

# The Yard, Field Lane, Littleton Upon Severn

# DRAINAGE STRATEGY REPORT

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James Morris & Catherine Meachin

Date: 19<sup>th</sup> March 2024

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P05	For Planning	19.03.2024	Permeable driveway added			



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# 1. INTRODUCTION

### 1.1 Brief

The Drainage Strategy Report has been prepared on behalf of James Morris & Catherine Meachin to provide information to South Gloucestershire Local Planning Authority and Building Control, to aid satisfying how the new development will discharge storm and foul water from the site and reduce the risk of flooding.

This assessment is to review the SUDs and associated storm and foul water drainage to ensure the proposed development does not increase the risk of flooding to the local area and to ensure the discharge method is in accordance with current design practice and standard.

The information has been reviewed against the following industry design standard to ensure the drainage is compliant;

- Building regulations Part H: Drainage & Waste Disposal;
- Sewers for Adoption/Design and Construction Guidance;
- The requirements of Wessex Water;
- CIRIA C753: The SuDS Manual; and
- Lead Local Flood Authority requirements;
- Flood and Water Management Act 2010
- BS EN 752 Drain and Sewer Systems Outside Buildings.
- Local Authority Guidance.
- National Planning Policy Framework (NPPF).
- DEFRA Non-Statutory Technical Standards for Sustainable Drainage.
- South Gloucestershire Local Flood and Risk Management Strategy (2022-2027)

The proposed development will effectively drain through on-site sustainable drainage techniques for storm water and how foul water will be dealt with. This report provides guidance and clarification of viable below ground drainage proposals and connections to local infrastructure.

The objectives of the report are to;

- Review the existing drainage arrangements on site for both surface and foul water;
- Assess the options for the disposal of storm water and foul water from the development; and
- Provide a design for surface water strategy

The following tasks will be undertaken to complete this report;

 Undertake a desktop investigation of the site's existing foul and surface water drainage arrangements;

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- Outline anticipated solutions for surface water disposal.
- Determine the area of impermeable surfaces that will be added by the proposed development and determine greenfield run-off rates for this area (where applicable);
- Assess the feasibility of using infiltration as a disposal method, based on soakaway test results or any other available information on ground and site conditions;
- Satisfy Condition 8 of the South Gloucestershire Council Planning Condition P23/00673/F

Condition 8: Prior to occupation details of the Sewage Package Treatment Plant must be submitted to and approved by the Local Planning Authority, including the location, and method of irrigation for the effluent overflow. A percolation test for discharge to a soakaway is necessary. The applicant must consult the Environment Agency for the need to obtain an 'Environmental Permit' and produce a copy if required. Package Treatment Plants must be located 10 metres away from any watercourse and structures including the public highway.

Reason:

To ensure a satisfactory means of drainage and pollution control in order to comply with South Gloucestershire Local Plan: Polices, Sites and Places Plan (Adopted) November 2017 Policy PSP21; and South Gloucestershire Local Plan: Core Strategy (Adopted) December 2013 Policy CS9.

This report is based on information available at the time of preparation. Consequently, there is potential for further information to become available. These changes may lead to future alteration to the conclusions drawn in this report for which Flow Civil Engineering cannot be held responsible.

### 1.2 Proposed Development

The proposed development is a residential conversion of an existing rural building to a 3-bedroom dwelling with associated parking and amenity space. This report is to be read in accordance with Mitchell Eley Gould architecture design package. Refer to Appendix A for proposed site layout.



# 2. SITE INFORMATION

### 2.1 Location

The site is situated in the grounds of The Yard, Field Lane, Littleton Upon Severn. The site location is shown in Figure 1, with the full address and Ordnance Survey Grid reference provided in Table 1. The development is sited on a brownfield land, at the west side of the plot, adjacent to Field lane. The site is situated in a residential area of a rural community.

Site Referencing Inf	Site Referencing Information				
Site Address	Site Address The Yard, Field Lane, Littleton Upon Severn, BS35 1NU				
Grid Referencing X 360006, Y 189757					



Table 1: Site referencing Information

Figure 1: Site Location

### 2.2 Existing land and drainage

The Yard is located a short distance to the east of Littleton-upon-Severn. The site as a whole extends to approximately 4.4 hectares (11 acres) and comprises pasture divided into paddocks in equestrian use, buildings in equestrian use, a manège, a horsewalker and a parking / yard area. The site as a whole is bounded to the west by Field Lane and a mature hedge with standard trees. The southern boundary is formed by Village Road and a mature hedge. Residential properties adjoin the wider site to the north and east, with agricultural land to the north-east.



A review of topographical survey data indicates an elevation of approx. 50.3m Above Ordnance Datum (AOD) in the north of the site proximal to the site access, with levels falling gently to the south (to approx. 49.1m AOD at the access to the adjoining paddock) to the existing historic stream / ditch. The existing buildings roof catchment and grounds discharge storm water into this ditch (Photo 1). The stream outfalls to a culvert (Photo 1) that crosses Field Lane to a watercourse in the verge. Storm water from this stream enters another culvert and crosses the main highway (to Littleton Upon Severn Village) entering a flowing stream along the side of Elmonger house (Photo 2 and 3). The stream then runs southwards connecting to a more significant watercourse (Photo 4), onwards to the River Severn. Refer to Figure 2 for mapping of these connections and photograph locations.

There are no foul drains on site. Wessex Water Sewer Maps show no records of foul or storm sewers in the vicinity for >100m radius around the site.

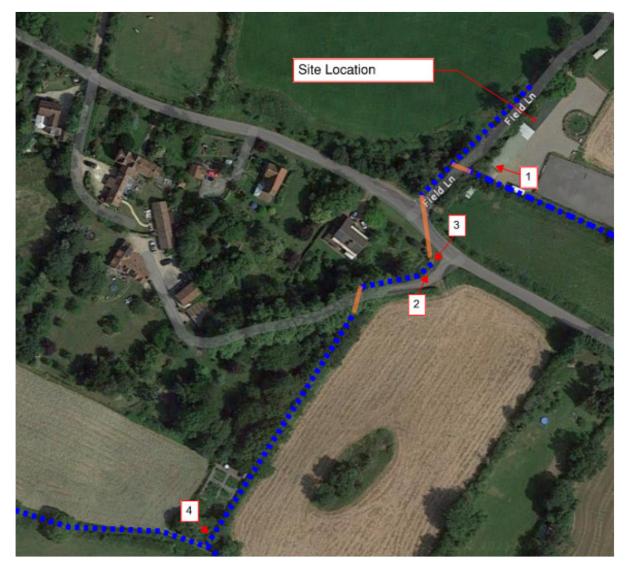


Figure 2: Stream network and photograph locations



Photo 1: Outfall from site to culvert across Field Lane



Photo 2 and 3: Stream adjacent to Elmonger House





Photo 4: Southern Watercourse

### 2.3 Existing Geology & Infiltration testing

A Geotechnical & Geo-environmental Ground Investigation was carried out by S10 dated the 29<sup>th</sup> November 2023. Refer to their report reference 23-230 for further information. The ground subgrade was found to be reddish-brown silty clay. As part of the ground investigation testing, infiltration testing was carried out in accordance with BRE 365 Digest and BS6297 Code of practice for design of drainage fields, to establish weather the ground conditions permit the use of soakaways.

S10 Geo-Consulting carried out the ground investigations and concluded the ground conditions has extremely poor infiltration properties and is not suitable for the use of storm soakaways or drainage fields to discharge storm and foul water from the proposed development. Refer to Appendix B for soakaway test record.

The poor percolation conditions were evident on Flow Civil Engineering site visit in September where there was standing water across site as shown in Photo 5.



Photo 5: Water-logged ground conditions on site

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# 3. FOUL DRAINAGE

### 3.1 Proposed Foul Drainage

Due to the site constraints and absence of existing foul drainage infrastructure, there is limited options to discharge foul drainage. An analysis of the options has been tabulated to identify the best viable solution. Refer to Table 1 below: -

Option	Description	Advantages	Disadvantages	Viability
1	Foul Water Treatment Plant	Treats the foul waste and provides 'clean' water discharge to soakaway /drainage field/watercourse. Running costs and maintenance is lower than cesspits and septic tank	Expensive upfront costs. Minimum annual minor maintenance required. A gravity connection to outfall is not possible due to site levels. Pump required.	There is a stream within site. Due to site ground conditions, it is not possible to discharge to a drainage field.
2	Drainage Field	Avoids the need for treatment plants	Requires a large flat area to install. Long lengths of pipe work required. Requires permeable ground conditions.	Not viable due to poor permeability.
3	Connection to existing drainage			Not viable as no foul water drainage systems exist on site
4	Connection to sewer	Minimises maintenance and very sustainable	Extremely long excavations required to connect to nearest sewer (which is unknown distance away > 500m).	Not viable.
5	Cesspit	Cheaper installation for tank. extremely expensive over the lifetime of the building for regular emptying requirements	Extremely expensive over the lifetime of the building for regular emptying requirements	Not viable for intended use for cost benefits when compare to other more sustainable alternatives.
6	Septic Tank		2020), discharge from a septic ield or soakaway constructed	Not viable.

The proposed foul water for the domestic sewage will be collected by gravity drains through to a foul treatment plant. The 'clean' water will overflow to a pump chamber and the treated foul water will be pumped to a break chamber and flow into the stream. Due to level constraints, it is not possible to use a gravity system only. The pump will also be utilised to discharge storm water. The treatment plant will be installed a minimum 10m from the proposed dwelling and 10m from the stream. This strategy complies with Planning condition 8. Approval from Building control will be required. An Environment



Agency Permit is not required to discharge to the surface water as the domestic sewage discharge is less than 5 cubic metres a day and the proposals meet all the general binding rules.

The flow rate is based on peak discharge average over an 8-hour period which reflects a typical period of occupation and allows a more conservative value where residents spend the majority of the day on site.

Foul discharge rate = (6 persons x 150 ltrs x 6 dry weather factor) / (8x60x60) = 0.19 l/s

### Foul discharge rate = 0.19 l/s

There will be a minimal foul flow from the single new plot. This is under the treatment plant daily capacity of  $0.9m^3$ . This strategy conforms to LLFA comments on Planning application P23/00673/F (09/03/2023).

Refer to Appendix C for foul drainage layout arrangement.

Refer to Appendix D for details on the Package treatment plant.

The pump specification provided by Duty Point for the packaged pump chamber is reference in Appendix K.



# 4. STORM DRAINAGE

### 4.0 Storm Water Design Objective

The objective of the drainage strategy is to provide guidance on how the proposed development site could effectively drain through on-site sustainable drainage techniques and to off-site drainage infrastructure, based on the drainage and ground condition information collected and reviewed to date. This document includes a fixed and calculated drainage strategy, in line with current legislation. The design of a successful compliant drainage system for this site is entirely dependent on sustainable drainage principles and requirements being fully incorporated into the site layout to meet the provisions of the Local Planning Authority and the Flood and Water Management Act 2010.

### (a) 4.1 Suitable run-off destinations

An appraisal has been undertaken to confirm the most suitable and sustainable method for managing surface water runoff from the development in accordance with the following hierarchy as highlighted in Part H of Building Regulations and the National Planning Policy Framework (NPPF):

- 1. Infiltration to the ground using a sustainable drainage system.
- 2. If this is not feasible, discharge to a watercourse or river; generally, at a controlled rate unless it does not affect flood risk e.g., if to the sea or an estuary.
- 3. Discharge at a controlled rate to a surface water sewer or drain.
- 4. Discharge at a controlled rate to a combined sewer system, with the approval from the Water Authority.
- 5. Only if the above have all been investigated and it has been proved that none of these options are suitable will discharge at a controlled rate to a foul sewer system, with the approval from the Water Authority.

The techniques consider the use of soakaways in accordance with the Building Regulations Approved Document H order of priority. As mentioned in Section 2.3, the existing ground conditions are not suitable for the use of soakaways. Consequently, storm water will discharge to the existing ditch.

The discharge of surface water run-off has been considered in accordance with the hierarchical approach:

Method	Reasoning	
Interception / Re-use	Deemed inappropriate.	Х
Infiltration	Ground is not suitable for infiltration methods	Х
Surface water body	Ditch connected to southern stream and culvert	$\checkmark$
To dedicated surface water sewer (public, highways or otherwise)	There is no storm sewer in the vicinity	Х
To a combined sewer	There is no combined sewer in the vicinity	Х
To a foul sewer	There is no foul sewer in the vicinity	Х

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### 4.3 Suitability of SuDS components

The drainage design should adopt the principles of SuDS where appropriate taking into consideration the site context and location. The principals of SuDS are that they should be designed to maximise the opportunities and benefits that can be secured surface water run-off management in terms of quality, quantity, flood risk, and amenity.

The implementation and selection of SuDS techniques is largely dependent on the site layout and context. Some SuDS techniques may be more appropriate than others.

### The suitability of SuDS components has been assessed as follows:

Hierarchy	Description	Setting	Required area	Implemented	
Green roofs	A planted soil layer is constructed on the roof of a building to create a living surface. Water is stored in the soil layer and absorbed by vegetation.	Building	Building integrated.	No. Architect to consider use of green roofs	X
Rainwater harvesting	Rainwater is collected from the roof of a building or from other paved surfaces and stored in an over ground or underground tank for treatment and reuse locally. Water could be used for toilet flushing and irrigation.	Building	Water storage (Underground or above ground).	No. Due to use as residential housing rainwater harvesting considered impractical. It is advised for water butts to be installed at rainwater pipe locations where possible	Х
Soakaway	A soakaway is designed to allow water to quickly soak into permeable layers of soil. Constructed like a dry well, an underground pit is dug filled with gravel or tank installed (i.e. cellular storage). Water can be piped to a soakaway where it will be stored and allowed to gradually seep into the ground.	Open space	Dependent on runoff volumes, water table and soils.	No. Soakaways are not suitable at this location	X
Filter Strips	Filter drains are shallow stone filled trenches that provide attenuation, conveyance and treatment of runoff	Open space	Dependent on runoff volumes	Yes for hardstanding areas and protect building from overland flows from adjacent fields	~
Permeable paving	Paving which allows water to soak through. Can be in the form of paving blocks with gaps between solid blocks or porous paving where water filters through the block itself. Water can be stored in the sub-base beneath or allowed to infiltrate into ground below.	Street / open space	Can typically drain double its area.	Yes.	$\checkmark$



					_
Hierarchy	Description	Setting	Required area	Implemented	
Bioretention area or Raingardens	A vegetated area with gravel and sand layers below designated to channel, filter and cleanse water vertically. Water can infiltrate into the ground below or drain to a perforated pipe and be conveyed elsewhere. Bioretention systems can be integrated with tree- pits or gardens.	Street / open space	Typically, surface area is 5-10% of drained area with storage below.	No. Landscape Architect to consider	Х
Swale/Raingarden	Swales and raingardens are shallow depressions designed to convoy and filter water. These can be 'wet' where water gathers above the surface, or 'dry' where water gathers in a gravel layer beneath. Can be lined or unlined to allow infiltration.	Street / open space	Account for width to allow safe maintenance typically 2–3 metres wide.	No, levels constraints,	Х
Hardscape storage	Hardscape water features can be used to store run-off above ground within a constructed container. Storage features can be integrated into public realm areas with a more urban character.	Street / open space	Could be above or below ground and sized to storage need.	No. Below ground storage considered preferable visually and due to limited space.	Х
Pond / Basin	Ponds can be used to store and treat water. 'Wet' ponds have a constant body of water and run-off is additional, while 'dry' ponds are empty during periods without rainfall. Ponds can be designed to allow infiltration into the ground or to store water for a period of time before discharge.	Open space	Dependent on runoff volumes and soils.	No. Levels constraints, and insufficient space	X
Wetland	Wetlands are shallow vegetated water bodies with a varying water level. Specially selected plant species are used to filter water. Water flows horizontally and is gradually treated before being discharged. Wetlands can be integrated with a natural or hardscape environment.	Open space	Typically, 5– 15% drainage area to provide good treatment.	No. Insufficient space within landscaping scheme for a wetland.	X
Underground storage	Water can be stored in tanks, gravel or plastic crates beneath the ground to provide attenuation.	Open space	Dependent on runoff volumes and soils.	Yes. Cellular storage will be utilised	$\checkmark$

### 4.4 Storm Water Design Strategy

Storm water from the dwelling roof is to discharge a below ground system and outfall to the stream at a controlled discharge rate, similar to greenfield runoff. Storm water will be attenuated using cellular units located in the gardens and will provide attenuation for 1 in 100 year storm events plus 45% climate change allowance. The driveway catchment area will discharge to a filter drain. This will aid in slowing down storm water, provide improved water quality to the outfall and provide some additional storm water attenuation using the 30% void content in the filter stone medium. This drain discharge to the cellular storage. Due to level constraints a pump and rising main will be installed downstream of the discharge control chamber and be pumped to a break chamber upstream of a headwall into the stream.

Refer to Appendix C for drainage layout.



### 4.5 Storm Water Design Parameters

The key design parameters for any new storm water drainage shall be:

- No surcharge within the pipe network up to and including a 1:2-year storm event;
- No flooding of the drainage system up to and including a 1:30 year storm event
- No flooding of the drainage system up to the 1:100-year storm event, and

National Planning Policy requires an allowance for the potential impact of climate change on the surface water runoff. This is a critical part of any assessment of flood risk. In accordance with Table 5 of the Planning Policy Technical Guidance, the following climate change allowance will be included in the infrastructure design for the proposed development.

• Surface Water Drainage: additional peak rainfall intensity added = 45%

The proposed storm water drainage has been modelled in Microdrainage software to size the drainage system and calculate the size of the attenuation needed. Refer to Appendix F. Calculations have been carried out for the whole catchment area mentioned above and show no flooding for 1 in 100 year storm event plus 45% allowance for climate change.

This strategy complies with Somerset Council requirements. The storm system will remain private and will not be offered for adoption.

### 4.7 Storm Water Design Parameters

The impermeable storm water catchment areas post-development are summarised in Table 2 below and shown in Appendix G: -

Post-Development Catchment	Area (m2)		
New dwelling	145		
Driveway and hardstanding areas	285		
Total surface water Area	430m <sup>2</sup> = 0.043 ha		
<b>T</b> / / <b>D</b> O			

Table 2: Summary of catchment areas

The existing roof and hardstanding area from the existing building discharges directly to the ground surface which is either positively drained by land drain in the yard area and outfalls into the stream, or, overflows directly into the ditch.

In accordance with South Gloucestershire Local Flood and Risk Management Strategy it is best practise to restrict storm water from site into the ditch at greenfield runoff rate QBAR, where possible. The greenfield runoff rate has been based on the above catchment area using ICP SUDS Mean Annual Flood software as follows: -

- QBAR = 0.5 l/s
- Q30 = 0.7 l/s
- Q100 = 0.8 l/s

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An orifice plate design with a hole has been design to restrict flow on the outgoing pipe. A restricted discharge rate of 0.5 l/s acquires an orifice plate less than 14mm. This is deemed a high flood risk item as the orifice is highly likely to frequently get blocked. Instead, the proposed restricted discharge rate has been increased marginally to 1 l/s. This allows for a 20mm orifice. This is a minor departure from Flood and Risk Management Strategy and consequently is to be approved by Building control. This rate is **substantially better** than the existing discharge rate from the existing barn and yard where there is no restricted discharge rate. A proposed restricted discharge rate of 1 l/s is therefore a betterment than the existing arrangement.

Where possible it is preferred to increase the permitted discharge to 5 l/s to further mitigate flood risk and will also decrease attenuation volume requirements. This is subject to LPA approval.

A proposed restricted discharge rate of 1 l/s is a betterment >40% than the existing arrangement.

### 4.5 Pollution Control measure

Incorporation of a filter drain for the access driveway, provides a natural filtration as rain water passes through the stone medium of the drain. This removes pollutants and impurities from the water, which can stop water pollution.

As an additional measure it is proposed to install a catchpit chamber to capture and retain sediments, trash and floatables from surface water runoff prior to the soakaway.

### 4.6 Exceedance routes

"It is inevitable that as a result of extreme rainfall the capacities of sewers, covered watercourses and other drainage systems will be exceeded on occasion. Periods of exceedance occur when the rate of surface runoff exceeds the drainage system inlet capacity, when the pipe system becomes overloaded, or when the outfall becomes restricted due to flood levels in the receiving water. Underground conveyance cannot economically or sustainably be built large enough for the most extreme events and, as a result, there will be occasions when surface water runoff will exceed the design capacity of drains. When drainage exceedance capacity is exceeded the excess water (exceedance flow) is conveyed above ground, and will travel along streets and paths, between and through buildings and across open space. Indiscriminate flooding of property can occur when this flow of water is not controlled." (CIRIA C753).

Surface levels will be designed to ensure finished levels fall away from the buildings to ensure excessive amount of surface water flow away from the building. Overland flow routes move away from the buildings to the southern and western boundary and flows into the ditch, watercourse and highway to the south. Refer to Appendix H.



### 4.7 Environment Agency Flood Risk Zone

The site development is less than 1 hector and is located within Flood zone 1, an area shown to be at less than 0.1% chance of flooding in any year. No Flood risk assessment is required for this site. Refer to Appendix I for Environment Agency data.

### 4.8 Maintenance and operation

The drainage system will be surveyed on completion to ensure that the system is fully operational and maintenance schedules provided in the O&M manual for the owner to maintain the drainage system. The new home owner will be responsible for maintaining SuDS on site, or using a specialist contractor to maintain the drainage systems. Refer to Appendix J for operation and maintenance schedule which shows the management and maintenance plan for the lifetime of the development SuDS and includes details of land ownership; maintenance responsibilities/arrangements for adoption by any public body or statutory undertaker, or any other arrangements to secure the operation of the sustainable urban drainage scheme throughout its lifetime; together with a description of the system, the identification of individual assets, services and access requirements and details of routine and periodic maintenance activities.

### 5. CONCLUSION

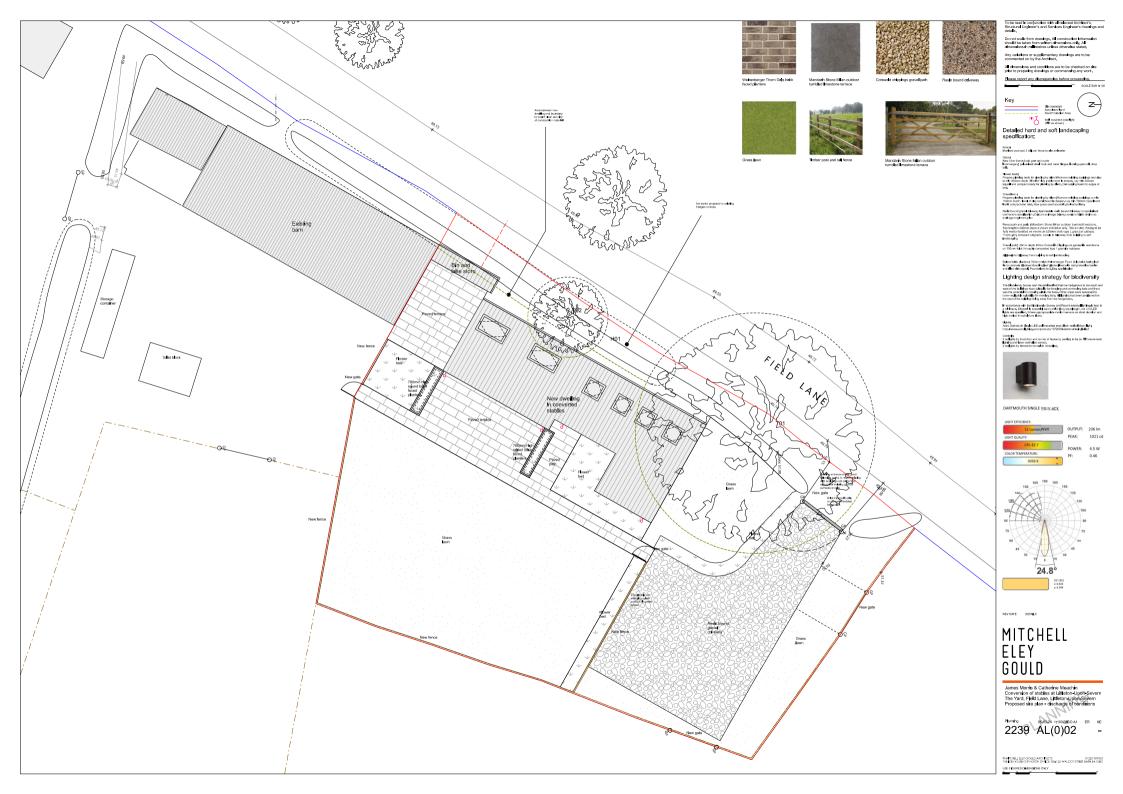
Storm water from the roof areas and driveway is to discharge to the southern perimeter historic stream at a restricted discharge of 1 l/s. During storm events rain water is attenuated within SuDS systems which has capacity for a 1 in 100 year storm event +45% climate change allowance. This achieves at least a 40% betterment than the existing arrangement. Approval from South Gloucestershire County Building Control is required.

Foul water is to discharge into a foul water treatment plant, and pump clean water to the southern boundary ditch. Approval from South Gloucestershire County Building Control is required.



# 6. APPENDIX A

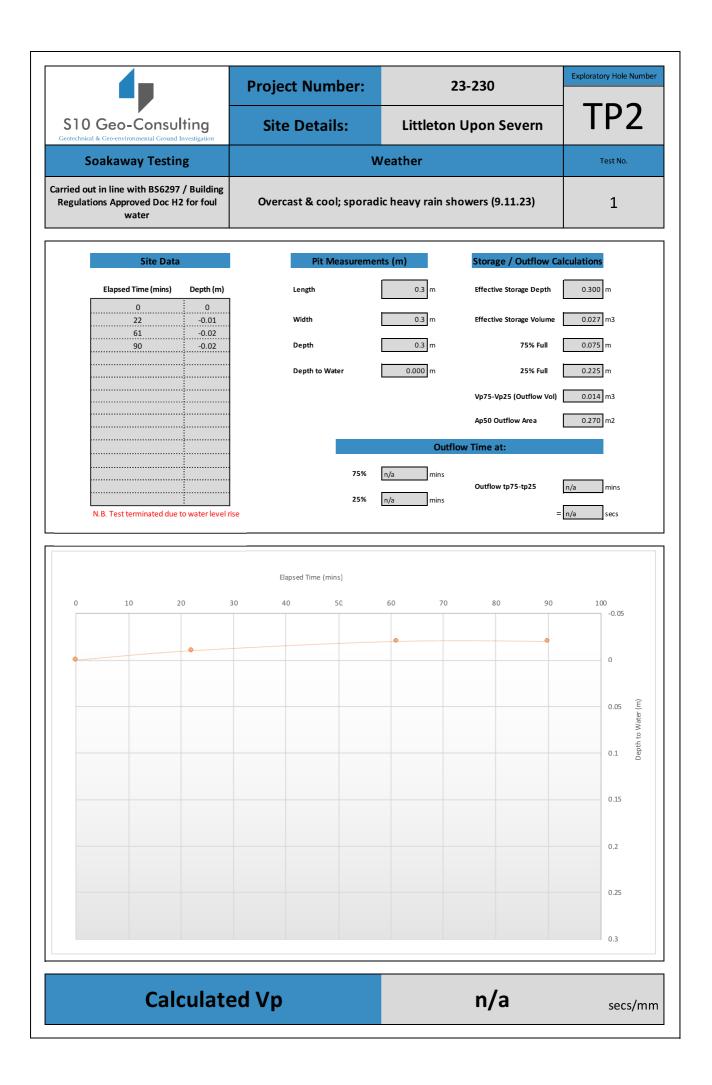
(Architects Layout)





# 7. APPENDIX B

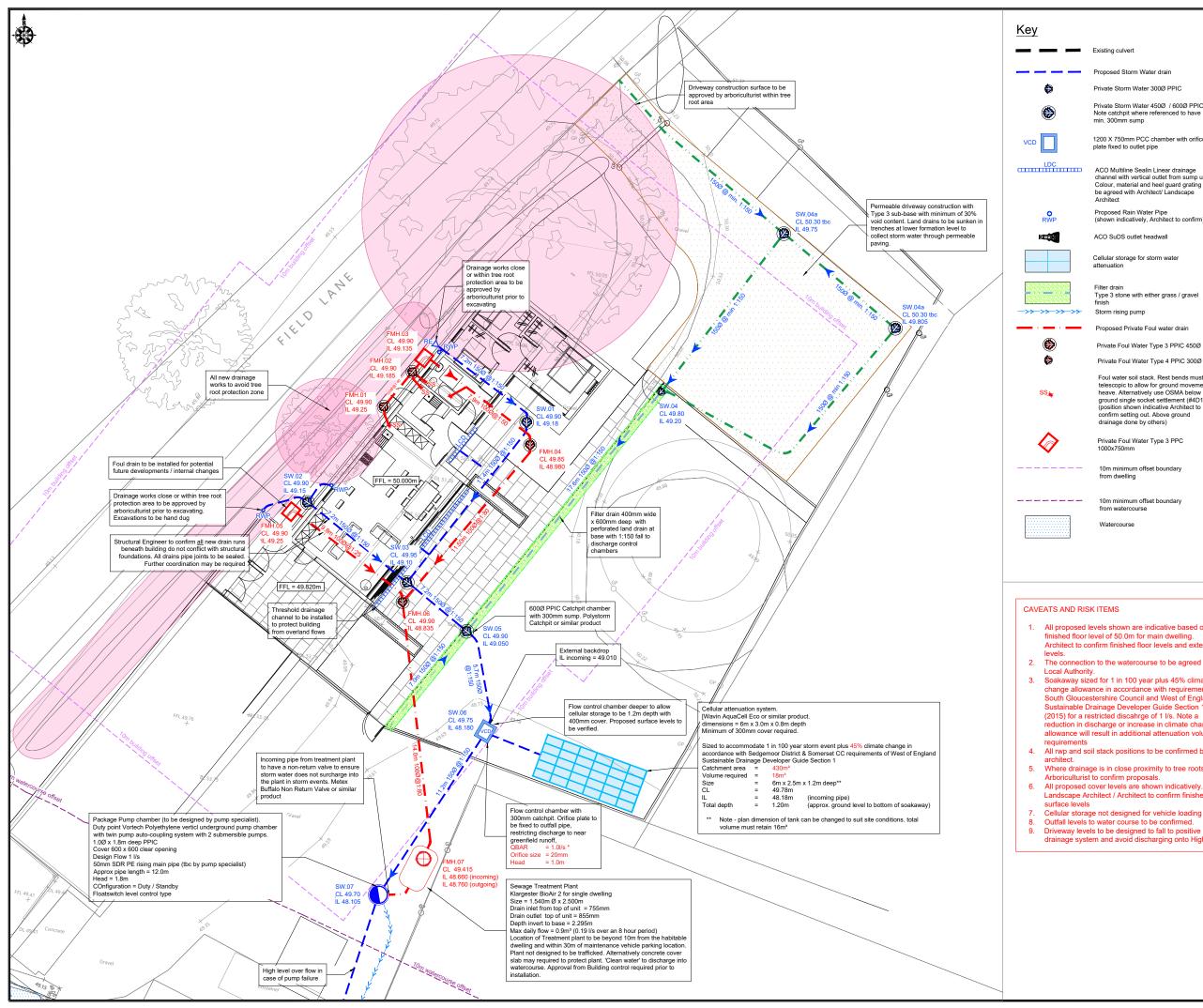
(Infiltration Test)





# 8. APPENDIX C

(Drainage Layout)



Existing culvert

Proposed Storm Water drain

Private Storm Water 300Ø PPIC

Private Storm Water 450Ø / 600Ø PPIC Note catchpit where referenced to have min. 300mm sump

1200 X 750mm PCC chamber with orifice plate fixed to outlet pipe

ACO Multiline Sealin Linear drainage channel with vertical outlet from sump unit. Colour, material and heel guard grating to be agreed with Architect/ Landscape Architect

Proposed Rain Water Pipe (shown indicatively, Architect to confirm)

ACO SuDS outlet headwall

Cellular storage for storm water

Filter drain Type 3 stone with either grass / gravel

Storm rising pump

Proposed Private Foul water drain

Private Foul Water Type 3 PPIC 450Ø Private Foul Water Type 4 PPIC 300Ø

Foul water soil stack. Rest bends must be telescopic to allow for ground movement / heave. Alternatively use OSMA below ground single socket settlement (#4D115) (position shown indicative Architect to confirm setting out. Above ground drainage done by others)

Private Foul Water Type 3 PPC 1000x750mm

10m minimum offset boundary from dwelling

10m minimum offset boundary from watercourse

Watercourse



### lotes

- This drawing is to be read in conjunction with relevant Architects, Engineers and All levels are shown in meters above Ordnance Datum (m AOD) unless otherwise shown. Any ambiguities or discrepancies within this drawing and any other information given ele-
- Instal Englished ing is communication of protein a factor of the second second
- It is recommended that all servers to the new development. The existing severational and working updream to the new development. All private drainage to comply with current Building Regulations and relevant British Standards an Codes of Practices. Connections to existing severs in accordance with the Local Water Authority guidelines.
- Connections to existing severe in accordance with the Local Water Autoryt guidelines & approximation of the several several
- A M access chambers covers and frames to be instabled to BSE 191 1/3.
  A M access chambers covers and frames to be instabled to BSE 191 1/3.
  A model to BSE 101 1/3.
  A model to BSE 101 1/3.
  B model to BSE 101 1/3.
  <

- excavating around existing services. It is the contactors and depth of all existing services, mains and cables prior to construction. Services in the service of the service of the devise stream manholes during the construction prior of the development in accordance with SFA 2.8.10 and the local serverage undertakes requirements. The pipe diameters over and invert levels of any existing manholes are to be verified on site prior to the pipe diameters.
- The pipe dualities over a link a link terms of any examplinations are to be related on size pip to the commencement of the works. All external drainage within trafficied areas with less than 1.2m cover to have type Z cover an surround. All external drainage within landscaped areas with cover less than 0.8m to have type C cover and surround. All drainage with greater cover than the minimum required to have type S b and surround.
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- n. levels are indicative, to be confirmed and coordinated with Las . All cover Arabitest

### CDM Residual Risks & Hazards

See project specific Mesh Engineering Ltd Specification document for CDM residual risks and hazards.

Project specific hazards are indicated on this drawing by an exclamation n within a triangle adjacent box notes.

### General notes :-

Do not scale off this drawing

Contractors to check all dimensions on site prior to fabrications and report any errors/ommissions to the engineer prior to construction.

This drawing is to be read in conjunction with all relevant Mesh Engineerir Ltd and architects drawings

Driveway updated to permeable paving	P07	GJ	19.03.2024
Site plan updated	P06	GJ	05.03.2024
Climate change allowance increased, discharge reduced, cellular storage increased	P05	GJ	03.03.2024
Tree protection areas updated	P04	GJ	02.01.2024
Revisions	Ref	Initial	Date



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James Morris & Catherine Meachin

Drainage Layout Sheet 1

### The Yard, Littleton Upon Severn Conversion of Stable

Drawing status	N				
Scale at A1 1:100	Scale at A3 1/2 Shown	Draw GJ	n by	Checke PH	ed by
Date 23.11.2023	Project number 2239		Drawing		Rev. P07

All proposed levels shown are indicative based on a finished floor level of 50.0m for main dwelling. Architect to confirm finished floor levels and external

The connection to the watercourse to be agreed with

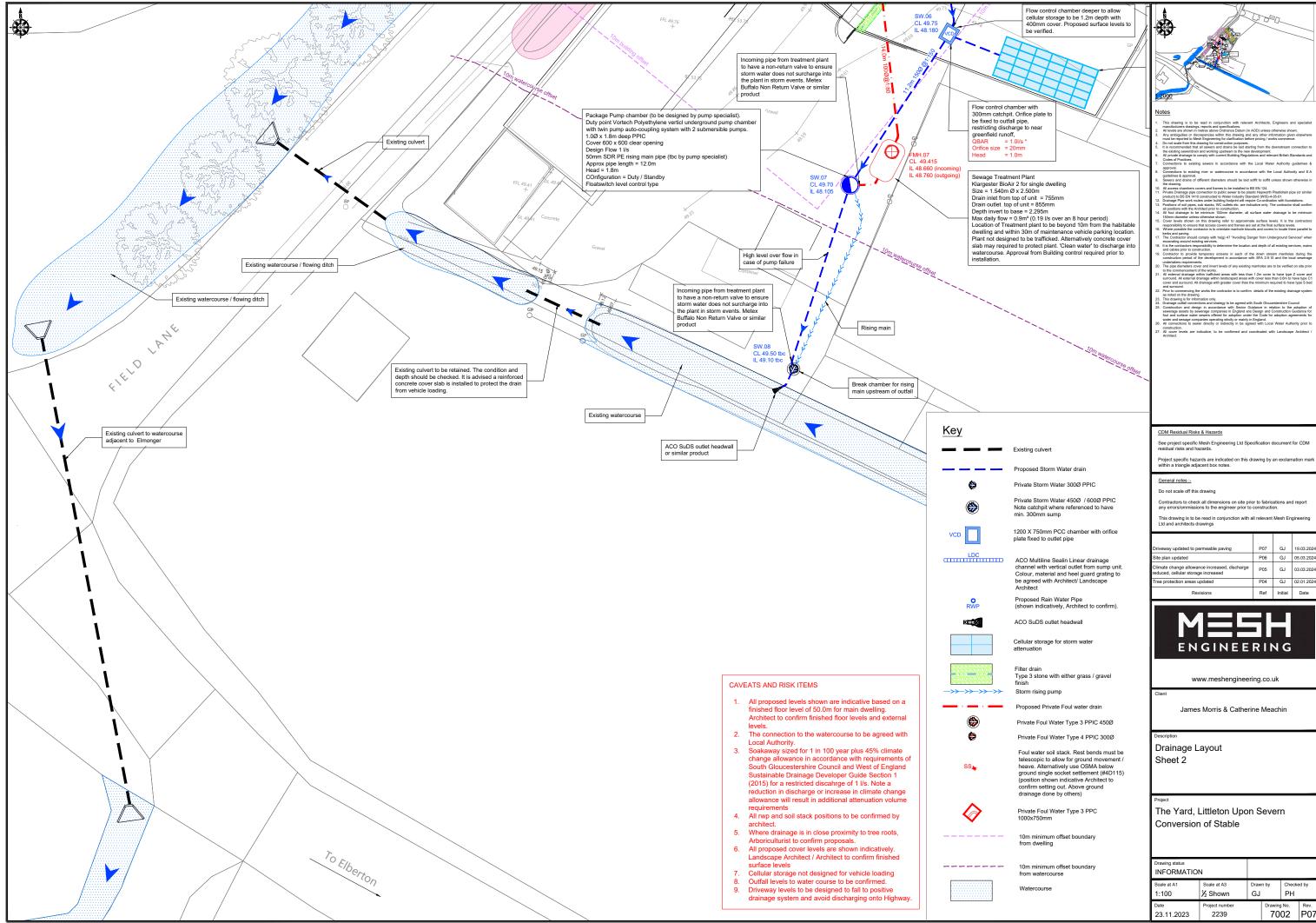
Soakaway sized for 1 in 100 year plus 45% climate change allowance in accordance with requirements of South Gloucestershire Council and West of England Sustainable Drainage Developer Guide Section 1 (2015) for a restricted discahrge of 1 l/s. Note a reduction in discharge or increase in climate change allowance will result in additional attenuation volume

All rwp and soil stack positions to be confirmed by

Where drainage is in close proximity to tree roots, Arboriculturist to confirm proposals. All proposed cover levels are shown indicatively.

Landscape Architect / Architect to confirm finished

Outfall levels to water course to be confirmed. Driveway levels to be designed to fall to positive drainage system and avoid discharging onto Highway



Driveway updated to permeable paving	P07	GJ	19.03.2024
Site plan updated	P06	GJ	05.03.2024
Climate change allowance increased, discharge reduced, cellular storage increased	P05	GJ	03.03.2024
Tree protection areas updated	P04	GJ	02.01.2024
Revisions	Ref	Initial	Date

Drawing status	N				
Scale at A1 1:100	Scale at A3 1/2 Shown	Draw GJ	n by	Checke PH	ed by
Date 23.11.2023	Project number 2239		Drawing		Rev. P07



# 9. APPENDIX D

(Foul Water Treatment Plant Specification)

### **BIOAIR 2, 3 & 5 MDPE - DECLARATION OF PERFORMANCE**

kingspan-klargester-bioair-2-3-5-dop-en-Mar2023-v1

1. Unique identification code of the product-type:

### Wastewater Treatment Plant for 6, 9 & 15 Population Equivalents BioAir 2 (6PE) & BioAir 3 (9PE) & BioAir 5 (15PE)

2. Type, batch or serial number or any other element allowing identification of the construction product as required under Article 11(4) of the CPR:

### BioAir Prefabricated Domestic Wastewater Treatment Plant: See CE marking affixed to product BioAir 2 (6PE) & BioAir 3 (9PE) & BioAir 5 (15PE)

3. Intended use/es of the product, in accordance with the applicable harmonized technical specification, as foreseen by the manufacturer:

### To be used for Collection & Treatment of Wastewater from Domestic applications up to 15 Population Equivalent

4. Manufacturer name, registered trade name or registered trademark and contact address as required under Article 11(5):

### Kingspan Water & Energy Ltd College Rd North Aston Clinton, Aylesbury, Buckinghamshire HP22 5EW

5. Where applicable, name and contact address of the authorised representative whose mandate covers the tasks specified in Article 12(2):

### N/A

6. System/s of assessment and verification of constancy of performance (AVCP) of the product as set out in CPR, Annex V:

3

7. In case of the declaration of performance concerning a construction product covered by a harmonised standard:

### EN:12566-3:2005+A2:2013

Notified body/ bodies:

### Notified Body No: 1739 + PIA Prüfinstitut für Abwassertechnik GmbH



Document date:	Document version no:	ECN no:
01 March 2023	V1.	NA

8. Declared performance/s:

Essential cho	aracteristics	Perf	Harmonised technical specification	
Structural I	Behaviour	Condition Height of Backfi BioFicient+2 = 1.26m r WET - BioFicient+2 : level from	Test under the following is - 1.5m Invert: ill (from top of Tank) - (Includes using extension necks) : 2.0m - Maximum water in bottom of the he Tank (top of tank itself)	
Reactio	n to fire		Class F	
Water Tightnes		Water Tig		
Material I		MFR (230/2,16) = (4 Density ≥ 930 k Tensile Strength	EN:12566- 3:2005+A2:2013	
	COD	93.2%	57 mg/l	
	BOD5	97.5%	9 mg/l	
Treatment	TN <sub>b</sub> **	<b>60</b> .1%	25.4 mg/l	
Efficiency	NH <sub>4</sub> -N	67.6%	15.6 mg/l	
	Ptot SS	46.9%	4.3 mg/l 16 mg/l	
		95.9% **determined for te 12° C in		
Electrical Co (measured durin		1.:	2kWh/d	
Emission of Substa	Dangerous		NPD	

9. The performance of the product identified in points 1 and 2 is in conformity with the declared performance in point 8. This declaration of performance is issued under the sole responsibility of the manufacturer identified in point 4.

Signed for and on behalf of the manufacturer by:

SIN.Ah

David Anderson - Water Business Unit Director

At Portadown on 01 March 2023



Document date:	Document version no:	ECN no:
01 March 2023	V1.	NA

Water Management Solutions

# *Klargester* BioAir Sewage Treatment Plant

The new Klargester BioAir wastewater treatment plant uses aerated technology to deliver a high level of water discharge quality. Offering flexible installation options to suit a variety of domestic sites and a low impact visual footprint, Klargester BioAir is a cost-efficient choice for your domestic wastewater treatment solution.



conomically pric<u>ed</u>

## Suitable for installation in traffic areas\* \*Structural advice

required

\*3 years on Premium model only, 12 months for economy





UP TO

PRANTY PE

ΥR

6C years

FTPERIENCE

-An



kingspan.com

# Technical Information

Applications

The Klargester BioAir 2-8 range is suitable for use across the following applications:

Single & Multiple Homes

Light Industrial Premises



Farms



Product features

97.5%





10



Improved effluent quality - BOD<sub>5</sub> 97.5%

Third party tested to EN 12566-3





Affordable service plans available

BioAir	Model	BioAir 2	BioAir 3	BioAir 4	BioAir 5	BioAir 6	BioAir 7	BioAir 8
Population Equivalent	Unit	6	9	12	15	20	25	35
Daily Flow	m³/d	0.9	1.35	1.8	2.25	3	3.75	5.25
Daily Load	kg BOD₅/d	0.36	0.54	0.72	0.9	1.2	1.5	2.1
Measurements								
Inlet Invert	mm	455-755	575-875	500-2000	645-945	500-2000	500-2000	500-2000
Discharge Option		Gravity /IPS	Gravity /IPS	Gravity /IPS	Gravity /IPS	Gravity	Gravity	Gravity
Outlet Invert	mm	555-855 /400-700	675-975 / 350-650	600-2100	745-1045 / 415-715	600-2100	600-2100	600-2100
Diameter	mm	1540	1690	1920	2010	1920	1920	1920
Length	mm	2500	2480	3238	3190	4400	5550	7400
Installation Depth	mm	1805-2105	2075-2375	2245-3745	2485-2785	2245-3745	2245-3745	2245-3745
Inlet Pipework	mm	Ø110	Ø110	Ø110	Ø110	Ø110	Ø110	Ø160
Outlet Pipework (Gravity /IPS)	mm	Ø110 / Ø50	Ø110 / Ø50	Ø110 /Ø50	Ø110 / Ø50	Ø110	Ø110	Ø160
Material Construction	MDPE/GRP	MDPE	MDPE	GRP	MDPE	GRP	GRP	GRP
Unit Weight	kg	170	200	500**	650	800**	1250**	1450**

\*BioAir 5 subject to availability \*\*Tank weight based on 500mm invert

For more information on our new Klargester BioAir: T: +44 (0) 1296 633 033 E: klargester@kingspan.com W: Kingspan.co.uk/Klargester





# 10. APPENDIX E

(Greenfield Runoff)

-		Page 1
•	Greenfield runoff	
	The Yard Field Lane	
	Littleton Upon Severn	Micro
Date 18/12/2023 08:55	Designed by G.Jones	Drainage
File	Checked by	Diamage
Innovyze	Source Control 2020.1.3	
<u>icp su</u>	DS Mean Annual Flood	
	Input	
	rs) 100 Soil 0.400 ha) 0.043 Urban 0.750 mm) 800 Region Number Region 8	

### Results 1/s

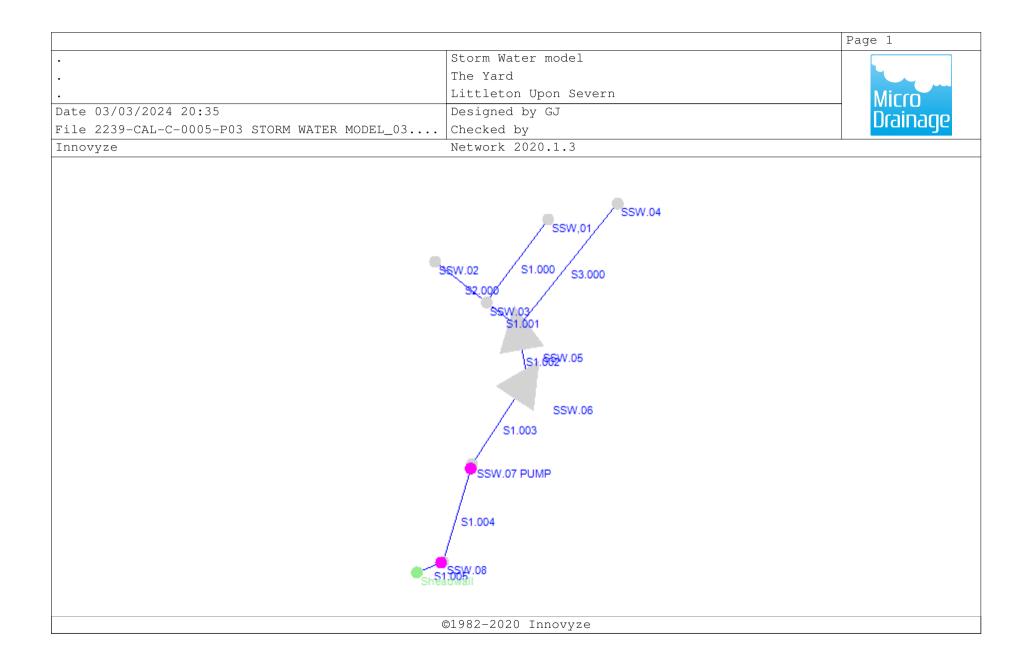
QBAR Rural 0.2 QBAR Urban 0.5 Q100 years 0.8 Q1 year 0.4 Q30 years 0.7 Q100 years 0.8

©1982-2020 Innovyze



# 11. APPENDIX F

(Microdrainage Calculations)



											Pag	je u
	_	_	_	_		orm Model	_			_		
					Th	e Yard						
					Li	ttleton Up	on Se	evern			Mi	icro
ate 03	3/03/20	)24 20	):33		De	signed by	GJ					ainag
ile 22	239-CAI	L-C-00	)05-P(	)3 STO	Ch	ecked by						מוו ומע
Innovyz	ze				Ne	twork 2020	.1.3					
	Ma m Time o Vo	n Crit Retur aximum of Conc Foul olumetr	Pip F rn Per: Rainfa centra L Sewac ric Run	for 2 be Sizes TSR Rain M5-60 Rat. all (mm tion (m ge (1/s noff Con De m for	239-CAI s STANDAH nfall Mod ars) (mm) 20. io R 0. /hr) ins) /ha) 0. eff. 0. signed w	AL-C-0005-	01 ST Sizes S ad and Add F Min Max ign De Vel fo n Slop offits	ORM W STANDA Wales low / imum H imum H pth fc r Auto e for	RD Clim Backd Backd Dr Op Des Opti:	ate Ch rop He rop He timisa ign on misati	EL.SWS PIMP (: ange (: ight () ight () tion () ly (m/ on (1:	- %) 10 %) m) 0.20 m) 0.20 m) 1.20 s) 0.7 X) 50
				(1	mins) (h							
Ne	twork	Desig	m Tak	Total A Tota	0-4 0. Area Cont al Pipe V	029 4-8 tributing (h	0.014 na) = C = 1.26	8	M WA	TER M	10DE1.	SWS
<u>N</u> e	Length	Fall	Slope	Total A Tota Die for I.Area	0-4 0. Area Cont al Pipe V r 2239-	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base	0.014 aa) = 0 = 1.26 5-P01 <b>k</b>	STOR	DIA		10DEL.	e Auto
				Total A Tota Die for I.Area	0-4 0. Area Cont al Pipe V r 2239-	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005	0.014 a) = 0 = 1.26 5-P01	58 STOR				
PN	Length	Fall (m)	Slope (1:X)	Total Z Tota Dle for I.Area (ha)	0-4 0. Area Cont al Pipe v r 2239- r T.E. (mins)	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s)	0.014 aa) = 0 = 1.26 5-P01 <b>k</b>	STOR	DIA (mm)	Secti		e Auto Desig
<b>PN</b> S1.000	Length (m) 11.362	Fall (m) 0.080	Slope (1:X) 142.0	Total A Tota Dle for I.Area (ha) 0.006	0-4 0. Area Cont al Pipe v <u>r 2239-</u> <b>t T.E.</b> (mins) 5 5.00	029 4-8 tributing (h Volume (m <sup>3</sup> ) <u>CAL-C-0005</u> Base Flow (l/s) 0.0	0.014 aa) = 0 = 1.26 5-P01 <b>k</b> (mm) 0.600	STOR HYD SECT 0	DIA (mm) 150	Secti Pipe/	<b>.on Typ</b> 'Condui	e Auto Desig t <b>ê</b>
PN	Length (m) 11.362	Fall (m)	Slope (1:X) 142.0	Total A Tota Dle for I.Area (ha) 0.006	0-4 0. Area Cont al Pipe v <u>r 2239-</u> <b>t T.E.</b> (mins) 5 5.00	029 4-8 tributing (h Volume (m <sup>3</sup> ) <u>CAL-C-0005</u> Base Flow (l/s) 0.0	0.014 (mm)	STOR HYD SECT	DIA (mm) 150	Secti Pipe/	on Typ	e Auto Desig t <b>e</b>
<b>PN</b> S1.000	Length (m) 11.362 7.233	Fall (m) 0.080 0.050	<b>Slope</b> (1:X) 142.0 144.7	Total <i>A</i> Tota <u>ole for</u> <b>I.Area</b> (ha) 0.006	0-4 0. Area Cont al Pipe 7 <u>r 2239-</u> <b>r T.E.</b> (mins) 5 5.00	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s) 0.0 0.0	0.014 aa) = 0 = 1.26 5-P01 <b>k</b> (mm) 0.600	STOR HYD SECT 0	<b>DIA</b> (mm) 150 150	Secti Pipe/ Pipe/	<b>.on Typ</b> 'Condui	e Auto Desig t <b>e</b>
PN \$1.000 \$2.000 \$1.001	Length (m) 11.362 7.233 4.404	<b>Fall</b> (m) 0.080 0.050 0.050	<b>Slope</b> (1:X) 142.0 144.7 88.1	Total A Tota Dle for I.Area (ha) 0.006 0.010 0.000	0-4 0. Area Cont al Pipe 7 r 2239- r T.E. (mins) 5 5.00 0 5.00	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s) 0.0 0.0	0.014 $aa) = 0$ $= 1.26$ $5-P01$ k (mm) 0.600 0.600 0.600	STOR HYD SECT 0 0	<b>DIA</b> (mm) 150 150	Secti Pipe/ Pipe/ Pipe/	<b>.on Typ</b> Condui Condui	e Auto Desig t e t
PN \$1.000 \$2.000 \$1.001	Length (m) 11.362 7.233	<b>Fall</b> (m) 0.080 0.050 0.050	<b>Slope</b> (1:X) 142.0 144.7 88.1	Total A Tota Dle for I.Area (ha) 0.006 0.010 0.000	0-4 0. Area Cont al Pipe 7 r 2239- r T.E. (mins) 5 5.00 0 5.00	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s) 0.0 0.0	0.014 aa) = 0 = 1.26 5-P01 <b>k</b> (mm) 0.600 0.600	STOR HYD SECT 0 0	<b>DIA</b> (mm) 150 150	Secti Pipe/ Pipe/ Pipe/	<b>.on Typ</b> Condui Condui	e Auto Desig t e t
PN \$1.000 \$2.000 \$1.001	Length (m) 11.362 7.233 4.404	<b>Fall</b> (m) 0.080 0.050 0.050	<b>Slope</b> (1:X) 142.0 144.7 88.1	Total <i>A</i> Tota Dele for <b>I.Area (ha)</b> 0.006 0.010 0.000 0.016	0-4 0. Area Cont al Pipe V r 2239- r T.E. (mins) 5 5.00 0 5.00 0 0.00 5 5.00	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s) 0.0 0.0	0.014 $aa) = 0$ $= 1.26$ $5-P01$ $k$ (mm) $0.600$ $0.600$ $0.600$ $0.600$	STOR HYD SECT 0 0	<b>DIA</b> (mm) 150 150	Secti Pipe/ Pipe/ Pipe/	<b>.on Typ</b> Condui Condui	e Auto Desig t e t
PN \$1.000 \$2.000 \$1.001	Length (m) 11.362 7.233 4.404	<b>Fall</b> (m) 0.080 0.050 0.050	<b>Slope</b> (1:X) 142.0 144.7 88.1	Total <i>A</i> Tota Dele for <b>I.Area (ha)</b> 0.006 0.010 0.000 0.016	0-4 0. Area Cont al Pipe V r 2239- r T.E. (mins) 5 5.00 0 5.00 0 0.00 5 5.00	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s) 0.0 0.0 0.0 0.0	0.014 $aa) = 0$ $= 1.26$ $5-P01$ $k$ (mm) $0.600$ $0.600$ $0.600$ $0.600$	STOR HYD SECT 0 0	<b>DIA</b> (mm) 150 150	Secti Pipe/ Pipe/ Pipe/	<b>.on Typ</b> Condui Condui	e Auto Desig t e t
PN S1.000 S2.000 S1.001	Length (m) 11.362 7.233 4.404 17.509	Fall (m) 0.080 0.050 0.050 0.150 in T	<b>Slope</b> (1:X) 142.0 144.7 88.1 116.7	Total A Tota Dele for I.Area (ha) 0.006 0.016 0.016 0.016 <u>N</u> US/IL	0-4 0. Area Cont al Pipe V r 2239- r 7.E. (mins) 5 5.00 0 5.00 0 0.00 5 5.00 0 0.00 6 5.00 0 0.00 0 0.00	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.014 aa) = C = 1.26 5-P01 k (mm) 0.600 0.600 0.600 0.600 able Foul	STOR HYD SECT 0 0 0 0 0	DIA (mm) 150 150 150 150	Secti Pipe/ Pipe/ Pipe/ Pipe/	.on Typ 'Condui 'Condui 'Condui 'Condui	e Auto Desig t 0 t 0 t 0 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1
PN \$1.000 \$2.000 \$1.001 \$3.000	Length (m) 11.362 7.233 4.404 17.509	Fall (m) 0.080 0.050 0.050 0.150	<b>Slope</b> (1:X) 142.0 144.7 88.1 116.7	Total A Tota Dele for I.Area (ha) 0.006 0.016 0.016 0.016	0-4 0. Area Cont al Pipe V r 2239- r T.E. (mins) 5 5.00 0 5.00 0 0.00 5 5.00	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s) 0.0 0.0 0.0 0.0 0.0 0.0	0.014 aa) = C = 1.26 5-P01 k (mm) 0.600 0.600 0.600 0.600 able Foul	STOR HYD SECT 0 0 0 0 0	DIA (mm) 150 150 150 150	Secti Pipe/ Pipe/ Pipe/ Pipe/	.on Typ 'Condui 'Condui 'Condui 'Condui	e Auto Desig t 0 t 0 t 0 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1
PN \$1.000 \$2.000 \$1.001 \$3.000	Length (m) 11.362 7.233 4.404 17.509	Fall (m) 0.080 0.050 0.050 0.150	Slope (1:X) 142.0 144.7 88.1 116.7 2.C. hins)	Total A Tota Dele for I.Area (ha) 0.006 0.016 0.016 0.016 <u>N</u> US/IL	0-4 0. Area Cont al Pipe V r 2239- r 7.E. (mins) 5 5.00 0 5.00 0 0.00 5 5.00 0 0.00 6 5.00 0 0.00 0 0.00	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	0.014 aa) = C = 1.26 5-P01 k (mm) 0.600 0.600 0.600 0.600 able Foul	STOR HYD SECT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DIA (mm) 150 150 150 150	Secti Pipe/ Pipe/ Pipe/ Pipe/	.on Typ 'Condui 'Condui 'Condui 'Condui	e Auto Desig t 0 t 0 t 0 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1 t 1
PN \$1.000 \$2.000 \$1.001 \$3.000 PN \$1.0	Length (m) 11.362 7.233 4.404 17.509 I Ra: (mm/	Fall (m) 0.080 0.050 0.150 in T (hr) (m	Slope (1:X) 142.0 144.7 88.1 116.7 2.C. hins) 5.23	Total A Tota Dle for I.Area (ha) 0.006 0.010 0.010 0.010 0.016 <u>N</u> US/IL 3 (m)	0-4 0. Area Cont al Pipe V r 2239- r 7.E. (mins) 5 5.00 0 5.00 0 0.00 5 5.00 0 0.00 6 5.00 0 0.00 6 5.00 0 0.00 6 5.00 0 0.00 6 5.00 0 0.00 6 5.00 0 0.00 6 5.00 1 E E E E E E E E E E E E E E E E E E E	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	0.014 aa) = 0 = 1.26 5-P01 k (mm) 0.600 0.600 0.600 0.600 0.600 0.600 able Foul (1/s) 0.0	STOR HYD SECT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DIA (mm) 150 150 150 150 Flow (s) 0.0	Secti Pipe/ Pipe/ Pipe/ Vel (m/s) 0.84	.on Typ Condui Condui Condui Condui Condui	e Auto Desig t i t t t f t f f f u (1/s)
PN \$1.000 \$2.000 \$1.001 \$3.000 PN	Length (m) 11.362 7.233 4.404 17.509 I Ra: (mm/	Fall (m) 0.080 0.050 0.150 in T (hr) (m	Slope (1:X) 142.0 144.7 88.1 116.7 2.C. hins) 5.23	Total A Tota Dle for I.Area (ha) 0.006 0.016 0.016 0.016 US/IL 1 (m)	0-4 0. Area Cont al Pipe V r 2239- r T.E. (mins) 5 5.00 0 5.00 0 0.00 5 5.00 0 0.00 5 5.00 0 0.00 5 5.00 0 0.00 5 5.00 0 0.00 5 5.00 0 0.00 5 5.00	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	0.014 aa) = 0 = 1.26 5-P01 k (mm) 0.600 0.600 0.600 0.600 0.600 0.600 able Foul (1/s) 0.0	STOR HYD SECT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DIA (mm) 150 150 150 150 Flow (s)	Secti Pipe/ Pipe/ Pipe/ Pipe/ Vel (m/s)	.on Typ Condui Condui Condui Condui	e Auto Desig t i t t t f t f f f u (1/s)
PN \$1.000 \$2.000 \$1.001 \$3.000 PN \$1.0 \$2.0	Length (m) 11.362 7.233 4.404 17.509 J Ra: (mm/ 000 50	Fall (m) 0.080 0.050 0.150 0.150 in T (hr) (m	Slope (1:X) 142.0 144.7 88.1 116.7 2.C. bins) 5.23 4 5.14 4	Total A Tota Dele for I.Area (ha) 0.006 0.010 0.010 0.016 <u>N</u> US/IL 3 (m) 49.180	0-4 0. Area Cont al Pipe V r 2239- A T.E. (mins) 5 5.00 0 5.00 0 0.000 5 5.00 0 0.000 6 5.00 0 0.000 6 5.00 0 0.000 6 5.00 0 0.000 6 5.00 0 0.000 6 5.00	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	0.014 aa) = 0 = 1.26 5-P01 k (mm) 0.600 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000000	STOR HYD SECT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DIA (mm) 150 150 150 150 <b>Flow</b> (s) 0.0 0.0	Secti Pipe/ Pipe/ Pipe/ Vel (m/s) 0.84 0.83	.on Typ Condui Condui Condui Condui Condui 14.9 14.7	e Auto Desig t 0 t 0 t 0 t 1 t 0 t 0 t 0 t 0 t 1.4
PN \$1.000 \$2.000 \$1.001 \$3.000 PN \$1.0	Length (m) 11.362 7.233 4.404 17.509 J Ra: (mm/ 000 50	Fall (m) 0.080 0.050 0.150 0.150 in T (hr) (m	Slope (1:X) 142.0 144.7 88.1 116.7 2.C. bins) 5.23 4 5.14 4	Total A Tota Dle for I.Area (ha) 0.006 0.010 0.010 0.010 0.016 <u>N</u> US/IL 3 (m)	0-4 0. Area Cont al Pipe V r 2239- r 7.E. (mins) 5 5.00 0 5.00 0 0.00 5 5.00 0 0.00 6 5.00 0 0.00 6 5.00 0 0.00 6 5.00 0 0.00 6 5.00 0 0.00 6 5.00 0 0.00 6 5.00 1 E E E E E E E E E E E E E E E E E E E	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	0.014 aa) = 0 = 1.26 5-P01 k (mm) 0.600 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000000	STOR HYD SECT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DIA (mm) 150 150 150 150 Flow (s) 0.0	Secti Pipe/ Pipe/ Pipe/ Vel (m/s) 0.84	.on Typ Condui Condui Condui Condui Condui	e Auto Desig t i t t t t f t f t t t t t t t t t t t t
PN \$1.000 \$2.000 \$1.001 \$3.000 PN \$1.0 \$2.0	Length (m) 11.362 7.233 4.404 17.509 J Ra: (mm/ 000 50 000 50 001 50	Fall (m) 0.080 0.050 0.150 0.150 in T (hr) (m	Slope (1:X) 142.0 144.7 88.1 116.7 2.C. bins) 5.23 5.14 5.29	Total A Tota Dele for I.Area (ha) 0.006 0.010 0.010 0.016 <u>N</u> US/IL 3 (m) 49.180	0-4 0. Area Cont al Pipe V r 2239- A T.E. (mins) 5 5.00 0 5.00 0 0.000 5 5.00 0 0.000 6 5.00 0 0.000 6 5.00 0 0.000 6 5.00 0 0.000 6 5.00 0 0.000 6 5.00	029 4-8 tributing (h Volume (m <sup>3</sup> ) CAL-C-0005 Base Flow (l/s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	0.014 aa) = 0 = 1.26 5-P01 k (mm) 0.600 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000000	STOR HYD SECT 0 0 0 0 0 Add 1 (1/	DIA (mm) 150 150 150 150 <b>Flow</b> (s) 0.0 0.0	Secti Pipe/ Pipe/ Pipe/ Vel (m/s) 0.84 0.83	.on Typ Condui Condui Condui Condui Condui 14.9 14.7 18.9	e Auto Desig t 0 t 0 t 0 t 1 t 0 t 0 t 0 t 0 t 1.4

	C-00	05-P0	3 STO. le for	Th Li De Ch Ne	orm Model e Yard ttleton U signed by ecked by twork 202	Upon Se GJ 20.1.3			TER MC		inago
9-CAL-(	C-00	05-P0		Li De Ch Ne	ttleton U signed by ecked by twork 202	GJ			TER MC	Dra	inago
9-CAL-(	C-00	05-P0		De Ch Ne	signed by ecked by twork 202	GJ			TER MC	Dra	inago
9-CAL-(	C-00	05-P0		Ch Ne	ecked by twork 202	0.1.3	STOP	 	TER MC	Dra	inago
				Ne	twork 202		STOP	 	TER MC		
vork De	esigr	n Tabi	le for				STOP	M WA	TER MC	)DEL.S	WS
vork De	esigr	n Tabi	le for	2239-	-CAL-C-00	)5-P01	STOP	M WA	TER MC	)DEL.S	WS
-		Slope (1:X)	I.Area (ha)			k (mm)	HYD SECT	DIA (mm)	Sectio	n Type	Auto Design
	0.4.0	145 0	0 011	0.00				1.5.0	D: (0		_
									-		<b>0</b> <b>0</b>
			0.000								
3.123 0.	.021	148.7	0.000	0.00	0.	0.600	0	150	Pipe/C	onduit	
			Ne	twork	Results	Table					
Rain			- •							<b>L</b>	Flow
5 L	(m) .808 0 .098 0 .192 0 .123 0 Rain	(m) (m) .808 0.040 .098 0.075 .192 0.075 .123 0.021 Rain T	<pre>(m) (m) (1:X) .808 0.040 145.2 .098 0.075 148.0 .192 0.075 149.2 .123 0.021 148.7 Rain T.C. U</pre>	(m) (m) (1:X) (ha) .808 0.040 145.2 0.011 .098 0.075 148.0 0.000 .192 0.075 149.2 0.000 .123 0.021 148.7 0.000 <u>Ne</u> Rain T.C. US/IL E	(m) (m) (1:X) (ha) (mins) .808 0.040 145.2 0.011 0.00 .098 0.075 148.0 0.000 0.00 .192 0.075 149.2 0.000 0.00 .123 0.021 148.7 0.000 0.00 <u>Network</u> Rain T.C. US/IL E I.Area	(m) (m) (1:X) (ha) (mins) Flow (1/s)          .808 0.040 145.2       0.011 0.00 0.0         .098 0.075 148.0       0.000 0.00 0.0         .192 0.075 149.2       0.000 0.00 0.0         .123 0.021 148.7       0.000 0.00 0.00         Network Results       Network Results         Rain       T.C.       US/IL Σ I.Area       Σ Base	(m)       (m)       (1:X)       (ha)       (mins)       Flow       (1/s)       (mm)         .808       0.040       145.2       0.011       0.00       0.0       0.600         .098       0.075       148.0       0.000       0.00       0.0       0.600         .192       0.075       149.2       0.000       0.00       0.0       0.600         .123       0.021       148.7       0.000       0.00       0.0       0.600         Network       Results       Table         Rain       T.C.       US/IL       E       I.Area       E       Base       Foul	(m) (m) (1:X) (ha) (mins) Flow (1/s) (mm) SECT .808 0.040 145.2 0.011 0.00 0.0 0.600 0 .098 0.075 148.0 0.000 0.00 0.0 0.600 0 .192 0.075 149.2 0.000 0.00 0.0 0.600 0 .123 0.021 148.7 0.000 0.00 0.0 0.600 0 Network Results Table Rain T.C. US/IL E I.Area E Base Foul Add I	(m)       (m)       (1:X)       (ha)       (mins)       Flow       (1/s)       (mm)       SECT       (mm)         .808       0.040       145.2       0.011       0.00       0.0       0.600       0       150         .098       0.075       148.0       0.000       0.00       0.0       0.600       0       150         .192       0.075       149.2       0.000       0.00       0.0       0.600       0       150         .123       0.021       148.7       0.000       0.00       0.0       0.600       0       150         Network       Results       Table       Rain       T.C.       US/IL       E       I.Area       E       Base       Foul       Add       Flow	(m) (m) (1:X) (ha) (mins) Flow (1/s) (mm) SECT (mm) .808 0.040 145.2 0.011 0.00 0.0 0.600 o 150 Pipe/C .098 0.075 148.0 0.000 0.00 0.0 0.600 o 150 Pipe/C .192 0.075 149.2 0.000 0.00 0.0 0.600 o 150 Pipe/C .123 0.021 148.7 0.000 0.00 0.00 0.0 0.600 o 150 Pipe/C <u>Network Results Table</u> Rain T.C. US/IL E I.Area E Base Foul Add Flow Vel	<ul> <li>(m) (n) (1:X) (ha) (mins) Flow (1/s) (mm) SECT (mm)</li> <li>.808 0.040 145.2 0.011 0.00 0.00 0.00 0.00 0.150 Pipe/Conduit</li> <li>.098 0.075 148.0 0.000 0.00 0.00 0.00 0.600 0 150 Pipe/Conduit</li> <li>.192 0.075 149.2 0.000 0.00 0.00 0.0 0.600 0 150 Pipe/Conduit</li> <li>.123 0.021 148.7 0.000 0.00 0.00 0.0 0.600 0 150 Pipe/Conduit</li> <li>.Network Results Table</li> <li>Rain T.C. US/IL E I.Area E Base Foul Add Flow Vel Cap</li> </ul>

S1.002	50.00	5.43 49.050	0.043	0.0	0.0	0.0	0.83	14.7	5.8
S1.003	50.00	5.65 48.180	0.043	0.0	0.0	0.0	0.82	14.6	5.8
S1.004	50.00	5.88 48.105	0.043	0.0	0.0	0.0	0.82	14.5	5.8
S1.005	50.00	5.95 48.030	0.043	0.0	0.0	0.0	0.82	14.5	5.8

								Page	2		
•				Storm Mod	lel						
				The Yard							
				Littletor	n Upon	Severn					
Date 03/03	3/2024	20:33		Designed	by GJ						
File 2239-	-CAL-C-	-0005-	-P03 STO	Checked b	ру			Digi	nage		
Innovyze				Network 2	2020.1.	3					
Man	hole So	chedul	les for 2239	9-CAL-C-00	05-P01	STORM WA	ATER MOD	EL.SWS			
МН	МН	мн	мн	мн		Pipe Out			Pipes In		
Name	CL (m)	Depth		Diam.,L*W	PN	Invert	Diameter	PN	Invert	Diameter	Ba
		(m)		(mm)		Level (m)	(mm)		Level (m)	(mm)	
	10.000			45.0	~1	40.400	1.5.0				
			Open Manhole		S1.000	49.180	150				
			Open Manhole		S2.000	49.150	150				
	49 950	10 850					4.5.0	~1 ~~~	40 400		
SSW.03	13.350	0.050	Open Manhole	450	S1.001	49.100	150	S1.000	49.100		
								S1.000 S2.000	49.100 49.100		
SSW.04	49.800	0.600	Open Manhole	450	\$3.000	49.200	150	S2.000	49.100	150	
SSW.04	49.800	0.600		450			150	s2.000 s1.001	49.100 49.050	150 150	
SSW.04 SSW.05	49.800 49.900	0.600 0.850	Open Manhole Open Manhole	450 450	S3.000 S1.002	49.200 49.050	150 150	S2.000 S1.001 S3.000	49.100 49.050 49.050	150 150 150	
SSW.04 SSW.05 SSW.06	49.800 49.900 49.800	0.600 0.850 1.620	Open Manhole Open Manhole Open Manhole	450 450 1200 x 750	s3.000 s1.002 s1.003	49.200 49.050 48.180	150 150 150	S2.000 S1.001 S3.000 S1.002	49.100 49.050 49.050 49.010	150 150 150 150	
SSW.04 SSW.05 SSW.06 SSW.07 PUMP	49.800 49.900 49.800 49.550	0.600 0.850 1.620 1.445	Open Manhole Open Manhole Open Manhole Open Manhole	450 450 1200 x 750 1000	S3.000 S1.002 S1.003 S1.004	49.200 49.050 48.180 48.105	150 150 150 150	S2.000 S1.001 S3.000 S1.002 S1.003	49.100 49.050 49.050 49.010 48.105	150 150 150 150 150	
SSW.04 SSW.05 SSW.06 SSW.07 PUMP SSW.08	49.800 49.900 49.800 49.550 49.500	0.600 0.850 1.620 1.445 1.470	Open Manhole Open Manhole Open Manhole	450 450 1200 x 750 1000	s3.000 s1.002 s1.003	49.200 49.050 48.180	150 150 150 150	S2.000 S1.001 S3.000 S1.002	49.100 49.050 49.050 49.010 48.105	150 150 150 150 150 150	

MH Name	Manhole Easting (m)	Manhole Northing (m)	Intersection Easting (m)	Intersection Northing (m)	Manhole Access	Layout (North)
SSW,01	359989.104	189754.951	359989.104	189754.951	Required	•
SSW.02	359976.623	189750.309	359976.623	189750.309	Required	
SSW.03	359982.313	189745.842	359982.313	189745.842	Required	$\sim$
SSW.04	359996.781	189756.686	359996.781	189756.686	Required	
SSW.05	359985.750	189743.090	359985.750	189743.090	Required	$\langle \cdot \rangle$
SSW.06	359986.763	189737.371	359986.763	189737.371	Required	
SSW.07 PUMP	359980.681	189728.088	359980.681	189728.088	Required	4
SSW.08	359977.494	189717.360	359977.494	189717.360	Required	
Sheadwall	359974.596	189716.196			No Entry	•
		©1982-	-2020 Innovy	ze		
		-	- 1			

		Page 3
•	Storm Model	
	The Yard	
	Littleton Upon Severn	Micro
Date 03/03/2024 20:33	Designed by GJ	Drainage
File 2239-CAL-C-0005-P03 STO	Checked by	Drainacje
Innovyze	Network 2020.1.3	

#### PIPELINE SCHEDULES for 2239-CAL-C-0005-P01 STORM WATER MODEL.SWS

#### Upstream Manhole

PN	Hyd Sect	Diam (mm)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
S1.000	0	150	SSW,01	49.900	49.180	0.570	Open Manhole	450
S2.000	0	150	SSW.02	49.900	49.150	0.600	Open Manhole	450
S1.001	0	150	SSW.03	49.950	49.100	0.700	Open Manhole	450
S3.000	0	150	SSW.04	49.800	49.200	0.450	Open Manhole	450
S1.002	0	150	SSW.05	49.900	49.050	0.700	Open Manhole	450
S1.003	0	150	SSW.06	49.800	48.180	1.470	Open Manhole	1200 x 750
S1.004	0	150	SSW.07 PUMP	49.550	48.105	1.295	Open Manhole	1000
S1.005	0	150	SSW.08	49.500	48.030	1.320	Open Manhole	450

#### Downstream Manhole

PN	Length (m)	Slope (1:X)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)	
S1.000	11.362	142.0	SSW.03	49.950	49.100	0.700	Open Manhole	450	
S2.000	7.233	144.7	SSW.03	49.950	49.100	0.700	Open Manhole	450	
S1.001	4.404	88.1	SSW.05	49.900	49.050	0.700	Open Manhole	450	
S3.000	17.509	116.7	SSW.05	49.900	49.050	0.700	Open Manhole	450	
	11.192	148.0 149.2	SSW.06 SSW.07 PUMP SSW.08 Sheadwall	49.800 49.550 49.500 49.500		1.295 1.320	Open Manhole Open Manhole Open Manhole	1200 x 750 1000 450 150	

Free Flowing Outfall Details for 2239-CAL-C-0005-P01 STORM WATER MODEL.SWS

Outfall Pipe Number	Outfall Name	C. Level (m)		_		
S1.005	Sheadwall	49.500	48.009	48.009	150	0

			Page 4
	Storm Model		
	The Yard		
	Littleton Up	oon Severn	– Micro
ate 03/03/2024 20:33	Designed by	GJ	Drainage
ile 2239-CAL-C-0005-P03	STO Checked by		Diamage
nnovyze	Network 2020	).1.3	
Simulation Criteria	for 2239-CAL-C-0005	-P01 STORM WATER MC	DEL.SWS
Areal Reductior Hot Start	: (mins) 0 vel (mm) 0 Flow per (Global) 0.500	D Factor * 10m³/ha Stor Inlet Coeffieci	rage 0.000 Lent 0.800 day) 0.000 Lns) 60
Number of On	t Hydrographs 0 Number o line Controls 2 Number o line Controls 0 Number o	of Time/Area Diagrams O	
	Synthetic Rainfall	Details	
M5-60 (1	rs) 2 ion England and Wales	Profile Type Su Cv (Summer) 0 Cv (Winter) 0 corm Duration (mins)	.750 .840

		Page 5
•	Storm Model	
	The Yard	
	Littleton Upon Severn	Mirro
Date 03/03/2024 20:33	Designed by GJ	Drainage
File 2239-CAL-C-0005-P03 STO	Checked by	Diamage
Innovyze	Network 2020.1.3	

Online Controls for 2239-CAL-C-0005-P01 STORM WATER MODEL.SWS

#### Orifice Manhole: SSW.07 PUMP, DS/PN: S1.004, Volume (m<sup>3</sup>): 1.3

Diameter (m) 0.020 Discharge Coefficient 0.600 Invert Level (m) 48.105

Pump Manhole: SSW.08, DS/PN: S1.005, Volume (m<sup>3</sup>): 0.4

Invert Level (m) 48.030

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	1.0000	1.000	1.0000	1.700 1.800	0.0000	2.500	0.0000
0.300 0.400 0.500	1.0000 1.0000 1.0000	1.200	0.0000 0.0000 0.0000	1.900 2.000 2.100	0.0000 0.0000 0.0000	2.700 2.800 2.900	0.0000 0.0000 0.0000
0.600 0.700 0.800	1.0000 1.0000 1.0000		0.0000 0.0000 0.0000	2.200 2.300 2.400	0.0000 0.0000 0.0000	3.000	0.0000

				Page 6
	Storm	Model		
	The Ya	ard		
	Little	eton Upon S	Severn	Micco
Date 03/03/2024 20:33		ned by GJ		— Micro
File 2239-CAL-C-0005-P03 STO	_	-		Drainage
Innovyze		ck 2020.1.3	3	
	1.00.01		·	
Storage Structures for	2239-CAL-	C-0005-P01	STORM WATE	R MODEL.SWS
Filter Drain	Manhole:	SSW.05. DS	/PN: S1.002	2
Infiltration Coefficient Bas Infiltration Coefficient Sid Safet Invert L Trench W	e (m/hr) 0. e (m/hr) 0. y Factor Porosity evel (m) 4 'idth (m)	00000 00000 Pipe De 2.0 0.30 9.050 0.4 Cap In	Pipe Diam epth above In Number Slo Cap Volume D	eter (m) 0.150
	ngth (m)			
<u>Cellular Stora</u>	ge Manhole	e: SSW.06,	US/PN: S1.(	103
Infiltration Coeffic: Infiltration Coeffic:	ient Base (m	/hr) 0.00000		
Depth (m) Area (m²) Inf	. Area (m²)	Depth (m) Ar	cea (m²) Inf.	Area (m²)
0.000 15.0 1.200 15.0	15.0 35.4	1.201	0.0	35.4
	A1002 2020	Therefore		
	©1982-2020	runovyze		

								Pa	.ge 7
				Storm					
				The Ya	rd				
				Little	ton Up	on Sev	ern	N	licro
ate 03	3/03/2024 2	20:33		Design	ed by	GJ		ň	rainaq
ile 22	239-CAL-C-0	0005-P03 S	бто	Checke	d by				rainay
innovy	ze			Networ	k 2020	1.3			
1 year	r Return Pe	eriod Summ	nary of	Critic	cal Res	sults b	y Maximu	m Level	(Rank 1
	f	or 2239-C	AL-C-0	005-P01	STORM	WATER	MODEL.SV	<u>IS</u>	
				mulation					
	Areal	Reduction Hot Start							
	Hot	Start Leve			MAD	D Factor	Inlet Coef		
	nhole Headlo Foul Sewage				ow per 1	Person p	per Day (1,	/per/day)	0.000
		er of Input							
		nber of Onli ber of Offli							
		Rainfall Mo		etic Rair	fall De FSR		io R 0.350		
				fland and			mer) 0.750		
							ter) 0.840		
	Margin :	for Flood R	isk Warn	ning (mm)				300.0	
		A	-	-		econd In	crement (E		
				'S Status 'D Status				ON OFF	
				a Status				OFF	
		Profil	e(s)				Summer	and Winter	
	Dur	ation(s) (m	ins)				240, 360,		
				720,	960, 14	40, 216	), 2880, 4	320, 5760, 640, 10080	
	Return Pe	riod(s) (ye	ars)					1, 30, 10080	
		mate Change						0, 0, 45	
PN	US/MH Name	Storm		Climate Change		t (X) harge	First (Y) Flood	First (Z) Overflow	Overflo Act.
S1.000	SSW,01	15 Winter	1	+0%	100/15	Summer			
S2.000	SSW.02	15 Winter	1		100/15				
S1.001	SSW.03	15 Winter			100/15				
S3.000	SSW.04	15 Winter			100/15				
	SSW.05	15 Winter 180 Winter	1	+0% +0%	100/15				
S1.002	0011 00			+0% +0%		Summer Summer			
S1.002 S1.003		360 Winter	1		1/15	Summer			
S1.002 S1.003	SSW.07 PUMP	360 Winter 180 Winter	1	+0%					
S1.002 S1.003 S1.004	SSW.07 PUMP	180 Winter					Half Dra	in Pipe	
S1.002 S1.003 S1.004	SSW.07 PUMP	180 Winter Water Surg			Flow /	Overflo	Half Dra w Time	in Pipe Flow	
S1.002 S1.003 S1.004	SSW.07 PUMP SSW.08	180 Winter Water Surg	charged	Flooded	Flow / Cap.	Overflo (1/s)		Flow	Status
S1.002 S1.003 S1.004 S1.005	SSW.07 PUMP SSW.08 US/MH Name	180 Winter Water Surd Level D (m)	charged epth (m)	Flooded Volume (m³)	Cap.		w Time	Flow (1/s)	
S1.002 S1.003 S1.004 S1.005	SSW.07 PUMP SSW.08 US/MH	180 Winter Water Surd Level D (m) 49.204	charged epth	Flooded Volume			w Time	Flow	Status

		Page 8
•	Storm Model	
	The Yard	
	Littleton Upon Severn	Mirro
Date 03/03/2024 20:33	Designed by GJ	Dcainago
File 2239-CAL-C-0005-P03 STO	Checked by	Diamage
Innovyze	Network 2020.1.3	•

<u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for 2239-CAL-C-0005-P01 STORM WATER MODEL.SWS</u>

PN	US/MH Name	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m <sup>3</sup> )		Overflow (1/s)	Half Drain Time (mins)	Pipe Flow (l/s)	Status
S3.000	SSW.04	49.237	-0.113	0.000	0.14			2.1	OK
S1.002	SSW.05	49.120	-0.080	0.000	0.45		6	5.5	OK
S1.003	SSW.06	48.406	0.076	0.000	0.07		105	1.0	SURCHARGED
S1.004	SSW.07 PUMP	48.441	0.186	0.000	0.03			0.4	SURCHARGED
S1.005	SSW.08	48.075	-0.105	0.000	0.04			0.4	OK

PN	US/MH Name	Level Exceeded
S1.000	SSW,01	
S2.000	SSW.02	
S1.001	SSW.03	
S3.000	SSW.04	
S1.002	SSW.05	
S1.003	SSW.06	
S1.004	SSW.07 PUMP	
S1.005	SSW.08	

•				Storm	Model				age 9
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	<u>f</u>	or 2239-C	AL-C-00	005-P01	STORM	WATER	MODEL.SW	IS	
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	ole Headlo	ss Coeff (C	Global)	0.500 Fl	ow per H				
	Numbe	er of Input	Hydrogr	anhs 0 N	lumber o	f Stora	a Structur	ros 2	
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	Numb	per of Offl	ine Cont	rols 0 N	Jumber o	f Real '	Time Contro	ols O	
		Rainfall M		etic Rain	fall De FSR		io R 0.350		
		Re	gion Eng	land and			mer) 0.750		
		M5-60	(mm)		20.000	Cv (Win	ter) 0.840		
	Margin :	for Flood R		-				300.0	
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	Dur		ine)	15 30	60 12	0 180		and Winter	
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		ation(s) (m					240, 360, 0, 2880, 43 7200, 86	480, 600, 320, 5760, 540, 10080	)
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PN	Return Pe Clin	ation(s) (m riod(s) (ye	ears) e (%) <b>Return</b>	720,	960, 14 First	40, 2160	240, 360, 0, 2880, 43 7200, 86	480, 600, 320, 5760, 540, 10080 1, 30, 100 0, 0, 45	) ) 5
S1.000	Return Pe. Clin US/MH Name SSW,01	ation(s) (m riod(s) (ye mate Change <b>Storm</b> 15 Winter	Return Period	720, Climate Change +0%	960, 14 First Surch 100/15	40, 2160 - (X) harge Summer	240, 360, 0, 2880, 43 7200, 86 First (Y)	480, 600, 320, 5760, 540, 10080 1, 30, 100 0, 0, 45 First (Z)	Overflow
S1.000 S2.000	Return Pe. Clin <b>US/MH</b> Name SSW,01 SSW.02	ation(s) (m riod(s) (ye mate Change <b>Storm</b> 15 Winter 15 Winter	Return Period	720, Climate Change +0% +0%	960, 14 First Surch 100/15 100/15	40, 2160 <b>c (X)</b> harge Summer Summer	240, 360, 0, 2880, 43 7200, 86 First (Y)	480, 600, 320, 5760, 540, 10080 1, 30, 100 0, 0, 45 First (Z)	Overflow
S1.000 S2.000 S1.001	Return Pe. Clin <b>US/MH</b> Name SSW,01 SSW.02 SSW.03	ation(s) (m riod(s) (ye mate Change <b>Storm</b> 15 Winter 15 Winter 15 Winter 15 Winter	ears) e (%) Return Period c 30 c 30 c 30	720, Climate Change +0% +0% +0%	960, 14 First Surch 100/15 100/15 100/15	40, 2160 c (X) harge Summer Summer Summer	240, 360, 0, 2880, 43 7200, 86 First (Y)	480, 600, 320, 5760, 540, 10080 1, 30, 100 0, 0, 45 First (Z)	Overflow
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S1.000 S2.000 S1.001 S3.000	Return Pe Clin US/MH Name SSW,01 SSW.02 SSW.03 SSW.04 SSW.05	ation(s) (m riod(s) (ye mate Change Storm 15 Winter 15 Winter 15 Winter 15 Winter 15 Winter	Return         Period         30         30         30         30         30         30         30         30         30         30         30         30         30         30         30         30         30         30	720, Climate Change +0% +0% +0% +0%	960, 14 First Surch 100/15 100/15 100/15 100/15 100/15	40, 2160 c (X) harge Summer Summer Summer Summer	240, 360, 0, 2880, 43 7200, 86 First (Y)	480, 600, 320, 5760, 540, 10080 1, 30, 100 0, 0, 45 First (Z)	Overflor
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S1.000 S2.000 S1.001 S3.000 S1.002 S1.003 S1.004 S	Return Pe Clin US/MH Name SSW,01 SSW.02 SSW.03 SSW.04 SSW.05 SSW.06 SW.07 PUMP	ation(s) (m riod(s) (ye mate Change Storm 15 Winter 15 Winter 15 Winter 15 Winter 18 Winter 180 Winter	Return         Period         30	720, <b>Climate</b> <b>Change</b> +0% +0% +0% +0% +0% +0% +0% +0%	960, 14 First Surch 100/15 100/15 100/15 100/15 100/15 1/30	40, 2160 c (X) harge Summer Summer Summer Summer Summer Summer	240, 360, 0, 2880, 43 7200, 86 First (Y)	480, 600, 320, 5760, 540, 10080 1, 30, 100 0, 0, 45 First (Z) Overflow	Overflor
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S1.000 S2.000 S1.001 S3.000 S1.002 S1.003 S1.004 S1.005	Return Pe Clin US/MH Name SSW,01 SSW.02 SSW.03 SSW.04 SSW.03 SSW.04 SSW.05 SSW.06 SW.07 PUMP SSW.08 US/MH Name	ation(s) (m riod(s) (ye mate Change Storm 15 Winter 15 Winter 15 Winter 15 Winter 180 Winter	ears) e (%) Return Period a 30 a 30 a 30 a 30 a 30 a 30 a 30 c 30	720, Climate Change +0% +0% +0% +0% +0% +0% +0% Flooded Volume (m <sup>3</sup> )	960, 14 First Surch 100/15 100/15 100/15 1/30 1/15 Flow / Cap.	40, 2160 c (X) harge Summer Summer Summer Summer Summer Summer	240, 360, 0, 2880, 43 7200, 86 First (Y) Flood Half Dra w Time	480, 600, 320, 5760, 540, 1008( 1, 30, 10( 0, 0, 45 First (Z) Overflow in Pipe Flow (1/s)	Overflow Act.
S1.000 S2.000 S1.001 S3.000 S1.002 S1.003 S1.004 S1.005	Return Pe Clin US/MH Name SSW,01 SSW.02 SSW.03 SSW.03 SSW.03 SSW.04 SSW.03 SSW.04 SSW.05 SSW.06 SW.07 PUMP SSW.08	ation(s) (m riod(s) (ye mate Change Storm 15 Winter 15 Winter 15 Winter 15 Winter 180 Winter	Return         Period         30         Charged         Depth	720, <b>Climate</b> <b>Change</b> +0% +0% +0% +0% +0% +0% +0% <b>Flooded</b> <b>Volume</b>	960, 14 First Surch 100/15 100/15 100/15 1/30 1/15 Flow /	40, 2160 c (X) harge Summer Summer Summer Summer Summer Summer	240, 360, 0, 2880, 43 7200, 86 First (Y) Flood Half Dra w Time	480, 600, 320, 5760, 540, 10080 1, 30, 100 0, 0, 45 First (Z) Overflow in Pipe Flow	Overflow Act.
\$1.000 \$2.000 \$1.001 \$3.000 \$1.002 \$1.003 \$1.004 \$1.005 <b>PN</b> \$1.000	Return Pe Clin US/MH Name SSW,01 SSW.02 SSW.03 SSW.04 SSW.03 SSW.04 SSW.05 SSW.05 SSW.06 SW.07 PUMP SSW.08 US/MH Name SSW,01	ation(s) (m riod(s) (ye mate Change Storm 15 Winter 15 Winter 15 Winter 15 Winter 180 Winter	ears) e (%) Return Period a 30 a 30 a 30 a 30 a 30 a 30 a 30 c 30	720, Climate Change +0% +0% +0% +0% +0% +0% +0% Flooded Volume (m <sup>3</sup> ) 0.000	960, 14 First Surch 100/15 100/15 100/15 1/30 1/15 Flow / Cap. 0.15	40, 2160 c (X) harge Summer Summer Summer Summer Summer Summer	240, 360, 0, 2880, 43 7200, 86 First (Y) Flood Half Dra w Time	480, 600, 320, 5760, 540, 1008( 1, 30, 10( 0, 0, 45 First (Z) Overflow in Pipe Flow (1/s) 2.0	Overflo Act.

		Page 10
•	Storm Model	
	The Yard	
	Littleton Upon Severn	Mirro
Date 03/03/2024 20:33	Designed by GJ	Drainage
File 2239-CAL-C-0005-P03 STO	Checked by	Diamage
Innovyze	Network 2020.1.3	

 30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)

 for 2239-CAL-C-0005-P01 STORM WATER MODEL.SWS

PN	US/MH Name	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m <sup>3</sup> )		Overflow (1/s)	Half Drain Time (mins)	Pipe Flow (1/s)	Status
S3.000	SSW.04	49.261	-0.089	0.000	0.34			5.2	OK
S1.002	SSW.05	49.196	-0.004	0.000	1.00		4	12.2	OK
S1.003	SSW.06	48.831	0.501	0.000	0.09		162	1.2	SURCHARGED
S1.004	SSW.07 PUMP	48.899	0.644	0.000	0.05			0.7	SURCHARGED
S1.005	SSW.08	48.101	-0.079	0.000	0.07			0.7	OK

PN	US/MH Name	Level Exceeded
S1.000	SSW,01	
S2.000	SSW.02	
S1.001	SSW.03	
S3.000	SSW.04	
S1.002	SSW.05	
S1.003	SSW.06	
S1.004	SSW.07 PUMP	
S1.005	SSW.08	

						Pag	je 11
			Storm	Model			
			The Ya	rd			
			Little	ton Upon Sev	ern	N/I	
ate 03/03/2024	4 20:33		Design	ed by GJ			
ile 2239-CAL-0	C-0005-P03 \$	STO	-	-			ainag
nnovyze				k 2020.1.3			
100 year Retu		-CAL-C-	0005-P0	1 STORM WATE			(Rank
H Manhole Head Foul Sewag	Hot Start Not Start Leve Noss Coeff (G ge per hectare	Factor 1 (mins) 1 (mm) 10bal) ( (1/s) (	000 2 0 0 0.500 F10	ow per Person p	* * 10m³/ha Inlet Coef Der Day (1/	a Storage 0 Efiecient 0 (per/day) 0	.000 .800
]	Number of Onl:	ine Cont:	rols 2 N	umber of Stora umber of Time/ umber of Real	Area Diagr	ams O	
		odel	land and	<u>fall Details</u> FSR Rat Wales Cv (Sum 20.000 Cv (Win			
Margi	n for Flood R A	nalysis DT DV	-		crement (E	300.0 xtended) ON OFF OFF	
D	Profil uration(s) (m			60, 120, 180, 960, 1440, 216	240, 360, ), 2880, 4		
	Period(s) (ye limate Change					1, 30, 100 0, 0, 45	
		Boturn	Climate	First (V)	First (V)	First (7)	Overfle
US/MH PN Name	Storm		Climate Change	First (X) Surcharge	Flood	First (Z) Overflow	Act.
s1.000 ssw,	01 180 Winter	100	+45%	100/15 Summer			
	02 180 Winter			100/15 Summer			
S1.001 SSW.	03 180 Winter		+45%	100/15 Summer			
	04 180 Winter			100/15 Summer			
	05 180 Winter		+45% +45%	100/15 Summer 1/30 Summer			
S1.002 SSW.	06 180 Winter		+45%	1/15 Summer			
\$1.002 SSW. \$1.003 SSW.	06 180 Winter MP 180 Winter	100		1,10 000001			
\$1.002 \$\$W. \$1.003 \$\$W. \$1.004 \$\$W.07 PU			+45%	1, 10 Daniel			
\$1.002 \$\$W. \$1.003 \$\$W. \$1.004 \$\$W.07 PU	MP 180 Winter		+45%	-)			

		Page 12
•	Storm Model	
	The Yard	
	Littleton Upon Severn	Mirro
Date 03/03/2024 20:33	Designed by GJ	Drainage
File 2239-CAL-C-0005-P03 STO	Checked by	Diamage
Innovyze	Network 2020.1.3	

100 year Return Period Summary of Critical Results by Maximum Level (Rank1) for 2239-CAL-C-0005-P01 STORM WATER MODEL.SWS

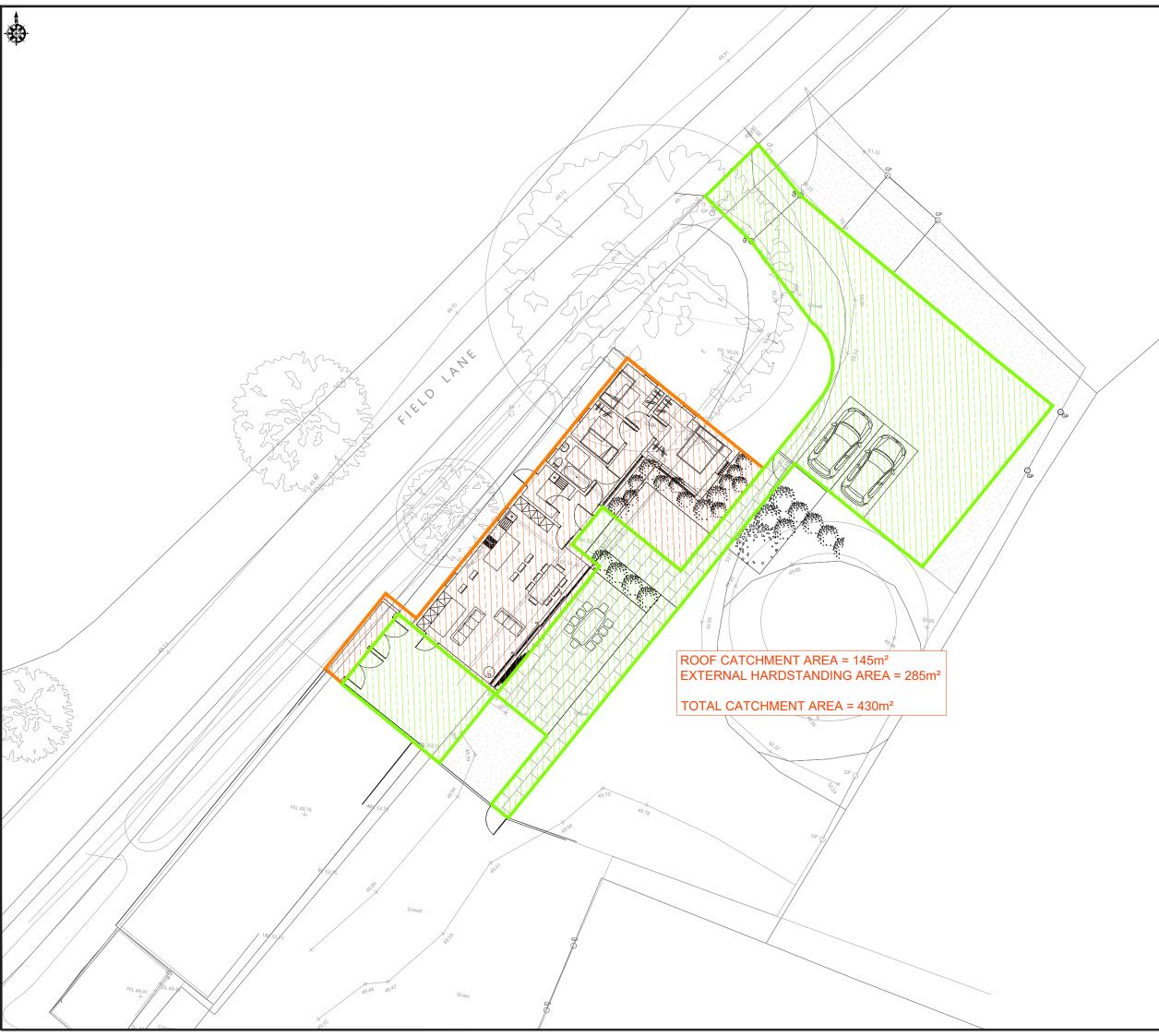
PN	US/MH Name	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m <sup>3</sup> )	Flow / Cap.	Overflow (1/s)	Half Drain Time (mins)	Pipe Flow (l/s)	Status
S1.000	SSW,01	49.546	0.216	0.000	0.07			0.9	SURCHARGED
S2.000	SSW.02	49.547	0.247	0.000	0.13			1.6	SURCHARGED
S1.001	SSW.03	49.546	0.296	0.000	0.18			2.5	SURCHARGED
S3.000	SSW.04	49.547	0.197	0.000	0.17			2.5	FLOOD RISK
S1.002	SSW.05	49.545	0.345	0.000	0.56		71	6.8	SURCHARGED
S1.003	SSW.06	49.543	1.213	0.000	0.08			1.1	FLOOD RISK
S1.004	SSW.07 PUMP	49.539	1.284	0.000	0.07			1.0	FLOOD RISK
S1.005	SSW.08	48.128	-0.052	0.000	0.09			1.0	OK

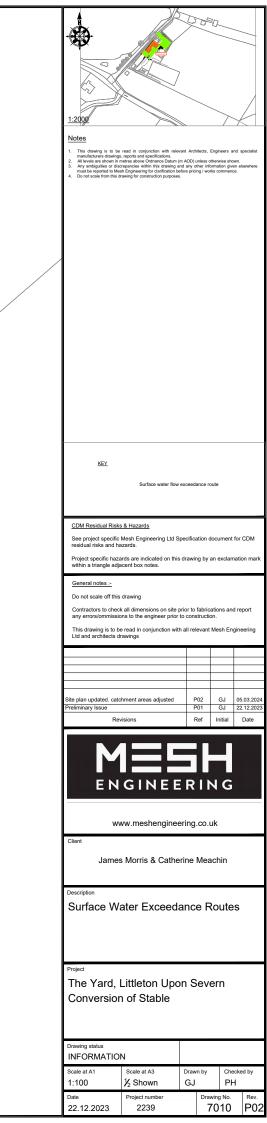
US/MH	Level
Name	Exceeded
0.014 0.1	
,	
SSW.02	
SSW.03	
SSW.04	
SSW.05	
SSW.06	
SSW.07 PUMP	
SSW.08	
	Name SSW,01 SSW.02 SSW.03 SSW.03 SSW.04 SSW.05 SSW.06 SSW.07 PUMP



# 12. APPENDIX G

(Catchment Area)







# 13. APPENDIX H

(Exceedance Routes)



	3.18				-	
		P /				
<u>1:2000</u>				$\geq$	$\land$	
minufactures downing     minufactures downing     Any antibulies or dis     must be reported to Me     the costing severitaria     the costing     the co	this drawing refer to approva had access overs and frames an arcafor is to crientale manhole bit and access access and frames an anophy with his[3] Xhouding L ong services. Truction. Truction. The devicepment in accordance in divertel twest or any existin the works. The works. The works areas with less th sanage with least cover than works the contractor is to confir 	n AOD) u di any di di any di fore prici arting fror prici arting fror di di avolta di avolta arting fror di avolta and and and and and and and an	nelses althorned in the information of the informat	ise show wing even internet tream co ritish Sta hority gu A Authorit shown c drain pipe drain	n, mendedon alo mendedon alo mendedon alo didelenea & y and EAA y and EAAA y and EAA y and EAAA y and EAA y and EAA y and EAA y and EAA y and EAA y and EAAA y and EAAA y and EAAA y and EAAA y and EAAA y and EAAA y and EAAAA y and EAAAA y and EAAAA y and EAAAAA y and EAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA	
residual risks and ha Project specific haza	Mesh Engineering Ltd Sp zards. rds are indicated on this					
within a triangle adja	cent box notes.		, _ , un e		di K	
General notes :- Do not scale off this drawing Contractors to check all dimensions on site prior to fabrications and report any errors/ommissions to the engineer prior to construction. This drawing is to be read in conjunction with all relevant Mesh Engineering Ltd and architects drawings						
		_				
Site plan updated					05.03.2024	
Preliminary Issue Rev	isions	R		itial	Date	
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Client	0	0				
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Surface Wa	ater Exceeda	ance	e Roi	utes	8	
Project The Yard, Littleton Upon Severn Conversion of Stable						
Drawing status						
INFORMATION Scale at A1	N Scale at A3	Drawr	1 by	Chec	ked by	
1:100	$\frac{1}{2}$ Shown	GJ	,	PH		
 Date 22.12.2023	Project number 2239		Drawing		Rev. P02	
		_	-			



# $14.\,\text{APPENDIX I}$

(EA Flood Map)



# Flood map for planning

Your reference The Yard Location (easting/northing) 359984/189703

Created **21 Dec 2023 15:53** 

Your selected location is in flood zone 1, an area with a low probability of flooding.

# You will need to do a flood risk assessment if your site is any of the following:

- bigger that 1 hectare (ha)
- In an area with critical drainage problems as notified by the Environment Agency
- identified as being at increased flood risk in future by the local authority's strategic flood risk assessment
- at risk from other sources of flooding (such as surface water or reservoirs) and its development would increase the vulnerability of its use (such as constructing an office on an undeveloped site or converting a shop to a dwelling)

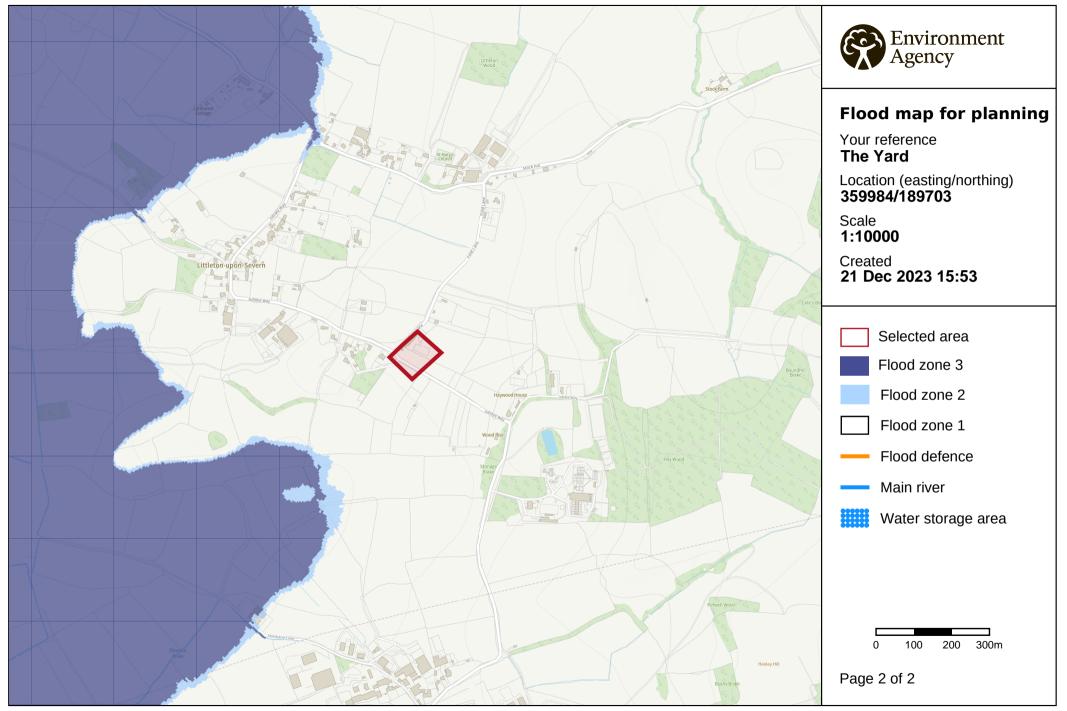
## Notes

The flood map for planning shows river and sea flooding data only. It doesn't include other sources of flooding. It is for use in development planning and flood risk assessments.

This information relates to the selected location and is not specific to any property within it. The map is updated regularly and is correct at the time of printing.

Flood risk data is covered by the Open Government Licence **which** sets out the terms and conditions for using government data. https://www.nationalarchives.gov.uk/doc/open-government-licence/version/3/

Use of the address and mapping data is subject to Ordnance Survey public viewing terms under Crown copyright and database rights 2022 OS 100024198. https://flood-map-for-planning.service.gov.uk/os-terms



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# 15. APPENDIX J

(Operations and maintenance manual)



## SUSTAINABLE URBAN DRAINAGE OPERATION AND MAINTENACE SCHEDULE

# The Yard, Littleton upon Severn

## Section 1.01 Guidance

This Drainage Management and Maintenance Plan provides details of the plan proposed for maintenance and management of the drainage scheme associated with the proposed development at The Yard, Field Lane, Littleton Upon Severn, BS35 1NU

On occupation of the development, the maintenance and management plan should be incorporated into the sites Operation and Maintenance Manual with the as-built drainage system operated and maintained in accordance with the regime set out in the tables below. All maintenance tasks will be the responsibility of the land owner.

To ensure longevity and effective operation of SuDS they must be maintained in accordance with

- CIRIA 753 guidance and operation and maintenance
- CIRIA report C768 Guidance on the construction of SuDS Maintenance plan outlined in section 5.2

Feature	Maintenance	Frequency
Private Drains	Inspection	CCTV survey every
		5-10 years.
	Regular Maintenance	Jet clean system
		fully every 5-10
		years.
		(Recommend prior
		to CCTV drainage
		survey)
	Remedial / Occasional Maintenance	Carry out remedial
		works as identified
		in CCTV survey.
Outfall pipes, non-return pipe	Inspection	Visually - Quarterly
flaps, and anti-	Regular Maintenance	Clearance of silt
naps, and anti-		and debris as
		necessary

## Section 1.02 Maintenance Plan



Feature	Maintenance	Frequency
scour mat flow channel	Remedial / Occasional Maintenance	Damage to pipes and headwall to be repaired as necessary
Discharge	Inspection	Quarterly
orifice manholes/flow control devices	Regular maintenance	Remove silt and debris as necessary to prevent build up.
Gullies &	Inspection	Quarterly
Drainage Channels	Regular Maintenance	Remove silt and debris as necessary to prevent build up.
Catchpits	Inspection	Quarterly
	Regular maintenance	Remove silt and debris as necessary to prevent build up.
Permeable and	Cleaning	Monthly or as
porous surface	Brush regularly and remove sweepings from all hard surfaces	required
	Permeable Pavements.	
	Brush and vacuum surface once a year to prevent silt blockage and enhance design life.	
	Remedial work	
	Monitor effectiveness of permeable pavement and when water does not infiltrate immediately advise Client of possible need for reinstatement of top layers or specialist cleaning.	
	Recent experience suggests jet washing and suction cleaning will substantially reinstate pavement to 90% efficiency.	
Overflows and flood routes	Overflows. Jet pipes leading from overflow structures annually and check by running water through the overflow. Check free flow at next SUDS feature – inlet to basin or chamber.	Annually



Feature	Maintenance	Frequency
	Remove any accumulated grass cuttings or other debris on top of grass weirs or stone filled baskets overflows.	Monthly
	Flood Routes. Make visual inspection. Check route is not blocked by new fences, walls, soil or other rubbish. Remove as necessary.	Monthly
	Overflows. If overflow is not clear then dismantle structure and reassemble to design detail.	As required
Planting and existing	Amenity Grass - Mow all grass verges, paths and amenity grass at 35-50mm with 75mm max.	16 visits
vegetation	All cuttings to remain in situ	
	Rough grass – Mow at 75-100mm but not to exceed 150mm	4 - 8 visits
	All cuttings to wildlife piles	
	Wildflower areas strimmed to 50mm in Sept-Oct	1 visit
	or	2 visit
	Wildflower areas strimmed to 50mm July and Sept	1 visit
	or	
	Wildflower areas strimmed to 50mm on 3 year rotation 30% each year	
	All cuttings to wildlife piles	
	Ornamental tree & shrub planting.	4 visits
	Weed all shrub beds as detailed spec as necessary.	
	Cut back planting from lights, paths and visibility sight lines in late autumn and as necessary.	
	Cut hedges slightly tapered back from base with flat top at specified height.	
	Do not mulch planting adjacent to permeable/ porous paving surfaces.	
	Remove stakes and ties from trees when no longer needed for support and within 3 years of planting.	
	Protect from strimmer damage and remove competitive growth until well established.	
	Native trees & shrub planting.	1 visit
	Prune to shape in year 1.	



Feature	Maintenance	Frequency
	Protect trees from strimmer damage and remove competitive growth until well established.	
	Remove stakes and ties from trees when no longer needed for support and within 3 years from planting.	
	Existing trees	1 visit
	Check existing trees for safety.	
	Replace trees and shrubs which fail in the first five years after planting.	
	Carry out tree surgery as necessary.	
	Non-biodegradable products to be deposited.	Daily
	The sewage station is designed to handle natural human waste, biodegradable products and foul and storm water. This could include nappies, cleaning wipes, sanitary towels, condoms or bandages. These products will not be able to break down in the water, and they should be thrown away in a bin.	
Filter Drains	Grass edges	Monthly or as
	Mow 1m min. wide grass surround to drain at 100mm and 150mm maximum to filter runoff and protect drain from silt.	required
	Weeds	As required
	Hand pull or spot treat individual weed growth only if necessary ensuring weedkiller does not enter the filter drain. Weed growth usually dies in dry weather.	
	Siltation at surface	As required
	Where there is no protective geotextile remove all stone and perforated pipe replacing as original Spec. and include separating geotextile as below.	
	Where there is a separating geotextile (see Spec.) then remove surface stone layer and separating geotextile that protects the stone drain below. Replace geotextile and top stone layer.	
Cellular storage	Ensure catchpits are installed upstream and downstream of cellular storage. These are to be emptied.	Quarterly
	Jetting should be carried out along main carrier drain through system.	As required



Feature	Maintenance	Frequency
Foul Treatment Plant (full O&M	Removal of solidified deposits. Chamber to be emptied to remove blockages. Dirt to be removed and cleaned including sand and gravel. Sump pump to be tested to ensure in full working order.	Annually
manual provided by Specialist	Check of alarm and electrical system	Annually
supplier)	Non-biodegradable products to be deposited. The sewage station is designed to handle natural human waste, biodegradable products and foul and storm water. This could include nappies, cleaning wipes, sanitary towels, condoms or bandages. These products will not be able to break down in the water, and they should be thrown away in a bin.	Daily
Pump Chamber (full O&M manual provided by Pump Specialist supplier)	<ul> <li>Pump specification to include the following: -</li> <li>Pump both treated foul and storm water effluent</li> <li>Polyethylene underground chamber with pre-fitted twin pump auto coupling system, check valves, isolation valve and float switch. 1m dia x 1.8m deep.</li> <li>2 no. submersible pumps restricting flow rate to 1 l/s.</li> <li>600 x 600mm opening, double sealed.</li> <li>24hr storage in case of pump failure.</li> </ul>	
	Removal of solidified deposits. Chamber to be emptied to remove blockages. Dirt to be removed and cleaned including sand and gravel. Sump pump to be tested to ensure in full working order.	Annually
	<ul> <li>Back up methodologies: -</li> <li>Dual pumps to be installed in case 1 of the pumps breaks down.</li> <li>Twin pump control panel with metal enclosure with high level alarm and amber warning light to alert client of pump maintenance is required.</li> <li>High level gravity overflow to allow water to discharge directly to the watercourse without causing localised flooding in case of pump failure</li> </ul>	
	Certified pump maintenance contractor to service the pump and check of alarm and electrical system. Contractor to be chosen by home owner and details to be given to new home owners upon the purchase of the property making them aware of their responsibilities for the structure. Recommend Duty Point Planned preventative maintenance, and adopt a maintenance programme which includes: -	Annually (min) 6 months (recommended)



Feature	Maintenance	Frequency
	<ul> <li>2 planned site visits per year</li> <li>24/7 emergency helpline</li> <li>Address: - Dutypoint Ltd, Unit A, Quedgeley West Business Park,</li> <li>Gloucester, GL2 4PA</li> <li>Tel:= 08082395776</li> </ul>	
	Non-biodegradable products to be deposited. The sewage pump station is designed to handle natural human waste, biodegradable products and foul and storm water. This could include nappies, cleaning wipes, sanitary towels, condoms or bandages. These products will not be able to break down in the water, and they should be thrown away in a bin.	Daily

# Section 1.03 Maintenance obligations and safety

The Site Manager should ensure that the Maintenance Contractor tasked with carrying out any maintenance works provides a risk assessment and method statement that adopts best practice health and safety policies for maintenance personnel throughout the duration of any maintenance works. Measures may include:

- Ensure the use of safe systems of work and procedures are followed.
- Certificated operatives only to be used for all confined space entry.

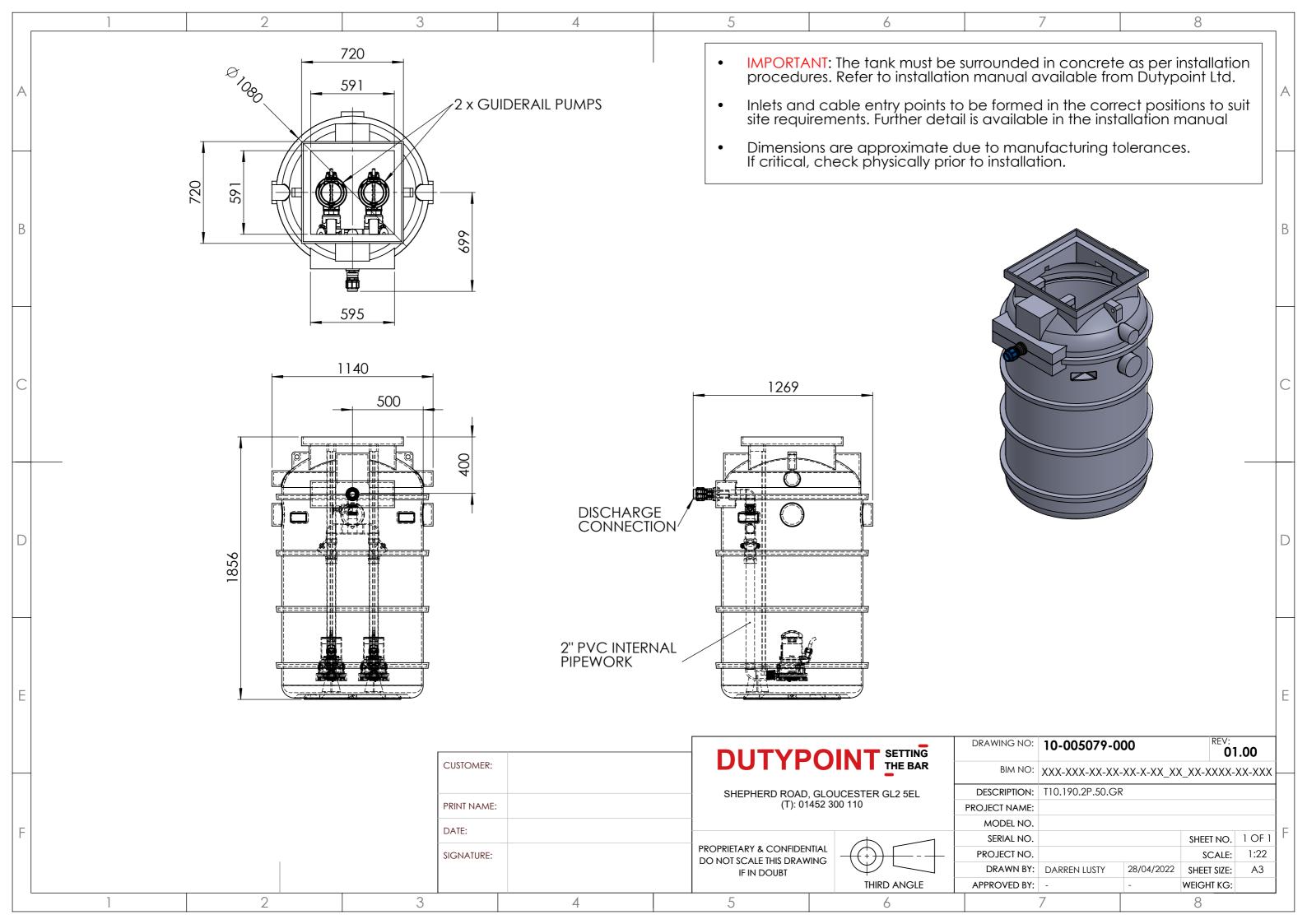
- Ensure appropriate PPE is worn at all times including the use of safety goggles, ear defenders and other relevant equipment when using high pressure jetting.

- Do not work in weather conditions where flooding or surging is likely.
- Erect barriers where appropriate and provide adequate lighting.
- No operations to be carried out by operatives working alone
- Time maintenance to not conflict with other on-site activities.
- Method statement to be prepared and approved prior to entry into confined space.



# 16. APPENDIX K

(Pump specification and design)





PUMPS | SYSTEMS | SERVICING | KNOW-HOW

Flow Civil Engineering 118 Tuffley Avenue Gloucester

	Proposal No.	501518/599277
Date		05/01/2024
Attention		Gareth Jones
Sales Conta	ct	Nick Tanner
Direct Dial		07385 974479
Email		nick.tanner@dutypoint.com
Your Ref	The Y	ard, Littleton Upon Severn -
four Rei		501518

GL1 5NS

# **Product Proposal**

# The Yard, Littleton Upon Severn - 501518

Dear Gareth,

Reference your enquiry for packaged pumping stations for above project, I have pleasure in offering a quotation for the pump station and other associated equipment.

Full details are attached but please do not hesitate to contact me should you require any further information.

Regards,

Nick Tanner

#### Notes:

- Please check the key selection criteria information stated within this quotation. Where key information is not
  available, assumptions may have been made in order to complete the selection for quoting purposes. Any
  changes to the selection criteria may result in a change of required pump station specification and assicated costs.
- Please check cable lengths specified. Cable is required to reach from the bottom of the chamber to the control panel via cable duct, with minimum 2m spare flex. If longer length is required additional costs will apply.



Project Reference The Yard, Littleton Upon Severn - 501518

## Pump Station 1 (Combined Pump Station)

Key Selection Criteria:		(Scheme Drainage Plans ref. 2239 - 7002 Rev.	P04)	
Effluent Type	:	Foul and SW	Final Outfall Level	49.100
Cover Level	:	49.700	Top Water Level :	48.375
Lowest Inlet Level	:	48.375 ( 1.325 m below CL)	Rising Main Length	26m
Maximum ground water level : 49.200		vel : 49.200 Distance from Pur	p Chamber to Control Panel :	<10m

#### Scope of supply:

- Vortech Polyethylene vertical underground chamber pre-fitted with twin pump auto-coupling system, guiderails, internal
  pipework, check valves, isolation valve and float switch bracket, c/w inlet and vent/duct connections to suit site requirements
- · 2no submersible drainage pumps c/w lifting chains and D shackles
- 400v DOL Twin Pump Control Panel with metal enclosure, adjustable overloads, VFC's, klixons, hand/off/auto selectors, run
  and trip lamps and high level alarm. Timer added to control panel to restrict flow to an average of 1 litres/sec.
- 4no Single Acting Float Switches
- Galvanized Pressed Steel Access Cover 600x600 clear opening, Facta AAA (2.5T SMWL) Load Rating, Double Seal with Locking Screws
- · Delivery to site of all the above (offloading by others)

#### Specification:

Civils Data:					
System Type	:	T10.190.2P.50P.GR02			
Chamber Size	:	1mØx1.8mdeep			
Access Size	:	600x600			
Cover Depth	:	100mm (depth from cover level to top of turret)	Inlet Con	necti	ions Included:
Total Storage Volume	:	1060 Litres	110mm:	:	0
Design Storage Volume	:	220 Litres (below TWL of 48.375)	160mm	:	2
Rising Main Required (by others)	:	50mm SDR11 PE100 Pipe	200mm	:	0
Discharge Connection	:	50mm Compression to suit PE pipe	300mm	:	0
			450mm	:	0

M&E	Data:

Pump Model	:	F-05U 0.4kW 2" 3ph
Design Flow Rate	:	1 l/sec
No of pumps	:	Two
Motor Rating	:	0.4 kW
Motor Speed	:	2780 RPM
Cable Length	:	10 m
Control Panel	:	CK19T/1-1.6
Supply Voltage	:	400/3/50

Impeller Type	:	Vortex
Design Total Head	:	1.8 m
Configuration	:	Duty / Standby
Full Load Current	:	1.3 Amps per pump
Internal Pipework	:	50mm PVC
Level Control Type	:	Floatswitch
Method of Starting	:	Direct Online

Total Package Price :	£3,440.00
Commissioning Price :	£550.00
Estimated Lead Time :	2 Weeks*

600mm

:

0





Project Reference The Yard, Littleton Upon Severn - 501518

#### **Optional Additional Items**

#### Commissioning

Commissioning is priced per pumping station (see previous pages) and is based on the selection criteria stated for each pump station. Any changes to this critera may affect the price.

Commissioning includes pulling pumps and float cables through the cable duct and connecting into the control panel, installing pumps into the chamber, setting float switches to the required levels, testing and commissioning the installation. Basic tasks as outlined in our pre-commissioning checklist are to be carried out by others prior to commissioning. Should an additional visit be required due to incompletion of any of these tasks (unless by prior agreement), additional charges will apply.

Please allow 4 weeks lead in from booking to commissioning date to allow for completion of the necessary pre-commissioning checks. In some cases we may arrange an engineer inspection visit prior to the commissioning date.

A package discount may be available If multiple pumping stations can be commissioned within the same visit. Please contact your sales representative for further information.

<b>SMS Autodial Alarm System (per pump station)</b> Messages including power failure, pump/s tripped, high level alarm can be sent to up to 3 mobile numbers/email addresses on the standard module, additional users can be added at extra cost.	£520.00
<b>GRP Kiosk (per pump station)</b> Weatherproof GRP Green Kiosk 1250 High x 750 Wide x 400 Deep. For protection of control panels where situated outdoors.	£560.00
Flashing Alarm Beacon 24V AC/DC Red LED Flashing beacon, suitable for direct mounting onto GRP Kiosk	£32.00
Hole Saw Kits - For correct drilling of holes in tank wall for fitting rubber inlet seals (poly tanks)	

HSK-140 - 140mm hole saw to suit 110mm wall seal	£35.00
HSK-177 - 177mm hole saw to suit 160mm wall seal	£43.00
Arbor for Hole Saw	£15.00



## Project Reference The Yard, Littleton Upon Severn - 501518

#### **Clients Responsibility:**

- Unloading at site (unless otherwise stated by Dutypoint in writing)
- Cable containment between pump chamber and control panel.
- Installation of control panel kiosk (if applicable)
- Mounting of control panel in final location
- Provision of mains power and isolation to the control panel
- All civil works including tank installation and inter-tank connections (if applicable)
- To make certain that any equipment purchased is suitable for the duty and medium type
- To assess ground conditions and advise if ground water could exceed 2m above the base of the manufactured chamber or there is a possibility of flooding. In this situation a different specification may be required.
- To assess vehicular loading requirements if applicable, and ensure the chamber backfill & cover slab design (by others) is sufficient to protect the chamber from direct loading.
- To assess required cable lengths. Standard cable length offered is stated in above specification. Minimum cable length required is the depth of chamber plus distance via duct/cable containment to the control panel, plus 3m
- To install equipment in accordance with instructions, paying attention to the effects of up-thrust created by chambers containing air when being installed and in operation.
- To ensure the solids handling capability of the pumps is suitable for the duty and to ensure the system is only required to handle waste water or human waste and normal toilet paper as appropriate. Systems to handle wipes or other fibrous material can be specified if required.
- \*Despatch: Lead times quoted are in working weeks, and subject to current production availability at time of order. Where drawing sign-off is required, the quoted lead time is from receipt of drawing approval.
   Validity: 30 days from date of quotation
- Carriage: Included (with offloading by others unless otherwise stated by Dutypoint in writing)
- Payment: 30 Days from invoice date subject to approved credit account
- VAT: All prices are subject to VAT at the relevant current rate
- Terms: Dutypoint Ltd Terms and Conditions of Sale apply available at www.dutypoint.com
- **Discount:** The prices quoted are net and main contractors discount is not applicable
- *Retention:* No retention time/percentage will apply unless otherwise stated by Dutypoint in writing
- **Contract:** The goods are quoted on a 'supply' basis and a sub-contract cannot be accepted for this quotation unless otherwise stated by Dutypoint in writing. Where installation or commissioning is quoted and the customer requires these elements to be carried out as a sub-contract, a separate sub-contract may be accepted subject to the specific terms.

Dutypoint Ltd registered in England and Wales No. 09045694 Shepherd Road, Gloucester. GL2 5EL T. 01452 300592 F. 01452 303691 E. sales@dutypoint.com www.dutypoint.com