

Foul and Surface Water Drainage Strategy

Project name:	30 Rosebery Road			
Project number:	D2234			
Client:	Mr. & Mrs. J Phare			
Prepared by and date:	S Burnett, January 2024			
Site address:	30 Rosebery Road, New Alresford, Winchester, Hampshire SO24 9HQ			
Grid Reference:	SU 58398 32051 / SU583320			
Eastings / Northings:	458398 / 132051			
Local Authority:	Winchester City Council			
Lead Local Flood Authority:	Hampshire County Council			
Proposed Development:	The proposed development involves the extension of an existing single-storey bungalow to provide a new first floor, in addition to the construction of a new single-storey garage.			
Site area:	The architectural development proposal is contained within Appendix A . 930m² (0.093Ha)			
Topography	J. Brotherton & Partners has undertaken a topographical survey at the site, dated April 2023. Levels are demonstrated as falling within the range of 90.63m AOD and 87.78m AOD, broadly falling in a south/south-westerly direction. Rosebery Road falls in a southerly direction, towards B3046.			
Greenfield run-off rate:	The following greenfield run-off rates have been established in relation to the site area of 930m² (0.093Ha): QBAR = 0.0186 I/s 1 year = 0.0186 I/s 30 year = 0.0465 I/s 100 year = 0.0558 I/s The above figures are based on a pro-rata calculation utilsing HR Wallingford's greenfield run-off tool, which considers a minimum site area of 0.1Ha.			
Brownfield run-off rate:	A brownfield run-off rate has been established in relation to the existing impermed area at the site, which totals 305m ² .			
Geology:	Reference has been made to the British Geological Survey (BGS) website, and specifically the Geology of Britain Viewer. This tool confirms the following: Bedrock Geology: Newhaven Chalk Formation - Chalk Superficial Deposits: None Mapping extracts are contained within Appendix B.			
Site Specific Invesitgation:	The BGS provides records of historic onshore boreholes. Reference has been made to this tool in the absence of site-specific intrusive investigation.			



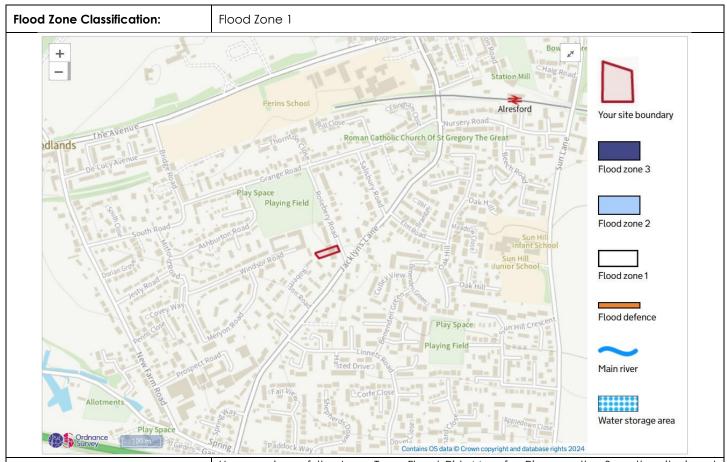
	The nearest borehole where records are available is located c. 260m north-east of the site (Ref: SU53SE79). The records for this location do not state the encountered geology,
	however.
	Attempts have also been made to review logs c. 430m north of the site (\$U53\$E86), although these records are confidential and not publicly available.
	Mapping extracts and records are contained within Appendix C .
Aquifer Designation:	For the following four sections, reference has been made to the MAGIC website (www.magic.defra.gov.uk) which provides authoritive geographic information about the natural environment from across government, in an interactive mapping tool format. Mapping extracts are contained within Appendix D .
	Bedrock: Principal Superficial Drift: Unproductive
Groundwater Vulnerability	'High' with a 'Soluble Rock Risk' identified
Zone: Groundwater Source Protection	
Zone:	None
Drinking Water Safeguarding Zone (Surface Water and/or Groundwater):	None
	Groundwater investigation has not been undertaken at the site.
Groundwater depth:	The BGS borehole records reviewed in relation to SU53SE79 confirms a ground level of 314.15ft AOD (95.75m AOD), with a rest water level of 307ft AOD (93.57m AOD).
	Groundwater investigation should be undertaken on site to confirm accurate groundwater levels.
	Infiltration testing has not been undertaken at the site.
Soil infiltration rate:	An assumed infiltration rate of 1x10 ⁻⁶ has been used for preliminary design purposes, in accordance with the typical figures provided in CIRIA 156, Table 4.4.
	Infiltration testing shall be undertaken to assist in the design of soakaways, post planning.
Nearby watercourses/rivers:	There are no ordinary watercourses within the immediate vicinity of the site.
	Southern Water's public sewer records are contained within Appendix E .
Nearby surface water sewer:	The records do not demonstrate any dedicated public surface water sewers within the vicinity of the site.
	A 100mm dia. public foul water sewer is located beneath Rosebery Road, which is shown to flow in a southerly direction, communicating with a 150mm dia. public foul water sewer beneath B3046, flowing in a westerly direction.
Additional drainage features	Rosebery Road is drained by traditional road gullies, located along the western channel line. It is assumed that these gullies discharge to a dedicated highway drainage system, although it has not been possible to confirm this at this stage.
	The proposed development involves the construction of a first-floor extension to the existing single-storey bungalow, in addition to the construction of a new single-storey garage.
Proposed method of disposal and reason:	The existing property will continue to drain as existing, although the client has expressed an interest in utilising a simple rainwater recycling system. There is to be no increase in the footprint / roof area associated with the existing bungalow further to the extension being implemented, therefore no increase in the drained area or catchment.
	The proposed garage will drain to a dedicated soakaway, serving the roof catchment of $22m^2$, subject to ground investigation and infiltration testing.
	If infiltration is found to be unviable for whatever reason, the garage will drain as per the existing arrangement of the existing bungalow.
Design storms considered:	1:10 Year (in accordance with Building Regulations, Approved Document H (H3, 3.2.7)



	The design considers the proposed new garage; the roof area associated with the existing bungalow is not increasing in view of the proposed development.
Climate change:	The design considers the proposed new garage; the roof area associated with the existing bungalow is not increasing in view of the proposed development.
Urban creep:	10% An allowance of 10% has been made for the potential future impacts of urban creep.
Proposed catchment areas:	Garage: 22m ² There will be no change to the drained area or catchment associated with the existing bungalow in view of the proposed development. The proposal concerns construction of a first-floor on the existing bungalow.
Proposed discharge rate:	An assumed infiltration rate of 1x10-6 has been used for preliminary design purposes, in accordance with the typical figures provided in CIRIA 156, Table 4.4. Infiltration testing shall be undertaken to assist in the design of soakaways, post planning.
Flow control method:	N/A
Volume of storage provided and method:	Storage will be provided in the form of a cellular soakaway (10.500m x 1.000m x 0.400m based on the assumed infiltration rate of 1×10^{-6}).
Offsite works:	None.



Flood Risk Summary



Rivers or the Sea:

Upon review of the Long-Term Flood Risk Map for Rivers or the Sea, the site is not identified as being at risk of flooding from such sources.

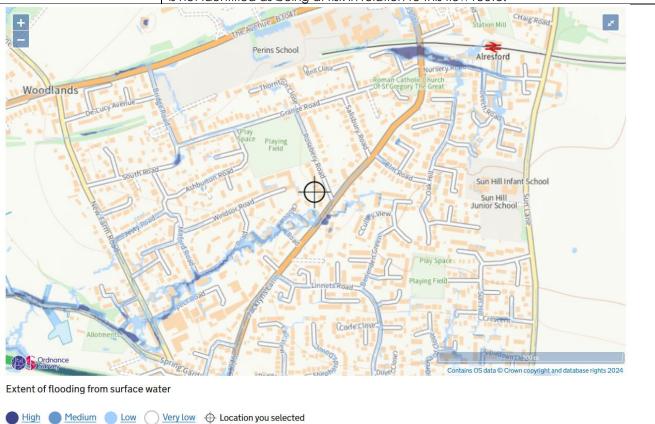




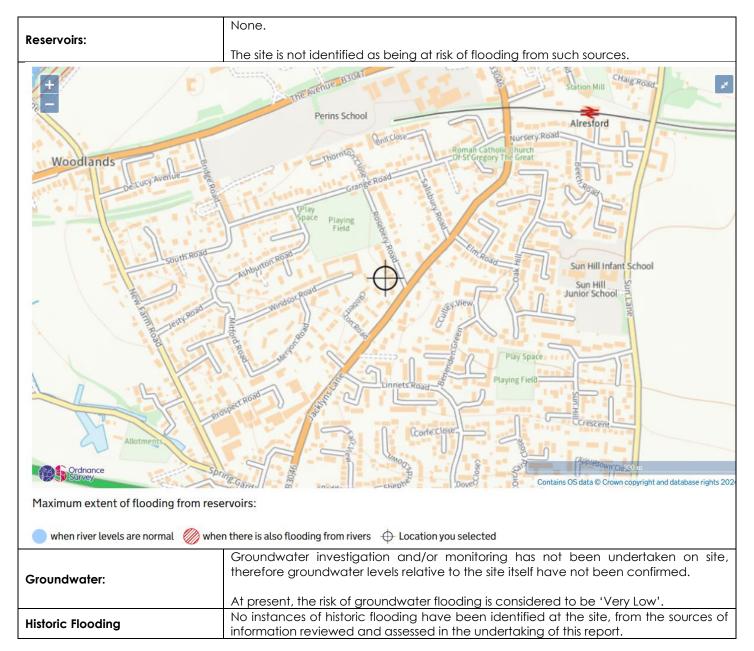
Surface Water:

The site is identified as being at 'Very Low' risk of surface water flooding, according to the Long-Term Flood Risk Map for Surface Water.

An overland flow route is identified to the south / south-west of the site with an associated risk of surface water flooding ranging from 'Low' to 'Medium'. The site itself is not identified as being at risk in relation to this flow route.







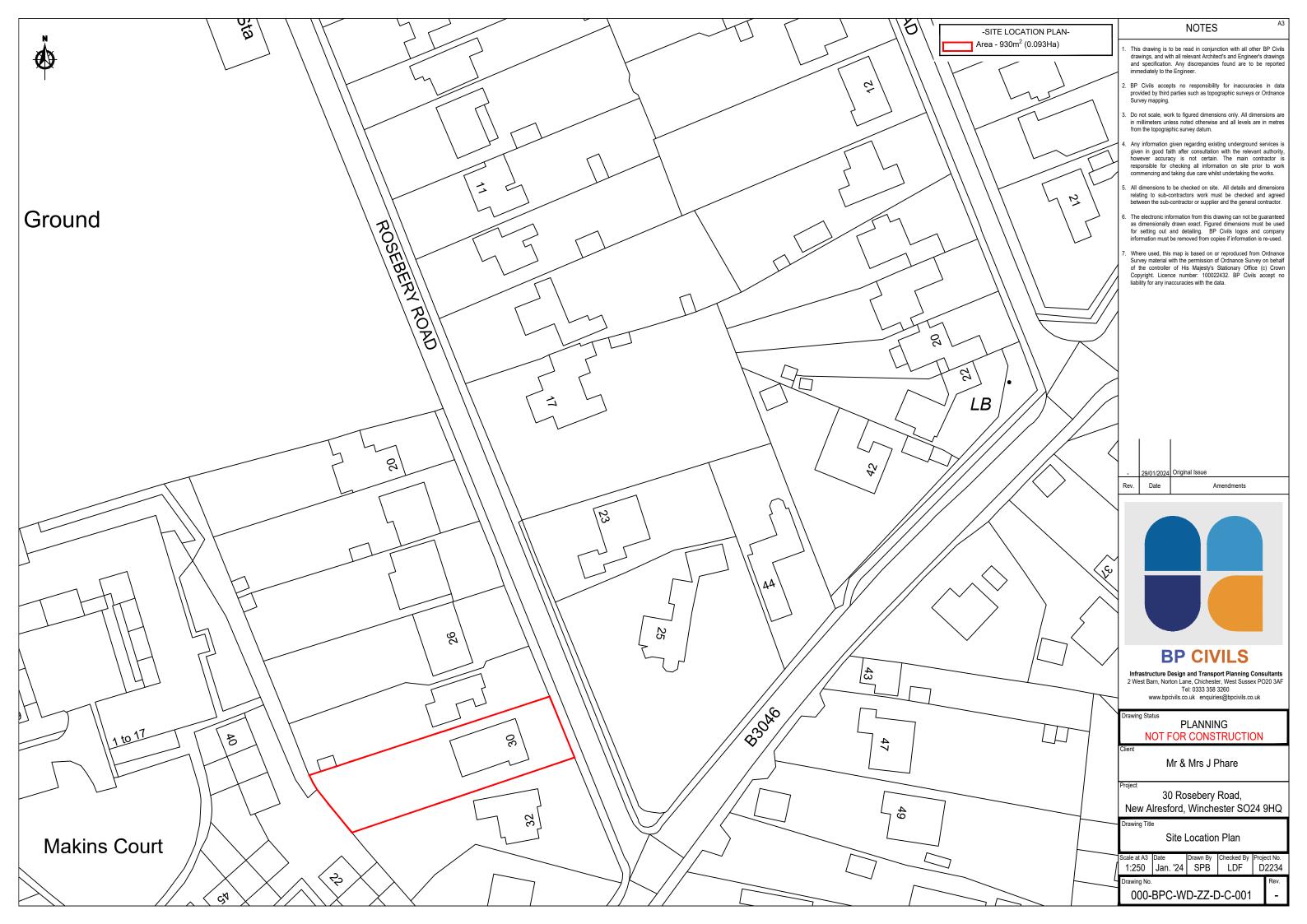


Foul Water Drainage Strategy

Number of properties:	1 No. existing dwelling
Method of discharge:	Southern Water's public sewer records identify a 100mm dia. public foul water sewer located beneath Rosebery Road, which is shown to flow in a southerly direction, communicating with a 150mm dia. public foul water sewer beneath B3046, flowing in a westerly direction. The existing bungalow drains to this sewer.
Point of discharge:	The site will continue to drain to Southern Water's public foul water sewer located beneath Rosebery Road.
Off-site works:	None. The existing connection to the public sewer network will be retained.

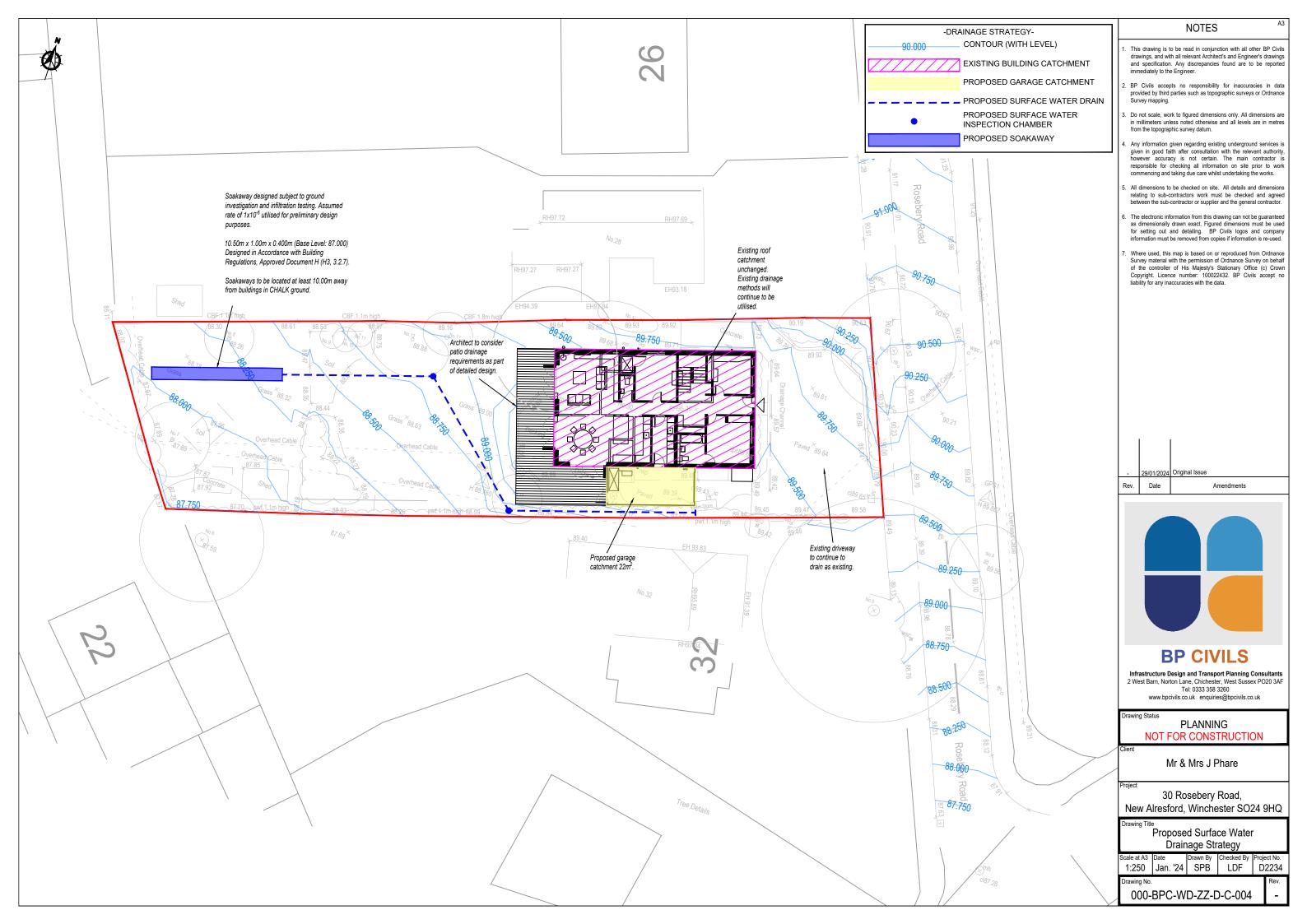


DRAWINGS











APPENDICES



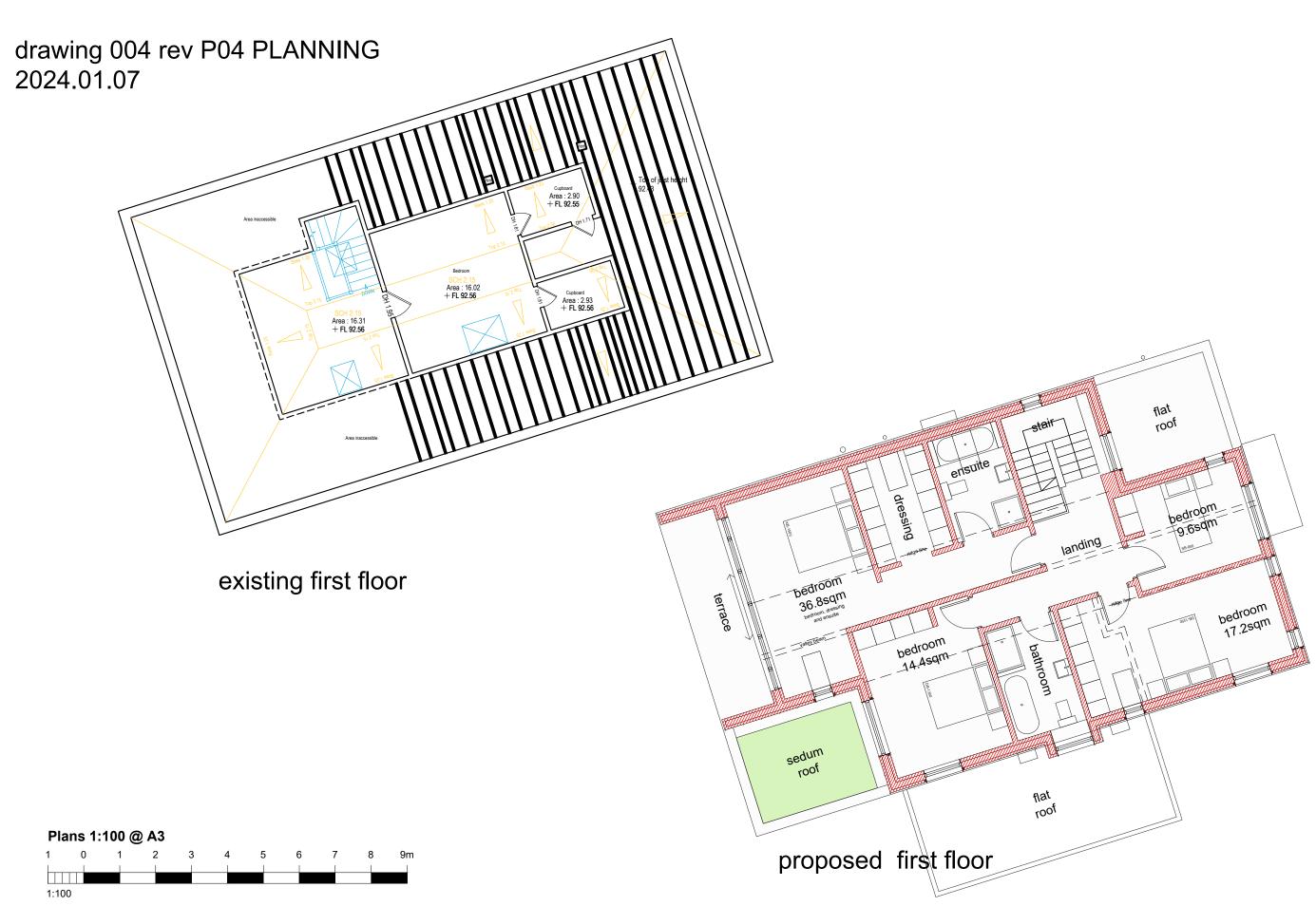
APPENDIX A – Development Proposals



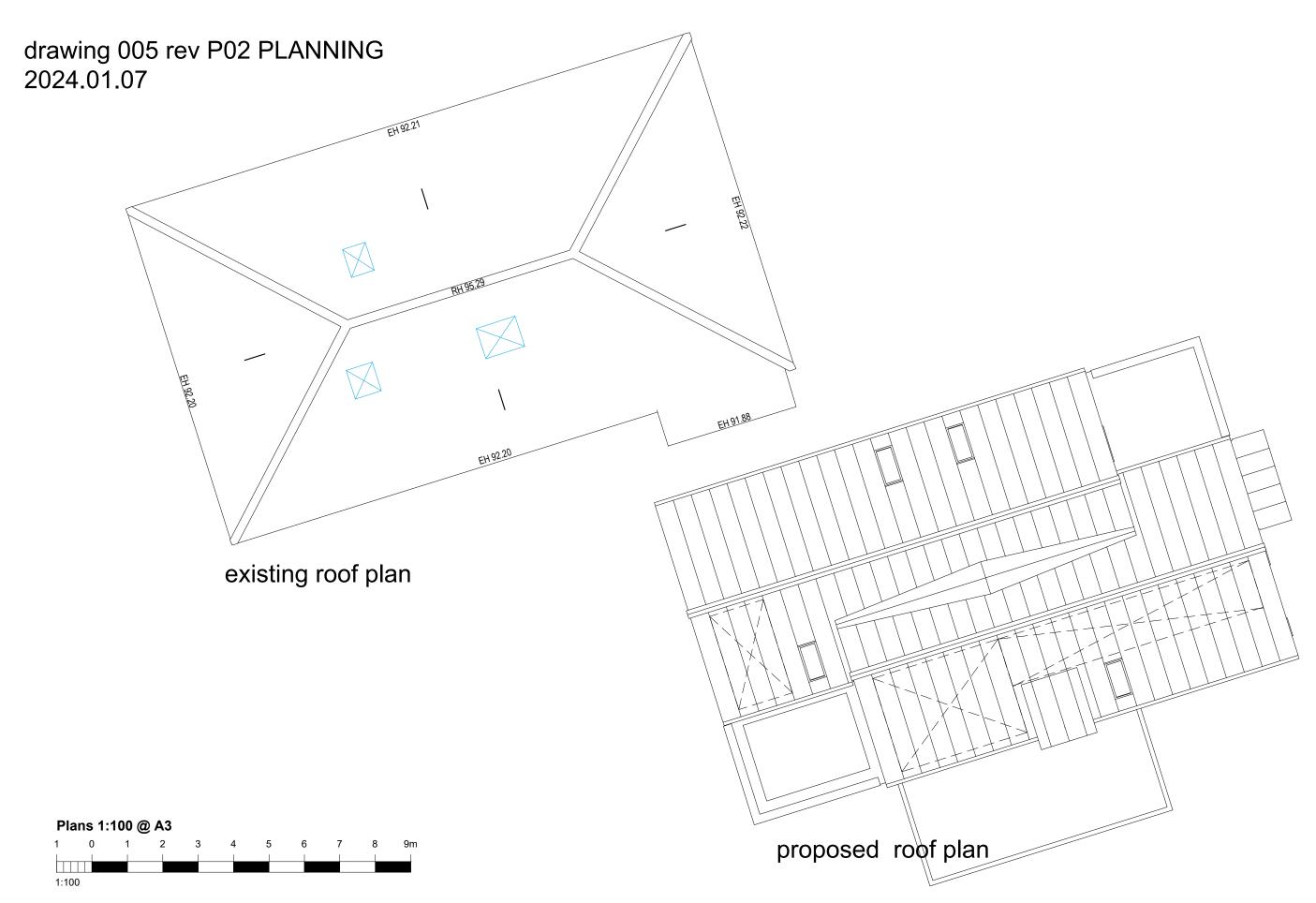
30 Rosebery Road, New Alresford floor plans - ground floor 1:200 at A3



30 Rosebery Road, New Alresford floor plans - first floor 1:200 at A3

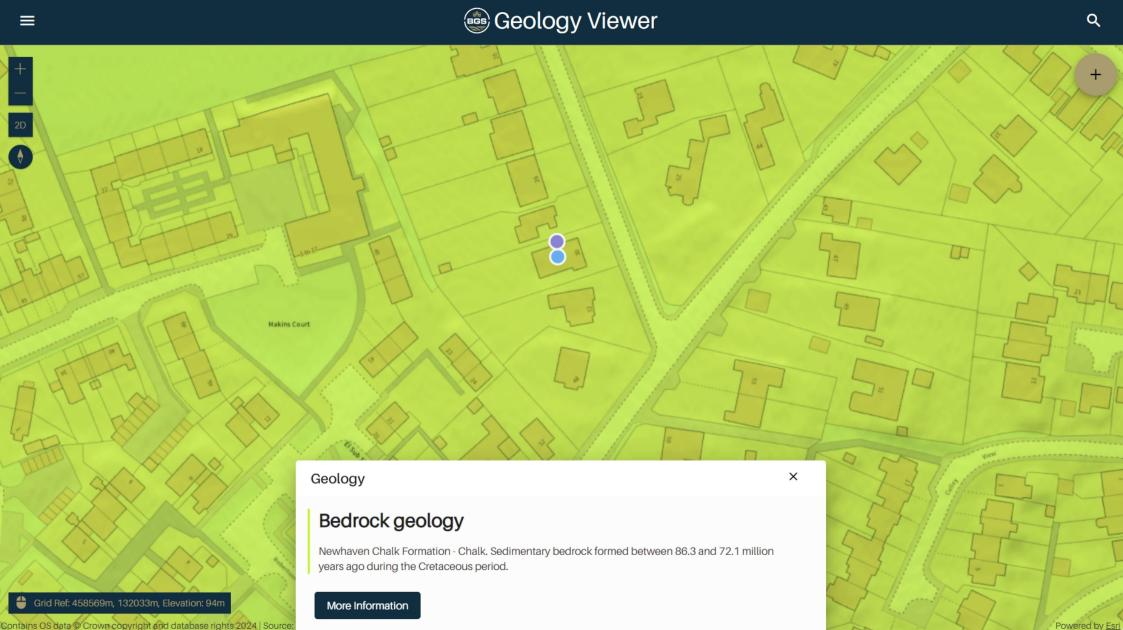


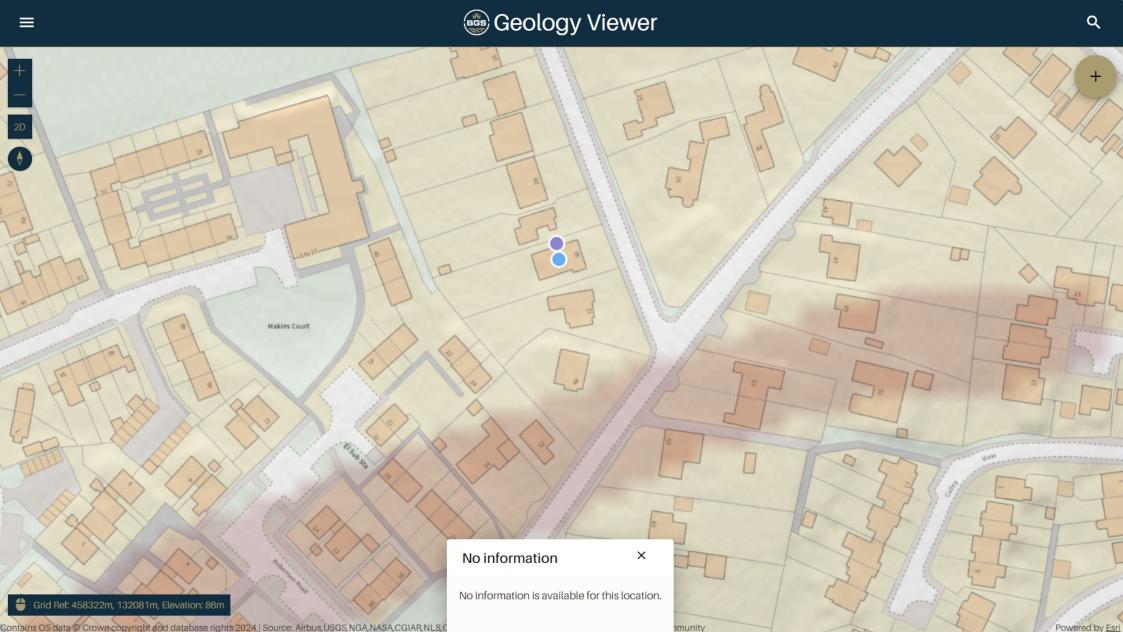
30 Rosebery Road, New Alresford floor plans - roof plan 1:200 at A3





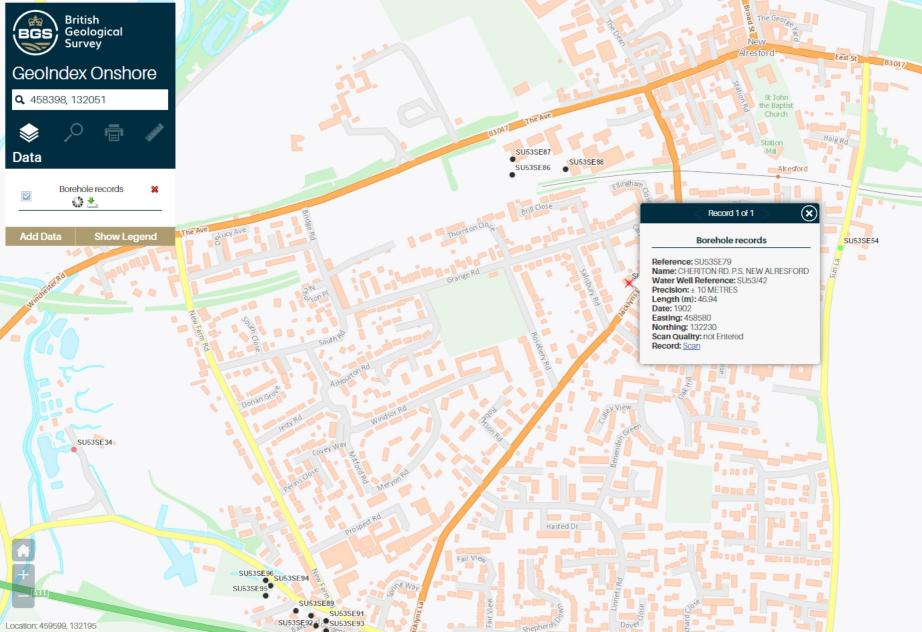
APPENDIX B - BGS Maps

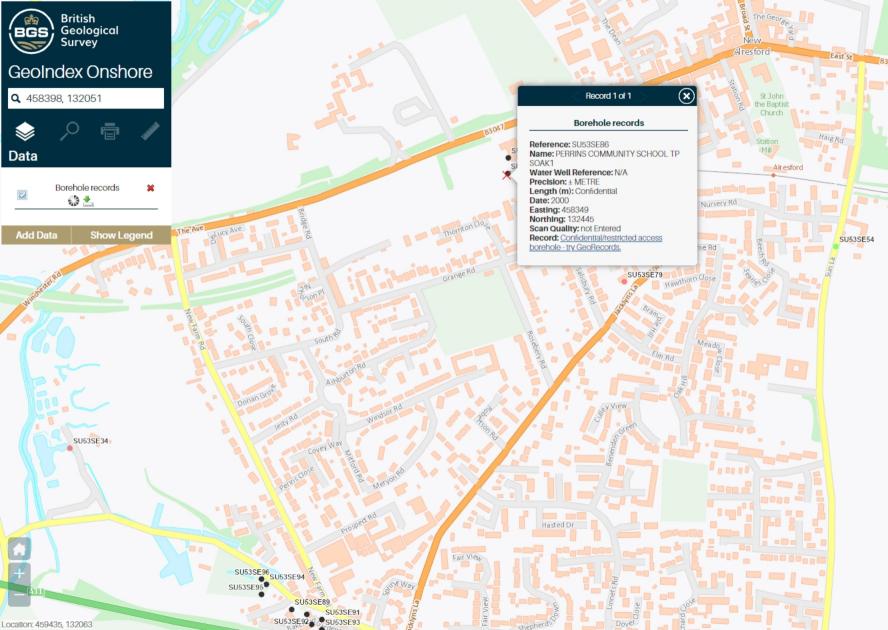


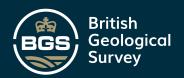




APPENDIX C - BG\$ Borehole Records









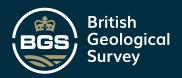


QUARTER SHEET SUSSE

BH REGISTRATION NUMBER

RECORDS ENTERED AND HELD BY WALLINGFORD

BH REGISTRATION NUMBER(S)



300/110 Winchester R.D.C., Pumping Station, Cheriton Road, New Alresford. (Filled in)

Surface +314. Shaft 110; rest bore 18 in. Water struck at +307.

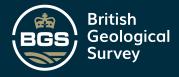
R.W.L. +307. c. 1902.

Suction +204. Recovered to R.W.L. in 5 min. Yield 3,500 g.p.h; 8 h.p.d. Hardness: P. 45, T. 195. 1935. Yield 3,500 g.p.h., 10 h.p.d. Apr. 1941. R.W.L. +206. P.W.L. +197. Yield 10,000 g.p.h. Oct. 1950. R.W.L. +203. P.W.L. +197. Yield 3,333 g.p.h. Mar. 1953.

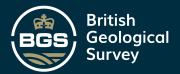
154 UCk

E stimated No detait Known. pp. C.P. Thomas Cleaning

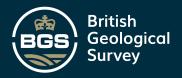
154



ANY, LTD.		Surve	nd Water -	
	ATER (RESFORD W	UndertakingAL	e or Description Authority or Und
rd, Hants	, Alre			
Parsi New alresport (1)	concepo	1953. . wa	now disused	Mesford
R Su 5858 3223	OUND W	OVER-GRO	. (4	
•		ds of levels of	ı take systematic recor	
				water in :— (1) rivers
			treams	(2) stream
			eservoirs	(3) reserve
			akes	(4) lakes
		ers	anals or navigable rive	(5) canals
U.C 154 feet				
UCK - 154 feet.		aken?	ften are the readings to	(c) How often a
Houts/N. W. (W). S Jam ey No. R. V. Hourd of			points at which the reco o or sketch would be h	
the also ford vector co.				
Details as elected, seasoft		er standard (in	the levels been related Level or to some other	Datum Leve
that funding is who for		st and lowest)	the levels (e.g., higher satisfactorily by the	(f) Are all the l
cat even a graphment sold				
PSB.7.4.44 Selten 31 Marg 1954: inclusion 8.D.C. Take one			rangements made for erise and fall of floods,	
obert 10 comes daidy H. F. B. F. Holder 31 Mars 1954 Color 31 Mars 1954 Color 31 Mars 1954 Color 31 Mars 1951 Color 31 M		etc.?	rise and fall of floods, es of systematic records a records of levels	What types of other than recregards:—
ps.B. 7.4.44 Solten 31 Mano 1954: incluster & D.C. Taken oner t. 1952		etc.?	rise and fall of floods, es of systematic records a records of levels ivers	What types of other than rec
		er standard (in standard)? st and lowest)	Level or to some other ter case please specify the levels (e.g., highe	Datum Leve the latter ca (f) Are all the l



• • •		\$ - E
(III) (a) Have measurements been made from which the data for levels can be converted to	(3G ^G)	2
records of discharge of:— (1) rivers and streams		
(i) Tivers and streams		
(1) reservoirs		•
(3) akes	. /	
(4) canals or navigable waterways	,	(80)
(b) If so, how have these measurements been made (e.g., by current meters, velocities of floats, surveys of sections, calibration of weirs, records of water used for locking, etc.)?		
(IV) (a) Are records kept in the case of springs breaking overground of the amount of water yielded?		
(b) If so, what form of recording is used?		,
(c) How often are readings taken?		
(d) Exact location of the spring (A map or sketch would be helpful.)		
		(BG)
(V) Since when have the records under I, II, III and IV been kept?	• ,	
(VI) Are past records available?		
(VII) REMARKS.		
(Please indicate here any further information or particulars which may be thought likely to assist in the survey.)		
	•	
	,	
		*





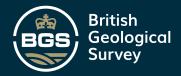
300 5453 42

(B) UNDERGROUND WATER-(WELLS AND BORINGS).

(In each case please state whether a well and/or boring is in question.)

10

NERAL.			
1. Exact site of well or boring	Cheri	ton Road and	
(A map or sketch showing position would be useful.)	Gran	ge Road,	
	New	Alresford, Hants	
2. Surface level of ground above Ordnance Datum	•	314,15	ft.
2. Data of according		47	
3. Date of construction	****	About 1902	
		(305)	
VELLS.			
4. Depth of well from surface level of ground (i.e., 2 abov	(a) If ton		•
of well is below the surface level of ground (i.e., 2 above of well is below the surface level of the ground (i.e., 2 al how much	bove) state	110	ft.
now internet	,,,		
5. Depth of floor of galleries at site of well: also dim direction of galleries	ension and	No galleries Only boring	ft. _ ` .
6. Depth of boring from surface level of ground (i.e., 2 boring is in bottom of well, state depth of well	above). If	Well 110	ft.
		Boring <u>44</u> 154	" feet
7. (a) Diameter of top of boring			
(b) Diameter of bottom of boring		18	3 in.
8. Tubed from top of boring to		No tubing Solid chalk	ft.
9. Lining tubes perforated at depths of	•		ft.
5. Dining tunes periorated at depths of		-	
10. Water struck during boring at depths of	Be f o	ore boring 7	ft.
11. What was rest level on completion of boring?		,	7 ft.
Wells and Borings.			
12. Is the water raised by pump or air lift?		Pump	
13. Depth from top of well or boring to bottom of suction p	oipe	110	ft.

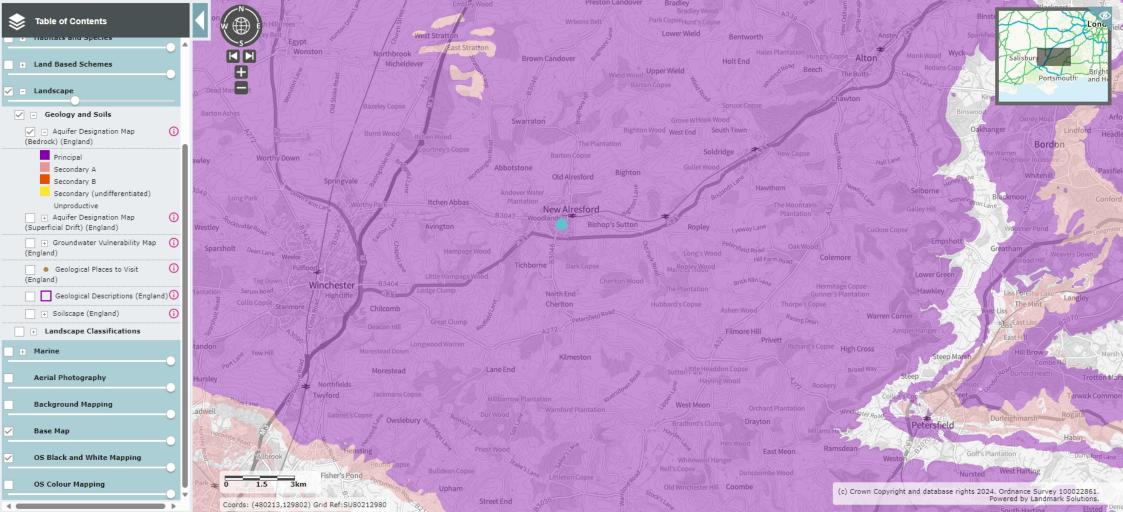


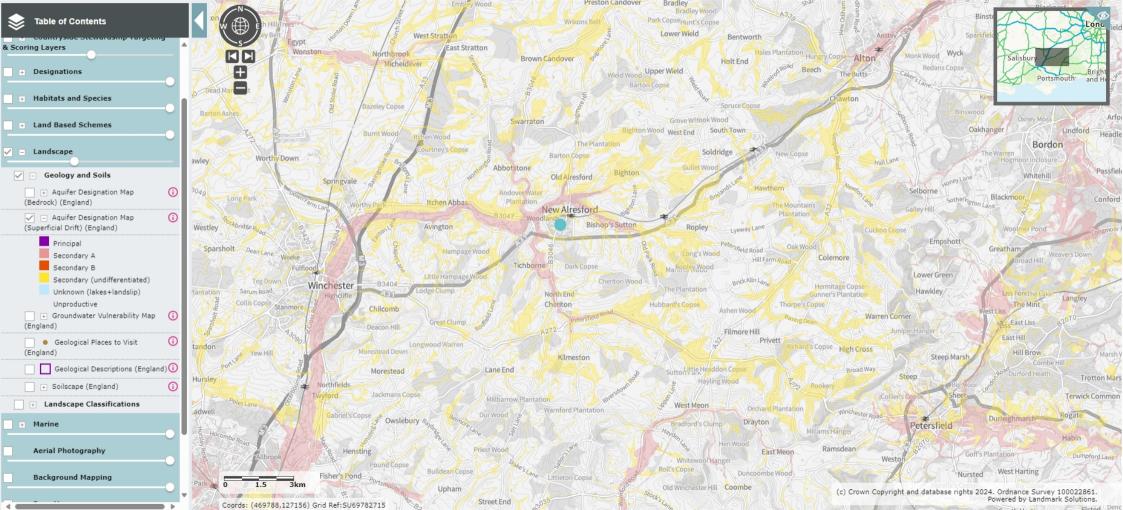
			The state of the s	,
•	II. If systematic measurements of water levels are			
	made, state whether these include:—			
	(a) Pumping JevelsYes(b)	Rest levels Yes		
	(c) Time of recovery to rest level on cessation of pr	umping	.Five.minutes	
	(d) Changes in pumping level, if rate of pumping is altered.		No changes	
	pumping is aftered.			
	Also state: (e) at what intervals records are taken etc.)	(i.e., daily, weekly,	Weekly	
- '				
	Please furnish a specimen graph of records taken over as long a period as available (up to	Very little v		
	1 year).		m 6 to 10 feet	
		according to s	eaon.	
-	III. If measurements are made only occasionally, please indicate what is, or has been, done in this			
-	respect and furnish examples of any graphs or figures available.			
١ .				
	IV. YIELDS.			
			* **	· (6
43	(1) Number of gallons pumped per hour		3500	
			*	
	(2) Is pumping continuous?		No.	
			10 kara perde	} ·
	- (3) If not, how many hours pumping per day?			
	(4) Maximum daily yields available As	meny hours pun	ping as required	
-				
	H	Estimated		
<u>-</u>	I	Based on actual tests		
	•		i	
(S)	V. If a section or record of strata can be given please attach to this form.			BG

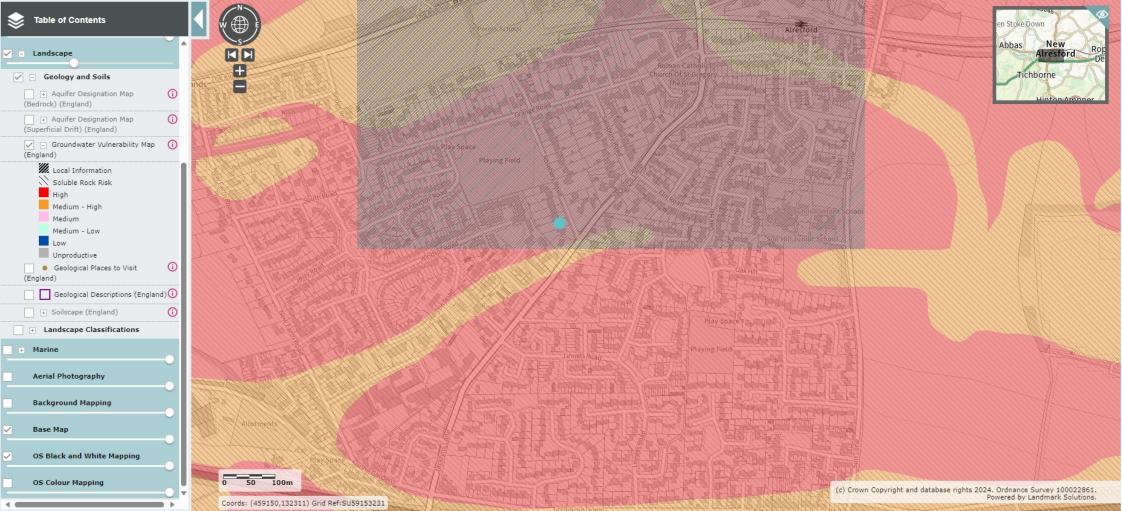
	VI. (1) If a chemical analysis can be given please attach.			
,	(2) If not state hardness	19.5 temp.	4.5 perm.	
	\$	_		=
	(3) For what purpose is the water used?	Domestic		
		Træde sli	ghtly•	•
	Data	Bank	f	



APPENDIX D - MAGIC Maps











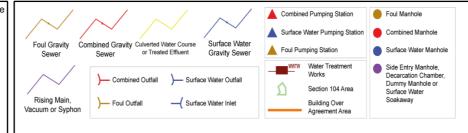
APPENDIX E – Public Sewer Records

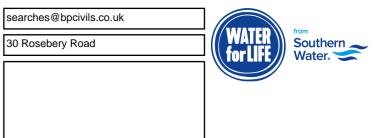


The positions of pipes shown on this plan are believed to be correct, but Southern Water Services Ltd accept no responsibility in the event of inaccuracy. The actual positions should be determined on site. This plan is produced by Southern Water Services Ltd (c) Crown copyright and database rights 2024 Ordnance Survey 100031673. This map is to be used for the purposes of viewing the location of Southern Water plant only. Any other uses of the map data or further copies is not permitted.

WARNING: BAC pipes are constructed of Bonded Asbestos Cement.

WARNING: Unknown (UNK) materials may include Bonded Asbestos Cement.





Manhole Reference	Liquid Type	Cover Level	Invert Level	Depth to Invert
1002	F	82.23	0.00	
1004	F	0.00	0.00	
1005	F	0.62	0.00	
1006	F	0.00	0.00	
1007	F	0.00	0.00	
1103	F	0.00	0.00	
1107	F	0.00	0.00	
1108	F	0.00	0.00	
1109	F	0.00	0.00	
1110	F	0.00	0.00	
1111	F	0.00	0.00	
1112	F	0.00	0.00	
1113	F	0.00	0.00	
1114	F	0.00	0.00	
1901	F	80.55	79.13	
1903	F	79.90	78.50	
1904	F	81.44	80.19	
2001	F	0.00	0.00	
2002	F	84.94	82.66	
2003	F	82.94	81.36	
2004	F	0.00	0.00	
2901	F	79.08	76.62	
2902	F	81.13	79.31	
2903	F	79.65	77.40	
2906	F	78.60	75.87	
2907	F	0.00	0.00	
2909	F	0.00	0.00	
2910	F	0.00	0.00	
2911	F	0.00	0.00	
3001	F	0.00	0.00	
3002	F	0.00	0.00	
3003	F	0.00	0.00	
3004	F	0.00	0.00	
3005	F	0.00	0.00	
3101	F	92.47	90.67	
3903	F	85.57	83.66	
3904	F	83.75	80.92	
3905	F	83.30	80.78	
3906	F	81.68	80.75	
3907	F	0.00	0.00	
	F			
4001	F	87.23	85.01	
4002		87.37	85.14	
4003	F	91.95	90.06	
4004	F	92.07	90.04	
4005	F	91.64	89.80	
4901	F	86.35	84.32	
4902	F	85.96	84.38	
4903	F	85.96	83.67	
4904	F	89.30	87.74	
4905	F	89.30	87.80	

Manhole Reference	Liquid Type	Cover Level	Invert Level	Depth to Invert
5001	F	93.65	91.13	
5002	F	94.62	92.30	
5101	F	95.61	93.87	
5102	F	95.90	93.80	
5103	F	95.95	94.12	
5104	F	96.05	94.08	
5901	F	98.12	0.00	
5902	F	94.47	0.00	
6001	F	97.09	95.14	
6101	F	96.92	95.22	
6103	F	97.04	96.34	
6104	F	0.00	0.00	
6105	F	0.00	0.00	
6902	F	98.19	96.62	
6903	F	101.35	99.85	
		101100	00.00	

Manhole Reference	Liquid Type	Cover Level	Invert Level	Depth to Invert



APPENDIX F – Wallingford Greenfield Run-off Calculations



Greenfield runoff rate estimation for sites

www.uksuds.com | Greenfield runoff tool

Calculated by:	Stuart Burnett
Site name:	30 Rosebery Road
Site location:	

Site Details

51.08480° N Latitude: 1.16764° W Longitude:

863370005

developments", SC030219 (2013), the SuDS Manual C753 (Ciria, 2015) and the non-statutory standards for SuDS (Defra, 2015). This information on greenfield runoff rates may be the basis Jan 29 2024 12:15

Runoff estimation approach

IH124

This is an estimation of the greenfield runoff rates that are used to meet normal best practice Reference:

criteria in line with Environment Agency guidance "Rainfall runoff management for

for setting consents for the drainage of surface water runoff from sites.

Site characteristics

Total site area (ha):

Methodology

QBAR estimation method:

SPR estimation method:

Calculate from SPR and SAAR

Calculate from SOIL type

Notes

(1) Is $Q_{BAR} < 2.0 \text{ I/s/ha}$?

When Q_{BAR} is < 2.0 l/s/ha then limiting discharge rates are set at 2.0 l/s/ha.

Soil characteristics

Default

N/A

0.1

Edited

1

N/A

0.1

HOST class:

SOIL type:

SPR/SPRHOST:

(2) Are flow rates < 5.0 l/s?

Where flow rates are less than 5.0 l/s consent for discharge is usually set at 5.0 l/s if blockage from vegetation and other materials is possible. Lower consent flow rates may be set where the blockage risk is addressed by using appropriate drainage elements.

Hydrological characteristics

SAAR (mm):

Hydrological region:

Growth curve factor 1 year:

Growth curve factor 30 years:

Growth curve factor 100 years:

Growth curve factor 200 years:

Default Edited

825 825

7 7

0.85 0.85

2.3 2.3

3.19 3.19

3.74 3.74 (3) Is $SPR/SPRHOST \le 0.3$?

Where groundwater levels are low enough the use of soakaways to avoid discharge offsite would normally be preferred for disposal of surface water runoff.

Ç) _{BAR} (I/s):	0.02	0.02
1	in 1 year (l/s):	0.02	0.02
1	in 30 years (I/s):	0.05	0.05
1	in 100 year (l/s):	0.06	0.06
1	in 200 years (I/s):	0.08	0.08

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at www.uksuds.com/terms-and-conditions.htm. The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.



APPENDIX F – Causeway Flow Hydraulic Calculations



File: D2234 Garage Soakaway.pfd

Network: Storm Network

Stuart Burnett 30/01/2024 Page 1 D2234 30 Rosebery Road

Design Settings

Rainfall Methodology Return Period (years) Additional Flow (%) CV Time of Entry (mins) Maximum Time of Concentration (mins)	2 0 1.000	Minimum Velocity (m/s) Connection Type Minimum Backdrop Height (m) Preferred Cover Depth (m) Include Intermediate Ground Enforce best practice design rules	0.500 1.200 ✓
Maximum Time of Concentration (mins) Maximum Rainfall (mm/hr)	30.00 50.0	Enforce best practice design rules	✓

Nodes

Name	Area	Cover	Depth
	(ha)	Level	(m)
		(m)	
Garage Soakaway	0.002	88.000	1.000

Simulation Settings

	ndology mer CV nter CV	FEH-22 1.000 1.000	Drair	Skip St	ysis Speed eady State ime (mins)	x	Ch	eck Discha	nge (m³/ha) rge Rate(s) ge Volume	20.0 x x
Storm Durations										
15	60	180	360	600	960	2160	4320	7200	10080	
30	120	240	480	720	1440	2880	5760	8640		

Return Period	Climate Change	Additional Area	Additional Flow	
(years)	(CC %)	(A %)	(Q %)	
2	0	0	0	
2	45	10	0	
10	0	0	0	
10	45	10	0	

Node Garage Soakaway Soakaway Storage Structure

Base Inf Coefficient (m/hr)	0.00360	Invert Level (m)	87.000	Depth (m)	0.400
Side Inf Coefficient (m/hr)	0.00360	Time to half empty (mins)	4404	Inf Depth (m)	0.400
Safety Factor	2.0	Pit Width (m)	10.500	Number Required	1
Porosity	0.95	Pit Length (m)	1.000		



File: D2234 Garage Soakaway.pfd Network: Storm Network

Stuart Burnett

30/01/2024

Page 2 D2234 30 Rosebery Road

Results for 2 year Critical Storm Duration. Lowest mass balance: 100.00%

Node Event US Peak Level Depth Inflow Node Flood **Status** Node (mins) (m) (m) (I/s) Vol (m³) (m³) 240 minute winter Garage Soakaway 87.035 0.035 0.1 0.3518 0.0000 OK 156

> **Link Event** US Link Outflow (Upstream Depth) (I/s) Node 240 minute winter Garage Soakaway Infiltration 0.0



File: D2234 Garage Soakaway.pfd Network: Storm Network

Stuart Burnett 30/01/2024 Page 3 D2234 30 Rosebery Road

Results for 2 year +45% CC +10% A Critical Storm Duration. Lowest mass balance: 100.00%

Node Event	US	Peak	Level	Depth	Inflow	Node	Flood	Status
	Node	(mins)	(m)	(m)	(I/s)	Vol (m³)	(m³)	
480 minute winter	Garage Soakaway	312	87.073	0.073	0.1	0.7354	0.0000	OK

Link EventUSLinkOutflow(Upstream Depth)Node(I/s)480 minute winterGarage SoakawayInfiltration0.0



File: D2234 Garage Soakaway.pfd

Network: Storm Network

Stuart Burnett 30/01/2024 Page 4 D2234 30 Rosebery Road

Results for 10 year Critical Storm Duration. Lowest mass balance: 100.00%

Node Event	US	Peak	Level	Depth	Inflow	Node	Flood	Status
	Node	(mins)	(m)	(m)	(I/s)	Vol (m³)	(m³)	
600 minute winter	Garage Soakaway	375	87.069	0.069	0.1	0.6891	0.0000	OK

Link EventUSLinkOutflow(Upstream Depth)Node(I/s)600 minute winterGarage SoakawayInfiltration0.0



File: D2234 Garage Soakaway.pfd Network: Storm Network

Stuart Burnett 30/01/2024

Page 5

D2234 30 Rosebery Road

Results for 10 year +45% CC +10% A Critical Storm Duration. Lowest mass balance: 100.00%

Node Event	US	Peak	Level	Depth	Inflow	Node	Flood	Status
	Node	(mins)	(m)	(m)	(I/s)	Vol (m³)	(m³)	
600 minute winter	Garage Soakaway	420	87.119	0.119	0.1	1.1937	0.0000	OK

Link EventUSLinkOutflow(Upstream Depth)Node(I/s)600 minute winterGarage SoakawayInfiltration0.0