

Drainage Philosophy

226254 – NETA Relocation, Stockton Riverside College, Stockton-on-Tees, Teesside



Drainage Philosophy

Project: NETA Relocation, Stockton Riverside College, Stockton-on-Tees, Teesside

Client: The Education Training Collective

LLFA: Stockton Borough Council

BGP Job No: 226254

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001 19/04/2024 Planning RJW

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1. Executive Summary / Project Background

- 1.1. This Drainage Philosophy has been prepared to supplement the planning application for the new Car park at Stockton Riverside College, Stockton-on-Tees. See Appendix A for the Site Location Plan and Appendix B for the proposals.
- 1.2. The proposals are to construct a new car parking facility to provide additional parking for Stockton Riverside College and the future NETA Relocation building that will be submitted as a future planning application. The new car park will be constructed on a greenfield parcel of land adjacent to Harvard Avenue.
- 1.3. Northumbrian Water (NWL) records have been obtained and the Tees Valley SuDS Design Guidance has been reviewed.
- 1.4. A hierarchy for the appropriate disposal of surface water is included within Building Regulations Part H3 which states the following:
 - "Rainwater from a system provided ... shall discharge to one of the following, listed in order of priority:
 - 1) An adequate soakaway or some other adequate infiltration system; or, where this is not reasonably practicable,
 - 2) A watercourse; or, where that is not reasonably practicable,
 - 3) A surface water sewer.
 - 4) A combined sewer.
- 1.5. The following Drainage Philosophy addresses each element of the above hierarchy and details how the surface water and foul water will be discharged from site.
- 1.6. BGP have prepared this report based on the current information available. This report is subject to change should new information be presented.



2. Existing Site & Drainage

2.1. Site Location

2.1.1. Site Name: NETA Relocation, Stockton Riverside College

2.1.2. Site Address: Harvard Avenue, Thornaby, Stockton-on-Tees, TS17 6FB

2.1.3. OS Grid Reference: E: 445454, N: 518693

2.1.4. National Grid Reference: NZ454186

2.2. Site Description

2.2.1. Site Area: 1.149ha

2.2.2. Existing Land Use: Greenfield parcel of land.

2.2.3. Proposed Land Use: Construction of a new car parking facility.

2.2.4. Local Planning Authority: Stockton Borough Council

2.2.5. Sewer Undertaker: Northumbrian Water (NWL)

2.2.6. The site is located approximately 1km east of Stockton Town Centre and approximately 4.2km southwest of Middlesbrough Town Centre. The site is within the boundaries of Stockton Riverside College campus. The site is bound by Harvard Avenue to the eastern boundary, University Boulevard to the northern boundary, Durham University Queen's campus to the eastern boundary and Princeton Drive to the southern boundary. Existing private office buildings are in proximity to the proposed developments.

2.3. Existing Watercourses

2.3.1. The nearest named watercourse is the river Tees. This is located approximately 25m north west of site and flows South to North initially and then changes direction to flow West to East.

2.4. Existing Public and Private Drainage

- 2.4.1. See Appendix D for locations of existing Northumbrian Water public drains.
- 2.4.2. There is a 225mm adopted Foul Water sewer that runs from north to south along the western boundary within the existing grassed area. This heads towards Princeton drive and then travels east towards Durham University Queen's campus.
- 2.4.3. The Northumbrian Water records (Appendix D) show that there are no surface water drains located within close proximity to the site. An existing NWL surface water sewer is located approximately 90 metres to the south west of our site. This network is located close to the roundabout that links Harvard Avenue, Princeton Drive, Radcliffe Crescent, and Station Street.



2.5. Existing Ground Conditions

- 2.5.1. A 'Phase 2 Site Investigation' has been carried out by Solmek dated April 2023.
- 2.5.2. In the area of the proposed car park the ground consisted of sandy slightly gravelly clay topsoil to depths of between 0.10mbgl and 0.20mbgl. Made ground was relatively uniform in this area, comprising of very gravelly sand fill with low to medium cobble content. This was encountered to depths of between 2.00mbgl and 2.50mbgl. The extent of the excavation in these areas was 2.5m depth. It can be assumed that depths below this will be similar in composition to the borehole samples taken nearby. A layer of organic soft locally very soft peat was encountered to depths of 5.40mbgl and 7.40mbl then natural ground generally comprised soft and very soft silty slightly sandy organic low strength clay to depths of between 11.5mbgl and 12.10mbgl.
- 2.5.3. The report notes Groundwater was encountered within the boreholes at depths of between 2.80m and 4.40m below ground level. Deeper strikes were encountered at depths between 9.30mbgl and 12.10mbgl.

2.6. Existing Flood Risk Assessment

- 2.6.1. A site-specific Flood Risk Assessment (April 2024) has been carried out by Billinghurst George & Partners and is to be provided separately to support this planning application.
- 2.6.2. The report states that the site is entirety within Flood Zone 1 and is at low risk of flooding from fluvial sources of flood risk. The surface water flood maps indicate the site is affected by overland surface water flooding due to the site levels being lower than surrounding levels. However, this will be mitigated by the introduction of a positive drainage system that will serve the car park. Therefore, the proposed site is suitable for development in accordance with the National Planning Policy Framework.
- 2.6.3. See Appendix E for Flood Maps for planning.



3. Review of Surface Water Discharge Hierarchy

3.1. Existing Wastewater Regime

3.1.1. Existing drainage is present that serves the existing Stockton Riverside College Buildings and car parks. It is understood that most of the surface water drainage outfalls to the River Tees via a headwall. It is understood that most of the existing foul drainage is collected via private drains within the site boundary and outfalls into the existing NWL foul sewer running close to the western boundary. This sewer is then directed east and runs parallel to Princeton Drive into the existing pumping station (NWL 5602) to the south east of Stockton Riverside College. See Appendix D for Existing NWL records. See Appendix C for existing utility information supplied by MurphyGS.

3.2. Current Guidelines

3.2.1. In accordance with Building Regulations and NPPF the disposal of surface water has been considered in the following order of priority; discharge to ground, where not reasonably practicable, a watercourse, or where not reasonably practicable a sewer.

3.3. Discharge to Ground

- 3.3.1. Discharge of surface water to ground via infiltration is suited to sites which have ground conditions made up of gravel, sand, or a mixture of the two. Sands and gravels permit rapid dispersion and infiltration of surface water which is necessary to ensure that overland flooding does not occur during intense rainfall periods.
- 3.3.2. A 'Phase 2 Site Investigation' has been carried out by Solmek dated April 2023. (Report No. S230207).
- 3.3.3. In the area of the proposed car park the ground consisted of sandy slightly gravelly clay topsoil to depths of between 0.10mbgl and 0.20mbgl. Made ground was relatively uniform in this area, comprising of very gravelly sand fill with low to medium cobble content. This was encountered to depths of between 2.00mbgl and 2.50mbgl. The extent of the excavation in these areas was 2.5m depth. It can be assumed that depths below this will be similar in composition to the borehole samples taken nearby. A layer of organic soft locally very soft peat was encountered to depths of 5.40mbgl and 7.40mbl then natural ground generally comprised soft and very soft silty slightly sandy organic low strength clay to depths of between 11.5mbgl and 12.10mbgl.
- 3.3.4. The above made ground strata is not typically suitable for infiltration and the Soilscapes website notes that this type of ground has 'impeded drainage' properties.
- 3.3.5. Due to the above findings, it is confirmed that it would not be feasible to discharge the sites surface water to the ground via infiltration.

3.4. Discharge to a Watercourse

3.4.1. The site is in close proximity to the River Tees and the majority of the existing site discharges to the river via an existing outfall. Under agreement with the LLFA, EA and Canal and Rivers trust, it is considered that surface water flows should outfall into the river via an indirect connection into the existing surface water sewer, located within the site, at a restricted discharge rate that is to be agreed.

3.5. Discharge to a Surface Water Sewer

3.5.1. As per the hierarchy and due to the suggestion of discharging to a watercourse, discharging to a surface water sewer is not required.



4. Proposed Surface Water Drainage Strategy

- 4.1. It is expected that surface water discharge rates will be restricted to as close to Greenfield rates as per the Tees Valley SuDS Design Guidance for Major Developments. BGP have conducted a greenfield run off estimation using the UK SuDS Tool (See Appendix G). The existing greenfield rate for the site is 2.55 l/s. This is considered too low to utilise due to the minimal orifice size that would be required. As such, a rate of 3.0 l/s has been used. This is subject to agreement with the LLFA, EA and Canal and Rivers trust.
- 4.2. Flows from the new training centre and car park will be collected and the discharge rate will be restricted to 3.0 l/s. All attenuation would be designed to store flows above this 3 l/s discharge rate for rainfall events up to and included the 1 in 100-year event with an allowance of 45% for climate change. An allowance will be made for additional volume within the attenuation tank to accommodate the future impermeable area from the proposed NETA Relocation Building as part of a future planning application. See blue dashed line on BGP drawing 226254-BGP-01-ZZ-D-C-01130 in Appendix F.
- 4.3. See Appendix F for the Proposed Drainage General Arrangement drawings. This is accompanied by the Microdrainage calculations for attenuation volume within Appendix G.
- 4.4. The proposed surface water system will be designed in line with Building Regulations Part H which ensures it is separate from the foul.
- 4.5. The proposed car park is situated to the west of the existing Stockton Riverside College Building 2on an area of green open space. The proposals are to have impermeable tarmac access ways and utilise permeable paving as a means of surface water collection treatment and conveyance. Flows onto the access way will fall at a suitable gradient towards permeable paved bays. Flows will then percolate into the sub-base of the permeable paving and be collected within perforated pipes. Flows will then fall via gravity towards the proposed attenuation tank.
- 4.6. The proposed NETA Relocation building (shown within Appendix B) is currently proposed to be located within the extents of an existing car park. As such, the proposed drainage to the training centre will be routed and designed to minimise the amount of works to the existing car park. Flows will be collected and drain towards the proposed car park via the plaza area. A stub connection will be provided as part of the proposed car park works to enable a future connection. (See Appendix F for Proposed Drainage Strategy).
- 4.7. Attenuation crates will be utilised to minimise land take and enable the storage volume to be provided beneath the car park. See Appendix F. The cover to the attenuation crates has been considered in accordance with the manufacturers specification to ensure that they are not overloaded. As such, the crates are two high with a minimum of 900mm cover.
- 4.8. The flows from the overall area will be collected and restricted to 31/s via a flow control device before connecting into the existing private surface water drain that eventually outfalls into the river tees approximately 20 metres downstream to the north west of the proposed car park.



5. Proposed Foul Water Drainage

- 5.1. There are no foul water requirements for the Proposed Car Park as part of this planning application. However, the existing NWL foul sewer and easement has been considered as part of the design to ensure access is available for future maintenance.
- 5.2. Future foul drainage for the NETA training centre will be required and will connect to the existing private foul drainage located within the site. See Appendix C for Existing Utility Information. This private drainage then connects into the adopted NWL Sewer (MH references 3702,3601,3602). The sewer is located close to the western boundary and can be seen in Appendix D. This will be covered in more detail as part of a future planning application.

9 | Page

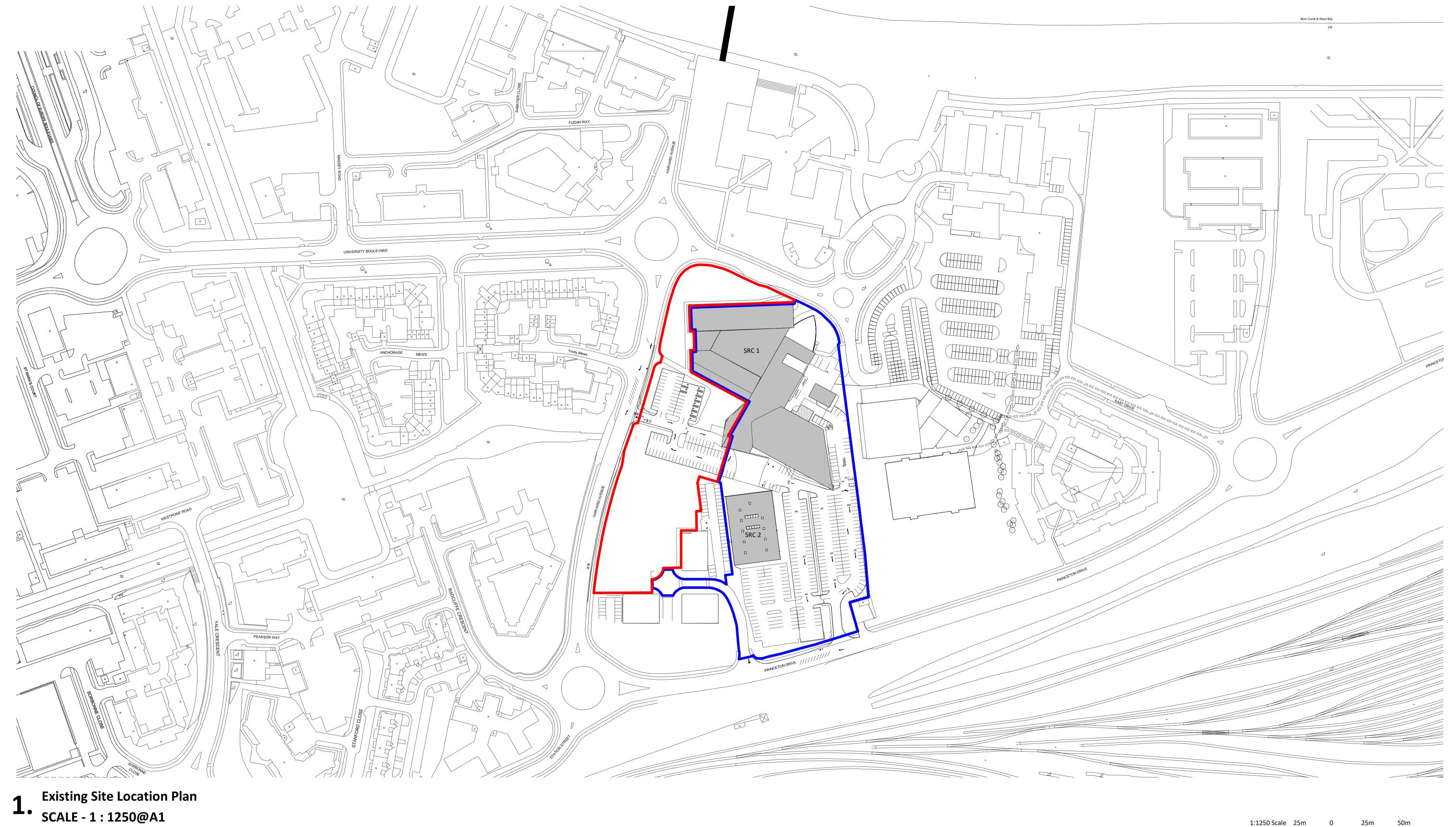


6. Conclusion

- 6.1. As per the hierarchy within Building Regulations Part H3, it is deemed necessary to discharge the surface water to a watercourse, due to the lack of infiltration capabilities in this location.
- 6.2. Discharge is to be restricted to suit the LLFA and EA requirements with attenuation provided for flows greater than this for design events up to the 1 in 100 year + 45% climate change rainfall event.
- 6.3. Proposed drainage layouts have been presenting within Appendix F with supporting calculations included within Appendix G.
- 6.4. This statement has been prepared with reference to the information available at the time of writing. The details of the report may be revised upon receipt of additional or further information.



Appendix A
Site Location Plan



1. Existing Site 1. SCALE - 1: 1250@A1

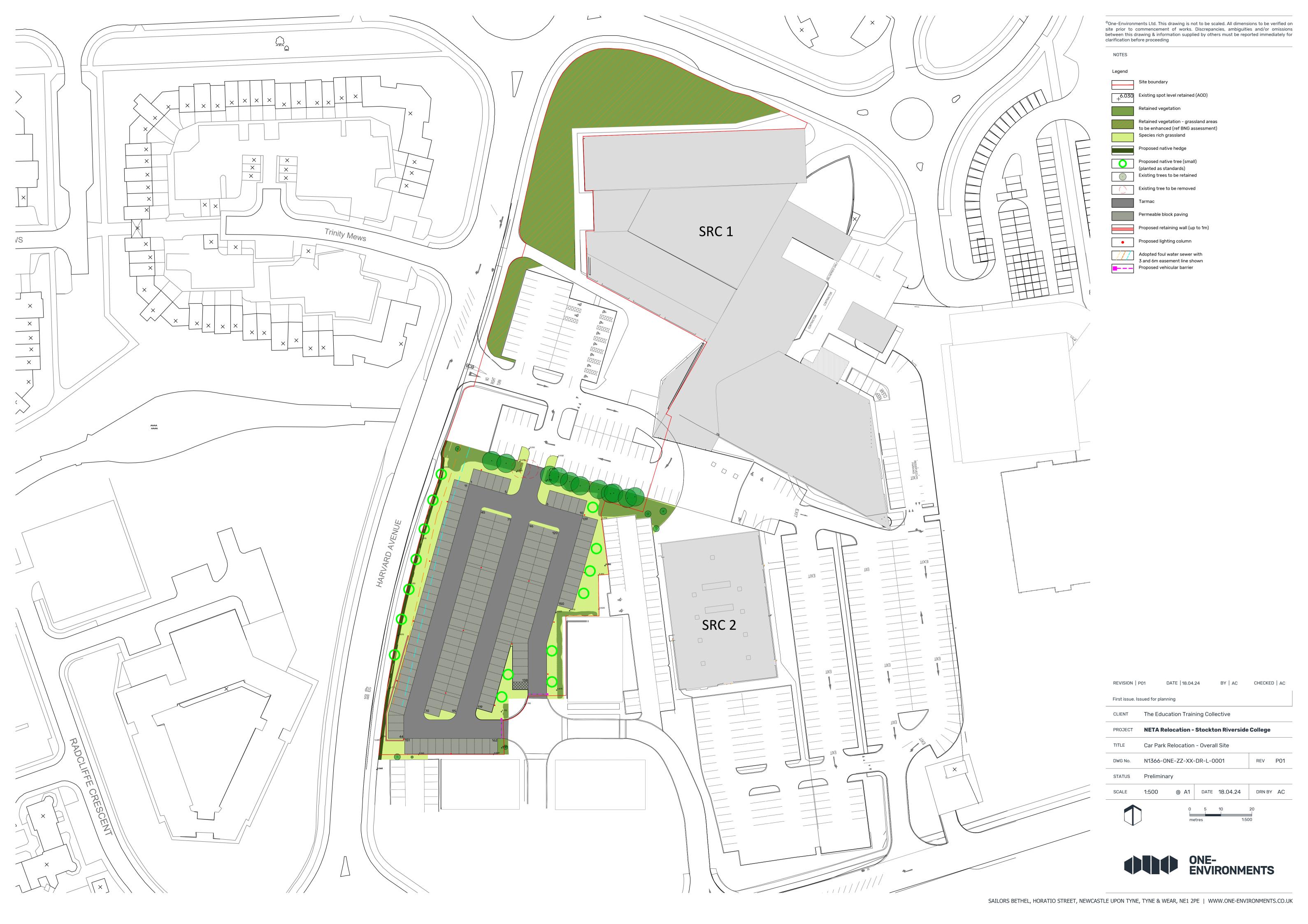
Key Plan Legend Other Land Owned by Applicant Project Title: NETA Relocation — Stockton Riverside College The Education Training Collective
Drawing Title:
Site Location Plan Scale @A1: 1:1250 Date: 16.01.24

P01 17.04.24 CMKC CMKC Boundary Amended

Drwg No: (S)01



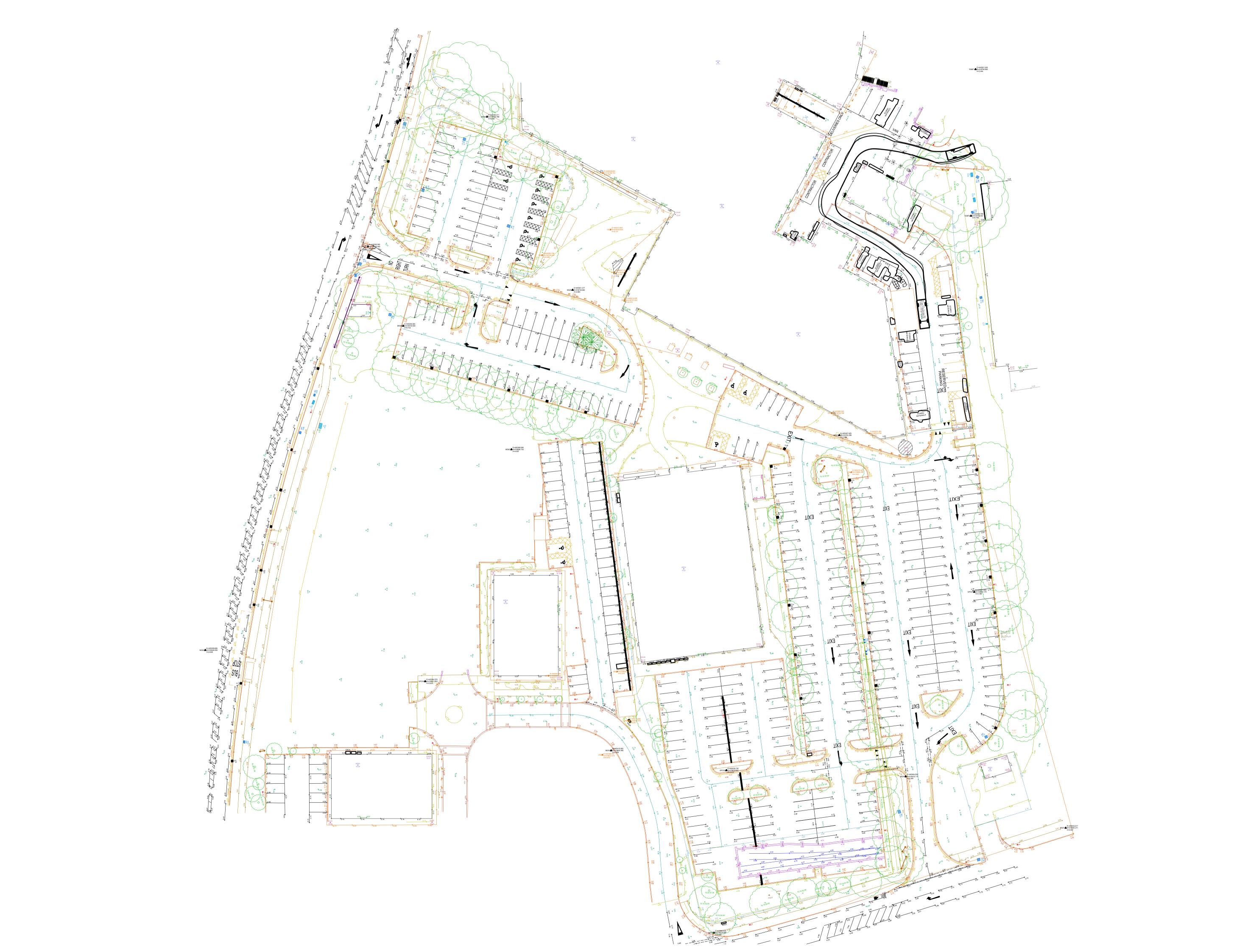
Appendix B
Proposed Site Layout

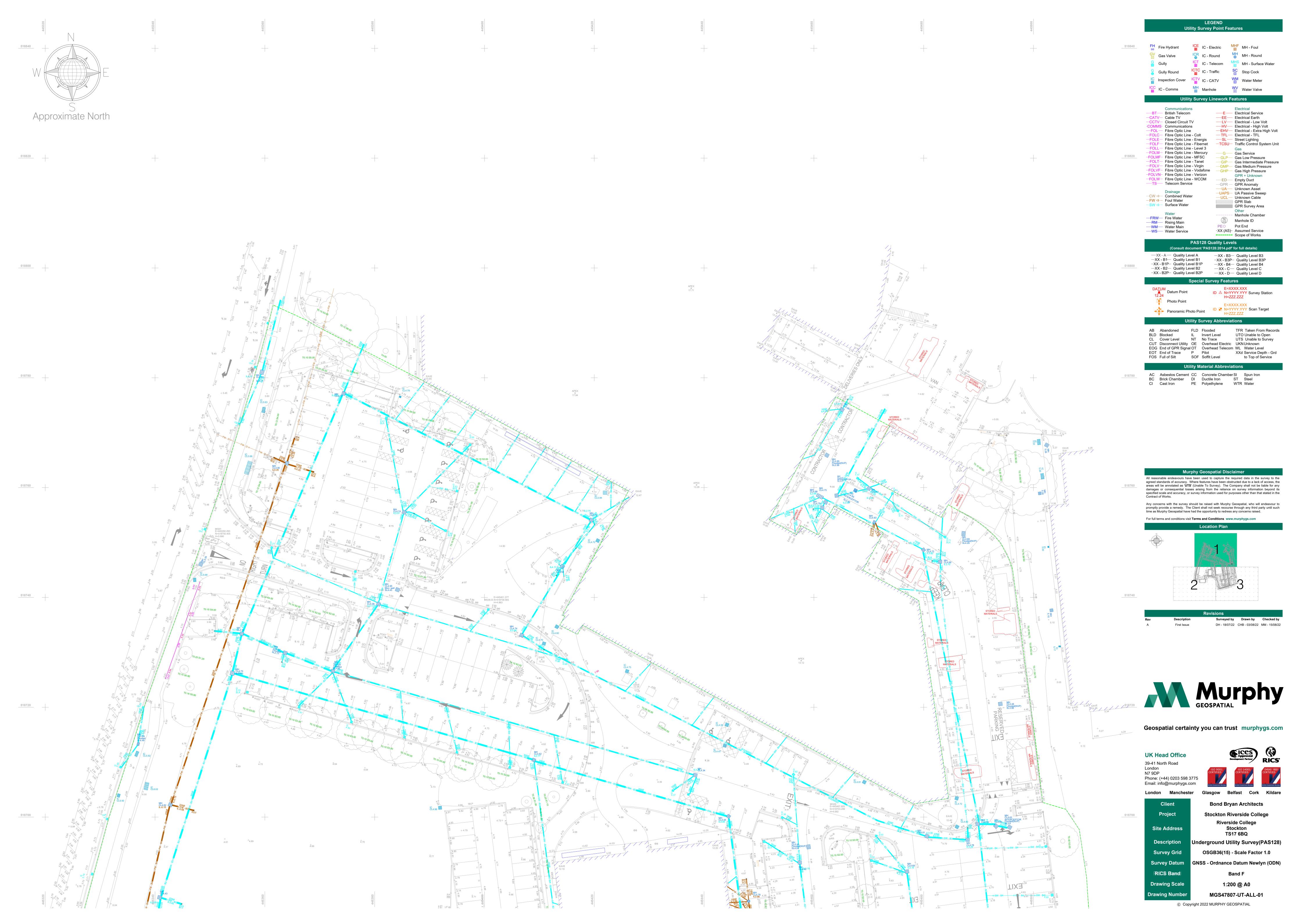






Appendix C Topographical & Utility Surveys







MGS47807-UT-ALL-02

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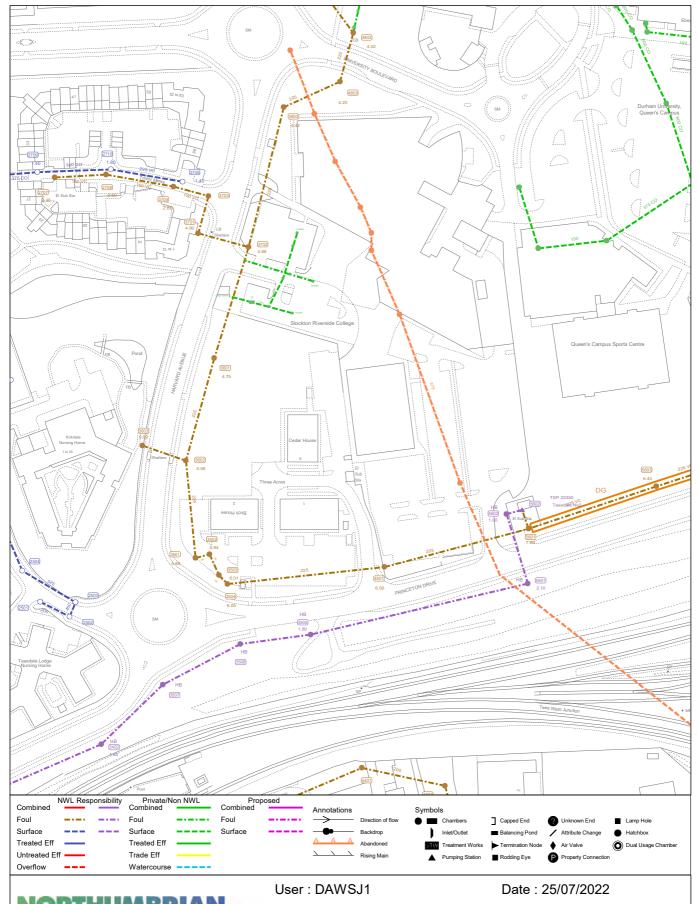


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Appendix D Northumbrian Water Records



NORTHUMBRIAN WATER liwing water

Title: 0000

Centre Point: 445415,518676 Map Sheet: NZ4518NW

The material contained on this plot has been reproduced from an Ordnance Survey map with permission of the controller of H.M.S.O. Crown Copyright Reserved. Licence No.10022480. The information shown on this plan should be regarded as approximate and is intended for guidance only. No Liability of any kind whatsoever is accepted by Northumbrian Water, it's servants or agents for any omission. The actual position of any water mains or sewers shown on the plan must be established by taking trial holes in all cases. In the case of water mains Northumbrian Water must be given two working days notice of their intention to excavate trial holes. With effect from 1 October 2011, private lateral drains and sewers automatically transferred to Northumbrian Water under a scheme made by the Secretary of State pursuant to section 105A Water Industry Act 1991. These former private drains and sewers together with existing private connections may not be shown but their presence should be anticipated. WARNING...Where indicated on the plan there could be abandoned asbestos cement materials or shards of pipe. If excavating in the vicinity of these abandoned asbestos cement materials, the appropriate Health & Safety precautions should be taken. Northumbrian Water accepts no liability in respect of claims, costs, losses or other liabilities which arise as the result of the presence of the pipes or any failure to take adequate precautions. Emergency Telephone Number: 0345 717 1100





Appendix E Flood Maps for Planning



Flood map for planning

Your reference Location (easting/northing) Created

<Unspecified> 445416/518713 18 Apr 2024 9:27

Your selected location is in flood zone 3, an area with a high probability of flooding.

This means:

- you must complete a flood risk assessment for development in this area
- you should follow the Environment Agency's standing advice for carrying out a flood risk assessment (see www.gov.uk/guidance/flood-risk-assessment-standing-advice)

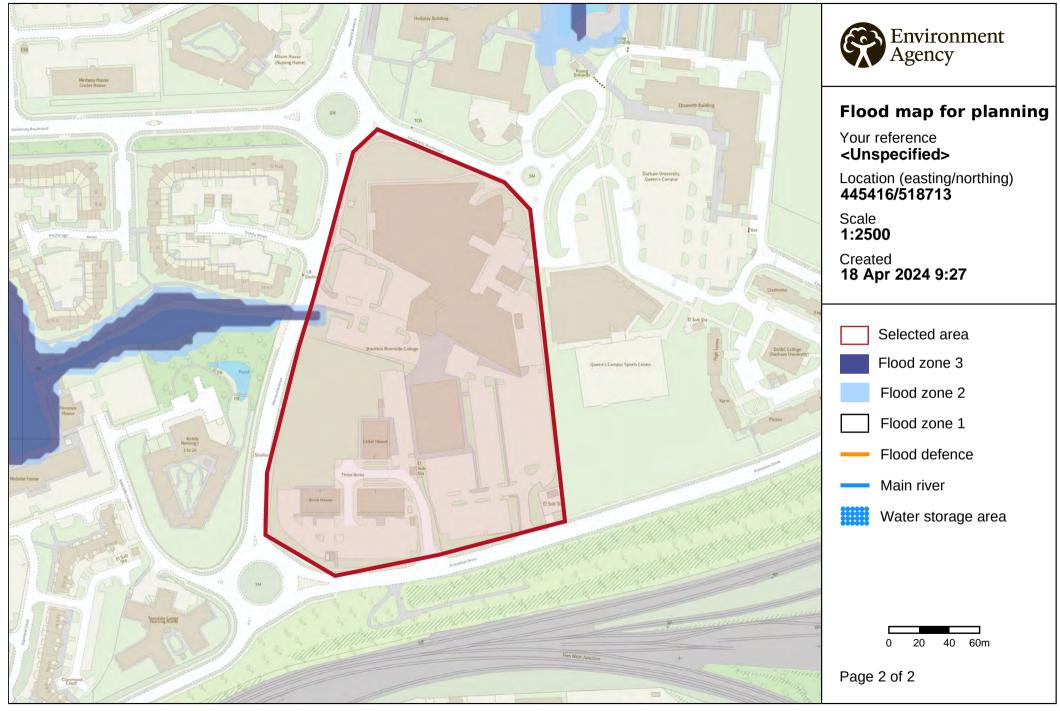
Notes

The flood map for planning shows river and sea flooding data only. It doesn't include other sources of flooding. It is for use in development planning and flood risk assessments.

This information relates to the selected location and is not specific to any property within it. The map is updated regularly and is correct at the time of printing.

Flood risk data is covered by the Open Government Licence which sets out the terms and conditions for using government data. https://www.nationalarchives.gov.uk/doc/open-government-licence/version/3/

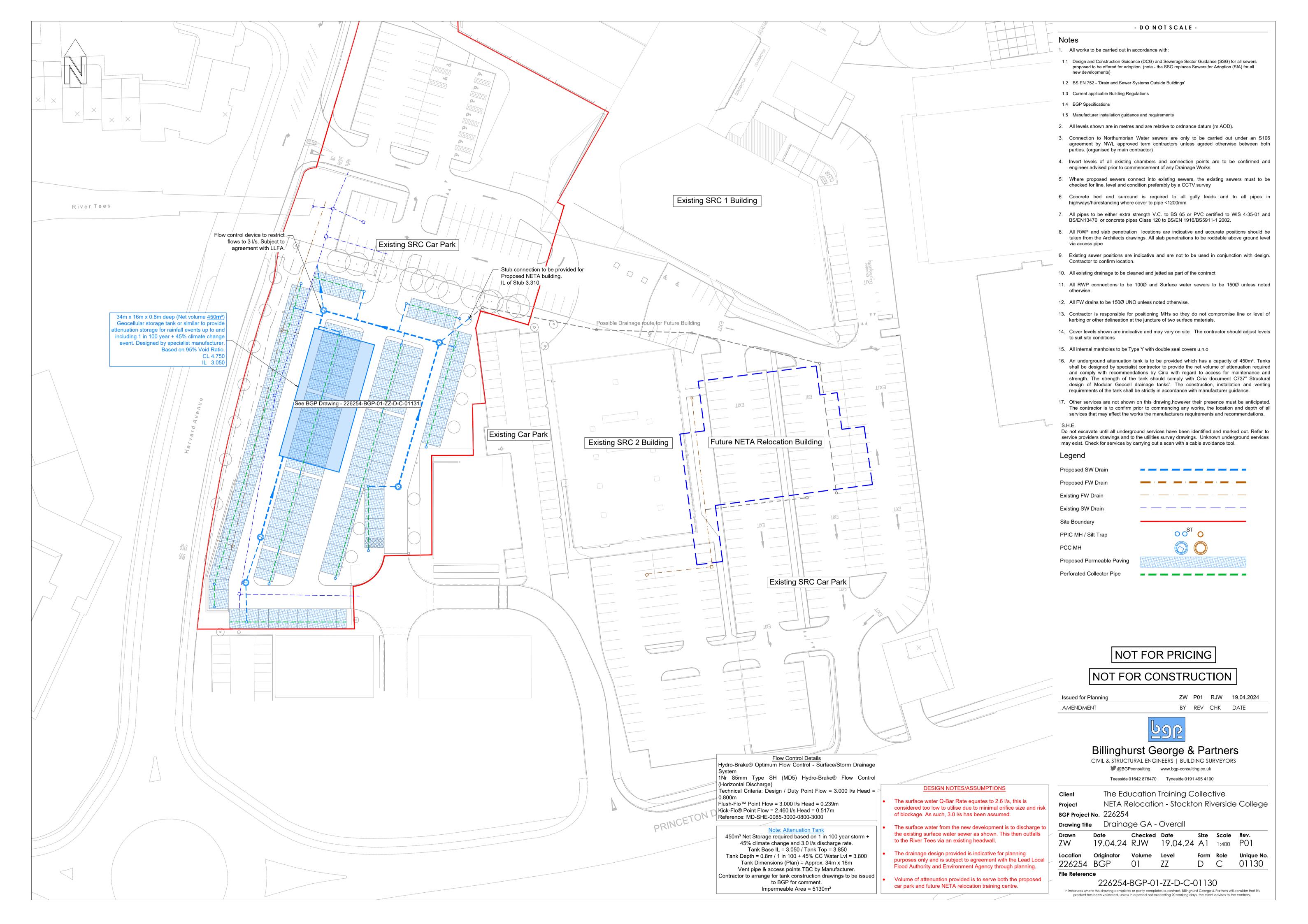
Use of the address and mapping data is subject to Ordnance Survey public viewing terms under Crown copyright and database rights 2022 OS 100024198. https://flood-map-for-planning.service.gov.uk/os-terms

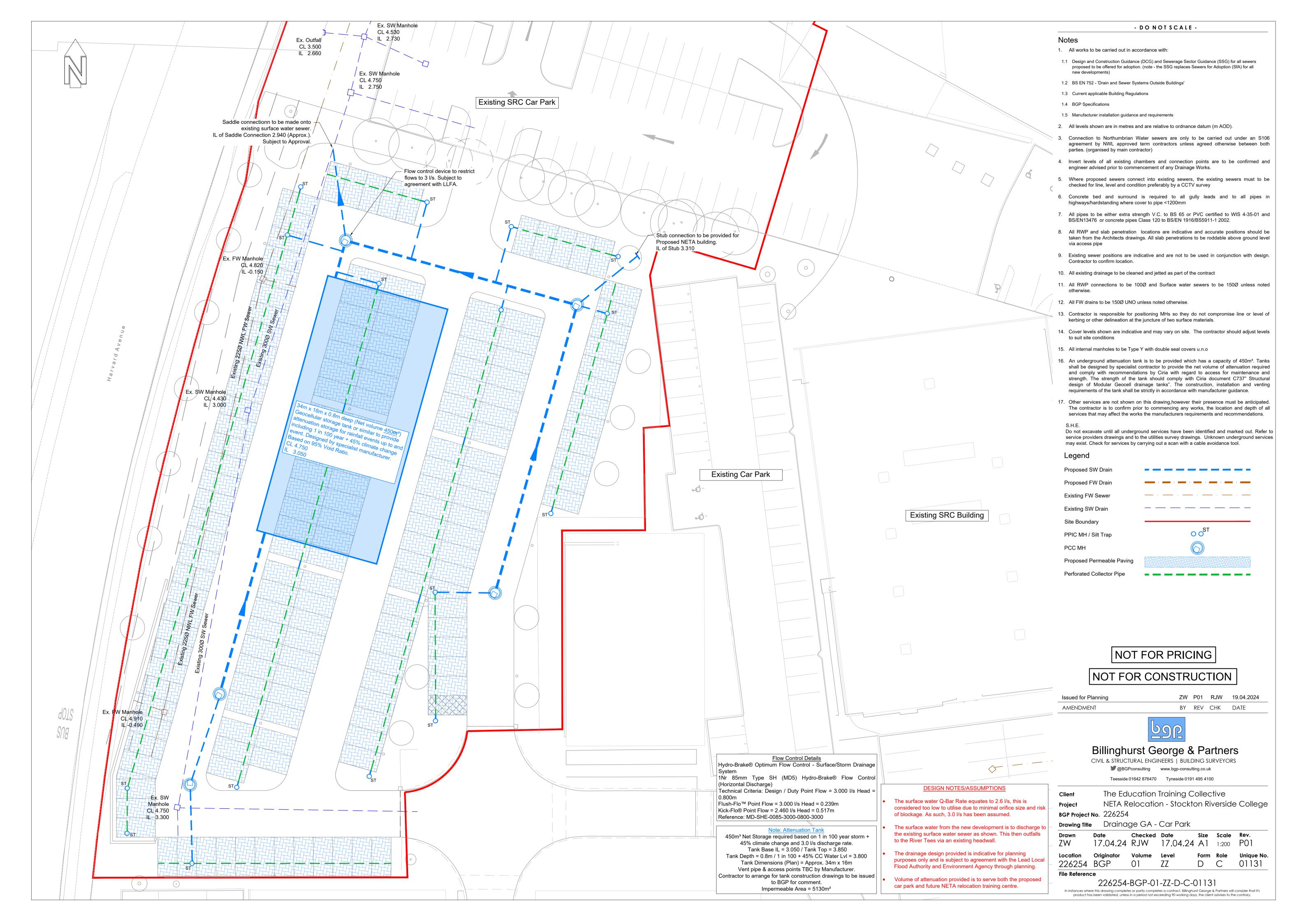


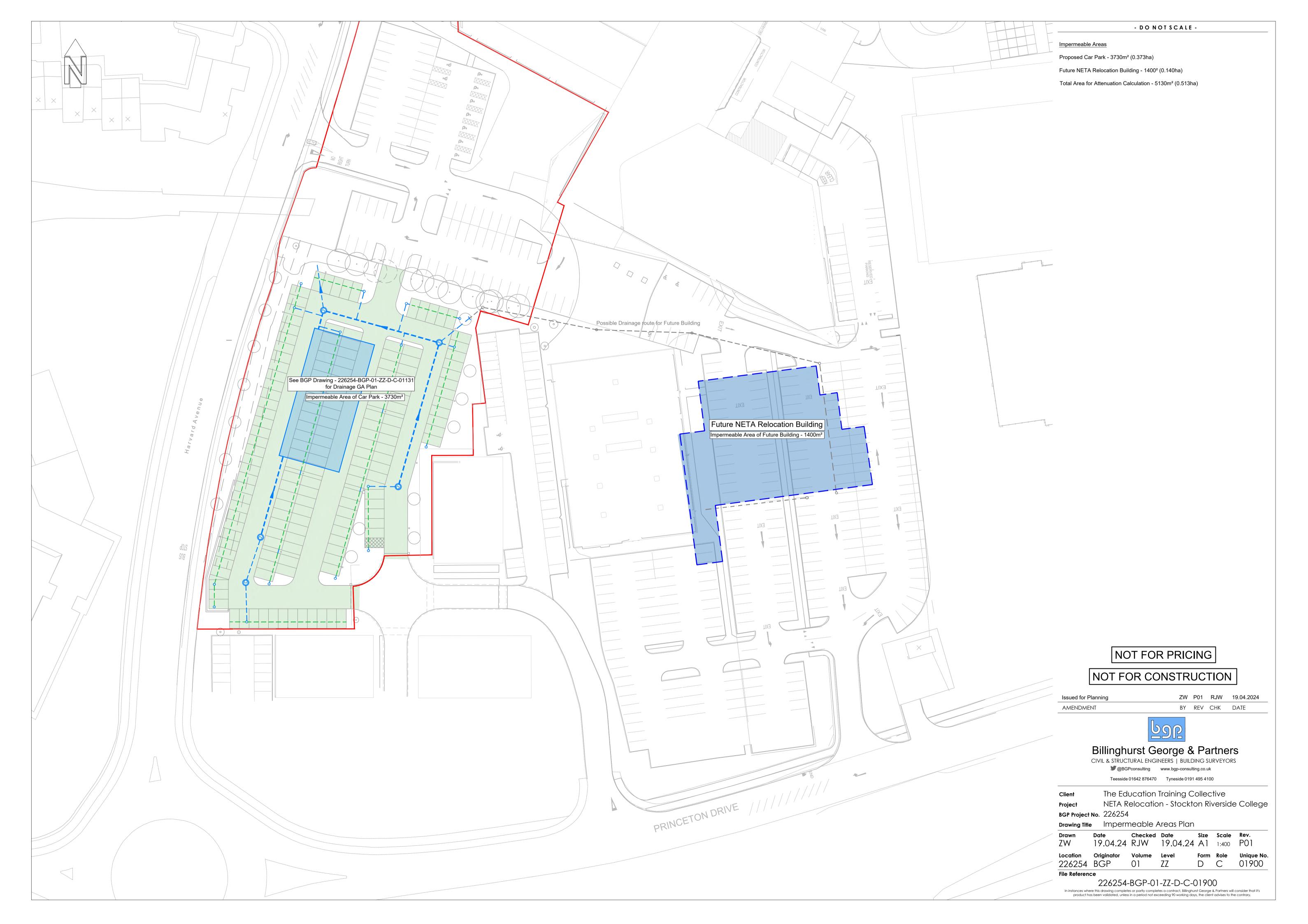
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Appendix F Proposed Drainage Drawings









Appendix G Microdrainage Calculations



Greenfield runoff rate estimation for sites

www.uksuds.com | Greenfield runoff tool

Calculated by:	Zach Waller
Site name:	NETA
Site location:	Stockton

Site Details

54.56156° N Latitude: 1.29889° W Longitude:

This is an estimation of the greenfield runoff rates that are used to meet normal best practice **Reference**: criteria in line with Environment Agency guidance "Rainfall runoff management for developments", SC030219 (2013), the SuDS Manual C753 (Ciria, 2015) and the non-statutory standards for SuDS (Defra, 2015). This information on greenfield runoff rates may be the basis for setting consents for the drainage of surface water runoff from sites.

Apr 17 2024 14:57

870257775

Runoff estimation approach

Site characteristics

Total site area (ha):

0.645

Methodology

QBAR estimation method:

Calculate from SPR and SAAR

SPR estimation method:

Calculate from SOIL type

Notes

(1) Is $Q_{BAR} < 2.0 \text{ I/s/ha}$?

Date:

When QBAR is < 2.0 l/s/ha then limiting discharge rates are set at 2.0 l/s/ha.

Soil characteristics

Default

Edited

SOIL type:

HOST class:

SPR/SPRHOST:

4	4
N/A	N/A
0.47	0.47

(2) Are flow rates < 5.0 l/s?

Where flow rates are less than 5.0 l/s consent for discharge is usually set at 5.0 l/s if blockage from vegetation and other materials is possible. Lower consent flow rates may be set where the blockage risk is addressed by using appropriate drainage elements.

Hydrological characteristics

SAAR (mm):

Hydrological region:

Growth curve factor 1 year.

Growth curve factor 30 years:

Growth curve factor 100 vears:

Growth curve factor 200 years:

Default	Edited
590	590
3	3
0.86	0.86
1.75	1.75
2.08	2.08
2.37	2.37

(3) Is $SPR/SPRHOST \le 0.3$?

Where groundwater levels are low enough the use of soakaways to avoid discharge offsite would normally be preferred for disposal of surface water runoff.

Q _{BAR} (I/s):	2.55	2.55
1 in 1 year (l/s):	2.19	2.19
1 in 30 years (l/s):	4.46	4.46
1 in 100 year (l/s):	5.3	5.3
1 in 200 years (l/s):	6.04	6.04

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at www.uksuds.com/terms-and-conditions.htm. The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.

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Wellington House, Wellington Court		
Preston Farm		The same of
Stockton on Tees, TS18 3TA		Micro
Date 18/04/2024 15:10	Designed by zach.waller	Drainage
File Attenuation Volume.SRCX	Checked by	Dialilade
XP Solutions	Source Control 2020 1 3	1

Summary of Results for 100 year Return Period (+45%)

	Stor	m	Max	Max	Max	Max	Status
	Even	t	Level	Depth	Control	Volume	
			(m)	(m)	(1/s)	(m³)	
1.5		Q	2 220	0 000	2 0	1	0.77
		Summer			3.0		
		Summer			3.0		
		Summer					
120	min	Summer	3.628	0.578	3.0		
180	min	Summer	3.683	0.633	3.0	341.6	O K
240	min	Summer	3.717	0.667	3.0	360.4	O K
360	min	Summer	3.757	0.707	3.0	381.7	O K
480	min	Summer	3.778	0.728	3.0	393.1	O K
600	min	Summer	3.790	0.740	3.0	399.6	O K
720	min	Summer	3.795	0.745	3.0	402.5	O K
960	min	Summer	3.793	0.743	3.0	401.5	O K
1440	min	Summer	3.774	0.724	3.0	390.7	O K
2160	min	Summer	3.740	0.690	3.0	372.5	O K
2880	min	Summer	3.705	0.655	3.0	353.6	O K
4320	min	Summer	3.635	0.585	3.0	315.8	O K
5760	min	Summer	3.561	0.511	3.0	275.9	O K
7200	min	Summer	3.485	0.435	3.0	234.6	O K
8640	min	Summer	3.421	0.371	3.0	200.3	O K
10080	min	Summer	3.366	0.316	3.0	170.6	O K
15	min	Winter	3.338	0.288	3.0	155.4	O K
30	min	Winter	3.431	0.381	3.0	205.6	O K
60	min	Winter	3.529	0.479	3.0	258.4	O K
120	min	Winter	3.628	0.578	3.0	312.2	O K
180	min	Winter	3.683	0.633	3.0	341.8	ОК

Storm		Rain	Flooded	Discharge	Time-Peak	
	Even	t	(mm/hr)	Volume	Volume	(mins)
				(m³)	(m³)	
15	min	Summer	123.557	0.0	147.8	26
		Summer	82.014	0.0	194.6	41
60		Summer	52.009	0.0	261.2	70
		Summer	31.946	0.0	320.3	130
		Summer	23.729	0.0	355.9	190
		Summer	19.111	0.0	381.0	248
		Summer	13.970	0.0	414.7	366
		Summer	11.166	0.0	437.1	486
		Summer	9.386	0.0	451.5	604
		Summer	8.141	0.0	457.7	722
		Summer	6.499	0.0	453.1	960
1440	min	Summer	4.723	0.0	432.9	1200
2160	min	Summer	3.426	0.0	627.8	1580
2880	min	Summer	2.726	0.0	664.7	1992
4320	min	Summer	1.971	0.0	714.1	2816
5760	min	Summer	1.565	0.0	769.0	3640
7200	min	Summer	1.307	0.0	802.8	4392
8640	min	Summer	1.128	0.0	830.7	5104
10080	min	Summer	0.996	0.0	853.5	5768
15	min	Winter	123.557	0.0	147.8	26
30	min	Winter	82.014	0.0	194.6	41
60	min	Winter	52.009	0.0	261.2	70
120	min	Winter	31.946	0.0	320.3	128
180	min	Winter	23.729	0.0	355.9	186

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BGP		Page 2
Wellington House, Wellington Court		
Preston Farm		
Stockton on Tees, TS18 3TA		Micro
Date 18/04/2024 15:10	Designed by zach.waller	Drainage
File Attenuation Volume.SRCX	Checked by	nialilade
XP Solutions	Source Control 2020.1.3	,

Summary of Results for 100 year Return Period (+45%)

	Stor		Max Level (m)	Max Depth (m)	Max Control (1/s)	Max Volume (m³)	Status
			\ /	\ ,	(-/-/	\ ,	
240	min	Winter	3.718	0.668	3.0	360.8	O K
360	min	Winter	3.758	0.708	3.0	382.3	O K
480	min	Winter	3.780	0.730	3.0	394.1	O K
600	min	Winter	3.793	0.743	3.0	401.0	O K
720	min	Winter	3.799	0.749	3.0	404.3	O K
960	min	Winter	3.799	0.749	3.0	404.3	O K
1440	min	Winter	3.774	0.724	3.0	391.1	O K
2160	min	Winter	3.731	0.681	3.0	367.7	O K
2880	min	Winter	3.682	0.632	3.0	341.4	O K
4320	min	Winter	3.574	0.524	3.0	283.1	O K
5760	min	Winter	3.454	0.404	3.0	218.2	O K
7200	min	Winter	3.359	0.309	3.0	167.1	O K
8640	min	Winter	3.285	0.235	3.0	126.7	O K
10080	min	Winter	3.230	0.180	3.0	97.0	O K

	Stor	m	Rain	Flooded	Discharge	Time-Peak
	Even	t	(mm/hr)	Volume	Volume	(mins)
				(m³)	(m³)	
240	min	Winter	19.111	0.0	381.1	244
360	min	Winter	13.970	0.0	414.7	360
480	min	Winter	11.166	0.0	437.2	476
600	min	Winter	9.386	0.0	451.7	590
720	min	Winter	8.141	0.0	457.9	702
960	min	Winter	6.499	0.0	453.5	924
1440	min	Winter	4.723	0.0	434.0	1328
2160	min	Winter	3.426	0.0	627.9	1652
2880	min	Winter	2.726	0.0	664.8	2132
4320	min	Winter	1.971	0.0	716.4	3064
5760	min	Winter	1.565	0.0	769.1	3800
7200	min	Winter	1.307	0.0	802.9	4480
8640	min	Winter	1.128	0.0	830.8	5184
10080	min	Winter	0.996	0.0	853.9	5760

BGP		Page 3
Wellington House, Wellington Court		
Preston Farm		
Stockton on Tees, TS18 3TA		Micro
Date 18/04/2024 15:10	Designed by zach.waller	
File Attenuation Volume.SRCX	Checked by	Drainage
XP Solutions	Source Control 2020.1.3	-

Rainfall Details

Return Period (years) 100 Cv (Summer) 1.000
Region England and Wales Cv (Winter) 1.000
M5-60 (mm) 17.800 Shortest Storm (mins) 15
Ratio R 0.379 Longest Storm (mins) 10080
Summer Storms Yes Climate Change % +45

<u>Time Area Diagram</u>

Total Area (ha) 0.513

Time	(mins)	Area	Time	(mins)	Area	Time	(mins)	Area
From:	To:	(ha)	From:	To:	(ha)	From:	To:	(ha)
0	4	0.171	4	8	0.171	8	12	0.171

BGP	Page 4	
Wellington House, Wellington Court		
Preston Farm		
Stockton on Tees, TS18 3TA		Micro
Date 18/04/2024 15:10	Designed by zach.waller	Drainage
File Attenuation Volume.SRCX	Checked by	Drainage
XP Solutions	Source Control 2020.1.3	1

Model Details

Storage is Online Cover Level (m) 4.750

Tank or Pond Structure

Invert Level (m) 3.050

Depth (m) Area (m²) Depth (m) Area (m²) Depth (m) Area (m²)
0.000 540.0 0.800 540.0 0.801 0.0

Hydro-Brake® Optimum Outflow Control

Unit Reference MD-SHE-0085-3000-0800-3000 Design Head (m) 0.800 Design Flow (1/s) 3.0 Flush-Flo™ Calculated Objective Minimise upstream storage Application Surface Sump Available Yes Diameter (mm) 85 3.050 Invert Level (m) Minimum Outlet Pipe Diameter (mm) 100 1200 Suggested Manhole Diameter (mm)

Control Poir	nts Head	(m) Flow	(1/s)	Control	Points	Head (m)	Flow (1/	s)
Design Point (Cal	culated) 0.	800	3.0		Kick-Flo®	0.517	2	. 5
Fl	ush-Flo $^{\text{\tiny TM}}$ 0.	239	3.0 Me	Mean Flow ove	r Head Range	_	2	. 6

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (1/s)								
0.100	2.6	0.800	3.0	2.000	4.6	4.000	6.3	7.000	8.3
0.200	3.0	1.000	3.3	2.200	4.8	4.500	6.7	7.500	8.5
0.300	3.0	1.200	3.6	2.400	5.0	5.000	7.0	8.000	8.8
0.400	2.9	1.400	3.9	2.600	5.2	5.500	7.4	8.500	9.0
0.500	2.6	1.600	4.1	3.000	5.5	6.000	7.7	9.000	9.3
0.600	2.6	1.800	4.4	3.500	6.0	6.500	8.0	9.500	9.6