## Site: Meikle whiterashes, Turiff, Aberdeenshire, AB53 5RA



The largest Pollution index is then used to calculate discharge stack height.

## Calculation of Ub (uncorrected Discharge Stack Height for buoyancy)

Substituting the relevant values into the equation elbow, the heat release $(Q)$ is calculated

$$
Q=\quad 0.060587 \mathrm{MW}
$$

*The ambitient temperature is assumed to be $10^{\circ} \mathrm{C}(283 \mathrm{~K})$

The uncorrected discharge stack height due to buoyancy Ub is determined by the fallowing equation
$\mathrm{Ub}=10^{\wedge} \mathrm{a}^{*} \mathrm{Pi}^{\wedge} \mathrm{b}$

|  | $\mathrm{Q}<=1 \mathrm{MW}$ | $\mathrm{Q}>1 \mathrm{MW}$ |
| :--- | ---: | :--- |
| a | -0.878651451 | -0.99209 |
| b | 0.48391188 | 0.476537 |

Ub $\quad 2.804339 \mathrm{~m}$
Min Ub $1.144685 \mathrm{~m} \quad$ Ubmin $=1.95^{*} \mathrm{Q}^{\wedge} 0.19$

Calculation of Um (Uncorrected Discharge Stack Height for momentum)
The discharge momentum, $M$, is determined using the equation below:
$\mathrm{M}=283 / \mathrm{Td}^{*} \mathrm{~V}^{*} \mathrm{w} \quad=\quad 1.6160093 \mathrm{~m} 4 / \mathrm{s} 2$
$\log 10$ Um $=x+\left(y^{*}\right.$ LOG10*Pi+z)^0.5

| $x=-3.7+(\log 10 \mathrm{M})^{\wedge} 0.9$ | -3.45616829 |
| :--- | ---: |
| $\mathrm{y}=5.9-0.624^{*} \log 10 \mathrm{M}$ | 5.769931037 |
| $\mathrm{z}=4.24-9.7^{*} \log 10 \mathrm{M}+1.47(\log 10 \mathrm{M})^{\wedge} 2-0.07(\log 10 \mathrm{M})^{\wedge} 3$ | 2.281330476 |


| log10Um | 0.797966058 |
| :--- | :--- |
| Um | 6.280092754 |
| Min Um | 0.956127665 |

Reference Distance
(5*Um) 31.40046377

| Buildings | H $^{*}$ | W | K | T | R |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Rock Cliff | 7.6 | 10.0 | 7.6 | 19 | 4.7 |
| Agri Workshop | 8.4 | 27.0 | 8.4 |  | 21 |
|  |  |  |  |  |  |

* Height from the boiler ground level.

| Hm | 8.4 |
| :--- | ---: |
| Tm | 21 |
| U | 2.804339 |
| A | 2.23942 |
| C | $\mathbf{1 2 . 6 6} \mathrm{m}$ |

Total Flue height $10 \mathrm{~m}+2.7 \mathrm{~m}$ boiler height.

Total calculated Stack Height
12.7 m

