

Newberry Homes Ltd

# Proposed Development on Land off Garstang Road East, Poulton-le-Fylde FY6 7HL FRA & Drainage Strategy

D3941-R-01

**PSA Design Ltd** 

Consulting Engineers The Old Bank House 6 Berry Lane Longridge Preston PR3 3JA March 2023

Tel. 01772 786066 Fax. 01772 786265

www.psadesign.co.uk mail@psadesign.co.uk

# Proposed Development on Land off Garstang Road East, Poulton-le-Fylde FY6 7HL

## FRA & Drainage Strategy

Job	Date	Issue	Сору
D3941	March 2023	Original	

Originator...... D Wallbank ..... Checker...... G Sanderson ..... Approver...... D Wallbank .....

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# 1. Introduction and Planning History

- 1.1. PSA Design Ltd have been commissioned to provide a Flood Risk Assessment (FRA) and Drainage Strategy to support the planning application for the erection of 21 residential dwellings.
- 1.2. The existing site and its location are illustrated at Appendix A. As can be seen, the site currently comprises predominantly 'greenfield' land. It is noted that the site has an extant planning consent for 21 dwellings (04/01484/FULMAJ) and the Council has confirmed in correspondence dated 10/04/2007 that the development was lawfully commenced. As part of the extant consent there was an approved Drainage Scheme (reproduced at Appendix B) with <u>unrestricted</u> discharge to the public surface water sewer located in Poulton Drive.
- 1.3. The Proposed Site Layout Plan reproduced at **Appendix C**.
- 1.4. This document sets of the issues relating to flood risk and seeks to set out the principles of the drainage strategy for the proposed development. Once these principles have been agreed with both the LPA, Council Drainage Engineer, LLFA and United Utilities via the planning application process, they will clearly be subject to subsequent detailed design and formal applications such as a part 1 s106 application to United Utilities for connection (direct or indirect) to the public sewer network.

# 2. Flood Risk Assessment

- 2.1. Although not specifically requested by the LPA, for completeness, consideration has been given to flood risk associated with the proposals.
- 2.2. The National Planning Policy Framework (NPPF) and Planning Practice Guidance (PPG) set out Government policy aims on development and flood risk for England. The aim is to ensure flood risk is taken into account at all stages of the planning process, to avoid inappropriate developments in areas at risk of flooding, and to direct development away from areas of highest risk.
- 2.3. Flood mapping from the EA website is reproduced at **Appendix D**. This clearly indicates that the site is located within Flood Zone 1 and is at very low risk of flooding. Accordingly, with reference to Table 2 from PPG, the proposed development would fall into the "less vulnerable" category and, in accordance with Table 3, the site proposals within Flood Zone 1 would be

deemed "appropriate".

# There will therefore be no requirement for a Sequential Test or Exception Test to be carried out for this development.

2.4. The EA mapping indicates there is a low risk of surface water flooding in a small, isolated area within the site. This is as expected and results from localised depressions within the existing greenfield areas which may collect shallow areas of water in more extreme storm events. These discrete areas are contained within the site so do not result in any flood risk off-site and in any event would be dealt with as part of the formal drainage system proposed for the site as set out below.

There are therefore no pre-existing risks associated with the site from a flood perspective.

# 3. Drainage Strategy

## 3.1. North West SuDS Pro-Forma

3.1.1. The LPA has requested that the North West SuDS Pro-Forma (NWSPF) be completed to demonstrate compliance of the proposed surface water scheme. The completed form is included at **Appendix E** with the relevant aspects and supporting information set out below with reference to the relevant section of NWSPF as appropriate.

## 3.2. **Existing Drainage Situation** (NWSPF – Section 2)

- 3.2.1. As noted above, the existing site currently comprises a predominantly 'greenfield' site. There are no existing formal drainage or watercourses on the site.
- 3.2.2. Off the site, there is an existing United Utilities' large diameter (1800mm) public SW sewer in Poulton Drive running across the site access road. There is also a 150mm diameter public foul sewer running alongside the SW sewer.
- 3.2.3. The UU sewer record is reproduced at **Appendix F**. The UU records confirm the sewer infrastructure as set out above.

#### 3.3. Proposed Surface Water Management Strategy

- 3.3.1. With respect to dealing with surface water, National Planning Policy Framework (NPPF, 2021), requires that, for the range of annual flow rate probabilities, up to and including the 1% annual probability (1 in 100-year event) the developed rate of run-off from a proposed site should be no greater than the undeveloped rate of run-off for the same event. Even when the site is brownfield, the site should be treated as greenfield.
- 3.3.2. It is also important to account for climate change (CC) when making assessment of surface water run-off. As the development site is located within the Wyre Management Catchment area, reference to the peak rainfall allowance map sets out the allowances below:

Scenario	Event	Central Allowance	Upper End Allowance
3.3% annual exceedance	2050s	25%	35%
rainfall event	2070s	30%	45%
1% annual exceedance	2050s	25%	40%
rainfall event	2070s	35%	50%

Catchment Peak Rainfall Allowances - Use '2050s' for development with a lifetime up 2060 and use the 2070s epoch for development with a lifetime between 2061 and 2125.

- 3.3.3. Therefore CC should be taken into account by increasing the proposed rainfall intensity by 45% when assessing against the 3.3% (1 in 30) storm event and 50% when assessing against the 1% (1 in 100) storm event.
- 3.3.4. Given the nature of the proposed residential development, an additional uplift of 10% has been applied to allow for Urban Creep (UC).
- 3.3.5. It is important to note that since the approved drainage scheme would not have included for either of the above CC or UC allowances, this approach is considered to be very robust.

#### Hierarchical Approach - Soakaways (NWSPF Section 7)

3.3.6. Taking cognisance of the above (and in accordance with the hierarchical approach), the preferred surface water solution is to discharge to ground via soakaways. Even when there

are alternative sewer connections or watercourses available, infiltration must still be utilised unless it is proved unfeasible.

3.3.7. To this end percolation test pits were dug on site on 14<sup>th</sup> February 2023 as illustrated at Appendix G. As indicated, in each of the 6 pits dug across the site, groundwater was encountered at depths of between 0.7m and 1.1m below ground level.

# 3.3.8. It can therefore be concluded that soakaways are not a feasible solution for dealing with surface water at this site.

#### Hierarchical Approach - Watercourse (NWSPF Section 7)

3.3.9. The second solution in the hierarchical approach would be discharge to a watercourse, however this would not be feasible at this location, as there are no watercourses within the ownership of the Applicant or immediately adjacent to the site. However, it should be noted that the public SW sewer into which it is proposed to discharge (see below) itself discharges to a culverted watercourse some 100m to the south west of the site.

#### Hierarchical Approach – Surface Water Sewer

- 3.3.10. The next hierarchical solution would therefore be discharge to a SW sewer. As noted above, there is a 1800mm diameter public SW sewer running in a westerly direction in Poulton Drive across the site access road. It is therefore proposed to discharge to this existing SW sewer but restricted to Greenfield run-off rates for all storm events up to (and including) a 1 in 100 year event plus 50% uplift for CC, and 10% for UC (NWSPF Section 5).
- 3.3.11. Given the nature of the ground conditions set out above, there is no scope to incorporate volume control/long term storage, consequently, the Qbar (Approach 2) has been adopted in accordance with Technical Standards S6 (NWSPF Section 2).
- 3.3.12. The Qbar (i.e. 1 in 2 year greenfield run-off rate) has been calculated for the site (See Appendix H) and is 6.71/s. Clearly, the restriction down to 6.71/s for all storm events would provide significant betterment for the extreme flood events for example, the existing greenfield run-off for the site in a 1 in 100 year storm event is currently 14.05 l/s (NWSPF Section 3 & 4) and more so when compared to the unrestricted discharge associated with the previously approved scheme which could have resulted in unrestricted discharges in excess of 200l/s for a 1 in 100 year storm event.

- 3.3.13. To restrict surface water run-off from the proposed development it would be necessary to provide some form of attenuation storage on site. There are numerous ways of providing this, however, given that the Developer is seeking to offer up the drainage system for adoption, oversized pipes are proposed in this instance. The design of the system should ensure that run-off is limited to 6.7I/s and that there is no flooding of the site up to and including the 1 in 100yr storm + 50% CC + 10% UC (NWSPF Section 5).
- 3.3.14. An outline design based on the above criteria has been modelled and illustrated on Drawing No. D3941-OD-01 reproduced at **Appendix I**. The supporting calculations are included as **Appendix J**. The calculations demonstrate that the above storm criteria base on a 6.7l/s restriction is adequately contained and maintained within the system (NWSPF Section 5).

#### Water Quality (NWSPF Section 6)

- 3.3.15. The SuDS design should seek to provide an appropriate management train of SuDS components to effectively mitigate the pollution risks associated with the different site uses.
- 3.3.16. In accordance with Table 4.3 of The SuDS Manual CIRIA C753, the pollution hazard level is considered to be 'Low' to 'Very Low' for the proposed development. Therefore, the requirements for discharge to surface waters state that the 'Simple index approach' should be used.
- 3.3.17. The first step of the simple index approach is to identify the pollution hazard indices for the proposed land use. Table 26.2 of The SuDS Manual states the following

Land use	Pollution hazard level	Total suspended solids (TSS)	Metals	Hydro- carbons
Residential Roofs	Very Low	0.2	0.2	0.05
Individual property driveways, residential car parks, low traffic roads and non-residential car parking with infrequent change (i.e. <300 movements/day)	Low	0.5	0.4	0.4
Total		0.7	0.6	0.45

#### Total Pollution Hazard Indices

3.3.18. Suitable SuDS should then be selected with a total pollution mitigation index that equals or exceeds the pollution hazard index. Given that the highest pollution hazard level (Low) is

associated with property driveways, it is proposed that these be formed in permeable paving in order to provide a level of primary treatment.

3.3.19. Table 26.3 of The SuDS Manual sets out the indices for proposed SuDS features. Those features included on the proposed design presented are listed in the table below. Where treatment components are used together in series a factor of 0.5 is used to account for the reduced performance of the secondary or tertiary components.

Type of SuDS Component	Total suspended solids (TSS)	Metals	Hydro-carbons
Permeable Pavement	0.7	0.6	0.7
Total	0.7	0.6	0.7

Total Pollution Hazard Indices – Proposed SuDS Features

3.3.20. It can be seen that the total mitigation index for the proposed SuDS features is greater or equal to the required pollution hazard index for the proposed land use. Therefore, the proposed system meets the water quality requirements.

# 3.3.21. It has therefore been demonstrated that a SuDS solution that meets with the requirements of current legislation is deliverable within the constraints of the site.

# 3.4. Surface Water Summary

- 3.4.1. Clearly the above approach represents a robust treatment of surface water attributable to the proposed development which would be in accordance with the 'hierarchical' approach and the NWSPF. Moreover, the proposals represent significant betterment to the unrestricted discharge previously approved for the site.
- 3.4.2. It is also clear that there will be ample capacity within the existing UU system downstream, as this was designed and constructed to accommodate unrestricted discharge from the previously approved scheme.

## 3.5. Proposed Foul Drainage System

- 3.5.1. As noted above, there is a 150mm diameter foul sewer running along Poulton Drive across the site frontage and it is therefore proposed to discharge foul drainage to this sewer. This is indicated on Drawing D3941-OD-01 reproduced at **Appendix I**.
- 3.5.2. Subject to United Utilities formal approval and formal s106 process, it is clear that there is a means of dealing with foul sewage from the proposed development.

## 3.6. Phasing

3.6.1. The drainage system will be constructed early in the construction phase and would be operational prior to occupation of any residential unit.

## 3.7. Maintenance of Proposed SuDS Systems (NWSPF Section 8)

- 3.7.1. It is important during any development process to consider the long-term maintenance of the proposed drainage system. The way this is processed will largely depend on how the system is taken forward at detailed design.
- 3.7.2. The SuDS will be reviewed and approved by the Local Planning Authority (LPA) in consultation with the Lead Local Flood Authority (LLFA) and United Utilities, to ensure it meets the relevant standards. It is understood that the system will be offered up for adoption by United Utilities. Failing this, the SuDS would remain private and be maintained and managed by the land owner in accordance with a SuDS management plan. This plan could also be secured through planning condition or legal agreement if necessary.

# 4. Conclusion

- 4.1. It has been demonstrated, that the proposed development would be deemed appropriate development in terms of flood risk and a SuDS solution that meets with the requirements of current legislation is deliverable within the constraints of the site and will ensure that flood risk both on and off site will not be exacerbated. Furthermore, the current proposals represent significant betterment when compared to the unrestricted discharge previously approved for the site.
- 4.2. The proposed strategy would therefore be in accordance with relevant Local Plan policy, NPPF and the North West SuDS Pro-Forma. Accordingly, there should be no flood risk or drainage reasons why the proposals should not be granted planning consent.

Appendix A

Existing Site and Location







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<b>PSA</b>						
D	Е	S	T	G	Ν	

PSA Design	Client	
6 Berry Lane, Longridge	Job	
Tel. 01772 786066	Title	

t	Newbury Homes Ltd	Drawn	HP	Date	ate 07/03/2023		Drawing No.					
	Garstang Road, Poulton	Checked	DLW			_ Figure 1						
	Site Location Plan (indicative site boundaries shown)	Approved	DLW	Scale	NTS	Rev				Τ	Τ	-





PSA Design	
The Old Bank House	L
6 Berry Lane, Longridge	
Preston, PR3 3JA	┝
Tel. 01772 786066	

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Client	Newbury Homes Ltd	Drawn	HP	Date	07/03/2023	Drawing No.					
Job	Garstang Road, Poulton	Checked	DLW			Figure 2					
Title	Site Area Plan	Approved	DLW	Scale	NTS	Rev					

Ν

# Appendix B

Approved Drainage Scheme – Extant Consent



				& surround 51
uare Access Gully nnection Detail 13-P Waste or RWP max od 58 mm dia or 65 square Access Gully 4A12A Polypropylene grid (provided)	Paved Area Gully Connection Detail GC6-P NB- A Raising Piece code 4A17E inserted between the Hopper & the base can be used to increase the gully depth to 600 mm max	Rodding Point Installation Detail AP1-P Square Rodding Point - code 4A10SA	Mini Access Chamber Installation Detail AP2-P Minl Access Chamber code SDAC1/1 max 600 mm deep Topsoll Topsoll	Polypropylene Inspection Chambe Installation Detail AP3-P Round Ductile Iron cover & frame code SPK8 Square otright cover & frame code SPCR8 Topsoli
movable	G.L. Paved Area Gully code 4A22A Removable Dip Tube	Concrete bed Short length of pipe cut to suit	Sited In landscaped areas	Sited In landscoped areas

Appendix C

Proposed Site Layout Plan



All project and associated works shall comply with the relevant statutory requirements including but not limited to the applicable planning and building control legislation whether or not specifically shown on this plan.

#### OVERALL SITE AREA

approx. 1.1067Ha (2.73a)

#### APPROVED EXTANT PERMISSION ref 04/01484 21 Dwellings = 2 affordable + 19 open market

housetype ref	description type	number of each housetype	overall no o open sale	of bedrooms affordable			
open market housing							
WD9A	5 bed detached	3	15				
WD8A	5 bed detached	3	15				
WD7A	4 bed detached	2	08				
WD6A	3 bed detached	5	15				
WD4A / 5A	2 bed flat	6	12				
	ket 19 units	65 bedrooms					
affordable housing							
anoraabie i							
WD4A	1 bed flat	2		2			
WD4A	1 bed flat total affordable	2 e 2 units	– – 2 bedre	2 poms			
WD4A overall total	1 bed flat total affordable	2 e 2 units 21 units	– – 2 bedro 67 overa	2 coms all bedrooms			
WD4A	1 bed flat total affordable	2 e 2 units 21 units	– – 2 bedro 67 overa	2 coms all bedrooms			
WD4A overall total approved P	1 bed flat total affordable OS 21 uni	2 e 2 units 21 units ts (67 beds)	 2 bedre 67 overa 0.084Ha	2 coms all bedrooms a (0.2a)			

#### PROPOSED AMENDED LAYOUT HOUSETYPES 21 Dwellings = 6 affordable + 15 open market

housetype	description	number of	overall no c	of bedrooms			
ici i	type	each nousetype	opensale	alloluable			
open market housing							
WD	4 bed detached	3	20				
BL	4 bed detached	4	16				
F	3 bed detached	3	09				
W	3 bed detached	3	09				
	total open mai	rket 15 units	54 bedro	ooms			
affordable h	nousing						
А	3 bed semi det	2		6			
В	2 bed mews	4		8			
	14 bedro	ooms					
overall total		21 units	68 overall bedroor				
proposed POS 21 units (68 beds) 0.147Ha (0.36a)							

increase in POS area of 75% above the current extant approval

# **JFYLDE** DESIGN

hello@fyldedesign.com telephone\_0773 954 2345 C Fylde Design Associates Ltd

g	PROP	OSED AM	IENDED SITE L	AYOUT
ject	Resider	ntial Dev	elopment ad	ljoining
	Gar	stang Ro	ad, Poulton l	e Fylde
nt	TH	E BAX	KTER GR	OUP
e	sheet	scale	drawing no	revision
07.2022	A3L	1;500	FD2102_10	A

Appendix D

EA Flood Mapping



# Flood map for planning

Your reference <Unspecified>

Location (easting/northing) 335786/439361

Created **7 Mar 2023 11:46** 

Your selected location is in flood zone 1, an area with a low probability of flooding.

# You will need to do a flood risk assessment if your site is any of the following:

- bigger that 1 hectare (ha)
- In an area with critical drainage problems as notified by the Environment Agency
- identified as being at increased flood risk in future by the local authority's strategic flood risk assessment
- at risk from other sources of flooding (such as surface water or reservoirs) and its development would increase the vulnerability of its use (such as constructing an office on an undeveloped site or converting a shop to a dwelling)

## Notes

The flood map for planning shows river and sea flooding data only. It doesn't include other sources of flooding. It is for use in development planning and flood risk assessments.

This information relates to the selected location and is not specific to any property within it. The map is updated regularly and is correct at the time of printing.

Flood risk data is covered by the Open Government Licence **which** sets out the terms and conditions for using government data. https://www.nationalarchives.gov.uk/doc/open-government-licence/version/3/

Use of the address and mapping data is subject to Ordnance Survey public viewing terms under Crown copyright and database rights 2022 OS 100024198. https://flood-map-for-planning.service.gov.uk/os-terms



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# Newberry Homes Ltd Proposed Development on Garstang Road East, Poulton-le-Fylde FY6 7HL FRA & Drainage Strategy





● High ● Medium ● Low ○ Very Low ◆ Location you selected

Appendix E

NW SuDS Pro-Forma

# **SECTION 1**. APPLICATION & DEVELOPMENT DETAILS

Diagning Application Reference (if quailable)	TE	BC
<b>State type of planning application</b> <i>i.e. Pre-application, Outline, Full, Hybrid, Reserved Matters</i> * *Information only required if drainage is to be considered as part of reserved matters application	Full App	blication
Developer(s) Name:	Newberry	Homes Ltd
Consultant(s) Name:	PSA De	sign Ltd
Development Address (including postcode)	Land off Garsta Poulton-le-Fy	ang Road East, /Ide FY6 7HL
Development Grid Reference (Eastings/Northings)	335797	439346
Total Development Site Area (Ha)	1.01	1Ha
Drained Area (Ha)* of Development	0.5	Ha
<b>Please indicate the flood zone that your development is in. Tick all that apply.</b> Based on the Environment Agency Flood Map for Planning and the relevant Local Authority Strategic Flood Risk Assessment (to identify Flood Zones 3a/3b).	Fl Flo Flo Flo	ood Zone 1 ✓ od Zone 2 □ od Zone 3a □ od Zone 3b □
What is the surface water risk of the site? Tick all that apply. Based on the Environment Agency Surface Water Flood Map.		High □ Medium □ Low ✓
Have you submitted a Site Specific Flood Risk Assessment (FRA)? See separate guidance notes for clarification on when a FRA is required	Yes ✓	No 🗆
Have you submitted a Sustainable Drainage Strategy?	Yes ✓	No 🗆
Does your drainage proposal provide multi-functional benefits via SuDS?	Yes ✓	No 🗆
<b>Expected Lifetime of Development (years)</b> Refer to Planning Practice Guidance "Flood Risk and Coastal Change" Paragraph 026	10	00
Development Type:		State Proposed Number of Units
Greenfield Site <ul> <li>Site is wholly undeveloped, and a new drainage system will be installed</li> </ul>	~	21
Previously Developed/ Brownfield Site		
<ul> <li>Site is already developed, and the <u>entirety</u> of the existing surface water drainage system will be used to serve the new development (evidence must be provided to prove existing surface water drainage system is reusable); <u>OR</u></li> </ul>		
<ul> <li>Where records of the previously developed system are not available so that the hydraulic characteristics of the system cannot be determined or where the drainage system is not in reasonable working order i.e. broken, blocked or no longer operational for other reasons.</li> </ul>		
Please list any relevant document and or drawing numbers (including revision reference) to support your answers to Section 1.	See FRA/ Draina Appendices	ge Strategy and

# **SECTION 2**: IMPERMEABLE AREA AND EXISTING DRAINAGE

	Existing (E)	Proposed (P)	Change (P – E)
State Impermeable Area (Ha)	0	0.5	0.5
<b>Evidence Required:</b> Plans showing development layout of site with existing and proposed impermeable areas.			~

Are there existing sewers, watercourses, water bodies, highway drains, soakaways or filter drains on the site?	Yes ✔No □ Don't Know □
Evidence Required:	
Plan(s) showing existing layout to include all:	$\checkmark$
Watercourses, open and culverted	
Water bodies – ponds, swales etc.	
Sewers, including manholes	
Highway drains, include manholes, gullies etc.	
Infiltration features - soakaways, filter drains etc.	

#### **Drainage Design**

<u>Outline planning applications</u> should be able to demonstrate that a suitable drainage system is achievable. <u>All other type of planning application</u> should provide full details or reference to previous planning application where drainage details have been submitted or approved.

 $\checkmark$ 

Select which design approach you are taking to manage water quantity (refer to Section 3.3 SuDS Manual)

#### Approach 1 – Volume control / Long Term Storage (Technical Standards S2/3, S4/5)

•	The attenuated runoff volume for the 1 in 100 year 6 hour event (plus climate change allowance) is limited
	to the greenfield runoff volume for the 1 in 100 year 6 hour event, with any additional runoff volume
	utilising long term storage and either infiltrated or released at 2 l/s/ha

- The discharge rate for the critical duration 1 in 1 year event is restricted to the 1 in 1 year greenfield runoff rate
- The discharge rate for the critical duration 1 in 100 year event (plus climate change allowance) is restricted to the 1 in 100 year greenfield runoff rate

#### Approach 2 – Qbar (Technical Standards S6)

• Justification has been provided that the provision of volume control/long term storage is not appropriate and an attenuation only approach is proposed. All events up to the critical duration 1 in 100 year event (plus climate change allowance) are limited to Qbar (1 in 2 year greenfield rate) or 2 l/s/ha, whichever is greater.

#### **Evidence Required:**

Plans showing:

- Existing flow routes and flood risks
- Modified flow routes
- Contributing and impermeable areas
- Current (if any) and proposed 'source control' and 'management train' locations of sustainable drainage components (C753 Chapter 7)
- Details of drainage ownership
- Details of exceedance routes (Technical Standards S9)
- Topographic survey
- Locations and number of existing and proposed discharge points

Note consideration should be given to manage surface water from both impermeable and permeable surfaces (including gardens and verges) likely to enter the drainage system.

Please list any relevant document and or drawing numbers (including revision	See FRA/ Drainage Strategy and
reference) to support your answers to Section 2.	Appendices

# **SECTION 3**: PEAK RUNOFF <u>RATES</u> - TECHNICAL STANDARDS S2, S3 AND S6 (UNLESS S1 APPLIES)

Rainfall Event	Existing Rate (I/s)	Greenfield Rate (l/s)	Proposed Rate (I/s) Previously developed sites - In line with S3 should be equivalent to Greenfield runoff rates – discuss with LLFA if this is not achievable pre-application
<b>Qbar</b> (Approach 2)		6.7	6.7
<b>1 in 1 Year Event</b> (Approach 1)		5.9	4.6
1 in 30 Year Event		11.5	4.81
1 in 100 Year Event* (Approach 1)		14.1	6.7

\* Total discharge at the 1 in 100 year rate should be restricted to the greenfield runoff volume for the 1 in 100 Year 6 hour event with additional volumes (long-term storage volume) released at a rate no greater than 2 l/s/ha where infiltration is not possible. The climate change allowance should only be applied to the proposed rate and not the existing or greenfield rate.

<b>Evidence Required:</b> Methodology used to calculate peak runoff rate clearly stated and justified.	$\checkmark$
Impermeable areas plan, supported by topographical survey confirming positive drainage.	$\checkmark$
Hydraulic calculations and details of software used.	

State the hydraulic method used in your calculations (Refer to Table 24.1 of The SuDS Manual)	IH124
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Please list any relevant document and or drawing numbers (including revision	See FRA/ Drainage Strategy and	
reference) to support your answers to Section 3.	Appendices	

# **SECTION 4**: DISCHARGE <u>VOLUME</u> – TECHNICAL STANDARDS S4, S5 AND S6 (UNLESS S1 APPLIES)

Rainfall Event	Existing Volume (m <sup>3</sup> )	Greenfield Volume (m <sup>3</sup> )	Proposed Volume (m³)
1 in 100 Year 6 Hour Event (Approach 1)N/AN/A		N/A	
<b>Does the below statement apply to your development proposal?</b> Long term storage is not achievable on this site and, in accordance with S6 of the Non Statutory Technical Standards for SuDS, the surface water discharge rates for events up to and including the 1 in 100 year critical event are limited to Qbar (Approach 2)			Yes ✔ No 🗆
<b>Evidence Required:</b> Approach to managing the quantity of surface water leaving the site clearly stated and justified			
Methodology used to calculate discharge volume clearly stated and justified. Hydraulic calculations and details of software used.			

Please list any relevant document and or drawing numbers (including revision reference)	
to support your answers to Section 4.	

# **SECTION 5**: STORAGE – TECHNICAL STANDARDS S 7 AND S 8

State climate change allowance used (%)	50
State housing density (houses per ha)	21
State urban creep allowance used (%)	10
<b>Evidence Required:</b> State / used in appropriate industry standard surface water management design software.	✓

State storage volume required (m <sup>3</sup> ) (excluding non-void spaces)	260	
Must include an allowance for climate change and urban creep		
Have you incorporated interception into your design? (Refer to Chapter 24 of The SuDS Manual C753) Where possible, infiltration or other techniques are to be used to try and achieve zero discharge to receiving waters for rainfall depths up to 5mm.	Yes 🗌 No 🗸	
<b>Evidence Required:</b> Drainage plans showing location of attenuation and all flow control devices and supporting calculations.	✓ See Report	

Summarise how storage will be provided for 1 in 30 year event on site.	Within oversized pipe system
Storage must be designed to ensure that at no flooding occurs onsite in a 1 in 30 year event except in designed areas <u>and</u> no flooding occurs offsite in a 1 in 100 year (plus climate change allowance) event.	
Summarise how storage will be provided for 1 in 100 year (plus climate change) event on site.	Within oversized pipe system
Where storage above the 1 in 30 year rainfall event is provided in designated areas designed to accommodate excess surface water volumes, plans showing storage locations and surface water depths and supported by calculations used in appropriate industry standard surface water management design software. It is important to run a range of duration events to ensure the worst case condition is found for each drainage element on the site	
<b>Evidence Required:</b> Plans showing size and location of storage and supporting calculations. Where there is controlled flooding, extents and depths must be indicated.	✓ See Report

Please list any relevant document and or drawing numbers (including revision	See FRA/ Drainage Strategy and	
reference) to support your answers to Section 5.	Appendices	

# SECTION 6: WATER QUALITY PROTECTION

Contaminated surface water run-off can have negative impacts on the quality of receiving water bodies. The potential level of contamination will influence final the design of an appropriate treatment train as part of your sustainable drainage system.

Is the proposal site known to be or potentially contaminated?	Yes 🗆	No√
•••		

• If the site is contaminated, it should be demonstrated that the sustainable drainage system will not increase the risk of pollution to controlled waters though the mobilisation of contaminants and/or creation of new pollution pathways.

Confirm the Pollution Hazard Level of the proposed development - Tick ALL that apply

*Refer to Pollution Hazard Indices for different Land Use Classifications in Table 26.2 of The SuDS Manual C753 for further guidance.* 

Pollution Hazard Level Tick <u>ALL</u> that apply		Surface water run-off from the proposed development will drain from:		
VERY LOW	$\checkmark$	Residential roofs		
LOW	~	<ul> <li>Other roofs (typically commercial/industrial roofs)</li> <li>Individual property driveways, residential car parks, low traffic roads (e.g. cul de sacs, home-zones and general access roads)</li> <li>Non-residential car parking with infrequent change (e.g. schools, offices) i.e. &lt; 300 traffic movements/day</li> </ul>		
MEDIUM		<ul> <li>Commercial yard and delivery areas</li> <li>Non-residential car parking with frequent change (e.g. hospitals, retail)</li> <li>All roads except low traffic roads and trunk roads/motorways<sup>2</sup></li> </ul>		
нідн 🗆		<ul> <li>Sites with heavy pollution (e.g. haulage yards, lorry parks, highly frequented lorry approaches to industrial estates, waste sites)</li> <li>Sites where chemicals and fuels (other than domestic fuel oil) are to be delivered, handled, stored, used or manufactured</li> <li>Industrial sites</li> <li>Trunk roads and motorways<sup>1</sup></li> </ul>		

If the development's Pollution Hazard Level is 'Very Low' or 'Low', has the sustainable drainage design been risk assessed and appropriate mitigation measures included? Yes ✓ No□

• If the proposed development has a very low or low polluting potential, you should design your sustainable drainage system to include an appropriate treatment train in accordance with The SuDS Manual (C753).

lf t su	he development's Pollution Hazard Level is 'Medium' or 'High', is the application oported by a detailed water quality risk assessment?	Yes 🗆	No□	
•	• If the proposed development has a high polluting potential, a detailed risk assessment will be required to identify an			

• If the proposed development has a high polluting potential, a detailed risk assessment <u>will</u> be required to identify an appropriate SuDS treatment train and ensure compliance with Paragraph 170 of the National Planning Policy Framework.

• If the proposed development has a medium polluting potential, a detailed risk assessment <u>may</u> be required depending on the nature, scale and location of the development.

Has pre-application advice on water quality been obtained from the Environment Agency?			No√
If YES, provide details:			

<sup>&</sup>lt;sup>2</sup>Motorways and trunk roads should follow the guidance and risk assessment process set out in Highways Agency (2009).

Please list any relevant document and or drawing numbers (including revision	See FRA/ Drainage Strategy and	
reference) to support your answers to Section 6.	Appendices	

# **SECTION 7** : DETAILS OF YOUR SUSTAINABLE DRAINAGE SYSTEM

# a) Function of your Sustainable Drainage System

Do your proposals store rainwater for later use (as a resource)?	Yes 🗌 🛛 No 🗸
Evidence Required:	
Please provide a brief sentence in the adjacent white box to describe how this function has	
been achieved.	

Do your proposals promote source control to manage rainfall close to where it falls? (e.g. promoting natural losses through soakage, infiltration and evapotranspiration)	Yes 🗆	No ✓
Evidence Required:		
Please provide a brief sentence in the adjacent white box to describe how this function has		
been achieved.		

Please list any relevant document and or drawing numbers (including revision reference) to support your answers to Section 7a.

# b) Hierarchy of Drainage Options – Planning Practice Guidance

The proposed method of discharge are set out within order of priority. Generally, the aim should be to discharge surface run off as high up the following hierarchy of drainage options as reasonably practicable.

Proposed method of surface water discharge		Is this proposed?	
Hierarchy Level 1: Into the ground (via infiltration)		Yes □ No ✓	
	If YES - Evidence Required		If NO – Evidence Required Tick <u>ALL</u> that apply
	<ul> <li>A. Completed Infiltration Checklist from The SuDS Manual (C753) Appendix B An editable version of this form is available on <u>SusDrain website.</u></li> <li>B. British Geological Survey (BGS) Infiltration SuDS Map</li> </ul>	<ul> <li>✓</li> </ul>	<ul> <li>A Site investigation to demonstrate that the ground is not free draining.</li> <li>Test results to be provided in accordance with:         <ul> <li>The methodology within BRE 365 (2016), <u>OR</u></li> <li>Falling head permeability tests BS EN ISO 22282-2: 2012</li> </ul> </li> <li>B. NOTE: where an applicant is unable to access a site to undertake testing, e.g. where unable to access a site for an</li> </ul>
			outline application, they can submit a <u>SuDS GeoReport</u> or similar.
	C. Infiltration testing to BRE 365 (2016) or falling head permeability tests to BS EN ISO 2228-2: 2012 (optional for outline)		C. Evidence to confirm that infiltration to ground would result in a risk of deterioration to ground water quality.
	'Plan B' sustainable drainage plan and statement of approach with an alternative discharge method, in case infiltration proposals are proven not feasible upon		D. Geotechnical advice from a competent person* which determines that infiltration of water to ground would pose an unacceptable risk of geohazards to the site and/or local area.

further site specific ground investigation
e.g. to consider seasonal variations to
groundwater

Proposed method of surface water discharge		Is this proposed?					
Hierarchy Level 2: To a surface water body (select type)		Yes 🗆 No 🗸	N/A 🗆				
NOTE: Co	nsent from LLFA or Permit from Environme	nt Ager	ісу	Main river	Canal		
may be re	equired – refer to guidance			Ordinary watercourse	Other water body		
If YES - Evidence Required			If NO – Evidence Requi Tick <u>ALL</u> that apply	red			
	Surface water body / watercourse survey		Plan sho	owing nearby watercourses and water	erbodies		
	and report	AND					
		~	Stateme	ent providing justification in your Sus	stainable Drainage Strategy		
			Note: W applicar	<b>Note:</b> Where discharge of any element in the hierarchy is discounted applicant should provide justification. If the reasoning for discounting			
		discharge of surface water to watercourse relates to issues associated					
		with third party who of the securing of any other required consent, it					
		may be necessary for the applicant to provide evidence to the local planning authority to support their proposed approach.					

Proposed method of surface water discharge			Is this propo	sed?	
Hierarchy Level 3: To a surface water sewer or highway drain (select type)			drain	Yes ✔ No 🗆	N/A 🗆
				✓ Surface water sewer	🗌 Highway drain
If YES - Evidence Required				If NO — Evidence Require Tick <u>ALL</u> that apply	ed
	Written correspondence from Water and Sewerage Company/ Highway Authority regarding proposed connection.	Plan showing nearby sewers and highway drains AND			ins
		Statement providing justification in your Sustainable Drainage S			ainable Drainage Strategy

Proposed method of surface water discharge		Is this propo	osed?	
Hierarchy Level 4: To combined sewer		Yes 🗆 No 🗸	N/A 🗆	
If YES - Evidence Required		If NO – Evidence Require	ed	
	Written correspondence from Water and Sewerage Company		N/A	

Please list any relevant document and or drawing numbers (including revision reference) to support your answers to Section 7b.	See FRA/ Drainage Strategy and Appendices	

# c) Proposed SuDS Component Types

	Tick ALL that apply				
Within property boundary	□ Rainwater harvesting	□ Green/ blue roofs	✓ Pervious avements [Type: A □ B □ C ✓	🗆 Soakaway	☐ Bio retention systems

	Tick ALL that apply				
	□ Infiltration system		Filter string	Filter drains	
	[ <b>Type:</b> 🗌 Surface le	vel 🗌 Below ground]	L Filter strips	Filter drains	
Within development site boundary	□ Bio retention system	Detention basins	Ponds and     wetlands	<ul> <li>Attenuation</li> <li>tanks/ Oversized</li> <li>pipes</li> </ul>	□ Other (state below)
(not property)	If 'Other' please state:				

Off site	Please state:
(not within the	
boundary of the	
proposed	
development)	

I confirm that the above selected components have been designed in accordance with The SuDS Manual (C753).	I confirm ✓
I confirm that the management of flows resulting from rainfall in excess of a 1 in 100 year plus climate change rainfall event, and their exceedance route(s), has been fully considered in order to minimise the risks to people, property (new and existing) and infrastructure.	I confirm ✓

Please list any relevant document and or drawing numbers (including revision	See FRA/ Drainage Strategy and Appendices	
reference) to support your answers to Section 7c.	, ppendicee	

# **SECTION 8:**OPERATION AND MAINTENANCE – TECHNICAL STANDARD S 12 AND NATIONAL PLANNING POLICY FRAMEWORK

The applicant is responsible to ensure that ALL components selected in Section 7 can be maintained for the design life of the development. This information is required so the Local Planning Authority can ensure the maintenance and management of the sustainable drainage system. The Local Planning Authority will discuss how this will be secured (e.g. via planning condition or planning obligation).

	Information Provided?
Management Plan	Yes □ No ✓ N/A
Evidence Required:	
Plan/ drawing provided to show the position of the different SuDS components with:	
<ul> <li>Key included to identify any of the adopting bodies that you will be offering your</li> </ul>	
sustainable drainage components for adoption (relates to maintenance and management arrangements below).	
Plan/ drawing to identify any areas where certain activities are prohibited, detailing	
reasons why.	
Action plan for accidental pollutant spillages.	

	Informati	on Provided?
Maintenance Schedule	Yes 🗆	No ✓ N/A
Evidence Required:		
A copy of the maintenance schedule including:		
1. Proactive and preventative maintenance		
Detailing regular, occasional and remedial maintenance activities including		
recommendations for inspection and monitoring. This should include recommended		
frequencies, advice on plant/ machinery required and an explanation of the objectives		
for the maintenance proposed and potential implications of not meeting them.		
2. Reactive and corrective maintenance (e.g. product repair and replacement).		
Including advice on excavations, or similar works, in locations that could affect the SuDS		

	Information Provided?
Maintenance and Management Arrangements	Yes イ No 🗆
<b>Evidence Required:</b> Evidence of formal agreement with the party responsible for undertaking maintenance.	
Please select any of the adopting bodies that you will be offering your sustainable drainage components for adoption. Tick all that apply.	
✓ Water and Sewerage Company Section 104 agreement (Water Industry Act 1991)	
Local Authority Public Open Space [Refer to Local Authority Policy]	
Please select the arrangement(s) for all non-adopted sustainable drainage components. Tick all that apply.	
□ Management Company ✓ Property Owner (for SuDS components within property boundary only)	
□ <b>Other</b> (please state)	

Please list any relevant document and or drawing numbers (including revision	See FRA/ Drainage Strategy and	
reference) to support your answers to Section 8.	Appendices	

# **DECLARATION AND SUBMISSION**

This pro-forma has been completed using evidence from information which has been submitted with the planning application.

The information submitted in the Sustainable Drainage Strategy and site-specific Flood Risk Assessment (FRA), where submitted, is proportionate to the site conditions, flood risks and magnitude of development and I agree that this information can be used as evidence to this sustainable drainage approach.

Submitter Details								
Completed by	G Sanderson	Email Address	gs@psadesign.co.uk					
<u>Completed</u> by		Telephone Number(s)	01772 786066					
Signed off by	D Wallbank	Accreditation(s) and/or Qualification(s) of Signatory	B.Eng (Hons) Civil Engineering, C Eng, MICE					
Date (dd/mm/yyyy)	7/3/2023	Company	PSA Design Ltd					

Client Details			
Name	Mr D Thornhill	Company	Newberry Homes Ltd

Appendix F

United Utilities' Sewer Record



Appendix G

**Percolation Test Pits** 



Trial Pit 1: Water encountered at 0.8m BGL

Trial Pit 2: Water encountered at 0.9m BGL

Trial Pit 3: Water encountered at 0.7m BGL

Trial Pit 4: Water encountered at 0.9m BGL

Trial Pit 5: Water encountered at 1.1m BGL

Trial Pit 6: Water encountered at 0.7m BGL

PSA	PSA Design The Old Bank House	Client	wberry Homes Ltd Draw		Drawn DW Da		February 2023	Drawing No.			
	6 Berry Lane, Longridge	Job	Land off the Blossoms, Poulton le Fylde	Checked				Figure 1			
engineering your environment	Tel. 01772 786066	1772 786066 Title	Percolation Test Locations	Approved		Scale	NTS	Rev			

Trial Pit 1	Trial Pit 2	Trial Pit 3	Trial Pit 4
Trial Pit 5	Trial Pit 6		Trial Pit 1: Water encountered at 0.8m BGL Trial Pit 2: Water encountered at 0.9m BGL Trial Pit 3: Water encountered at 0.7m BGL Trial Pit 4: Water encountered at 0.9m BGL Trial Pit 5: Water encountered at 1.1m BGL Trial Pit 6: Water encountered at 0.7m BGL
<b>DCA</b> PSA Design	Client Nowberry Homes Ltd		Drawing No.

PSA	PSA Design The Old Bank House	Client	Newberry Homes Ltd Drawn DW		Newberry Homes Ltd Drawn DW Date February		February 2023	Brawing No.				
	6 Berry Lane, Longridge	Job	Land off the Blossoms, Poulton le Fylde	Checked			Figure 2					
engineering your environment	Tel. 01772 786066	Title	Percolation Test Pits	Approved	Scale	NTS	Rev			Τ		

Appendix H

Qbar Greenfield Run-off Calculations



# Greenfield runoff rate estimation for sites

# www.uksuds.com | Greenfield runoff tool

Calculated by:	Graham Sanderson			
Site name:	Land off Poulton Drive		Latitude:	53.84639° N
Site location:	Poulton		Longitude:	2.97755° W
This is an estimatio with Environment Ag	n of the greenfield runoff rates that gency guidance "Rainfall runoff mana	Reference:	214753685	
SuDS Manual C753 ( greenfield runoff ra	Ciria, 2015) and the non-statutory sta tes may be the basis for setting con	ndards for SuDS (Defra, 2015). This information on sents for the drainage of surface water runoff from	Date:	Mar 06 2023 12:08

#### Runoff estimation approach IH124

Site characteristics				Notes			
Total site area (ha): 1	.010						
Methodology				(1) IS Q <sub>BAR</sub> < 2.0 I/S/ha?			
Q <sub>BAR</sub> estimation metho	d: Calcu	ulate from SPF	and SAAR	When $Q_{BAR}$ is < 2.0 l/s/ha then limiting discharge rates			
SPR estimation method	l: Calcu	ulate from SOI	Ltype	are set at 2.0 l/s/ha.			
Soil characteristics		lt Edite	ed				
SOIL type:	4	4		(2) Are flow rates < 5.0 l/s?			
HOST class:	N/A	N/A		Where flow rates are less than 5.01/2 someont for			
SPR/SPRHOST:	0.47	0.47		discharge is usually set at 5.0 l/s if blockage from			
Hydrological charac	teristics	Default	Edited	vegetation and other materials is possible. Lower consent flow rates may be set where the blockage			
SAAR (mm):		925	925	risk is addressed by using appropriate drainage			
Hydrological region:		10	10	elements.			
Growth curve factor 1 y	vear:	0.87	0.87	(3) Is SPR/SPRHOST ≤ 0.3?			
Growth curve factor 30	years:	1.7	1.7	Where are unductor levels are low analysis the use of			
Growth curve factor 10	0 years:	2.08	2.08	soakaways to avoid discharge offsite would normally			
Growth curve factor 200 years:		2.37	2.37	be preferred for disposal of surface water runoff.			

Greenfield runoff rates	Default	Edited
Q <sub>BAR</sub> (I/s):	6.76	6.76
1 in 1 year (l/s):	5.88	5.88
1 in 30 years (l/s):	11.49	11.49
1 in 100 year (l/s):	14.05	14.05
1 in 200 years (l/s):	16.01	16.01

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at www.uksuds.com/terms-and-conditions.htm. The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.

Appendix I

Proposed Drawings D3566-OD-01 - Proposed Drainage Strategy D3566-OD-02 – Areas Drawing



# Notes

- 1. Do not scale from this drawing, work to levels and dimensions shown, if not available refer to notes, if in doubt, refer to Engineer.
- 2. The Engineer shall be notified immediately, in writing, should any errors or discrepancies be found prior to to be commencement or continuation of any works.
- 3. Drawing to be read in conjunction with all other scheme drawings and relevant specifications.
- 4. Contractor to be responsible for the location and protection of all existing services.
- 5. Work to be undertaken in accordance in accordance with Design and Construction Guidance for foul and surface water sewers (App Ver 2.0) and Building Regulations - Document H.
- 6. All existing land drains encountered on site during construction are to be re-connected/diverted as necessary (not connected into the new system without prior approval)
- 7. All drains to be laid soffit to soffit unless otherwise indicated.
- 8. Steeper gradients may be used instead of backdrops.
- 9. Cover levels shown are approximate only and should be altered to suit finished surface levels.
- 10. Minimum depth of cover to crown of pipe without protection should be as follows:
- 0.35m Gardens and Pathways with no vehicular loading
- 0.50m Driveways, Parking Areas and Narrow Accesses with height restrictions to prevent entry by vehicles with a gross weight in excess of 7.5 tonnes
- 0.9m Driveways, Parking Areas and Narrow Accesses with limited access to vehicles with a gross weight in excess of 7.5 tonnes. Agricultural land and public open space.
- 1.2m Other Highways and Parking Areas with unrestricted access to vehicles with a gross weight in excess of 7.5 tonnes
- 11. All rainwater pipes (RWP) to be terminated at roddable gullies connected to a minimum 100mm dia. drain.
- 12. Unless stipulated otherwise or invert levels are provided, all surface water pipes to be minimum 100mm dia. laid at 1 in 100. Foul sewers to be minimum 100mm dia laid at 1 in 80 (1 in 40 if no WC connected).
- 13. Proposed PCC Manholes & Inspection Chambers and access points are to be as those defined in Design and Construction Guidance for foul and surface water sewers (App Ver 2.0). MH & IC diameters specified are minimum diameters and if necessary should be increased to accommodate minimum benching widths.
- 14. 450Ø diameter IC's > 1,2m deep to include reducing ring to reduce opening to max 350mm Ø

- 15. Drainage under carriageways Pipes up to 300mmØ to be structured walled PVCu or Clay. Pipes greater than 300Ø to be Concrete in accordance with BS 5911-1 and BS EN 1916. All pipes to be in accordance with Design and Construction Guidance for foul and surface water sewers (App Ver 2.0).
- 16. All plot drainage to be in accordance with Building Regulations Document H.
- 17. Road gullies shall be trapped 450Ø x 900mm deep with Class D400 frame and grating to BS EN 124 (unless otherwise approved. Outlets to be minimum 150mm diameter.
- 18. All drains in the vicinity of existing or proposed trees to be constructed in accordance with the requirements of NHBC.
- 19. Any drains passing through brick footings are to have r.c. lintels over and flexible joints either side. All drainage passing through external walls to have cement fibre sheet collars provided either side of wall to prevent vermin entry. All drains running under building to be encased in 100mm granular fill.
- 20. Where drain is within 1m of a building, the trench is filled with concrete up to the underside of the foundations and where the trench is further away than 1m from the building, the trench is filled with concrete to a level below the lowest level for the building equal to the distance from the building, less 150mm.
- 21. Installation of threshold drains to be the responsibility of the contractor in consultation with the scheme Architect. Threshold drainage should be installed where appropriate to ensure no surface water migration into properties. Where possible the contractor should assure that all private driveways are laid to disperse surface water to adjoining landscaped areas.
- 22. Drainage indicated on drawing around buildings spaced out for illustrative purposes, exact positions of drains may be altered to suit and determined on site prior to commencement of work (subject to maintaining minimum gradients and cover). Any revisions are to be subject to the approval of the Local Building Inspector and Structural Engineer.
- 23. Not all soil & rainwater pipes may be shown. Additional connections to be approved with Engineer, subject to minimum gradients and diameters.
- 24. All outfall levels and existing pipe levels should be checked prior to construction to ensure the design is deliverable and no clashes occur. Contractor to report any discrepancies to Engineer immediately.
- 25. Condition of any existing drainage to be used as part of proposed system to be checked prior to construction and any defects remedied.
- 26. All building drainage up to connection into chambers shown to be as per Architects Building Regulations drawings.

		Outfall connec Drainage sche	tion subject to S106 Part 1 and 2	Approval.			
P1	07/03/23	For Planning	0	GS	DLW		GS
		ľ	Newberry Homes Limte	ed	1-		Davi
	Land off Garstang Road East Poulton-le-Fylde Outline Drainage Proposal			Drwg F D39	941-OD-	-01 P1	
				Scale	ScaleSheet SAs ShownA1		
		<b>SA</b>	PSA Design Ltd The Old Bank House, 6 Berry Lane Longridge, Preston, PR3 3JA Tel. 01772 786066 www.psadesign.co.uk mail@psadesign.co.uk	e, Date Drawn <b>GS</b>	7 March Checke	n 20	<b>023</b> Approved





**Contributing Areas Drawing** 

Appendix J

Surface Water System Hydraulic Calculations









**Contributing Areas Drawing** 





#### Design Settings

Rainfall Methodology	FSR	Maximum Time of Concentration (mins)	30.00
Return Period (years)	1	Maximum Rainfall (mm/hr)	50.0
Additional Flow (%)	0	Minimum Velocity (m/s)	1.00
FSR Region	England and Wales	Connection Type	Level Soffits
M5-60 (mm)	17.000	Minimum Backdrop Height (m)	0.200
Ratio-R	0.400	Preferred Cover Depth (m)	1.200
CV	0.750	Include Intermediate Ground	$\checkmark$
Time of Entry (mins)	4.00	Enforce best practice design rules	$\checkmark$

#### <u>Nodes</u>

Name	Area (ha)	T of E (mins)	Cover Level (m)	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
MH1	0.062	4.00	14.200	1500	464.358	737.825	1.850
MH2	0.087	4.00	14.200	1500	437.079	723.571	2.160
MH3	0.068	4.00	13.700	1500	454.111	691.995	2.020
MH4	0.035	4.00	13.700	2400	454.661	685.323	3.360
MH5	0.052	4.00	13.700	2400	466.784	660.930	3.500
MH6	0.018	4.00	13.900	2400	479.050	667.197	3.750
MH7	0.062	4.00	14.200	2400	495.122	742.836	1.850
MH8	0.030	4.00	14.200	1500	511.360	718.853	2.200
MH9	0.007	4.00	14.200	1500	515.931	706.267	2.360
MH10	0.030	4.00	14.200	2400	513.971	691.704	3.815
MH11	0.010	4.00	14.200	2400	503.673	677.523	4.030
MH12	0.036	4.00	14.000	3000	491.036	667.223	3.900
UU			13.710	1500	502.056	639.047	3.920

<u>Links</u>

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)
1.000	MH1	MH2	30.779	0.600	12.350	12.040	0.310	99.3	225	4.39	49.3
1.001	MH2	MH3	35.877	0.600	12.040	11.680	0.360	99.7	225	4.85	47.3
1.002	MH3	MH4	6.695	0.600	11.680	11.610	0.070	95.6	225	4.93	47.0
1.003	MH4	MH5	27.239	0.600	10.340	10.200	0.140	194.6	1500	5.08	46.4
1.004	MH5	MH6	13.774	0.600	10.200	10.150	0.050	275.5	1500	5.17	46.0
1.005	MH6	MH12	11.986	0.600	10.150	10.100	0.050	239.7	1500	5.24	45.7
2.000 2.001	MH7 MH8	MH8 MH9	28.963 13.390	0.600 0.600	12.350 12.000	12.000 11.840	0.350 0.160	82.8 83.7	225 225	4.34 4.49	49.6 48.8

Name	Vel (m/s)	Cap (1/s)	Flow (I/s)	US Denth	DS Denth	Σ Area (ha)	Σ Add Inflow	Pro Denth	Pro Velocity
	(1173)	(1/3)	(1/3)	(m)	(m)	(na)	(I/s)	(mm)	(m/s)
1.000	1.312	52.2	8.3	1.625	1.935	0.062	0.0	60	0.963
1.001	1.309	52.1	19.1	1.935	1.795	0.149	0.0	94	1.213
1.002	1.337	53.2	27.6	1.795	1.865	0.217	0.0	115	1.347
1.003	3.071	5427.4	31.7	1.860	2.000	0.252	0.0	79	0.884
1.004	2.579	4557.5	37.9	2.000	2.250	0.304	0.0	94	0.824
1.005	2.766	4887.3	39.9	2.250	2.400	0.322	0.0	93	0.880
2.000	1.438	57.2	8.3	1.625	1.975	0.062	0.0	58	1.030
2.001	1.430	56.9	12.2	1.975	2.135	0.092	0.0	71	1.146





File: Outline SW Drainage Mod	Page 2
Network: Storm Network	
Graham Sanderson	
07/03/2023	

## <u>Links</u>

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)
2.002	MH9	MH10	14.694	0.600	11.840	11.660	0.180	81.6	225	4.66	48.1
2.003	MH10	MH11	17.526	0.600	10.385	10.170	0.215	81.5	1500	4.72	47.8
2.004	MH11	MH12	16.303	0.600	10.170	10.100	0.070	232.9	1500	4.82	47.4
1.006	MH12	UU	30.254	0.600	10.100	9.790	0.310	97.6	1500	5.36	45.3

Name	Vel (m/s)	Cap (l/s)	Flow (I/s)	US Depth (m)	DS Depth (m)	Σ Area (ha)	Σ Add Inflow (I/s)	Pro Depth (mm)	Pro Velocity (m/s)
2.002	1.448	57.6	12.9	2.135	2.315	0.099	0.0	73	1.176
2.003	4.752	8397.6	16.7	2.315	2.530	0.129	0.0	48	0.994
2.004	2.806	4958.7	17.9	2.530	2.400	0.139	0.0	63	0.698
1.006	4.342	7672.7	61.0	2.400	2.420	0.497	0.0	92	1.372

#### **Pipeline Schedule**

Link	Length	Slope	Dia	Link	US CL	US IL	US Depth	DS CL	DS IL	DS Depth
	(m)	(1:X)	(mm)	Туре	(m)	(m)	(m)	(m)	(m)	(m)
1.000	30.779	99.3	225	Circular	14.200	12.350	1.625	14.200	12.040	1.935
1.001	35.877	99.7	225	Circular	14.200	12.040	1.935	13.700	11.680	1.795
1.002	6.695	95.6	225	Circular	13.700	11.680	1.795	13.700	11.610	1.865
1.003	27.239	194.6	1500	Circular	13.700	10.340	1.860	13.700	10.200	2.000
1.004	13.774	275.5	1500	Circular	13.700	10.200	2.000	13.900	10.150	2.250
1.005	11.986	239.7	1500	Circular	13.900	10.150	2.250	14.000	10.100	2.400
2.000	28.963	82.8	225	Circular	14.200	12.350	1.625	14.200	12.000	1.975
2.001	13.390	83.7	225	Circular	14.200	12.000	1.975	14.200	11.840	2.135
2.002	14.694	81.6	225	Circular	14.200	11.840	2.135	14.200	11.660	2.315
2.003	17.526	81.5	1500	Circular	14.200	10.385	2.315	14.200	10.170	2.530
2.004	16.303	232.9	1500	Circular	14.200	10.170	2.530	14.000	10.100	2.400
1.006	30.254	97.6	1500	Circular	14.000	10.100	2.400	13.710	9.790	2.420

Link	US Node	Dia (mm)	Node Type	МН Туре	DS Node	Dia (mm)	Node Type	МН Туре
1.000	MH1	1500	Manhole	PCC	MH2	1500	Manhole	PCC
1.001	MH2	1500	Manhole	PCC	MH3	1500	Manhole	PCC
1.002	MH3	1500	Manhole	PCC	MH4	2400	Manhole	PCC
1.003	MH4	2400	Manhole	PCC	MH5	2400	Manhole	PCC
1.004	MH5	2400	Manhole	PCC	MH6	2400	Manhole	PCC
1.005	MH6	2400	Manhole	PCC	MH12	3000	Manhole	PCC
2.000	MH7	2400	Manhole	PCC	MH8	1500	Manhole	PCC
2.001	MH8	1500	Manhole	PCC	MH9	1500	Manhole	PCC
2.002	MH9	1500	Manhole	PCC	MH10	2400	Manhole	PCC
2.003	MH10	2400	Manhole	PCC	MH11	2400	Manhole	PCC
2.004	MH11	2400	Manhole	PCC	MH12	3000	Manhole	PCC
1.006	MH12	3000	Manhole	PCC	UU	1500	Manhole	PCC





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#### Manhole Schedule

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connections	5	Link	IL (m)	Dia (mm)
MH1	464.358	737.825	14.200	1.850	1500					
						0	0	1 000	42.250	225
N4112	427.070	772 574	14 200	2 1 6 0	1500		0	1.000	12.350	225
IVIH2	437.079	723.571	14.200	2.160	1500		1	1.000	12.040	225
	45 4 4 4 4	604.005	40.700	2 0 2 0	4500	0	0	1.001	12.040	225
MH3	454.111	691.995	13.700	2.020	1500		1	1.001	11.680	225
						Ŏ	0	1.002	11.680	225
MH4	454.661	685.323	13.700	3.360	2400		1	1.002	11.610	225
						0	0	1.003	10.340	1500
MH5	466.784	660.930	13.700	3.500	2400	1	1	1.003	10.200	1500
							0	1.004	10.200	1500
MH6	479.050	667.197	13.900	3.750	2400		1	1.004	10.150	1500
							0	1.005	10.150	1500
MH7	495.122	742.836	14.200	1.850	2400	Q,	0	2 000	12 250	225
	511 260	710 052	14 200	2 200	1500		1	2.000	12.350	225
ΝΠΟ	511.500	/10.005	14.200	2.200	1300		1	2.000	12.000	225
	E1E 021	706 267	14 200	2 260	1500	0	0	2.001	12.000	225
WIT5	515.551	/00.207	14.200	2.300	1300	,	T	2.001	11.840	223
	542.074	CO4 704	44.200	2.045	2400	0 d	0	2.002	11.840	225
MH10	513.971	691.704	14.200	3.815	2400	ý	1	2.002	11.660	225
						0	0	2.003	10.385	1500
MH11	503.673	677.523	14.200	4.030	2400		1	2.003	10.170	1500
							0	2.004	10.170	1500
MH12	491.036	667.223	14.000	3.900	3000	,1	1	2.004	10.100	1500
						2	2	1.005	10.100	1500
	F02 0FC	620.047	12 710	2 0 2 0	1500	0	0	1.006	10.100	1500
UU	502.056	039.047	13./10	3.920	1200		Ţ	1.006	9.790	1200



# Simulation Settings

Rainfall Methodology FSR Region M5-60 (mm) Ratio-R Summer CV Winter CV	FSR England and Wales 17.000 0.400 0.750 0.840	A Skip Drain Down Additional Sto Check Disc Check Disch	nalysis Speed o Steady State n Time (mins) orage (m³/ha) harge Rate(s) narge Volume	Detailed x 240 20.0 x x	
15 30 60 120	<b>Storm Dur</b> 180 240 36	ations 50 480	600 720	960	1440
Return Period (years) 1 30 100	Climate Change A (CC %) 45 45 50	dditional Area (A %) 10 10 10	Additional Flo (Q %)	<b>w</b> 0 0 0	
Ν	ode MH12 Online Hv	dro-Brake® Cont	rol		

Flap Valve	х	Objective	(HE) Minimise upstream storage
Replaces Downstream Link	$\checkmark$	Sump Available	$\checkmark$
Invert Level (m)	10.100	Product Number	CTL-SHE-0096-6700-3100-6700
Design Depth (m)	3.100	Min Outlet Diameter (m)	0.150
Design Flow (I/s)	6.7	Min Node Diameter (mm)	1200

#### PSA Design Ltd



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Results for 1 year +45% CC +10% A Critical Storm Duration. Lowest mass balance: 99.81%

Node Eve	ent	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Stat	us
15 minute w	inter	MH1	10	12.424	0.074	12.5	0.1864	0.0000	ОК	
15 minute su	ummer	MH2	10	12.161	0.121	30.0	0.3220	0.0000	ОК	
15 minute winter		MH3	10	11.858	0.178	43.6	0.4475	0.0000	ОК	
120 minute	winter	MH4	118	10.713	0.373	15.5	1.7731	0.0000	ОК	
120 minute	winter	MH5	114	10.714	0.514	17.3	2.4955	0.0000	ОК	
120 minute	winter	MH6	114	10.714	0.564	16.9	2.6114	0.0000	ОК	
15 minute w	inter	MH7	10	12.421	0.071	12.5	0.3726	0.0000	ОК	
15 minute w	inter	MH8	10	12.093	0.093	18.4	0.1930	0.0000	ОК	
15 minute w	inter	MH9	10	11.936	0.096	19.7	0.1756	0.0000	ОК	
120 minute	winter	MH10	114	10.715	0.330	7.9	1.5478	0.0000	ОК	
120 minute	winter	MH11	112	10.713	0.543	8.9	2.4856	0.0000	ОК	
120 minute winter		MH12	118	10.715	0.615	13.8	4.4690	0.0000	ОК	
15 minute summer		UU	1	9.790	0.000	4.6	0.0000	0.0000	OK	
Link Event	US	Lin	k	DS	Outflow	Velocity	Flow/Ca	ap Lir	nk	Discharge
(Upstream Depth)	Node			Node	(I/s)	(m/s)		Vol (	m³)	Vol (m³)
15 minute winter	MH1	1.000		MH2	12.5	0.754	0.23	39 0.5	115	
15 minute summer	MH2	1.001		MH3	30.0	1.069	0.57	76 0.9	961	
15 minute winter	MH3	1.002		MH4	43.0	1.377	0.80	0.2	083	
120 minute winter	MH4	1.003		MH5	14.3	0.393	0.00	03 11.8	914	
120 minute winter	MH5	1.004		MH6	15.8	0.384	0.00	03 7.8	449	
120 minute winter	MH6	1.005		MH12	11.2	0.253	0.00	02 7.6	885	
15 minute winter	MH7	2.000		MH8	12.4	0.950	0.22	17 0.3	801	
15 minute winter	MH8	2.001		MH9	18.3	1.156	0.32	22 0.2	120	
15 minute winter	MH9	2.002		MH10	19.4	1.262	0.33	37 0.2	261	
120 minute winter	MH10	2.003		MH11	8.3	0.370	0.00	01 7.5	350	
120 minute winter	MH11	2.004		MH12	6.3	0.128	0.00	01 10.2	175	
120 minute winter	MH12	Hydro-E	Brake®	UU	4.6					87.6





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Results for 30 year +45% CC +10% A Critical Storm Duration. Lowest mass balance: 99.81%

Node Event	US	Peak	Level	Depth	Inflow	Node	Flood	Status	
	Node	(mins)	(m)	(m)	(I/s)	Vol (m³)	(m³)		
15 minute winter	MH1	11	12.851	0.501	30.5	1.2548	0.0000	SURCHARGED	
15 minute winter	MH2	11	12.761	0.721	66.1	1.9128	0.0000	SURCHARGED	
15 minute winter	MH3	11	12.168	0.488	90.9	1.2248	0.0000	SURCHARGED	
240 minute winter	MH4	236	11.635	1.295	22.3	6.1535	0.0000	ОК	
240 minute winter	MH5	236	11.635	1.435	21.0	6.9625	0.0000	ОК	
240 minute winter	MH6	236	11.635	1.485	15.1	6.8756	0.0000	ОК	
15 minute summer	MH7	10	12.469	0.119	30.5	0.6249	0.0000	ОК	
15 minute winter	MH8	10	12.173	0.173	45.2	0.3572	0.0000	ОК	
15 minute winter	MH9	10	12.015	0.175	48.3	0.3202	0.0000	ОК	
240 minute winter	MH10	232	11.635	1.250	11.5	5.8702	0.0000	ОК	
240 minute winter	MH11	236	11.635	1.465	13.1	6.7065	0.0000	ОК	
240 minute winter	MH12	236	11.635	1.535	17.3	11.1641	0.0000	SURCHARGED	
15 minute summer	UU	1	9.790	0.000	4.6	0.0000	0.0000	ОК	

Link Event	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
15 minute winter	MH1	1.000	MH2	26.3	0.827	0.504	1.2241	
15 minute winter	MH2	1.001	MH3	61.7	1.550	1.184	1.4269	
15 minute winter	MH3	1.002	MH4	90.7	2.282	1.707	0.2636	
240 minute winter	MH4	1.003	MH5	16.7	0.411	0.003	45.6338	
240 minute winter	MH5	1.004	MH6	13.6	0.404	0.003	24.0532	
240 minute winter	MH6	1.005	MH12	10.3	0.251	0.002	21.0869	
15 minute summer	MH7	2.000	MH8	30.5	1.125	0.534	0.7812	
15 minute winter	MH8	2.001	MH9	44.9	1.364	0.790	0.4407	
15 minute winter	MH9	2.002	MH10	47.7	1.537	0.829	0.4567	
240 minute winter	MH10	2.003	MH11	9.8	0.392	0.001	29.0754	
240 minute winter	MH11	2.004	MH12	3.9	0.126	0.001	28.6142	
240 minute winter	MH12	Hydro-Brake <sup>®</sup>	UU	4.8				122.9





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Results for 100 year +50% CC +10% A Critical Storm Duration. Lowest mass balance: 99.81%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
15 minute winter	MH1	11	13.496	1.146	40.6	2.8693	0.0000	SURCHARGED
15 minute winter	MH2	11	13.355	1.315	84.9	3.4884	0.0000	SURCHARGED
240 minute winter	MH3	232	13.231	1.551	26.1	3.8911	0.0000	SURCHARGED
240 minute winter	MH4	232	13.231	2.891	30.3	13.7416	0.0000	SURCHARGED
240 minute winter	MH5	232	13.231	3.031	28.9	14.7041	0.0000	SURCHARGED
240 minute winter	MH6	232	13.231	3.081	25.9	14.2626	0.0000	SURCHARGED
240 minute winter	MH7	232	13.231	0.881	7.4	4.6374	0.0000	SURCHARGED
240 minute winter	MH8	232	13.231	1.231	11.0	2.5452	0.0000	SURCHARGED
240 minute winter	MH9	232	13.231	1.391	11.8	2.5488	0.0000	SURCHARGED
240 minute winter	MH10	232	13.231	2.846	15.4	13.3683	0.0000	SURCHARGED
240 minute winter	MH11	232	13.231	3.061	19.7	14.0139	0.0000	SURCHARGED
240 minute winter	MH12	232	13.231	3.131	23.2	22.7697	0.0000	SURCHARGED
15 minute summer	UU	1	9.790	0.000	4.6	0.0000	0.0000	ОК

Link Event	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
15 minute winter	MH1	1.000	MH2	33.7	0.847	0.646	1.2241	
15 minute winter	MH2	1.001	MH3	78.4	1.971	1.505	1.4269	
240 minute winter	MH3	1.002	MH4	26.1	1.238	0.491	0.2663	
240 minute winter	MH4	1.003	MH5	22.7	0.442	0.004	47.9538	
240 minute winter	MH5	1.004	MH6	23.8	0.398	0.005	24.2489	
240 minute winter	MH6	1.005	MH12	17.1	0.254	0.003	21.1011	
240 minute winter	MH7	2.000	MH8	7.4	0.831	0.129	1.1519	
240 minute winter	MH8	2.001	MH9	11.0	1.024	0.193	0.5325	
240 minute winter	MH9	2.002	MH10	11.8	1.112	0.205	0.5844	
240 minute winter	MH10	2.003	MH11	11.3	0.413	0.001	30.8542	
240 minute winter	MH11	2.004	MH12	-8.8	0.124	-0.002	28.7012	
240 minute winter	MH12	Hydro-Brake <sup>®</sup>	UU	6.7				152.9