# **Newbold Farm, Duntisbourne Abbots**

## **Mr and Mrs Scudamore**

Technical Note – Drainage Strategy

231064-KTN-RP-01-A 26<sup>th</sup> November 2023



The Site
24 Chosen View Road
Cheltenham
GL51 9LT



## **DOCUMENT CONTROL**

## **Document Status**

Revision	Date	Document Author	Status
Α	27.11.23	Kris Tovey	Final

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National Standards, regulations and Council policy do change which could affect the validity of this Report. The methodologies adopted and the sources of information used by K-Ten Consulting Ltd in providing its services are outlined within the report. Any information provided by third parties and referred to within the report and appendices has not been checked or verified by K-Ten Consulting Ltd, unless otherwise expressly stated within this Report.



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## 1.0 INTRODUCTION

- 1.1 K-Ten Consulting Ltd (K-Ten) provide professional Flood Risk, Infrastructure and Drainage services throughout the UK.
- 1.2 K-Ten have been commissioned by Mr and Mrs Scudamore (applicant) to prepare technical surface and foul drainage design information to support a planning application at Newbold Farm, Duntisbourne Abbots.
- 1.3 The project consists of the conversion and extension of an existing barn to provide a residential dwelling with associated external works. Refer to **Appendix A** for proposed site layout.
- 1.4 This technical note will summarise the below ground drainage requirements on site in accordance with Council water management guidelines and national standards.



## 2.0 EXISTING SITE DETAILS

### Site Location

- 2.1 The site is located in the north of Duntisbourne Abbots, Cirencester. The approximate site coordinates are E 396980, N 208050 and National Grid SO969080, with the nearest post code GL7 7JN.
- 2.2 Refer to **Appendix B** for site location plan.
- 2.3 The current site comprises an existing residential building, associated out buildings and surrounding soft landscaping.

## **Existing Drainage**

- 2.4 Thames Water asset records show no existing public drainage assets within close proximity to the site.
- 2.5 Refer to **Appendix C** for Thames Water Asset Records.
- 2.6 The current site buildings discharge foul waste to an existing septic tank.
- 2.7 Surface Water from the current impermeable areas of hardstanding and roof area discharges naturally to ground and existing soakaways on site.

## **Existing Hydrology**

- 2.8 The closest watercourse is a spring fed stream running through Duntisbourne Abbots south towards Cirencester.
- 2.9 Online soil maps indicate the site to be underlain by freely draining shallow lime rich strata over chalk or limestone, which would suggest good natural drainage conditions.

## Topography

- 2.10 A detailed topographical survey was completed in October 2021, a copy of which is included in **Appendix D**.
- 2.11 Ground levels within the area of proposed development are relatively flat with levels in the region of 195.40m AOD.
- 2.12 The site rises steeply to the north west via an earth bank and a raised soft landscaped area which continues to rise to the northern boundary.

### **Site Testing**

2.13 Infiltration Testing was completed on 14<sup>th</sup> November 2023 under the supervision of K-Ten Consulting Ltd and in accordance with BRE365. Refer to **Appendix E** for site records and test calculations.



## 3.0 PROPOSED SURFACE WATER DRAINAGE STRATEGY

- 3.1 The existing barn roof drainage discharges uncontrolled directly to ground.
- 3.2 The existing and new roof areas within the proposed development will introduce impermeable areas totalling 440m<sup>2</sup>.
- 3.3 Refer to **Appendix A** for proposed site layout.
- 3.4 A surface water strategy is proposed to manage and reduce the flood risk and surface water run-off from the development, with consideration to SuDS.
- 3.5 The SuDS hierarchy dictates that surface water run off should be managed as high up the following list as practically possible:
  - a) into the ground (via infiltration) and re-use, or then;
  - b) to a surface water body, or then;
  - c) to a surface water sewer, highway drain or another drainage system, or then;
  - d) to a combined sewer.
- 3.6 Infiltration testing was undertaken on site and concluded infiltration is a viable method of discharge with a design rate of **0.098 m/sec** recorded. Refer to **Appendix E** for infiltration rates.
- 3.7 All roof run off will be captured within a positive gravity drainage system and discharged to a below ground cellular soakaway offering 95% void ratio. The soakaway will be designed to cater for the 1 in 100 year rainfall event with a 40% allowance for climate change and design factor of safety of 2.0.
- 3.8 The soakaway will be 3.5 m x 7.0 m x 1.0 m deep with a maximum water level of 987 mm and maximum volume of  $23.55 \text{m}^3$ .
- 3.9 Refer to **Appendix F** for Drainage Calculations
- 3.10 Half drain time is less than 24 hours.
- 3.11 The soakaway will be located a minimum of 5m from any structure with suitable cover for the anticipated loading classification it will receive.
- 3.12 Inspection chambers will be fitted with silt traps upstream of the soakaway.
- 3.13 All other development areas will be constructed with permeable surfacing.
- 3.14 Refer to **Appendix G** for surface water drainage strategy.
- 3.15 Any exceedance flows above the 100 year event plus climate change will be directed towards the site access and follow natural topography to the south.
- 3.16 All proposed development run off for the 100 year event plus and allowance for climate change will be contained within the site.



## 4.0 WATER QUALITY AND POLLUTION

- 4.1 Water quality has been assessed in accordance with The SuDS Manual (CIRIA C753) which states the design of surface water should consider minimising contaminants within surface water runoff discharged from the site.
- 4.2 The level of treatment required is dependent on the proposed land use according to the pollution hazard indices (refer to SuDS Manual table 26.2). For this development the contaminant risks come from the *Residential Roofs*, which is classified as <u>very low pollution hazard level</u>.
- 4.3 As the discharge is directly to ground the mitigation indices against Pollution Hazard indices is not required.
- 4.4 It is good practice that gullies and chambers have suitable silt traps/catchpits to reduce sediments within the drainage system.



## 5.0 PROPOSED FOUL DRAINAGE STRATEGY

- 5.1 Development wastewater will connect to an on site primary and secondary treatment plant with clean water discharge to an effluent field in accordance with Building Regulations H and British Standards BS 6297:2007.
- 5.2 The anticipated development waste loads have been calculated in accordance with British Loading and Flows Tables 4 for a 4 Bed dwelling = 6P.
- 5.3 The wastewater treatment plant will include a visual and audible high level alarm.
- 5.4 In accordance with Building Regulations H a  $V_p$  of 12 sec/mm has been interpolated from the BRE365 site infiltration rates. This rate sites within the 12-100 sec/mm allowable range for effluent field design.
- 5.5 An effluent field plan area of 6P x Vp12 x 0.2 = 15m<sup>2</sup> will be required.
- 5.6 The drainage field will be constructed 600mm below ground level and in accordance with Diagram 1 Building Regulations H.
- 5.7 Refer to **Appendix G** for surface water drainage strategy.



## 6.0 MAINTENANCE AND MANAGEMENT

- 6.1 Maintenance of SuDS features is required in order to ensure that the surface water drainage system operates effectively, and the risk of flooding of the site and surrounding areas is reduced.
- 6.2 A maintenance schedule should be undertaken to ensure that the drainage system remains fully operational for the design lifetime. The below table summarises a maintenance plan for the drainage systems and components within the development.
- 6.3 The SuDS Manual (CIRIA C753) and specific product suppliers guidelines should also be referred to for further information on maintenance and frequency.
- 6.4 All on site drainage will be maintained and managed through a private management company.

Drainage Component	Required Action	Typical Frequency	
	Stabilise adjacent areas	As required	
	Remove weeds and vegetation	As required	
General pipework,	Clear/Jet any poor performing structures	As required	
manholes,	Inspect all drainage features for poor	3 monthly, 48 hours	
chambers, silt	operation	after large storms in	
traps and	operation	first six months	
headwalls	Monitor inspection chambers and silt traps.		
	Inspect silt accumulation and determine silt	Annually	
	clearance frequencies		
Cellular Soakaways	Inspection of inlets, oulets and silt traps	As required	
Cellulai Soakaways	Silt removal	Annually	
	Surface visual inspection for ponding,	Annually or after major	
	damaged blocks and build up of silt/detritus	storm events	
	Stabilise and mow contributing and adjacent areas	As required	
	Removal of weeds or management using	As required – once per	
Permeable Paving,	glyphospate applied directly into the weeds by	year on less frequently	
if used.	an applicator rather than spraying	used pavements	
	Remove litter, weeds and debris	Monthly	
	Vacuum sweeping and brush replacement of approved jointing material	Annually	
	Replace geotextile and bedding layer	Every 30 year	

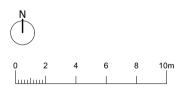


## **APPENDIX A**

PROPOSED SITE LAYOUT



Site Plan - Roof Level



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   Any discrepancies between site and drawings to be reported to the architect immediately.
   Read in conjunction with all relevant structural and mechanical & electrical engineers drawings.
   Survey undertaken by:

REVISIONS PROJECT 21.18 Newbold Farm Barn



Site Plan - Ground Level

Blake Architects Limited

1 Coves Barn, Winstone Gloucestershire. GL7 7JZ

[t] 01285 841407 [e] mail@blakearchitects.co.uk

www.blakearchitects.co.uk

Proposed Site Plan

21.18.03.11

PLANNING STATUS CHECKED SCALE 14.11.23 1:250 @ A1

REVISION

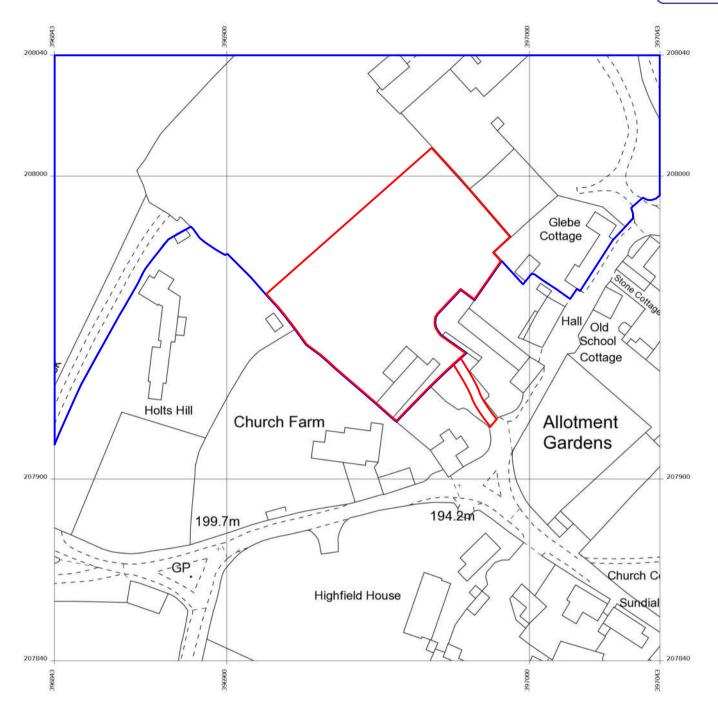


## **APPENDIX B**

SITE LOCATION PLAN

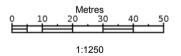




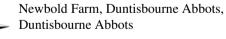


Produced 24 Jun 2022 from the Ordnance Survey MasterMap (Topography) Database and incorporating surveyed revision available at this date.

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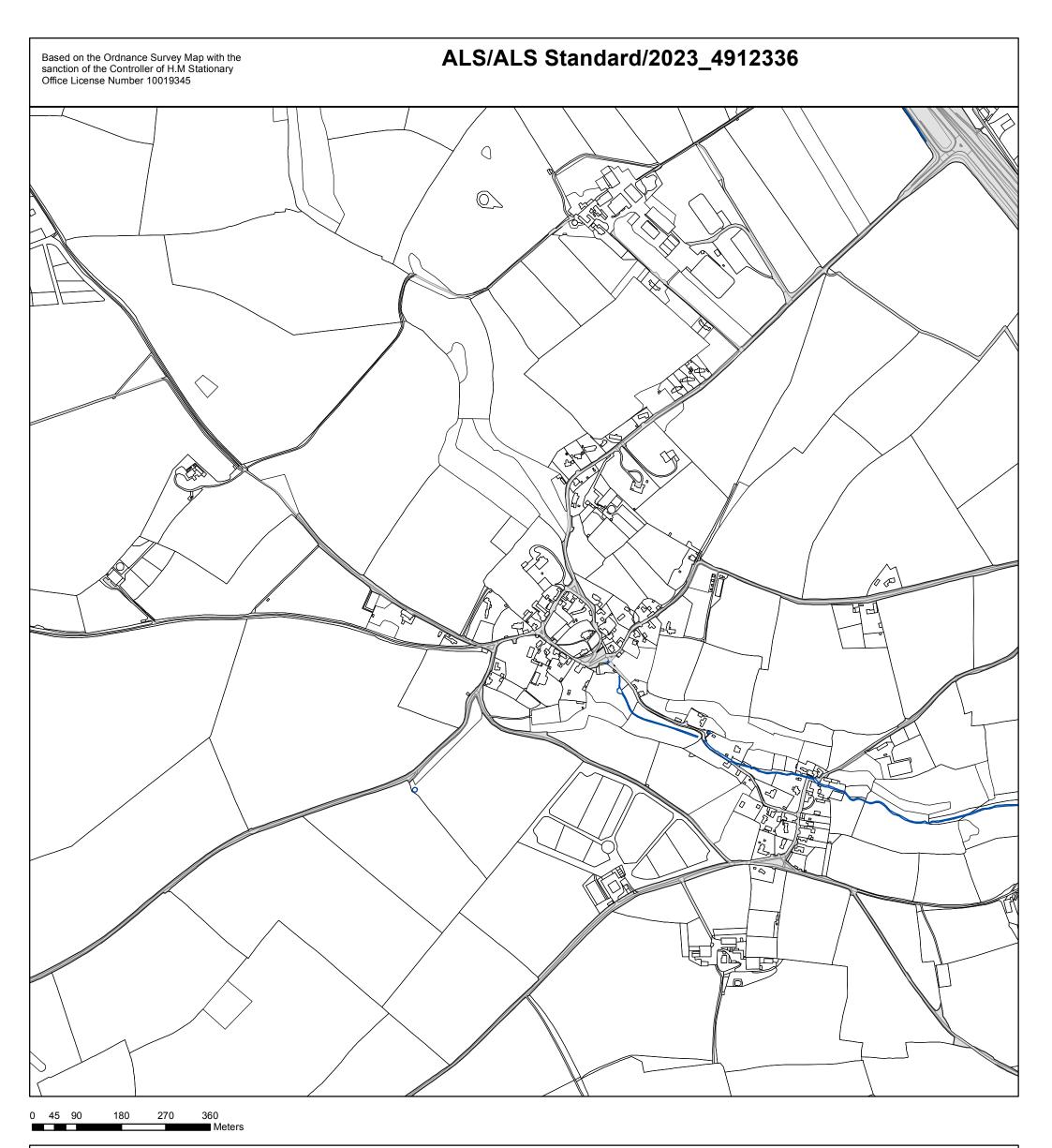
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   Read in conjunction with all relevant structural and mechanical & electrical engineers drawings.
   Survey undertaken by:

REVISIONS						
PROJECT	21.18 Ne	wbold Farn	n Barn			
ADDRESS	Duntisbourne A	Abbots,Glouceste	rshire, GL7 7JN			
BLAKE ARCHI TECTS	Blake Architects Limited  1 Coves Barn, Winstone Gloucestershire. GL7 7JZ  [1] 01285 841407 [e] mail@blakearchitects.co.uk  www.blakearchitects.co.uk					
TITLE	Location Plan					
DRAWING NUMBER	21.18.03.01					
STATUS	PLANNING					
DRAWN	CHECKED	DATE	SCALE	REVISION		
HG	JN	24.06.22	1:1250 @ A3	-		



## **APPENDIX C**

THAMES WATER SEWER RECORDS



The position of the apparatus shown on this plan is given without obligation and warranty, and the accuracy cannot be guaranteed. Service pipes are not shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified before any works are undertaken. Crown copyright Reserved

Scale:	1:7161
Width:	2000m
Printed By:	ASuji
Print Date:	16/11/2023
Map Centre:	396953,207960
Grid Reference:	SO9607NE

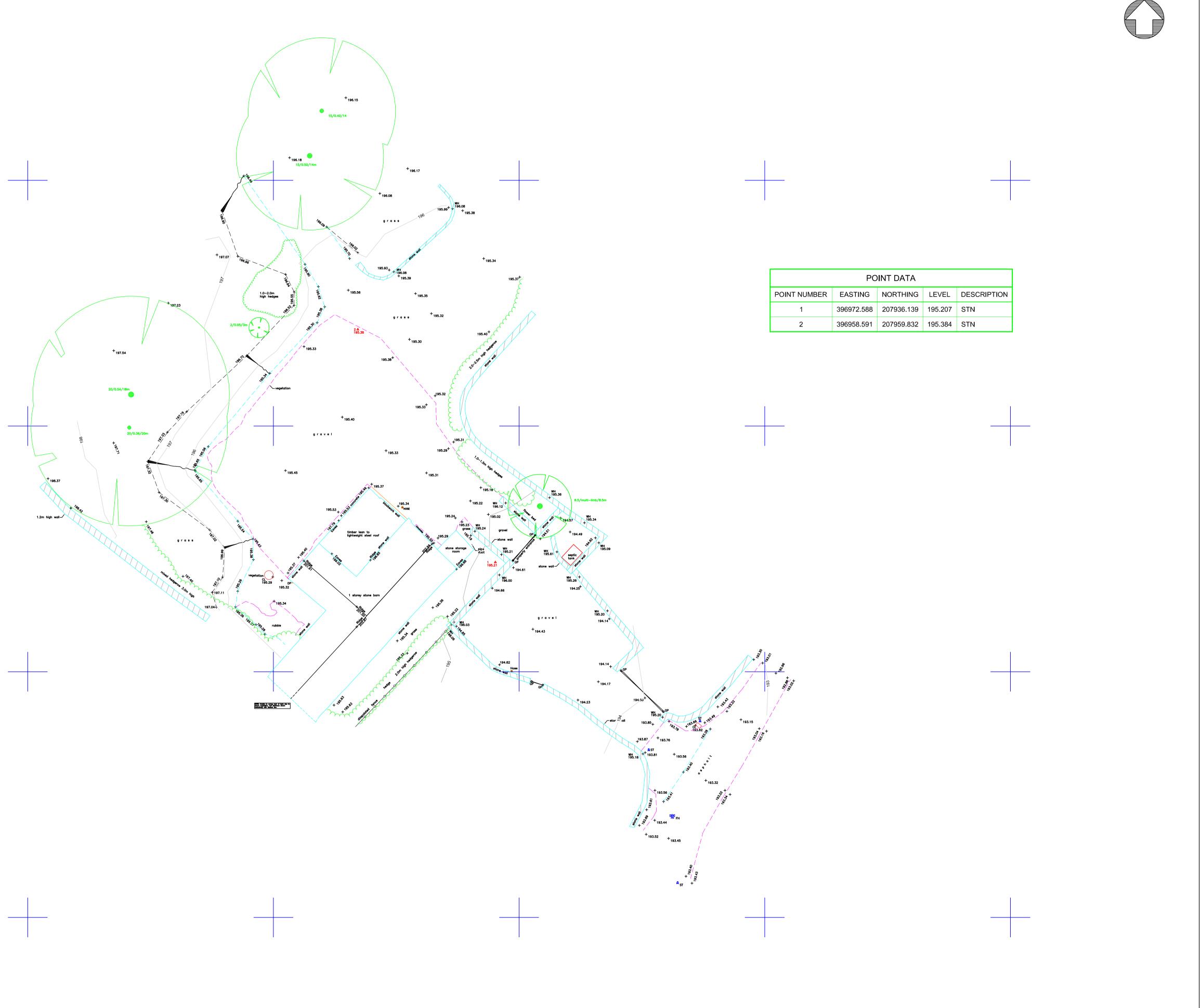
Comr	nent	s.	



## **APPENDIX D**

**TOPOGRAPHICAL SURVEY** 







DO NOT SCALE

1. Levels are related to Ordnance Datum Newlyn 2. Grid is related to Ordnance Datum North 3. Drainage pipe sizes are estimated from the surface 4. Tree sizes are measured 1m from the ground

AV AIR VALVE BB BELISHA BEACON BH BOREHOLE OL OUTSIDE LIGHT LV LOW VOLTAGE BH BOREHOLE MH MANHOLE COVER
BOL BOLLLARD MK MARKER
BM BENCH MARK MKE MARKER ELECTRIC
BS BUS STOP MKFH MARKER FIRE HYDRANT
BT BRITISH TELECOM COVER MKSV MARKER SLUICE VALVE B-W BARBED WIRE MKT MARKER TELEPHONE

B-W BARBED WIRE

CB CONTROL BOX

C-B CLOSE BOARDED

CL COVER LEVEL

CP CATCH PIT

CPS CONCRETE PAVING SLABS

DP DISTRIBUTION POST

EOT END OF TRACE

EP ELECTRIC POLE

ER EARTH ROD

ER EARTH ROD

FH FIRE HYDRANT

STP

STAND PIPE

STAND PIPE

STAND

HY HIGH VOLTAGE
IC INSPECTION COVER
I—R IRON RAILING
KO KERB OUTLET
LP LAMP POST

TIL TRAFFIC LIGHT

TM TICKET MACHINE

TP TELEPHONE POLE

UTT UNABLE TO TRACE

UTL UNABLE TO LIFT

WH WALL HEIGHT

WM WATER METER WO WASH OUT
VT VENT

## LINETYPE MENU

---- Telephone Bottom Bank ------ Low Voltage —ε—ε— Water line ——ww——ww—— Gas line Ducting Hedge -0-0-0-0-0-0-0-0-Tree Spread/Dia/Height Manhole/ \_\_\_\_\_Inspection Unknown Overhead Cable \_\_\_\_\_ \_\_\_\_\_ General Coms \_\_6c\_\_6c\_\_6c\_\_6c + 0.56m Foul Water —FWS—FWS— ——нv——нv—— Surface Water ——sws——sws— Cable TV \_\_\_\_\_\_\_cv\_\_\_cv\_\_\_cv\_\_\_

# Topo & Building Survey



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**Blake Architects** 

<sup>ct</sup> Duntinsbourne Abbots, The Old Rectory Newbold Farm, Survey Drawings

Topographic Survey

Scale (at A1) 01/11/21 1:200 DBA-GEO-XX-GF-DR-C-0001



## **APPENDIX E**

SITE INFILTRATION RECORDS AND CALCULATIONS



Soakaway Test Record			
Location Newbold	Grange	Test Pit Number	
Duntisbo	U A .	Test Number	1 of 3
GL7 7.7		Date	14/11/23
	20		-1-1
Nex	Depth versus tir	ne measurements	
Depth below datum (mm)	Time (minutes)	Depth below datum (mm)	Time (minutes)
START HERE \$		CONTINUE HERE ❖	
43	5	687	90
86	10	7-23	95
127 127	15	759	100
167	10	793	105
205	25	828	110
243	30	862	us
243 280	35	897	120
319	40	932	125
359	45	967	130
396	50	1000	135
431	50 55		
467	60		
503	65		
540	70		
5 <del>1</del> 6	75		
613	80		
650	85		



Soakaway/Test/Record	•		
	D CARANCE	Test Pit Number	
	BOURNE A		2 of 3
GL7	ATH	Date	14/11/23
	15.4		-1111
,	Ogaliwarupili	emenence de la contraction de	
Depth below datum (mm)	Time (minutes)	Depth below datum (mm)	Time (minutes)
START HERE ₽		CONTINUE HERE ₽	
35	5	629	90
69	O	663	95
107	15	695	100
142	१०	731	105
176	25	766	110
211	30	801	115
246	35	833	120
282	40	869	125
314	45	904	130
351	50	939	135
384	55	974	140
419	60	1000	142
455	65		
487	70		
. 523	75		
558	80		
594	85		



Soakaway Test Record					
Location NEWRO	40 CAA	Test Pit Number			
	BOURNE		3 of 3		
GL7	NZF	Date	14/11/23		
	•				
9	Depth versus tin	ne measurements			
Depth below datum (mm)	Time (minutes)	Depth below datum (mm)	Time (minutes)		
START HERE ₺		CONTINUE HERE ₽			
34	5	586	90		
69	10	619	95		
(७३	15	651	100		
137	20	684	105		
	25	716	110		
193	30	747	115		
226	35	778	120		
260	40	820	125		
294	45	850	130		
327	50	882	135		
360	55	912	140		
392	60	941	145		
425	65	970	150		
457	700	1000	155		
488	75				
521	80				
554	85				

## **Infiltration Test Results**

in accordance with BRE Digest 365

Project Name	Newbold Fa	Newbold Farm		
Project Number	23-1064			
Test Date	14.11.23			
Test Pit	01-Jan-00			



Pit Dimensions:			Length = 1.000 m
			Width = 0.450 m
			Depth = 1.500 m
Test Number: 01			
Distance from ground to top of water = Total drop below water level at end of test =			0.500 m 1.000 m
rotal drop below water level at end or test			1.000
75% of effective depth below datum = 25% of effective depth below datum =	0.250 0.750	m m	Time, $t_{75} = 31$ mins Time, $t_{25} = 100$ mins
$V_{p75-25} = 0.225$ m3 $A_{p50} = 1.900$ m2			t <sub>p75-25</sub> = 69 mins
			Soil infiltration rate, f = <b>2.9E-05</b> m/sec Soil infiltration rate, f = <b>0.103</b> m/hr
Test Number: 02			
Distance from ground to top of water =			0.500 m
Total drop below water level at end of test =			1.000 m
75% of effective depth below datum =	0.250	m	Time, $t_{75} = 35$ mins
25% of effective depth below datum =	0.750	m	Time, $t_{25} = 107$ mins
$V_{p75-25} = 0.225$ m3 $A_{p50} = 1.900$ m2			t <sub>p75-25</sub> = 72 mins
			Soil infiltration rate, f = <b>2.7E-05</b> m/sec Soil infiltration rate, f = <b>0.099</b> m/hr
Test Number: 03			
Distance from ground to top of water = Total drop below water level at end of test =			0.500 m 1.000 m
75% of effective depth below datum =	0.250	m	Time, t <sub>75</sub> = 38 mins
25% of effective depth below datum =	0.750	m	Time, $t_{25} = 115$ mins
$V_{p75-25} = 0.225$ m3 $A_{p50} = 1.900$ m2			t <sub>p75-25</sub> = 77 mins
			Soil infiltration rate, f = <b>2.6E-05</b> m/sec Soil infiltration rate, f = <b>0.092</b> m/hr



## **APPENDIX F**

**DRAINAGE CALCULATIONS** 



File: soakaway.pfd Network: Storm Network Kris Tovey 18.11.23 Page 1 Newbold Farm Duntisbourne Abbots Soakaway Calc

## **Design Settings**

Rainfall Methodology FEH-22 Minimum Velocity (m/s) 1.00 Return Period (years) 2 Connection Type Level Soffits Additional Flow (%) Minimum Backdrop Height (m) 0.200 0 CV 0.750 Preferred Cover Depth (m) 1.200 Time of Entry (mins) 4.00 Include Intermediate Ground Maximum Time of Concentration (mins) 30.00 Enforce best practice design rules ✓ Maximum Rainfall (mm/hr) 50.0

### **Nodes**

Name		T of E (mins)		Easting (m)	Northing (m)	Depth (m)
			(m)			
Soakaway 01	0.044	4.00	195.300	0.000	0.000	1.500

## **Simulation Settings**

Rainfall Methodology   F		FEH-22	Analysis Speed		Normal	Additional Storage (m³/ha)			20.0		
Summer CV		0.750	Skip Steady State		Χ	Check Discharge Rate(s)			X		
Winter CV		0.840	Drain Down Time (mins)			240	Check Discharge Volume			х	
Storm Durations											
15	60	180	360	600	960	2160	4320	7200	10080		
30	120	240	480	720	1///0	2880	5760	8640			

<b>Return Period</b>	Climate Change	<b>Additional Area</b>	<b>Additional Flow</b>	
(years)	(CC %)	(A %)	(Q %)	
2	0	0	0	
10	0	0	0	
30	0	0	0	
100	0	0	0	
100	40	0	0	

## Node Soakaway 01 Soakaway Storage Structure

Base Inf Coefficient (m/hr)	0.09800	Invert Level (m)	193.800	Depth (m)	1.000
Side Inf Coefficient (m/hr)	0.09800	Time to half empty (mins)	407	Inf Depth (m)	
Safety Factor	2.0	Pit Width (m)	3.500	Number Required	1
Porosity	0.95	Pit Length (m)	7.000		



File: soakaway.pfd Network: Storm Network Kris Tovey Page 2 Newbold Farm Duntisbourne Abbots Soakaway Calc

## Results for 2 year Critical Storm Duration. Lowest mass balance: 100.00%

18.11.23

**Node Event** US Peak Level Depth Inflow Node Flood **Status** Node (mins) (m) (m) (I/s) Vol (m³) (m³) 240 minute winter Soakaway 01 180 193.986 0.185 1.4 4.4253 0.0000 OK

Link EventUSLinkOutflow(Upstream Depth)Node(I/s)240 minute winterSoakaway 01Infiltration0.4



File: soakaway.pfd Network: Storm Network Kris Tovey Page 3 Newbold Farm Duntisbourne Abbots Soakaway Calc

## Results for 10 year Critical Storm Duration. Lowest mass balance: 100.00%

18.11.23

**Node Event** US Peak Level Depth Inflow Node Flood **Status** Node (mins) (m) (m) (I/s) Vol (m³) (m³) Soakaway 01 240 minute winter 192 194.156 0.356 2.3 8.4885 0.0000 OK

Link EventUSLinkOutflow(Upstream Depth)Node(I/s)240 minute winterSoakaway 01Infiltration0.4



File: soakaway.pfd Network: Storm Network Kris Tovey Page 4 Newbold Farm Duntisbourne Abbots Soakaway Calc

## Results for 30 year Critical Storm Duration. Lowest mass balance: 100.00%

18.11.23

**Node Event** US Peak Level Depth Inflow Node Flood **Status** Node (mins) (m) (m) (I/s) Vol (m³) (m³) 240 minute winter Soakaway 01 224 194.279 0.479 2.9 11.4399 0.0000 OK

Link EventUSLinkOutflow(Upstream Depth)Node(I/s)240 minute winterSoakaway 01Infiltration0.5



File: soakaway.pfd Network: Storm Network Kris Tovey Page 5 Newbold Farm Duntisbourne Abbots Soakaway Calc

## Results for 100 year Critical Storm Duration. Lowest mass balance: 100.00%

18.11.23

**Node Event** US Peak Level Depth Inflow Node Flood **Status** Node (mins) (m) (m) (I/s) Vol (m³) (m³) 480 minute winter 368 194.445 0.645 2.2 15.3971 0.0000 OK Soakaway 01

Link EventUSLinkOutflow(Upstream Depth)Node(I/s)480 minute winterSoakaway 01Infiltration0.5



File: soakaway.pfd Network: Storm Network Kris Tovey Page 6 Newbold Farm Duntisbourne Abbots Soakaway Calc

## Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 100.00%

18.11.23

**Node Event** US Peak Level Depth Inflow Node Flood **Status** Node (mins) (m) (m) (I/s) Vol (m³) (m³) 465 600 minute winter 194.787 0.987 2.7 23.5524 0.0000 OK Soakaway 01

Link EventUSLinkOutflow(Upstream Depth)Node(I/s)600 minute winterSoakaway 01Infiltration0.6



## **APPENDIX G**

**DRAINAGE STRATEGY** 

