 | 21 | 20 | 20 | 20 | 22 | 25 | 31 | 38 | 45 | \$3 | 83 | 48 | \$o | 140 | ${ }^{4} 4$ | ${ }^{3} 4$ | 35 | 44 | 28 | ${ }^{17}$ | $\bigcirc$ |
| 8 | 10 | ${ }^{17}$ | 25 | 29 | 27 | 29 | 33 | 28 | 22 | 20 | 20 | 21 | ${ }_{23}$ | 25 | 28 | 32 | 38 | 41 | 48 | \%6 | 70 | 36 | 117 | 89 | 42 | 44 | 35 | 12 | 14 |  |
| 8 | 9 | 14 | 20 | 23 | 22 | 19 | 28 | 25 | 21 | 21 | 21 | 22 | 24 | 28 | 29 | 32 | 35 | 39 | 44 | ${ }_{53}$ | 88 | 34 | \$o | 47 | ${ }^{37}$ | 38 | 29 | is | 12 | 888 |
| $\stackrel{3}{8}$ | 3 |  | simo |  | $20$ | is | 23 | ${ }_{23}^{23}$ | $i_{2}$ | $2_{21}$ | $22$ | $22$ | ${ }_{24}^{24}$ |  |  | 习习1 | $L_{34}^{34}$ | $38$ | $43$ | $5_{3}$ |  |  |  | $32$ |  |  |  |  |  |  |

Following the guidelines of the ILP we have assumed that this site would be within an E3 zone.

| E3 | Suburban | Medium district <br> brightness | Well inhabited rural and urban settlements, small <br> town centres of suburban locations |
| :--- | :--- | :--- | :--- |

The resulting allowable levels are:

10 Lux on the houses / Gardens

| Light technical parameter | Application conditions | Environmental zone |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | E0 | E1 | E2 | E3 | E4 |
| Illuminance in the vertical plane ( $\mathrm{E}_{\mathrm{v}}$ ) | Pre-curfew | n/a | 21 x | 51 x | 10 lx | 25 lx |
|  | Post-curfew | n/a | $<0.1 \mathrm{~lx}^{*}$ | 1 lx | 21 x | 5 lx |

Also the candelas must lay within the following permitters.

The Amnis fitting is 0.5 m 2 and as such can achieve up to 10,000 candelas. The table provided from AGI shows that no grid point is above the 10,000 candelas allowable and confirms the below Pass and the Design write up

| Light technical parameter | Application conditions | Luminaire group (projected area $\mathrm{A}_{\mathrm{p}}$ in $\mathrm{m}^{\mathbf{2}}$ ) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} 0<A_{p} \\ \leq 0.002 \end{gathered}$ | $\begin{gathered} 0.002<A_{p} \\ \leq 0.01 \end{gathered}$ | $\begin{gathered} 0.01<A_{p} \\ \leq 0.03 \end{gathered}$ | $\begin{gathered} 0.03<A_{p} \\ \leq 0.13 \end{gathered}$ | $\begin{gathered} 0.13<A_{p} \\ \leq 0.50 \end{gathered}$ | $A_{p}>0.5$ |
| Maximum luminous intensity emitted by luminaire ( $I$ in cd) ${ }^{5}$ | E0 Pre-curfew Post-curfew | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ |
|  | E1 <br> Pre-curfew Post-curfew | $\begin{gathered} 0.29 d \\ 0 \end{gathered}$ | $\begin{gathered} 0.63 d \\ 0 \end{gathered}$ | $\underset{0}{1.3 d}$ | $\underset{0}{2.5 d}$ | $\underset{0}{5.1 d}$ | $\begin{gathered} 2,500 \\ 0 \end{gathered}$ |
|  | E2 <br> Pre-curfew Post-curfew | $\begin{aligned} & 0.57 d \\ & 0.29 d \end{aligned}$ | $\begin{aligned} & 1.3 d \\ & 0.63 d \end{aligned}$ | $\begin{aligned} & 2.5 \mathrm{~d} \\ & 1.3 \mathrm{~d} \end{aligned}$ | $\begin{aligned} & 5.0 \mathrm{~d} \\ & 2.5 \mathrm{~d} \end{aligned}$ | $\begin{aligned} & 10 \mathrm{~d} \\ & 5.1 \mathrm{~d} \end{aligned}$ | $\begin{gathered} 7,500 \\ 500 \end{gathered}$ |
|  | E3 <br> Pre-curfew Post-curfew | $\begin{aligned} & 0.86 d \\ & 0.29 d \end{aligned}$ | $\begin{aligned} & 1.9 d \\ & 0.63 d \end{aligned}$ | $\begin{aligned} & 3.8 \mathrm{~d} \\ & 1.3 \mathrm{~d} \end{aligned}$ | $\begin{aligned} & 7.5 d \\ & 2.5 d \end{aligned}$ | $\begin{aligned} & 15 d \\ & 5.1 d \end{aligned}$ | $\begin{gathered} 10.000 \\ 1,000 \end{gathered}$ |
|  | E4 <br> Pre-curfew Post-curfew | $\begin{aligned} & 1.4 d \\ & 0.29 d \end{aligned}$ | $\begin{aligned} & 3.1 d \\ & 0.63 d \end{aligned}$ | $\begin{aligned} & 6.3 \mathrm{~d} \\ & 1.3 \mathrm{~d} \end{aligned}$ | $\begin{aligned} & 13 d \\ & 2.5 d \end{aligned}$ | $\begin{aligned} & 26 d \\ & 5.1 d \end{aligned}$ | $\begin{gathered} 25,000 \\ 2,500 \end{gathered}$ |

The new LED installation compliance test follows:

## Obtrusive Light - Compliance Report

CIE 150:2017, E3-Medium District Brightness, Pre-Curfew
Filename: Welling united FC Design Rev B
25/11/2023 17:35:39

## Illuminance

Maximum Allowable Value: 10 Lux
Calculations Tested (9):

| Calculation Label | Test <br> Results | Max. <br> Illum. |
| :--- | :--- | :--- |
| House Row 1_IIISSeg1 | PASS | 1 |
| House Row 2_IIIISeg1 | PASS | 1 |
| House Row 3_III_Seg1 | PASS | 1 |
| House Row 4_III_Seg1 | PASS | 0 |
| Tree Line_III_Seg1 | FAIL | 17 |
| Tree Line_III_Seg2 | FAIL | 1848 |
| House Row 5_IIISSeg1 | FAIL | 1560 |
| House Row 5_IIISSeg2 | FAIL | 1652 |
| House Row 5_III_Seg3 | FAIL | 998 |

Failed Meter Locations (>250, only first 250 shown):

| Calculation Label | Lux | Meter Coords |
| :---: | :---: | :---: |
| House Row 5_III_Seg1 | 39 | 80.882, 120.878, 0.5 |
| House Row 5_III_Seg1 | 41 | 80.751, 111.879, 0.5 |
| House Row 5_III_Seg1 | 42 | 80.707, 108.88, 0.5 |
| House Row 5_III_Seg1 | 44 | 80.838, 117.879, 0.5 |
| House Row 5_III_Seg1 | 45 | 80.794, 114.879, 0.5 |
| House Row 5_III_Seg1 | 47 | 80.663, 105.88, 0.5 |
| Tree Line_III_Seg1 | 13 | 0.224, 12.959, 2.25 |
| Tree Line_III_Seg1 | 13 | 0.224, 12.959, 3.75 |
| Tree Line_III_Seg1 | 14 | 0.224, 12.959, 0.75 |
| Tree Line_III_Seg1 | 16 | 0.224, 15.959, 2.25 |
| Tree Line_III_Seg1 | 16 | 0.224, 15.959, 3.75 |
| Tree Line_III_Seg1 | 16 | 0.224, 15.959, 5.25 |
| Tree Line_III_Seg1 | 17 | 0.224, 15.959, 0.75 |
| Tree Line_III_Seg2 | 11 | 88.776, 17.963, 8.25 |
| Tree Line_III_Seg2 | 11 | 49.874, 15.201, 9.75 |
| Tree Line_III_Seg2 | 11 | 43.89, 14.776, 11.25 |
| Tree Line_III_Seg2 | 12 | 4.987, 12.013, 3.75 |
| Tree Line_III_Seg2 | 12 | 88.776, 17.963, 9.75 |
| Tree Line_III_Seg2 | 12 | 58.852, 15.838, 9.75 |
| Tree Line_III_Seg2 | 12 | 88.776, 17.963, 12.75 |
| Tree Line_III_Seg2 | 12 | 67.829, 16.476, 12.75 |
| Tree Line_III_Seg2 | 13 | 85.784, 17.751, 0.75 |
| Tree Line_III_Seg2 | 13 | 7.98, 12.226, 0.75 |
| Tree Line_III_Seg2 | 13 | 85.784, 17.751, 2.25 |
| Tree Line_III_Seg2 | 14 | 85.784, 17.751, 3.75 |
| Tree Line_III_Seg2 | 14 | 4.987, 12.013, 5.25 |
| Tree Line_III_Seg2 | 14 | 46.882, 14.988, 9.75 |
| Tree Line_III_Seg2 | 14 | 88.776, 17.963, 11.25 |
| Tree Line_III_Seg2 | 15 | 7.98, 12.226, 2.25 |
| Tree Line_III_Seg2 | 15 | 52.867, 15.413, 8.25 |
| Tree Line_III_Seg2 | 16 | 82.792, 17.538, 0.75 |
| Tree Line_III_Seg2 | 16 | 55.859, 15.626, 8.25 |
| Tree Line_III_Seg2 | 16 | 40.897, 14.563, 11.25 |

# Kingfisher Lighting 

| Tree Line_III_Seg2 | 17 |
| :---: | :---: |
| Tree Line_III_Seg2 | 17 |
| Tree Line_III_Seg2 | 17 |
| Tree Line_III_Seg2 | 17 |
| Tree Line_III_Seg2 | 17 |
| Tree Line_III_Seg2 | 18 |
| Tree Line_III_Seg2 | 18 |
| Tree Line_III_Seg2 | 18 |
| Tree Line_III_Seg2 | 18 |
| Tree Line_III_Seg2 | 18 |
| Tree Line_III_Seg2 | 18 |
| Tree Line_III_Seg2 | 18 |
| Tree Line_Ill_Seg2 | 19 |
| Tree Line_III_Seg2 | 19 |
| Tree Line_III_Seg2 | 19 |
| Tree Line_III_Seg2 | 19 |
| Tree Line_III_Seg2 | 19 |
| Tree Line_III_Seg2 | 19 |
| Tree Line_III_Seg2 | 20 |
| Tree Line_Ill_Seg2 | 20 |
| Tree Line_III_Seg2 | 20 |
| Tree Line_III_Seg2 | 20 |
| Tree Line_III_Seg2 | 20 |
| Tree Line_III_Seg2 | 20 |
| Tree Line_III_Seg2 | 20 |
| Tree Line_III_Seg2 | 20 |
| Tree Line_III_Seg2 | 20 |
| Tree Line_III_Seg2 | 20 |
| Tree Line_III_Seg2 | 21 |
| Tree Line_III_Seg2 | 21 |
| Tree Line_III_Seg2 | 21 |
| Tree Line_III_Seg2 | 21 |
| Tree Line_III_Seg2 | 21 |
| Tree Line_III_Seg2 | 21 |
| Tree Line_III_Seg2 | 21 |
| Tree Line_III_Seg2 | 22 |
| Tree Line_III_Seg2 | 22 |
| Tree Line_III_Seg2 | 22 |
| Tree Line_III_Seg2 | 22 |
| Tree Line_III_Seg2 | 22 |
| Tree Line_III_Seg2 | 22 |
| Tree Line_III_Seg2 | 22 |
| Tree Line_III_Seg2 | 22 |
| Tree Line_III_Seg2 | 22 |
| Tree Line_III_Seg2 | 22 |
| Tree Line_III_Seg2 | 22 |
| Tree Line_III_Seg2 | 22 |
| Tree Line_III_Seg2 | 23 |
| Tree Line_III_Seg2 | 23 |
| Tree Line_III_Seg2 | 23 |
| Tree Line_III_Seg2 | 23 |
| Tree Line_III_Seg2 | 23 |
| Tree Line_III_Seg2 | 23 |
| Tree Line_III_Seg2 | 24 |
| Tree Line_III_Seg2 | 24 |
| Tree Line_III_Seg2 | 24 |
| Tree Line_III_Seg2 | 24 |
| Tree Line_III_Seg2 | 25 |
| Tree Line_III_Seg2 | 25 |
| Tree Line_III_Seg2 | 25 |

Tree Line_III_Seg2 17
Tree Line_III_Seg2 17
Tree Line_III_Seg2 17

- 18
Tree Line_III_Seg2 18
Tree Line_III Seg2 18
Tree Line III Seg2 18
Tree Line_III_Seg2 18
18
Tree Line III Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Line III Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line-III-Seg2
Tree Line_III_Seg2
Tree Line III Seg2
Tree Line III Seg2
Tree Line_III_Seg2
ree Line ill Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Seg2
Tree Line III Seg2
Tree Line_III_Seg2
Tree Line_m_Seg2
Tree Line_III_Seg2
Tree Line III Seg2
ree Line_ill Seg2
Tree Line_III_Seg2
Line 11 Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line III Seg2

Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line III Seg
Tree Line III Seg2
Tree Line_III_Seg2
Tree Line-III Seg2
25
Tree Line_III_Seg2
82.792, 17.538, 2.25
85.784, 17.751, 5.25
4.987, 12.013, 6.75
49.874, 15.201, 8.25
34.912, 14.138, 12.75
79.799, 17.326, 0.75
76.807, 17.113, 0.75
73.814, 16.901, 0.75
73.814, 16.901, 2.25
7.98, 12.226, 3.75
58.852, 15.838, 8.25
25.935, 13.501, 14.25
79.799, 17.326, 2.25
73.814, 16.901, 3.75
61.844, 16.051, 9.75
43.89, 14.776, 9.75
64.837, 16.263, 11.25
73.814, 16.901, 14.25
70.822, 16.688, 0.75
76.807, 17.113, 2.25
82.792, 17.538, 3.75
61.844, 16.051, 5.25
58.852, 15.838, 5.25
85.784, 17.751, 6.75
58.852, 15.838, 6.75
55.859, 15.626, 6.75
52.867, 15.413, 6.75
46.882, 14.988, 8.25
10.972, 12.438, 0.75
61.844, 16.051, 2.25
64.837, 16.263, 3.75 61.844, 16.051, 3.75 58.852, 15.838, 3.75 55.859, 15.626, 5.25 61.844, 16.051, 6.75 64.837, 16.263, 0.75 61.844, 16.051, 0.75 58.852, 15.838, 0.75 64.837, 16.263, 2.25 58.852, 15.838, 2.25 55.859, 15.626, 2.25 76.807, 17.113, 3.75 55.859, 15.626, 3.75 64.837, 16.263, 5.25 7.98, 12.226, 5.25 49.874, 15.201, 6.75 61.844, 16.051, 8.25 67.829, 16.476, 0.75 70.822, 16.688, 2.25 67.829, 16.476, 2.25 79.799, 17.326, 3.75 52.867, 15.413, 5.25 64.837, 16.263, 6.75 55.859, 15.626, 0.75 52.867, 15.413, 2.25 10.972, 12.438, 2.25 52.867, 15.413, 3.75 52.867, 15.413, 0.75 67.829, 16.476, 3.75 82.792, 17.538, 5.25


# Kingfisher Lighting 

| Tree Line_III_Seg2 | 25 |
| :---: | :---: |
| Tree Line_III_Seg2 | 25 |
| Tree Line_III_Seg2 | 25 |
| Tree Line_III_Seg2 | 26 |
| Tree Line_III_Seg2 | 26 |
| Tree Line_III_Seg2 | 26 |
| Tree Line_III_Seg2 | 26 |
| Tree Line_III_Seg2 | 26 |
| Tree Line_III_Seg2 | 26 |
| Tree Line_III_Seg2 | 27 |
| Tree Line_III_Seg2 | 27 |
| Tree Line_III_Seg2 | 27 |
| Tree Line_Ill_Seg2 | 27 |
| Tree Line_III_Seg2 | 28 |
| Tree Line_III_Seg2 | 28 |
| Tree Line_III_Seg2 | 28 |
| Tree Line_III_Seg2 | 28 |
| Tree Line_III_Seg2 | 29 |
| Tree Line_III_Seg2 | 29 |
| Tree Line_III_Seg2 | 29 |
| Tree Line_III_Seg2 | 29 |
| Tree Line_III_Seg2 | 29 |
| Tree Line_III_Seg2 | 29 |
| Tree Line_III_Seg2 | 29 |
| Tree Line_III_Seg2 | 29 |
| Tree Line_III_Seg2 | 30 |
| Tree Line_III_Seg2 | 30 |
| Tree Line_III_Seg2 | 30 |
| Tree Line_III_Seg2 | 31 |
| Tree Line_III_Seg2 | 32 |
| Tree Line_III_Seg2 | 32 |
| Tree Line_Ill_Seg2 | 32 |
| Tree Line_III_Seg2 | 32 |
| Tree Line_III_Seg2 | 32 |
| Tree Line_III_Seg2 | 32 |
| Tree Line_III_Seg2 | 33 |
| Tree Line_III_Seg2 | 33 |
| Tree Line_III_Seg2 | 33 |
| Tree Line_Ill_Seg2 | 33 |
| Tree Line_III_Seg2 | 34 |
| Tree Line_III_Seg2 | 34 |
| Tree Line_III_Seg2 | 34 |
| Tree Line_III_Seg2 | 35 |
| Tree Line_III_Seg2 | 35 |
| Tree Line_III_Seg2 | 35 |
| Tree Line_III_Seg2 | 36 |
| Tree Line_III_Seg2 | 36 |
| Tree Line_III_Seg2 | 37 |
| Tree Line_III_Seg2 | 38 |
| Tree Line_III_Seg2 | 38 |
| Tree Line_III_Seg2 | 38 |
| Tree Line_Ill_Seg2 | 38 |
| Tree Line_III_Seg2 | 39 |
| Tree Line_III_Seg2 | 39 |
| Tree Line_III_Seg2 | 39 |
| Tree Line_III_Seg2 | 40 |
| Tree Line_III_Seg2 | 40 |
| Tree Line_III_Seg2 | 41 |
| Tree Line_III_Seg2 | 41 |
| Tree Line_III_Seg2 | 42 |

Tree Line_III_Seg2 25
Tree Line_III_Seg2 26
Tree Line_III_Seg2 26
Tree Line III Seg2
Tree Line_III_Seg2 26
Tree Line III Seg2 26
Tree Line_III_Seg2 27
Tree Line_III_Seg2 27
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line IIII Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line III Seg2
Tree Line III Seg2
31
Tree Line_III_Seg2 32
Tree Line_III_Seg2
Tree Line- III-Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line IIII Seg2
Tree Line_III_Seg2
Tree Line III Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line III Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_li-Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line III Seg2
Tree Line-II Seg
Tree Line III Seg2
Tree Line_III_Seg2
9
0
30
3025
49.874, 15.201, 5.25
46.882, 14.988, 6.75
37.905, 14.351, 11.25
13.965, 12.651, 0.75
49.874, 15.201, 2.25
49.874, 15.201, 3.75
67.829, 16.476, 5.25
85.784, 17.751, 8.25
64.837, 16.263, 8.25
49.874, 15.201, 0.75
76.807, 17.113, 5.25
43.89, 14.776, 8.25
40.897, 14.563, 9.75
19.95, 13.076, 0.75
70.822, 16.688, 3.75
46.882, 14.988, 5.25
7.98, 12.226, 6.75
46.882, 14.988, 0.75
16.957, 12.863, 0.75
46.882, 14.988, 2.25
46.882, 14.988, 3.75
10.972, 12.438, 3.75
79.799, 17.326, 5.25
73.814, 16.901, 5.25
67.829, 16.476, 6.75
13.965, 12.651, 2.25
64.837, 16.263, 9.75
31.92, 13.926, 12.75
43.89, 14.776, 6.75
43.89, 14.776, 0.75
43.89, 14.776, 2.25
19.95, 13.076, 2.25
16.957, 12.863, 2.25
43.89, 14.776, 3.75
43.89, 14.776, 5.25
70.822, 16.688, 5.25
76.807, 17.113, 6.75
67.829, 16.476, 8.25
85.784, 17.751, 9.75
40.897, 14.563, 0.75
40.897, 14.563, 2.25
82.792, 17.538, 6.75
40.897, 14.563, 3.75
10.972, 12.438, 5.25
40.897, 14.563, 8.25
13.965, 12.651, 3.75
40.897, 14.563, 5.25
16.957, 12.863, 3.75
37.905, 14.351, 0.75
37.905, 14.351, 2.25
40.897, 14.563, 6.75
7.98, 12.226, 8.25
37.905, 14.351, 3.75
70.822, 16.688, 6.75
22.942, 13.288, 14.25
79.799, 17.326, 6.75
37.905, 14.351, 9.75
37.905, 14.351, 5.25
34.912, 14.138, 11.25
22.942, 13.288, 0.75

## Kingfisher Lighting

| Tree Line_III_Seg2 | 42 |
| :---: | :---: |
| Tree Line_III_Seg2 | 42 |
| Tree Line_III_Seg2 | 43 |
| Tree Line_III_Seg2 | 44 |
| Tree Line_III_Seg2 | 44 |
| Tree Line_III_Seg2 | 44 |
| Tree Line_III_Seg2 | 44 |
| Tree Line_III_Seg2 | 45 |
| Tree Line_III_Seg2 | 46 |
| Tree Line_III_Seg2 | 46 |
| Tree Line_III_Seg2 | 46 |
| Tree Line_III_Seg2 | 46 |
| Tree Line_III_Seg2 | 47 |
| Tree Line_III_Seg2 | 47 |
| Tree Line_III_Seg2 | 48 |
| Tree Line_III_Seg2 | 48 |
| Tree Line_III_Seg2 | 51 |
| Tree Line_III_Seg2 | 51 |
| Tree Line_III_Seg2 | 52 |
| Tree Line_III_Seg2 | 52 |
| Tree Line_III_Seg2 | 53 |
| Tree Line_III_Seg2 | 53 |
| Tree Line_III_Seg2 | 53 |
| Tree Line_III_Seg2 | 54 |
| Tree Line_III_Seg2 | 55 |
| Tree Line_III_Seg2 | 55 |
| Tree Line_III_Seg2 | 56 |
| Tree Line_III_Seg2 | 56 |
| Tree Line_III_Seg2 | 58 |
| Tree Line_III_Seg2 | 58 |
| Tree Line_III_Seg2 | 58 |
| Tree Line_III_Seg2 | 59 |
| Tree Line_III_Seg2 | 60 |
| Tree Line_III_Seg2 | 60 |
| Tree Line_III_Seg2 | 61 |
| Tree Line_III_Seg2 | 63 |
| Tree Line_III_Seg2 | 63 |
| Tree Line_III_Seg2 | 65 |
| Tree Line_III_Seg2 | 66 |
| Tree Line_III_Seg2 | 67 |
| Tree Line_III_Seg2 | 68 |
| Tree Line_III_Seg2 | 69 |
| Tree Line_III_Seg2 | 70 |
| Tree Line_III_Seg2 | 74 |
| Tree Line_III_Seg2 | 74 |
| Tree Line_III_Seg2 | 75 |
| Tree Line_III_Seg2 | 76 |
| Tree Line_III_Seg2 | 76 |
| Tree Line_III_Seg2 | 78 |
| Tree Line_III_Seg2 | 81 |
| Tree Line_III_Seg2 | 84 |
| Tree Line_III_Seg2 | 84 |
| Tree Line_III_Seg2 | 86 |
| Tree Line_III_Seg2 | 86 |
| Tree Line_III_Seg2 | 89 |
| Tree Line_III_Seg2 | 89 |
| Tree Line_III_Seg2 | 90 |
| Tree Line_III_Seg2 | 91 |
| Tree Line_III_Seg2 | 92 |
| Tree Line_III_Seg2 | 95 |

16.957, 12.863, 5.25 67.829, 16.476, 9.75 34.912, 14.138, 2.25 34.912, 14.138, 0.75 34.912, 14.138, 3.75 13.965, 12.651, 5.25 10.972, 12.438, 6.75 37.905, 14.351, 6.75 76.807, 17.113, 8.25 70.822, 16.688, 8.25 85.784, 17.751, 11.25 67.829, 16.476, 11.25 19.95, 13.076, 3.75 37.905, 14.351, 8.25 34.912, 14.138, 5.25 7.98, 12.226, 9.75 31.92, 13.926, 0.75 82.792, 17.538, 8.25 73.814, 16.901, 6.75 70.822, 16.688, 12.75 31.92, 13.926, 2.25 31.92, 13.926, 3.75 34.912, 14.138, 6.75 16.957, 12.863, 6.75 13.965, 12.651, 6.75 10.972, 12.438, 8.25 31.92, 13.926, 5.25 28.927, 13.713, 12.75 28.927, 13.713, 0.75 70.822, 16.688, 9.75 13.965, 12.651, 14.25 79.799, 17.326, 8.25 25.935, 13.501, 0.75 34.912, 14.138, 9.75 34.912, 14.138, 8.25 28.927, 13.713, 2.25 31.92, 13.926, 6.75 22.942, 13.288, 2.25 13.965, 12.651, 8.25 10.972, 12.438, 9.75 28.927, 13.713, 3.75 31.92, 13.926, 11.25 28.927, 13.713, 5.25 25.935, 13.501, 2.25 73.814, 16.901, 8.25 31.92, 13.926, 8.25 28.927, 13.713, 6.75 13.965, 12.651, 9.75 13.965, 12.651, 11.25 82.792, 17.538, 9.75 25.935, 13.501, 3.75 10.972, 12.438, 11.25 31.92, 13.926, 9.75 70.822, 16.688, 11.25 19.95, 13.076, 5.25 28.927, 13.713, 8.25 22.942, 13.288, 3.75 10.972, 12.438, 12.75 79.799, 17.326, 9.75 19.95, 13.076, 14.25

| Tree Line_III_Seg2 | 96 |
| :---: | :---: |
| Tree Line_III_Seg2 | 96 |
| Tree Line_III_Seg2 | 99 |
| Tree Line_III_Seg2 | 111 |
| Tree Line_III_Seg2 | 112 |
| Tree Line_III_Seg2 | 113 |
| Tree Line_III_Seg2 | 114 |
| Tree Line_III_Seg2 | 116 |
| Tree Line_III_Seg2 | 117 |
| Tree Line_III_Seg2 | 135 |
| Tree Line_III_Seg2 | 136 |
| Tree Line_III_Seg2 | 140 |
| Tree Line_III_Seg2 | 146 |
| Tree Line_III_Seg2 | 146 |
| Tree Line_III_Seg2 | 147 |
| Tree Line_III_Seg2 | 147 |
| Tree Line_III_Seg2 | 149 |
| Tree Line_III_Seg2 | 158 |
| Tree Line_III_Seg2 | 171 |
| Tree Line_III_Seg2 | 176 |
| Tree Line_III_Seg2 | 196 |
| Tree Line_III_Seg2 | 218 |
| Tree Line_III_Seg2 | 220 |
| Tree Line_III_Seg2 | 220 |
| Tree Line_III_Seg2 | 224 |
| Tree Line_III_Seg2 | 230 |
| Tree Line_III_Seg2 | 238 |
| Tree Line_III_Seg2 | 249 |
| Tree Line_III_Seg2 | 266 |
| Tree Line_III_Seg2 | 270 |
| Tree Line_III_Seg2 | 281 |
| Tree Line_III_Seg2 | 296 |
| Tree Line_III_Seg2 | 330 |
| Tree Line_III_Seg2 | 366 |
| Tree Line_III_Seg2 | 371 |
| Tree Line_III_Seg2 | 469 |
| Tree Line_III_Seg2 | 1848 |

Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
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Tree Line_III_Seg2
Line_II_Seg2

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Tree Line_III_Seg2
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Tree Line_III_Seg2
Tree Line_III_Seg2
Line_III Seg 2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
Tree Line_III_Seg2
25.935, 13.501, 5.25 73.814, 16.901, 9.75 25.935, 13.501, 6.75 25.935, 13.501, 8.25 25.935, 13.501, 12.75 28.927, 13.713, 9.75 28.927, 13.713, 11.25
16.957, 12.863, 8.25
22.942, 13.288, 5.25
73.814, 16.901, 11.25
25.935, 13.501, 9.75
22.942, 13.288, 6.75
76.807, 17.113, 9.75
82.792, 17.538, 11.25
19.95, 13.076, 6.75
79.799, 17.326, 11.25
22.942, 13.288, 8.25
13.965, 12.651, 12.75
22.942, 13.288, 9.75
25.935, 13.501, 11.25
19.95, 13.076, 8.25
76.807, 17.113, 14.25
22.942, 13.288, 11.25
73.814, 16.901, 12.75
16.957, 12.863, 14.25
19.95, 13.076, 9.75
22.942, 13.288, 12.75
16.957, 12.863, 9.75
19.95, 13.076, 11.25
79.799, 17.326, 12.75
82.792, 17.538, 12.75
76.807, 17.113, 11.25
16.957, 12.863, 11.25
19.95, 13.076, 12.75
16.957, 12.863, 12.75
76.807, 17.113, 12.75
79.799, 17.326, 14.25

## Luminous Intensity (Cd) At Vertical Planes

Maximum Allowable Value calculated from CIE 150:2017 (varies by Projected Area sq.m. and Distance Factor)
For E3-Medium District Brightness, Projected Area and Distance Factors:
(0.002, 0.86) $(0.01,1.9)(0.03,3.8)(0.13,7.5)(0.5,15)$

Projected Area (sq.m) = Approx. projected emitting area of luminaire in direction of observer
Distance ( m ) = Distance from luminaire to observer
Max Cd Allowed = Projected Area Factor * Distance
Calculations Tested (9):

| Calculation Label | Test <br> Results |
| :--- | :--- |
| House Row 1_Cd_Seg1 | PASS |
| House Row 2_Cd_Seg1 | PASS |
| House Row 3_Cd_Seg1 | PASS |
| House Row 4_Cd_Seg1 | PASS |
| Tree Line_Cd_Seg1 | FAIL |
| Tree Line_Cd_Seg2 | FAIL |
| House Row 5_Cd_Seg1 | FAIL |
| House Row 5_Cd_Seg2 | FAIL |
| House Row 5_Cd_Seg3 | FAIL |

Failed Meter Locations (825 total, first 100 shown):

| Offending <br> Lum. No. | Label | Cd | Meter Coords |
| :---: | :---: | :---: | :---: |
| 1 | B 1 NST 1300w 5k | 78564 | 22.388, 124.138, 1.5 |
| 1 | B 1 NST 1300w 5k | 86553 | 25.388, 124.085, 1.5 |
| 1 | B 1 NST 1300w 5k | 28394 | 13.39, 124.3, 2.5 |
| 1 | B 1 NST 1300w 5k | 30405 | 16.389, 124.246, 2.5 |
| 1 | B 1 NST 1300w 5k | 45409 | 19.389, 124.192, 2.5 |
| 1 | B 1 NST 1300w 5k | 81981 | 22.388, 124.138, 2.5 |
| 1 | B 1 NST 1300w 5k | 88161 | 25.388, 124.085, 2.5 |
| 1 | B 1 NST 1300w 5k | 94333 | 28.387, 124.031, 2.5 |
| 1 | B 1 NST 1300w 5k | 98052 | 31.387, 123.977, 2.5 |
| 1 | B 1 NST 1300w 5k | 28376 | 13.39, 124.3, 3.5 |
| 1 | B 1 NST 1300w 5k | 31582 | 16.389, 124.246, 3.5 |
| 1 | B 1 NST 1300w 5k | 60152 | 19.389, 124.192, 3.5 |
| 1 | B 1 NST 1300w 5k | 83539 | 22.388, 124.138, 3.5 |
| 1 | B 1 NST 1300w 5k | 89980 | 25.388, 124.085, 3.5 |
| 1 | B 1 NST 1300w 5k | 95817 | 28.387, 124.031, 3.5 |
| 1 | B 1 NST 1300w 5k | 95990 | 31.387, 123.977, 3.5 |
| 1 | B 1 NST 1300w 5k | 90003 | 34.386, 123.923, 3.5 |
| 1 | B 1 NST 1300w 5k | 28182 | 13.39, 124.3, 4.5 |
| 1 | B 1 NST 1300w 5k | 33316 | 16.389, 124.246, 4.5 |
| 1 | B 1 NST 1300w 5k | 73539 | 19.389, 124.192, 4.5 |
| 1 | B 1 NST 1300w 5k | 84834 | 22.388, 124.138, 4.5 |
| 1 | B 1 NST 1300w 5k | 92004 | 25.388, 124.085, 4.5 |
| 1 | B 1 NST 1300w 5k | 95394 | 28.387, 124.031, 4.5 |
| 1 | B 1 NST 1300w 5k | 90813 | 31.387, 123.977, 4.5 |
| 1 | B 1 NST 1300w 5k | 27663 | 13.39, 124.3, 5.5 |
| 1 | B 1 NST 1300w 5k | 35283 | 16.389, 124.246, 5.5 |
| 1 | B 1 NST 1300w 5k | 79261 | 19.389, 124.192, 5.5 |
| 1 | B 1 NST 1300w 5k | 86801 | 22.388, 124.138, 5.5 |
| 1 | B 1 NST 1300w 5k | 93246 | 25.388, 124.085, 5.5 |
| 1 | B 1 NST 1300w 5k | 91494 | 28.387, 124.031, 5.5 |
| 1 | B 1 NST 1300w 5k | 27215 | 13.39, 124.3, 6.5 |
| 1 | B 1 NST 1300w 5k | 45036 | 16.389, 124.246, 6.5 |
| 1 | B 1 NST 1300w 5k | 80850 | 19.389, 124.192, 6.5 |
| 1 | B 1 NST 1300w 5k | 88725 | 22.388, 124.138, 6.5 |

# Kingfisher Lighting 

B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k B 1 NST 1300w 5k C 1 WST 1300w 5 k C 1 WST 1300w 5 k C 1 WST 1300w 5k C 1 WST 1300w 5k C 1 WST 1300w 5 k C 1 WST 1300w 5k

91286
22413 27508 66960 82427 89217 84175 12143 22479
29322
74481
84032
84229
11637
31783
75707
82651
11024
47036
76351
10182
64218
70278
19642
22047
22057
22336
21343
22220
20688
22025
20328
21614
20560
20919
18814
19889
18835
18596
18771
12883
17427
18489
12523
17398
17915
12053
35065
18650
16697
11467
14399
10711
10076
13156
13181
11230
11227
11101
10846
25.388, 124.085, 6.5 10.39, 124.354, 7.5 13.39, 124.3, 7.5 16.389, 124.246, 7.5 19.389, 124.192, 7.5 22.388, 124.138, 7.5 25.388, 124.085, 7.5 7.391, 124.408, 8.5 10.39, 124.354, 8.5 13.39, 124.3, 8.5 16.389, 124.246, 8.5 19.389, 124.192, 8.5 22.388, 124.138, 8.5 7.391, 124.408, 9.5 13.39, 124.3, 9.5 16.389, 124.246, 9.5 19.389, 124.192, 9.5 7.391, 124.408, 10.5 13.39, 124.3, 10.5 16.389, 124.246, 10.5 7.391, 124.408, 11.5 13.39, 124.3, 11.5 16.389, 124.246, 11.5 10.39, 124.354, 13.5 5.938, 110.195, 1.5 5.921, 113.195, 1.5 5.903, 116.195, 1.5 5.921, 113.195, 2.5 5.903, 116.195, 2.5 5.921, 113.195, 3.5 5.903, 116.195, 3.5 5.921, 113.195, 4.5 5.903, 116.195, 4.5 5.921, 113.195, 5.5 5.903, 116.195, 5.5 5.886, 119.195, 5.5 5.903, 116.195, 6.5 $5.886,119.195,6.5$ 5.903, 116.195, 7.5 5.886, 119.195, 7.5 5.869, 122.195, 7.5 5.903, 116.195, 8.5 $5.886,119.195,8.5$ $5.869,122.195,8.5$ 5.903, 116.195, 9.5 5.886, 119.195, 9.5 $5.869,122.195,9.5$ 5.921, 113.195, 10.5 $5.903,116.195,10.5$ $5.886,119.195,10.5$ $5.869,122.195,10.5$ 5.886, 119.195, 11.5 $5.869,122.195,11.5$ 5.886, 119.195, 13.5 13.965, 12.651, 6.75 10.972, 12.438, 6.75 13.965, 12.651, 8.25 10.972, 12.438, 8.25
7.98, 12.226, 8.25 4.987, 12.013, 8.25

## Kingfisher Lighting

C 1 WST 1300w 5k
C 1 WST 1300w 5k
C 1 WST 1300w 5 k
85695
5695
90529
1.995, 11.801, 8.25

C 1 WST 1300w 5 k
91821
C 1 WST 1300w 5k
92222
93753 80.882, 120.878, 0.5 80.838, 117.879, 0.5
80.794, 114.879, 0.5
80.751, 111.879, 0.5
80.707, 108.88, 0.5

Floodlight used

## Kingfisher SPORT

Datasheet

## Amnis Flood

## Specification Text

The luminaire shall be manufactured from high pressure die-cast aluminium. It shall have an LED efficacy of up to 139 luminaire $1 \mathrm{~m} / \mathrm{W}$ and will be capable of producing up to 175,000 luminaire lumens at 4000 K with a CRI $>70$. It shall have an asymmetric forward throw optic and is rated at IP66 and IK08.

| Specification |  |
| :--- | :--- |
| Weight: |  |
| Fitting: <br> Driven | 27.5 kg |
|  | 13.0 kg |
|  | Fitting with integral diver: |
|  | 32.5 kg |


| Windage: | $0.19 \mathrm{~m}^{2}$ |
| :--- | :--- |
| Material: | Dle-cast Aluminium |
| Paint Finish: | Marine Grade <br> Powder Coated <br> Anthracite Grey |

## Optics

NST


## Key Features

- 900w - 1350 W
- 118,000-175,000 Luminaire Lumens
- Efficacy up to $1391 \mathrm{~m} / \mathrm{W}$
- 2700K, 4000K
- CRI $>70, \mathrm{CRI}>80, \mathrm{CRI}>90$
- Lifetime $>100,000 \mathrm{hr}$
- Asymmetrical
- Driver options
- Marine grade paint



A survey to ascertain the current impact of flood lighting to Welling united football club was carried out on Thursday $28^{\text {th }}$ September 2023 at 8.30pm. During the survey vertical levels were taken along the top (Park view road), Bottom (tree line) and several locations to the West (Roseacre Road side). These levels were take at 1 m and 2 m above floor level every 3 m to investigate levels achieved by the current 2 kw flood lighting on site.


During the survey the weather was clear and dry. A Extech Easy view 33 lux meter was used to conduct the survey. A current calibration certificate can be found at the end of the report.

The below is a report showing the levels taken along with photographs taken during the survey. It was not possible to gain access to the properties on Roseacre road and so levels were taken on the site perimeter to look at the vertical impact.

Bottom tree line edge


Tree line

| Tree line |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 m | 84 | 100 | 140 | 193 | 191 | 188 | 180 | 181 | 127 | 96 | 100 | 80 | 72 | 70 | 50 | 50 | 52 | 59 | 48 | 50 | 45 | 73 | 83 | 83 | 108 | 118 | 109 | 155 | 178 | 205 | 172 | 160 | 133 | 85 | 84 |
| 2 m | 91 | 121 | 142 | 204 | 230 | 243 | 203 | 170 | 190 | 150 | 98 | 95 | 86 | 65 | 62 | 48 | 50 | 48 | 43 | 49 | 41 | 37 | 62 | 51 | 92 | 91 | 103 | 115 | 136 | 170 | 123 | 120 | 128 | 81 | 71 |

Highest level recorded at 2m 243 lux


N/B - There was some over hanging tree line during the survey which may have caused lover levels at height taken

## Kingfisher Lighting

Park view road edge


Park view road taken 2.5 m from pitch fence


Highest level recorded at 1m 183 lux


N/B - At the time of the survey it was reported that two flood lights on the North west corner mast were un operational due to lamp failure. This will have resulted in lower vertical levels on this side. In particular on the side of the mast in question


| Roseacre Road South side of the stand |  |  |  |  |  |  |  |  | Area behind stand |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 m | 150 | 200 | 247 | 263 | 283 | 301 | 298 | 245 | 169 |  |  | 37 | 86 | 68 | 59 | 57 | 55 |  |
| 2 m | 115 | 186 | 180 | 208 | 308 | 316 | 265 | 237 | 187 |  |  | 83 | 76 | 74 | 66 | 48 | 43 |  |

Highest level recorded at $2 m 308$ lux

Roseacre Road side. North side of stand


Roseacre Road North side of the stand

| 1 m | 22 | 27 | 27 | 30 | 28 |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 2 m | 21 | 24 | 23 | 24 | 24 |  |  |

Highest level recorded at 1 m 30 lux

# Kingfisher Lighting 

## Appendix

## Standards and Guidance

The following guidance notes and documentation have been used for reference;

- ILP ‘Guidance notes for the Reduction of Obtrusive Light’ 2021
- The Society of Light and Lighting (CIBSE), Lighting Guide 4 'Sports Lighting' 2006
- BS EN 12193 'Sports Lighting'
- FA Lighting Guidance (Football).


## Glossary

Lux
The standard unit of light (luminous flux) used in describing light emitted by a source or received by a surface.

Illuminance and Maintained Illuminance (lumens/m2 or lux)
Illuminance is the term used to describe the level of light on a surface in lumens/square metre or lux.

## Maintained

Maintained illuminance is the term used to describe the average light level on a reference surface

## Horizontal Illuminance

The level of light falling on to a horizontal plane (i.e. the ground).
Vertical Illuminance
The level of light falling on to a vertical plane (i.e. the walls of a house).

## Light Output Ratio (LOR)

This is the ratio of the total light output of a luminaire, relative to the total light output of the lamp/s under reference conditions. Total LOR can be divided into downward (DLOR) and upward (ULOR) light output ratios if appropriate.

## Light Intrusion (Light trespass, Overspill, Light into windows)

The flow of light spilling outside the location boundary. With inadequate control Intrusive light may be sufficiently great as to provide a serious nuisance and disturbance to adjacent areas.

## Glare

Glare may be divided into two types known as 'disability' and 'discomfort' glare. In a Sports Lighting context, it relates primarily to direct viewing of the flood lights. Only in severe situations would 'disability glare' be experienced. In most instances it is 'discomfort glare' that may be a result, causing annoyance to the users of the site, in the case that adequate screening of flood lights is not provided.

## Threshold Increment

Threshold Increment (TI) is a measure of the loss of visibility caused by the 'disability glare' from a proposed lighting installation.

## Sky Glow

The general term for the Halo-effect caused by upwardly directed light, forming a glow in the night sky. It can cause diminished contrast of stars against their dark background making astronomical observations difficult or even impossible. The upwardly directed light can be caused by direct waste light from flood lights or redirected light from the sports surface.

## ILP

The Institution of Lighting Professionals.

## ILP 'Guidance notes for the reduction of light pollution'

A booklet produced by the ILP providing advice on reducing the impact of exterior lighting installations on the environment. This documentation goes into detail about overspill and ULOR, which both vary depending on the environmental zone as categorized in the guidance notes. Full documents can be supplied at a request.

